September 18, 2003

Mr. Ron Timm Washington State Department of Ecology 3190 160th Avenue S.E. Bellevue, WA 98008-5452

SUBJECT: RESULTS OF GROUNDWATER WELL INSTALLATION AND SAMPLING-

SHOPS AT FIRST STREET, 100 108<sup>TH</sup> AVE NE, BELLEVUE WA

Dear Mr. Timm:

On behalf of Benenson Bellevue Associates II (Benenson), the owner of the above-referenced site, Floyd Snider McCarthy, Inc. (FSM) has prepared this letter to provide you with the results of the groundwater investigation conducted at the site.

### **BACKGROUND**

During site redevelopment in 1994, perchloroethylene (PCE) was discovered in site soil. The PCE was attributed to releases from a former dry cleaning operation. PCE-impacted soil underlying the former dry cleaning facility was excavated to a depth of 15 feet. Subsequent sampling during the Remedial Investigation (Kennedy/Jenks, 1994) revealed the presence of PCE in soil below the excavated area and in soil beneath a stormwater manhole located within the site parking lot. In both locations PCE concentrations decreased significantly with depth but were consistently detected to the maximum depth sampled (90-100 feet below ground surface [bgs]). Concentrations at depth were typically less than 1 mg/kg. A soil vapor extraction (SVE) system was installed near the manhole and operated from 1996 until 2000. In 2002, three monitoring wells were installed at the site. The purpose of the wells was to assess groundwater quality near the former dry cleaning facility and storm manhole, and to obtain a preliminary determination of groundwater flow direction.

Groundwater was first encountered in sands lying approximately 100 feet bgs. Each well was screened across the upper 15 feet of saturated sands. Groundwater flow was calculated to be to the south-southwest with a moderate horizontal gradient of 3 feet vertical per 1000 feet horizontal.

The wells were sampled twice over a three-week period. PCE was detected in Wells MW-2 (located cross-gradient of the manhole) at 19 and 99 ug/L and in MW-3 (located downgradient of the former dry cleaners) at 21 and 51 ug/L (Figure 1). The MTCA Method A Cleanup level for PCE in groundwater is 5 ug/L. Other volatile organic compounds (VOCs) were also detected, but at concentrations less than applicable cleanup levels.

SEP 1 9 2003

#### ADDITIONAL INVESTIGATION

The purpose of the additional investigation was to address the following data gaps as described in the work plan letter submitted to you May 15, 2003 (FSM 2003).

- Better determine groundwater flow directions and seasonal variance Prior to this investigation, the three existing wells allowed only a rough estimate of groundwater flow direction at this site. Additional groundwater elevation monitoring points were deemed necessary to establish more accurate groundwater flow directions at the site.
- Site Hydrogeology The PCE plume is apparently contained within a sand aquifer.
  However, basic information such as the thickness of this aquifer, the presence of
  intervening aquitards, and the aquifer's lateral continuity were not established during
  the initial investigation.
- Evaluate the Presence of Dense Non-aqueous Phase Liquids (DNAPL) The
  concentration of PCE concentration at depth in the aquifer may indicate the
  possibility of DNAPL pools.

To evaluate the above data gaps, two borings were advanced at the site, in locations presumed to be hydrologically downgradient of existing Wells MW-2 and MW-3, which are in turn either downgradient or directly adjacent to PCE release areas. Figure 1 shows the locations of the original three borings and the two new borings. Driven spilt-spoons samples were obtained at 10-foot intervals until saturated soil conditions were observed, after which the sampling interval decreased to every 2.5 feet. Well MW-4 was advanced to a depth of 112.5 feet and Well MW-5 to a depth of 125 feet. The driller reported the beginning of "sand lock" of his augers at the base of each boring indicating deeper drilling was not possible using a hollow-stem auger. Clean tap water was added during drilling of each well to control sand heave. A Washington State Licensed Hydrogeologist (LHG) logged each soil sample. Copies of the soil logs for each boring are included as Attachment A.

Soil samples were screened for volatile organic vapors using a photo-ionization detector (PID). A subset of 12 samples, six from each boring, were submitted to CCI Analytical for analysis of halogenated VOCs by USEPA Method 8260.

# **Results of VOC Screening and Analyses**

None of the samples showed PID readings greater than background levels. Samples from throughout the unsaturated and saturated zones were submitted for testing. VOCs were not reported in any of the 12 samples analyzed, including those at the base of each boring. Copies of the analytical reports are provided as Attachment B.

### **Hydrogeologic Conditions**

The subsurface soils exhibited significant differences at depth in each boring. In Wells MW-4 and MW-5, very dense glacially deposited and compacted silty sands with some gravel were observed to a depth of approximately 60 feet in Well MW-4 and to depths of greater than 100

feet in Well MW-5. Similar results were observed in Wells MW-1, MW-2 and MW-3. Underlying the glacial deposits in Well MW-4 is a 20-foot thick sand deposit, underlain by 10 feet of sandy silt. The top of the water table aquifer was located under the silt at a depth of 90 feet in medium sand that was continuous to the base of the boring at 112 feet. No intervening aquitards were observed in this saturated interval.

In contrast, soils in Well MW-5 were comprised consistently of dense to very dense very silty fine sand with some gravel to a depth of 125 feet. Groundwater in MW-5 was first encountered during drilling at a depth between 92 and 102 feet. The sand aquifer observed at Well MW-4 was not observed in MW-5. No significant aquitards were noted in either boring.

After completion of the borings, 2-inch diameter PVC monitoring wells were installed. Each well was screened across the upper 20 feet of saturated soil. Each well was then developed in two stages. The first stage occurred immediately following well installation. A bailer was used to remove sand and approximately 15-20 gallons of turbid water from each well. One week following initial well development, the second stage occurred. A submersible pump was used to remove remaining turbidity and as much of the drilling water as practical. Promptly after pumping was initiated, the discharge water from MW-4 became clear. In contrast, the water pumped from MW-5 remained slightly turbid throughout pumping, due to the increased silt content of the formation at that location.

#### **Groundwater Flow Direction**

To evaluate the direction of groundwater flow at the site, the top of the PVC casing was surveyed in, using the existing well elevations as a benchmark. Static depth-to-groundwater readings were then collected from each well one-week following well development. Figure 1 displays the site wide groundwater elevation contours and Table 1 lists the depth to groundwater, well casing elevations, and calculated groundwater surface elevations. The contours indicate that groundwater flow at the site is to the south-southwest. The groundwater elevation at MW-4 is significantly lower than surrounding wells, indicating a steeper incline of the gradient at that location. This is likely due to local topography, which drops sharply in elevation south of Main Street. Based on this first round of groundwater elevation data, it appears that Well MW-4 is located directly downgradient of the storm sewer manhole, and MW-5 is located downgradient of the former dry cleaners.

The saturated sand unit observed at MW-4 appears to have much greater hydraulic conductivity as compared to the silty sand in MW-5. Both the steeper gradient and high hydraulic conductivity of the sand result in a greater aquifer transmissivity. The higher transmissivity results in a larger volume and more rapid flow of site groundwater at the location of MW-4, as compared to MW-5.

### **PCE CONCENTRATIONS**

Groundwater samples were collected from all site wells except upgradient Well MW-1. As defined in the project the work plan, two methods of sample collection were used: passive diffusion bags (PDBs) and a submersible pump. The PDBs were used for sample collection at the upper and lower intervals of the 20-foot well screen in Wells MW-4 and MW-5. A PDB was

also set at the mid-screen elevation in Well MW-2, which contained the highest PCE concentration in 2002. Upgradient Wells MW-2 and MW-3 were constructed with only 10 feet of well screen, which were too short for the collection of two PDB depth interval samples. Therefore, the single PDB was set in each of these wells at mid-screen elevation. The PDBs were placed in the wells immediately after the second round of well development. The PDBs remained in place for the recommended two-week sampling period, after which they were removed from the well, the bags opened, and then the sample vials filled.

To compare the PDB to the submersible pump methodologies (which was used to collect the 2002 samples), a Redi-Flo submersible pump was lowered to the base of Wells MW-4 and MW-5 directly after the PDBs were pulled. A low-flow sampling rate of less than one liter per minute was used to purge the well. After 2-3 gallons of water was purged, the sample was collected. The water level in each well was monitored to ensure that minimal drawdown occurred during pumping. The pump and discharge hose were then decontaminated by purging with 10 gallons of municipal water. A blank sample was collected after one of the decontamination events. The samples were analyzed for halogenated VOCs using USEPA Method 8260.

#### Results

PCE was the only VOC detected in all of the well samples. Only chloroform was detected in the decontamination blank sample<sup>1</sup>. Figure 2 shows the sample results and Table 2 lists the PCE concentrations, including results of prior sampling. The PCE concentrations in the samples from the PDB were approximately twice the concentrations of the corresponding submersible pump samples. It is likely that this is a consequence of the pump drawing water from seams of both contaminated and uncontaminated waters, resulting a less concentrated sample. While the submersible pump samples are more representative of the overall PCE concentrations across a screened interval, the PDB samples are representative of the maximum concentrations within that interval, so should be considered conservative concentrations. The following observations are noted:

- Well MW-4: The PCE concentrations in both of the PDB samples were 9 ug/L indicating no PCE stratification with depth. The sample from the pump contained PCE at 4 ug/L.
- Well MW-2: The PCE in MW-2 as collected by PDB was 43 ug/L. The pumped sample contained 24 ug/L, which is approximately equivalent to the results obtained from the June 2002 pump sample, indicating no change in concentration over the past year.
- Well MW-3: The PCE concentration in MW-3 by PDB was 93 ug/L, which was also similar to results detected in 2002. If a pump sample was collected, a lower concentration would have been expected. This indicates that the PCE concentrations in this well have probably declined over the past year.

<sup>&</sup>lt;sup>1</sup> Chloroform occurrence is due to the chlorination of municipal water.

Well MW-5: The PCE concentration in MW-5 at the lower screen depth was 98 ug/L
or approximately equivalent to that in upgradient well MW-3. A lower concentration
of 40 ug/L was detected in the upper screen interval, indicating some stratification
with depth.

### PRELIMINARY CONCLUSIONS

PCE concentrations in existing wells do not appear to have significantly changed in the past year. The concentration of PCE in Well MW-4, downgradient of the storm manhole, is close to the 5 ug/L cleanup level. PCE concentrations at Well MW-5, downgradient of the former dry cleaner facility, is approximately the same as in Well MW-3, located upgradient. The stratification of PCE with depth in MW-4 is likely a result of less contaminated groundwater near the top of the aquifer. The concentrations of PCE measured, while greater than the MTCA cleanup level are under 1/1000<sup>th</sup> of the solubility of PCE in water (150,000 ug/L). Therefore, they do not indicate NAPL in groundwater at this site.

Future work will involve quarterly collection of groundwater elevations to further define the year-round flow directions. After this is complete, additional samples (using only PDBs) will be taken to evaluate trends and the need and/or potential location of additional downgradient wells.

Sincerely yours,

Floyd Snider McCarthy, Inc.

Tom Colligan, L.H.G/ Senior Project Manager Hydrogeologist 605

Thomas Henry Colligan

Encl.:

Attachment A Well Logs

Attachment B Analytical Results

Figure 1 Monitoring Well Locations and Groundwater Contour Map, July 2003

Figure 2 PCE Concentrations, July 2003
Table 1 Groundwater Monitoring Elevations

Table 2 PCE Concentrations in Groundwater Monitoring Wells

Copies: Leonard Kreppel, Benenson Capital, Tom Newlon, Stoel Rives

#### References:

Kennedy/Jenks Consultants. 1994. Remedial Investigation / Feasibility Study Report (Revised). The Shops at First Street Project Site. Bellevue, WA. November.

Table 1
Monitoring Well Elevation Summary for The Shops at First Street

	TOC1	MW-1 - 153.9 ft erval <sup>2</sup> : 100-115	тос	MW-2 - 150.04 ft iterval: 95-110	тос	MW-3 - 144.86 ft terval: 105-115	тос	MW-4 - 143.56 ft terval: 92-112	тос	MW-5 - 141.23 ft Iterval: 92-112
Date	Depth to Water (ft)	Groundwater Elevation (ft)	Depth to Water (ft)	Groundwater Elevation (ft)	Depth to Water (ft)	Groundwater Elevation (ft)	Depth to Water (ft)	Groundwater Elevation (ft)	Depth to Water (ft)	Groundwater Elevation (ft)
5/22/2002 <sup>3</sup>	103.65	50.25	106.13	43.91	109.31	35.55	-	-	-	-
5/31/2002 <sup>3</sup>	103.56	50.34	100.25	49.79	95.02	49.84		-	-	-
6/18/2002 <sup>3</sup>	103.44	50.46	100.07	49.97	94.88	49.98	-		-	-
7/10/2003 <sup>4</sup>	103.92	49.98	100.62	49.42	95.45	49.41	94.90	48.66	91.65	49.58
7/21/2003 <sup>4</sup>	103.91	49.99	100.61	49.43	95.44	49.42	94.91	48.65	92.08	49.15
7/25/2003 <sup>4</sup>	NM <sup>5</sup>	МИ	100.54	49.50	NM	NM	94.92	48.64	92.10	49.13

#### Notes:

- 1. TOC = Top of Casing Elevation, feet above mean sea level.
- 2. Screen Interval: depth, ft., from top of casing.
- 3. Measured by Kennedy Jenks Consultants
- 4. Measured by Floyd Snider McCarthy, Inc.
- 5. NM = Not measured

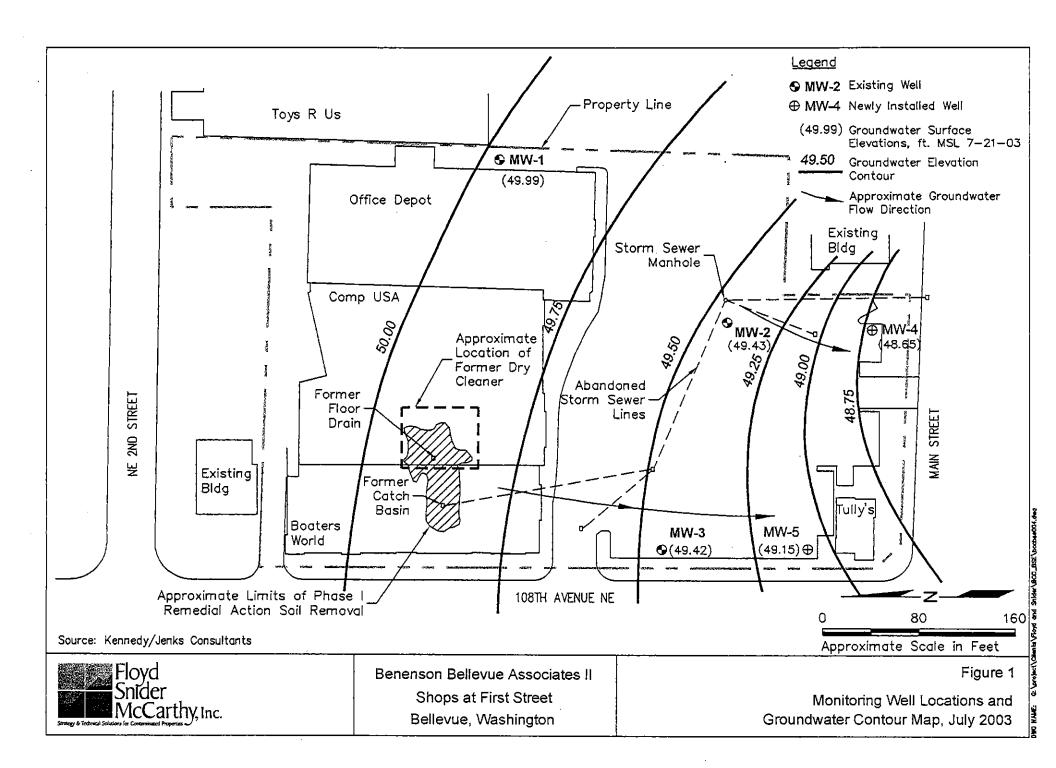
# **Groundwater Investigation Results**

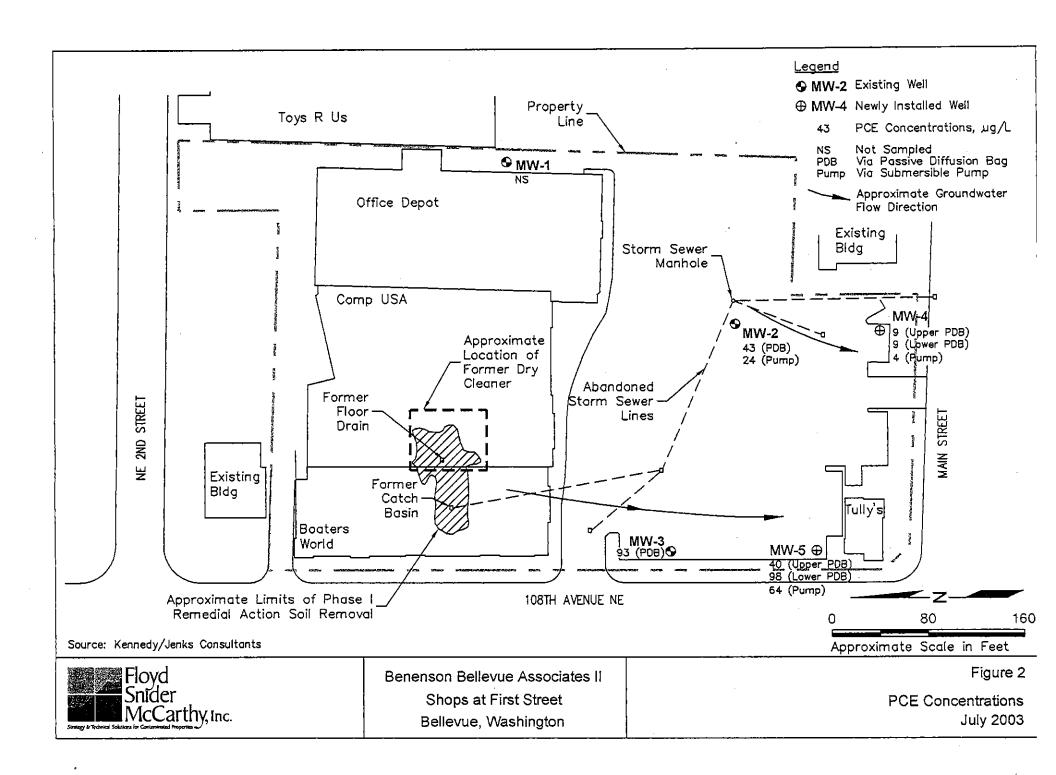
Table 2
PCE Concentrations in Groundwater Monitoring Wells

			PCE Co	ncentratio	ns, µg/L
Well ID	Sampling Method	Sampling Elevation <sup>1</sup>	5/22/02 <sup>2</sup>	6/18/02 <sup>2</sup>	7/25/03 <sup>3</sup>
MW-1	Submersible Pump	NA <sup>4</sup>	< 0.2	< 0.2	NS⁵
MW-2	Submersible Pump	NA / 47.54 (Mid-Screen) <sup>6</sup>	19	21	24
MW-2	PDB	47.54 (Mid-Screen)	-	-	43
<u>.</u>					
MW-3	Submersible Pump	NA	99	51	-
MW-3	PDB	34.86 (Mid-Screen)	-	-	93
MW-4	Submersible Pump	41.56 (Mid-Screen)	-	_	4
MW-4	PDB	46.56 (Top of Screen)	-	-	9
MW-4	PDB	32.06 (Bottom of Screen)	_	-	9
		-			
MW-5	Submersible Pump	39.23 (Mid-Screen)	-	-	64
MW-5	PDB	47.23 (Top of Screen)	-	-	40
MW-5	PDB	32.73 (Boltom of Screen)	-	-	98 .

#### Notes:

- 1. Sampling Elevation, feet above mean sea level (MSL)
- 2. Sampled by Kennedy Jenks Consultants (KJC)
- 3. Sampled by Floyd Snider McCarthy, Inc. (FSM)
- 4. NA = Not available
- 5. NS = Not sampled
- 6. KJC's sample elevations are NA, FSM's sample elevation is 47.54 feet above MSL.





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	PID (ppm)	From		SAMI PECO (F1	VERY	Penetration Resistance USCS Symbol	MAJOR CONSTITUENT NON-SOIL SUBSTANCES: Odor, staining, sheen, scrap, sleg, elc.	Log
MW-5/52.5'	0.1	52,5	54	1.5'	X	50- -45 -50/4 ML	Gray to olive gray, slightly clayey SILT, dry, very dense (TILL)	
MW-5/62.5'	0.1	62.5	64	1.5'	$\boxtimes$	60-	No recovery, started drilling with water, very slow drilling from 50' to 60'	
MW-5/72.5	0.1	72.5	74	1.5'		70 50/6 SM	Gray to olive-gray, fine, trace gravelly, very silty, fine SAND, dry, very dense	2° PVC Casing
MW-5/82.5'	0.1	82.5	84	1.5'	X	80	Olive-gray, silty, very silty, fine SAND, wet, dense (perched zone?)	Bentonite Grout
MW-5/92.5 <sup>1</sup>	0.1	92.5	94	1.5	·×	90	Gray, slightly clayey, very silty, fine SAND, damp, very dense to dense	2' Schedule 40 PVC 0.02 Slot Screen  Colorado Silica Sand Pack 10-20

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MW-5/107.5						<u> </u>	-			Glavelly line SAND, wet, very dense	
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MW-5/112.5' 0.1 112.5 11.5' 11.5	MW-5/107.5'	0.1	107.5	109	1.5'	ŀΧ	108-	ļ <u></u> -	SM	Olive-gray, slightly silty to trace silt, slightly fine,	
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MW-5/112.5						<u> </u>	-		1		
MW-5/112.5		ŀ				L	-				
MW-5/115'   0.1   115   116.5   1.5'   116   31   117   118   12   120   121   121   121   121   121   122   122   124   1.5'   123   32   32   32   32   33   34   39   30   30   30   30   30   30   30	MW-5/112 5'	0.1	112.5	114	1.5	١V	113-		SM	Olive-gray, trace silt to slightly silty, fine SAND, wet,	
MW-5/115' 0.1 115 116.5 1.5' 118 31 116 31 SM Olive-gray, slightly silty to trace silty, fine SAND, wet, dense  MW-5/117.5' 0.1 117.5 119 1.5' 118 7 12 SM Olive-gray, trace silt, slightly silty, fine SAND, wet, medium dense  MW-5/120' 0.1 120 121.5 1.5' 120 50/9 121 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/122.5' 0.1 122.5 124 1.5' 123 30 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/125' 0.1 125 126.5 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense	1777-57 112.0		,,,,,,,			$\mathbb{Z}$	114-	50/8			
MW-5/115' 0.1 115 116.5 1.5'		ĺ			ł		-				Native Backfill* —
MW-5/122.5' 0.1 125 126.5 1.5' \  \frac{125}{126} \  \frac{39}{39} \  \text{SM} \  \text{Olive-gray, trace silt, slightly silty, fine SAND, wet, medium dense} \  \text{Well casing puffed up from 125' to slightly silty, fine SAND, wet, dense} \  \text{MW-5/125'} \  \text{0.1 125 126.5 1.5'} \  \text{125 28 SM} \  \text{Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense} \  \text{MW-5/125'} \  \text{0.1 125 126.5 1.5'} \  \text{125 28 SM} \  \text{Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense} \  \text{MW-5/125'} \  \text{0.1 125 126.5 1.5'} \  \text{126 39 SM} \  \text{Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense} \  \text{MW-5/125'} \  \text{0.1 125 126.5 1.5'} \  \text{126 39 SM} \  \text{Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense} \  \text{MW-5/125'} \  \text{127 126 126.5 1.5'} \  \text{127 126 39 SM} \  \text{Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense} \  \text{Note: Well casing puffed up from 125' to 112' during installation} \  \text{MW-5/125'} \  \text{127 0.1 125 126.5 1.5'} \  \text{128 0.1 125 126.5 1.5'} \  128 0.1 125 126.5	1	ł				7	115-	18	j.	·	
MW-5/120' 0.1 120 121.5 1.5' 120 50/8 121 SM Olive-gray, trace silt, slightly silty, fine SAND, wet, medium dense    MW-5/120' 0.1 120 121.5 1.5' 120 50/8 121 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense    MW-5/122.5' 0.1 122.5 124 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense    MW-5/125' 0.1 125 126.5 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND,    *Note: Well casing pulled up from 125' to 112 during installation	MW-5/115'	0.1	115	116.5	1.5	ΊX	116-		SM		
MW-5/120' 0.1 120 121.5 1.5' 120 50/8 SM Olive-gray, trace silt, slightly silty, fine SAND, wet, medium dense  MW-5/120' 0.1 120 121.5 1.5' 120 50/8 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/122.5' 0.1 122.5 124 1.5' 123 32 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/125' 0.1 125 126.5 1.5' 126 38 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense	1	1				$\vdash$		42		wet, dense	
MW-5/120' 0.1 12.5 1.5' 124 1.5' 125 28 SM Olive-gray, trace silt, slightly silty, fine SAND, wet, medium dense    MW-5/125' 0.1 125 126.5 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense    MW-5/125' 0.1 125 126.5 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense    *Note: Well casing putted up from 125' to 112' during installation			1				117-				
MW-5/120' 0.1 120 121.5 1.5'   120   50/8   SM   Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense   122   32   50/5   SM   Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense   123   50/5   SM   Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense   125   126.5   1.5'   125   28   SM   Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense   127   128   1	MAI 5/117 5'	١,,	1175	110	1 5	N	118-		SM	Olive gray trace sift slightly sifty fine SAND.	
MW-5/120' 0.1 120 121.5 1.5' 120 50/8 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/122.5' 0.1 122.5 124 1.5' 123 32 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/125' 0.1 125 126.5 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  *Note: Well casing pulled up from 125' to 112' during installation	JV144-0/117.5	0.1	17.5	113	'	$\triangle$	110-			wet, medium dense	
MW-5/120' 0.1 120 121.5 1.5' 121 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/122.5' 0.1 122.5 124 1.5' 123 32 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/125' 0.1 125 126.5 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  *Note: Well casing pufed up from 125' to 112' during installation					İ		-		-		
MW-5/122.5' 0.1 122.5 124 1.5' 123 32 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/125' 0.1 125 126.5 1.5' 126 39 SM Olive-gray, trace silt, to slightly silty, fine SAND, *Note: Well casing pulled up from 125' to 112' during installation		Ì	ŀ		1	$\overline{}$	120-	50/8	1	·	
Wet, dense  Wet, dense	MW-5/120'	0.1	120	121.5	1.5	łΧ	121~		SM		
MW-5/122.5' 0.1 122.5 124 1.5' 123 32 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense    MW-5/125' 0.1 125 126.5 1.5' 126 39 SM Olive-gray, trace silt, to slightly silty, fine SAND,    *Note: Well casing pulled up from 125' to 112' during installation						۲-	١ -	<del> </del>		wet, dense	
MW-5/122.5' 0.1 122.5 124 1.5' 123 50/5 SM Olive-gray, trace silt, to slightly silty, fine SAND, wet, dense  MW-5/125' 0.1 125 126.5 1.5' 126 38 SM Olive-gray, trace silt, to slightly silty, fine SAND,  *Note: Well casing pulled up from 125' to 112' during installation							122-				
wet, dense  wet, dense  wet, dense  wet, dense  wet, dense  wet, dense  wet, dense  *Note: Well casing pulled up from 125' to 112' during installation	MANA E HOO E	0.4	122 5	104	1 =	N	123-		SM	Olive-gray trace silt to slightly silty fine SAND	
MW-5/125' 0.1 125 126.5 1.5' 125 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, *Note: Well casing pulled up from 125' to 112' during installation	G.521 (C-9919)	".	122.0	] '24	'.3	$\mathbb{N}$	-	5575	] ""		
MW-5/125' 0.1 125 126.5 1.5' 28 SM Olive-gray, trace silt, to slightly silty, fine SAND, *Note: Well casing puffed up from 125' to 112' during installation							- 24				
MW-5/125' 0.1 125 126.5 1.5' X 126 39 SM Olive-gray, nace shit, to slightly shity, life 3ARD, 112 during installation						$\vdash$	125-	28			#Note: Wall engine outled up from 105' to
	MW-5/125'	0.1	125	126.5	1.5	ΊX	126	39 50/5	SM	Olive-gray, trace sitt, to slightly sitty, fine SAND, wet, dense	

							Flov	d Sni	ider McCarthy, Inc.	
	Fl	OV/	1				Well	N	IW-4 Date_ June 30, 2003	Sheet <u>3</u> of <u>3</u>
	Ċ	11/1/	u or				Job_	s	hops at First Street Job No. BC	C-BSE
10 to 10 to			LI 'ari	-bs					y <u>Tom Colligan/Tom Cammarata</u> v Holt Drilling	veather Cloudy, Cool, 10s
Surategy and Technical S	IIV Monsfe		art		, in	С.	Drille	a By. Nooli	Method 4" ID Hollow Stem Auger	
			,				Sami	olina	Method Split Spoon 3" Diameter, 300 lb Hammer	
Obs. Well Ins	all.	<b>7</b> 86	No	1			Botto			92 Feet No
		DEF	TH.				tion	v g	DESCRIPTION: Den., moist, color, minor, MAJOR CONSTITUENT	Well Construction
SAMPLE ID	PID (com)	From	То	RECC	IPLE OVERY :T)	0	Penetration Resistance	Symi	NON-SOIL SUBSTANCES: Odor,	Log
		110111			<u>''</u>		<u>т.</u>		staining, sheen, scrap, slag, etc.	
MW-4/100'	0.1	100	100.5	6"	X	100-	50/5	SP	Olive-gray, slightly silty to trace silt, slightly fine	
"""	'	,		,	<u></u>	-		) . 	gravelly, fine SAND, wet, very dense	
		}				101		1	addies water to control begge	
	ľ					102-			adding water to control heave	Colorado Sirca — 77.4 Sand Pack 10-20
1					<u> </u>	۔ ال				
		ļ			N/	1 103-			•	2' Schedule 40 PVC 0.02
MW-4/102.5'	0.2	102.5	104	1.5'	IX	_	50/8	SP	Olive-gray, slightly silty to silty fine SAND, trace fine	Slot Screen
				ŀ	<u> </u>	104-			to coarse gravel, wet, dense	
1		ŀ	1			-				
1	1	}	1			105-	29			
MW-4/105	D 1	105	106.5	15	₽V	-	50/3	SP	Olive-gray, slightly silty to silty, trace fine to gravelly	
11111	0.1	100			Μ	106-	30,0	5	fine SAND, wet, dense	
						-				
						107~				
				İ	7	ļ <sup>-</sup>	30			
MW-4/107.5'	0.1	107.5	109	1.5	1X	108-	50/5	SP	Olive-gray, slightly silty to silty, fine SAND, wet, dense	
					$\mathbb{Z}$	109-				
						-				
					_	110-				
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		440		4 5	.[\/	] -	32		1 - 1 - 1 - 1 - C - C - C - C - C - C -	
MW-4/110'	0.2	110	131.0	1.5	ΙĀ	111-	50/3	SP	1st 7" olive-gray, very dense, slightly silty, fine SAND, wet, dense, over 3" of olive-gray, coarse	
			ŀ		$\vdash$	4 -			SAND, wet, dense	
						112-				
1				1	ŀ	-		}	Stopped drilling at 112' due to sand locking	
Ĭ.					-	113-			up augers, install well.	
1		1		1			-	ĺ		
]		1				114-				
		]			-	115				
						,,,,	<u> </u>			
						116-				
			1			_	ļ			
		}				117-				
						-		1		
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						-		1		
	]					119-		1		
				-		-		1		

	s ri	_					Floye Well	l Sni	der McCarthy, Inc. W-4 Date June 30, 2003	Sheet 1 of 3
	1 日	ΟΥ	1				VVER	S	nops at First Street Job No. BC	
	Sı	าเส	d er Cart				Logo	ed R	Tom Colligan/Tom Cammarata V	/eather Cloudy, Cool, 70s
<b>添</b> 了	ĭλ	lcC	'art	hv	· In	_			Holt Drilling	
Strategy and Technical S	IV Solutrons fo	i Coxxum	∠ <b>⊘IL</b> ated Propert	μıy,	HIC	C.	Drill 1	vnell	Method 4" ID Hollow Stem Auger	
• •							Samt	olina	Method Split Spoon 3" Diameter, 300 lb Hammer	
Obs, Well Ins	stall.	Yes	No	]			Bollo	m of	Well 112 Feet ATD Water Level Depth	92 Feet No
		DEF		,	1				DESCRIPTION: Den., moist, color, minor,	Well Construction
SAMPLEID	PID (ppm)			SAMI RECOV (F1	PLE VERY 1)	0	Penetration Resistance	SOSU Sympo	MAJOR CONSTITUENT NON-SOIL SUBSTANCES: Odor, staining, sheen, scrap, stag, etc.	Log
						0-			Asphalt surface (parking stall)  Logged by Tom Colligan	Flush Mounted Monument
									Brown gravelly SAND and SILT, moist, dense	Concrete —
	1		1 1			-			most, defice	
	ì	i							Note: No split spoon samples collected for first 20	L appropriate Market Market
i						5	-		feet. Logged from cuttings	2º PVC Casing
İ						_	-		•	
	ŀ							SM-		
	1					_		GМ		
						10-			•	Benionite Grout
						_				
	1					-				
			ļ							
	Ì	[	1			15—		]		
		[	ļ			-				
	1 .					-				
						-				
						20-		1		
						↓ Ξ	50	SM-	Brown silty very fine SAND with GRAVEL to	
MW-4/22'	0.1	22	22.5	6"	$\boxtimes$	-	iXU_	GМ	silty, very fine SANDY GRAVEL, dense, moist	
			1			-			(GLACIALLY COMPACTED?)	
					,	25—				
	1					]				
		1				_				
	-	1	}			-				<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>
						30-	<u> </u>	1		
			<u>.</u> .		ļ	] =		SM-	Brown, gravelly very fine silty SAND to silty sandy	
MW-4/32'	0.1	32	32.5	6"	⋈	1 _	50	GM-	GRAVEL, dense, moist (GLACIALLY COMPACTED?)	1 <i>V//\\ \\</i> //\\
			1			-		]	,	<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>
	٠.					35-	===	1		
l I	1		1			=		1		\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
		-				-		1		
		1				-		1		
			1		1	40-	<u> </u>		Driller reports wetness in augers at 40'	
,			1			] -	<u> </u>	1	Perched GW Zone?	<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>
MW-4/42'	0.1	42	43	12"	$\boxtimes$	] [	50/6	SM-	Brown, gravelly, very fine sandy SILT to silly, gravelly,	<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>
}					-	-	ļ <u> </u>	GM	very fine SAND, dense to very dense: 43' sample	
1		1		1		45~		]	appears "moist", not wet, but soil moist to wet from 42' to 42.5' (GLACIALLY COMPACTED?)	\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
			1			-	+	1	42 10 42.0 (GENOINELI COMITACILE)	
1		1	1	'	1	]		1		\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
	-	1				[ ]		1		<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>
		1		1	<u>L</u> .	50-	<u> </u>	1		\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\

# Well Log MW-4

Production has been dead	. <b>.</b>		3				<b>Floy</b> o Well		der McCarthy, Inc. W-4 Dale June 30, 2003	Sheel2of	3
	H	oya 1ide	1			ŀ	Joh	SI	nops at First Street Job No. BC		
	Si	ıĭde	er				Logge	ed By	Tom Colligan/Tom Cammarata V	Veather Cloudy, Cool, 70s	
<u>@%</u> ≓.	$\bar{\Lambda}$	lcC	art	hv	/ In/	,	Driller	1 Bv	Holt Drilling		
Smakegy and Technical Sc	lutions fo	r Contamiru	ted Parper	,,	, 1111	٠.	Drill T	ine/N	Method 4" ID Hollow Stem Auger		
							Samp	oling l	Method Split Spoon 3" Diameter, 300 lb Hammer		
Obs. Well Inst	all.	<b>7</b>	No				Bollo	m of '	Well 112 Feet ATD Water Level Depth	92 Feet No	
SAMPLE ID	PID	DEP		SAM RECO	PLE VERY	0	Penetration Resistance	USCS	DESCRIPTION: Den., moist, color, minor, MAJOR CONSTITUENT. NON-SOIL SUBSTANCES. Odor,	Well Construction Log	
	(ppm)	From	To	(F	T)	•	<u>s</u> &	-0	staining, sheen, scrap, slag, etc.	W/// W	///
MW-4/52	0.1	52	52.5	6"		1	50/6	SM- GM	Brown, gravelly, silty SAND to sandy, silty GRAVEL, dense to very dense		
						55-					
MW-4/62'	0.4	62	62.5	8"		65	50)6	SP	Gray-brown, silty, very fine to medium SAND with some silt, loose to medium dense (fluvial?)		
MW-4/72'	0.1	72	73	12"	×	70	50/6	SP	Whitish grey, very fine to medium SAND, trace silt, loose, dry		
	-					80-	14	ML	Easier drilling  Greenish brown, sandy SILT with trace gravel,	2*PVC Casing	
MW-4/82'	0.1	82	83.5	1.5		85	24		moist to very moist, stiff	Bentonite Grout	
						90-		$\nabla$	Plug tip wet at 90' - reduce sampling interval to every 2.5'		
MW-4/92'	0.3	92	93,5	1.5'	X	-	12 18 34	SP	Olive-gray, dense, trace silt, trace fine † Tom Cammarala to gravelly, fine SAND, damp to wet	2' Schedule 40 PVC 0.02 Slot Screen	
MW-4/94.5	0.1	94.5	96	1.5'	X	95	18 27 37		Olive-gray, dense, trace silt, fine SAND, damp to wet		
MW-4/97'	0.1	97	98.5	1.5	$\boxtimes$	-    -	28 50/5		Olive-gray, dense, slightly silty, fine SAND, wet	Colorado Silica Sand Pack 10-20	