APPENDIX 2A Supplemental Investigation Data Report 2013 Investigation

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APPENDIX 2A SUPPLEMENTAL INVESTIGATION DATA REPORT, 2013 INVESTIGATION

1.0 INTRODUCTION

The 2013 Supplemental Investigation (SI) was undertaken to meet the requirements of Agreed Order DE 2008 (Ecology 2005) between Washington State Department of Ecology (Ecology), Puget Sound Energy (PSE) and the City of Seattle (City), as amended (Ecology 2013). The purpose of the SI was to collect additional data from the upland portion of the area of investigation (AOI) to support completion of a remedial investigation/feasibility study (RI/FS) for the Gas Works Parks Site (GWPS) on the north shore of Lake Union in Seattle. In years past, a manufactured gas plant (MGP) and related industries occupied parts of the upland portion of the AOI, which has since been developed into a Seattle Parks and Recreation Department park (Gas Works Park). The SI was designed to meet specific objectives relating to chemical contaminants and their adverse effects:

- Evaluate historical and potential current source areas that may impact the upland.
- Characterize upland soil in targeted areas to assess potential ongoing impacts to groundwater.
- Characterize upland groundwater impacts to assess the pathway by which contaminants in groundwater may contribute to contamination in the sediment of the in-water portion of the AOI (i.e., the groundwater-to-sediment pathway).
- Assess the occurrence and mobility of light and dense non-aqueous phase liquid (LNAPL and DNAPL) that is present below ground surface in the upland, relative to potential impacts to sediment.

The SI followed a work plan (GeoEngineers 2013) documenting the field procedures to be used during the investigation. The resulting data are intended to allow further assessment of impacted soil and groundwater associated with former MGP, tar refinery and other industrial operations located at Gas Works Park and the Seattle Police Department Harbor Patrol property, in the upland portion of the AOI. Ecology approved the Supplemental Investigation Work Plan (SIWP) on March 11, 2013.

Field investigations occurred from February to October 2013 according to the procedures in the Ecology-approved SIWP, SI sampling and analysis plan (SAP) and SI quality assurance project plan (QAPP). Field elements in February to April 2013 included a well conditions survey, geophysical survey, laser-induced fluorescence probing (TarGOST®), geoprobe soil borings, shoreline well installation, monitoring well repair, a geotechnical investigation, petrophysical soil core collection, groundwater monitoring (well gauging, groundwater sampling, and NAPL sampling), NAPL baildown testing, slug testing and a professional survey of all wells and SI explorations. Field elements in October 2013 included groundwater monitoring (well gauging and groundwater sampling). This data report presents results of the investigation and deviations from the SIWP.

2.0 FIELD EXPLORATION METHODS

Several types of field exploration methods were used during the SI. Investigations were conducted sequentially, allowing refinement of later efforts using findings of the previous investigations. The field elements are presented in the table below, framed according to potential pathways evaluated.



Field Element	Season	Drill Rig Type	Source Character- ization	Leaching to Ground- water	Groundwater Transport to Sediment and Surface Water	NAPL Transport to Sediment and Surface Water
Well Conditions Survey	Spring	-	-		-	-
Monitoring Well Repair and Cap/Lock Replacement	Spring					
Geophysical Survey (EM, Magnetic and GPR)	Spring		х			
Laser Induced Fluorescence (TarGOST®)	Spring	Geoprobe with TarGOST®	х	Х	-	х
Environmental Soil Borings, Subsurface Soil Sampling	Spring	Geoprobe	х	х		Х
Shoreline Monitoring Well Installation and Development	Spring	Sonic		х	х	х
Geotechnical Drilling	Spring	Mud rotary/ sonic/HSA				
Petrophysical Borings	Spring	Sonic	Х		-	Х
Groundwater Monitoring (Gauging, GW Sampling, NAPL Sampling)	Spring and fall	-	х	Х	Х	х
NAPL Baildown Testing	Spring to summer					Х
Slug Testing	Spring	-	-		Х	
Professional Survey of All Monitoring Wells and SI Explorations	Spring	-			-	-

SI explorations are shown on Figure 2A-1 and noted below:

- Drilled explorations
 - TarGOST[®] borings (TG-01 through TG-46, TG-18B, and TG-42R)
 - Environmental soil borings (GEI-1 through GEI-15)
 - Geotechnical borings (GEO-1 through GEO-3)
 - Petrophysical borings (PT-01, PT-01B, PT-02, and PT-03)
 - Monitoring wells (MW-32S to MW-40S, MW-32D, MW36D, and MW-39D)
- Existing monitoring wells that were gauged, sampled, or both.

2.1. General Procedures

General field procedures for drilling, logging and sampling are discussed below. Specific methods for each field investigation element are discussed in Sections 2.2 to 2.9.

2.1.1. Drilling

Soil borings were drilled and logged with the following purposes:

- Collect soil samples for visual observation, field screening, and chemical analysis;
- Collect soil samples for physical properties testing to support geotechnical evaluations;
- Collect soil samples for petrophysical testing; and
- Install monitoring wells.

Drilling methods used include direct push, hollow-stem auger and sonic rotary (sonic). Drilling activities conformed to state and local regulations including Washington Administrative Code (WAC) 173-160, Minimum Standards for Construction and Maintenance of Wells. Before entering the GWPS, the drilling rigs and equipment were visually inspected for signs of contamination. Vehicles were inspected for fluid leaks before being allowed on-site. Only clean, unused sampling sleeves and bags were used. Management of investigation-derived waste (IDW) generated during drilling is discussed in Section 4. To avoid drilling through shallow utilities, including the Park's irrigation system, a post-hole digger was used to excavate the first 2 feet of soil at each location before drilling. Discrete soil samples were collected in laboratory-supplied containers and submitted for chemical analysis. Soil sampling strategy is described in Section 2.1.3.

2.1.1.1. Direct Push

Environmental soil borings were advanced using a track-mounted GeoProbe. The direct-push method uses hydraulically driven probes and a 4-foot soil sampler until reaching the planned boring depth or probe refusal. Soil sampler probes were lined with disposable acetate sleeves.

2.1.1.2. Sonic

Soil borings for monitoring well installation and petrophysical soil sampling were advanced using a track-mounted rotary sonic rig. The sonic drilling method advanced the borings by vibrating a steel casing and an internal sample barrel into the ground. Sonic drilling provided a continuous sample representative of subsurface conditions by advancing an inner sample barrel lined with a sample bag into the formation ahead of the casing.

In general, petrophysical and shallow monitoring well borings were advanced using a 6-inch casing for the first several feet, with a 4-inch casing advanced through a bentonite seal at the bottom of the 6-inch casing to the bottom of the boring. Deep monitoring well borings were drilled in a similar manner, except that a 10-inch casing was used in lieu of the 6-inch casing for the first several feet, and a 6-inch casing was used in lieu of the bottom the bottom of the bortom.

2.1.1.3. Hollow-Stem Auger and Mud Rotary

Geotechnical borings were advanced using hollow-stem augers with or without mud rotary. Soil samples and geotechnical data were obtained by dropping a 140-pound or 300-pound hammer on a split-barrel sampler from a vertical distance of approximately 30 inches. The number of hammer blows required to advance the sampler the final 18 inches was recorded on the boring logs.



2.1.2. Borehole Logging

Lithology and field screening observations were recorded on the boring logs.

2.1.2.1. Lithologic Logging

As outlined in the SIWP, lithology was described in accordance with ASTM International (ASTM) D 2488 Standard Practice for Description and Identification of Soils and recorded on the boring logs. Percent recoveries, hammer blow counts, and sample depths were also recorded on the logs.

2.1.2.2. Field Screening

Soil samples were field-screened for evidence of possible contamination using four methods: visual screening, water sheen screening, headspace vapor screening, and shake test as described in the SIWP and below.

2.1.2.3. Visual Screening

Visual screening was performed as prescribed in the SIWP SAP. Soil samples, samplers, and gloves were observed for potential signs of contamination. Unusual odor, staining, color, and any other evidence of NAPL were recorded in the boring logs. Sidewalls of the sampling sleeves were observed for signs of staining. Wet material was observed for the nature of saturation and type of liquid (water or NAPL).

2.1.2.4. Water Sheen Screening and Headspace Vapor Screening

Water sheen screening and headspace vapor screening were performed as prescribed in the SIWP SAP.

Water sheen screening involved placing soil, approximately 1 cubic inch or about 1 tablespoon, in a black plastic pan partially filled with water and observing the water surface for signs of sheen.

Headspace vapor screening involved placing soil in a plastic bag, closing the bag and shaking the bag to expose soil vapors. The probe of a photoionization detector (PID) was then inserted into the bag and the PID measured the concentration of volatile organic vapors present within the sample bag headspace.

2.1.2.5. Shake Test

NAPL shake testing was performed on select samples where NAPL was suspected or observed to evaluate the presence, nature (i.e., DNAPL or LNAPL) and amount of NAPL present. A small volume of soil (5 to 10 grams) was removed from the sampler and placed in a small glass container (typical 4-ounce jar). Water was added until the container was approximately two-thirds full. The container was vigorously shaken until NAPL, if present, was displaced from the core matrix. The boring logs contain observations about staining and evidence of NAPL in the soil/NAPL/water solution; the shape and percent coverage of sheens on the surface of the solution was also recorded. The sidewalls of the jar were used to estimate the thickness of LNAPL on the water surface and the thickness of DNAPL accumulated at the bottom of the jar. The amount of sheen and blebs in the water surface was quantified using categories similar to those of the water sheen test. Naturally occurring sheen, which is often found in the field, was discerned from hydrocarbon sheen by its ability to dissolve or break up upon agitation. Results of the shake tests were characterized using the guidelines noted in the following table:



Appearance	Visual Description	Percent Coverage									
Color and Shape of NAPL and Sheen Observations											
Rainbow	Multicolored	-									
Metallic	Metallic gray-colored	-									
Florets	Circular and multicolored	-									
Blebs	Circular and black/brown	-									
Streaks	Long and flowing shape	-									
Sheen Classification											
None, trace	-	<2									
Slight	-	2-15									
Moderate	-	15-40									
Moderate to heavy	-	40-70									
Heavy	-	>70									

2.1.3. Soil Sampling Strategy

Soil samples submitted for chemical analysis were placed into laboratory-supplied containers, lightly but securely packed and capped with a plastic lid. The samples were maintained on ice and delivered under chain-of-custody to the analytical laboratories Analytical Resources, Inc. (ARI) and PTS Laboratories. In general, soil samples were analyzed for benzene, toluene, ethylbenzene, and xylenes (BTEX); polycyclic aromatic hydrocarbons (PAHs); and arsenic, using the methods presented in the SAP. Some samples also were analyzed for alkylated PAHs.

Soil samples submitted for chemical analysis were primarily from subsurface soils rather than surface soils since most of the upland portion of the AOI has a vegetated cap. In general, samples were collected at the depth where the highest field screening impacts were observed and within the saturated zone; some of the samples targeted the water table and geologic horizons such as the Fill-native contact and top of Till.

Soil sampling was completed according to the SI SAP and QAPP. Field quality control (QC) samples collected include equipment rinsate blanks, trip blanks and field duplicates.

2.2. Monitoring Well Conditions Survey/Well Repair/Lock Replacement

An initial monitoring well survey was performed on February 27 and March 1, 2013 to identify existing, usable wells in the upland. Field staff recorded the condition of monuments and casings, signs of surface water infiltration, and sedimentation in the monitoring wells. Using an oil/water interface probe properly decontaminated between readings, field staff also recorded depth to groundwater, depth to LNAPL and DNAPL, and total monitoring well depth for all the usable wells except the multi-level sampler (MLS) wells.

Based on the well conditions survey, MW-17 was chosen for repair. The damaged flush-mount monument and surface seal were replaced to prevent surface infiltration. The repair was performed by Boart Longyear and GeoEngineers on March 2, 2013.

Lockable J-Plug well caps and keyed-alike padlocks were placed on May 13, 2013. On July 12, 2013, GeoEngineers replaced threaded bolts and repaired bolt holes with a heli-coil on all wells where they were missing.

The monitoring well survey, well repair and lock replacement was performed according to the SI SAP, except for the following:

- Multilevel sampler MLS-3 could not be located and was not surveyed.
- Monitoring wells PZ-5 and PZ-6, which had not been listed as potentially usable in the SI Work Plan, were located, surveyed, found to be in good condition and added to the list of usable monitoring wells.
- Monitoring well PZ-4 was discovered by GeoEngineers at the end of the spring investigation and was identified by using previous investigations maps (EPRI and PSE 1998). It was considered unusable because of a broken monument rim and clogged casing. Although considered neither repairable nor usable, it was not abandoned because of time constraints. Professional land surveyors surveyed the broken monument rim.

Bulk NAPL samples were not collected during the monitoring well conditions survey but rather during the spring groundwater monitoring event. However, small representative NAPL samples were collected during the monitoring well survey; these samples were submitted to Dakota Technologies, Inc. (Dakota) before mobilization for the spring TarGOST® drilling event to evaluate whether TarGOST® technology would be effective. Small NAPL samples (DNAPL from DW-4, DW-5, DW-7, and MW-18, as well as LNAPL from MW-9) were collected for TarGOST® readings using a disposable polycarbonate bailer and placed into 40-millileter (ml) volatile organic analysis (VOA) bottles before being sent to Dakota. LNAPL but not DNAPL was collected from monitoring well MW-09; the disposable polycarbonate bailer could not displace the viscous LNAPL on the surface of the groundwater to reach the deeper DNAPL.

2.3. Geophysical Investigation

Non-intrusive geophysical surveys were completed from March 5 through 8, 2013, using magnetic (MAG), electromagnetic (EM) and ground penetrating radar (GPR) technologies. Areas surveyed are shown in Figure 2A-2. The information obtained from the geophysical surveys was used to identify areas of potential anomalies for subsequent TarGOST[®] explorations and soil borings. Zonge International, Inc. (Zonge) conducted the geophysical survey. The draft report is included as Attachment 2A-1 to this appendix.

The geophysical surveys were completed using the procedures presented in the SI SAP, except that GPR was used where above-grade metal objects such as historical MGP structures and fences created interference (i.e., near MW-09 and the Northeast Corner). Penetration depth using GPR was limited to 2 to 3 feet in these areas because higher conductivity soils were encountered (Attachment 2A-1).

2.4. Laser Induced Fluorescent Investigation (TarGOST®)

TarGOST® was used for the following reasons:

- To evaluate areas where NAPL or tar has been encountered or suspected;
- To further delineate the extent of NAPL impacts in areas of limited data along the shoreline, or in historical or potential current source areas;



- To better locate soil borings; and
- To assess anomalies identified by the geophysical surveys.

TarGOST[®] explorations were performed from March 18 through 26, 2013 in locations shown on Figure 2A-1. The TarGOST[®] report, TarGOST[®] logs and accompanying material are in Attachment 2A-2.

In accordance with the SI SAP, the TarGOST[®] system was advanced with a GeoProbe. Dakota's fiber optic cables were strung through the driller's rods; the TarGOST[®] tip along with the rods were advanced into the ground with the rig. Depth was tracked with a string potentiometer system connected to the direct push rig and computer.

Forty-five TarGOST[®] explorations (TG-1 to TG-45) and two collocated explorations (TG-12R/46 and TG-42R) were advanced during the SI. In each area of proposed TarGOST[®] exploration, as designated in the SIWP, a primary TarGOST[®] exploration was drilled. Decisions regarding secondary and offset locations were based on observed TarGOST[®] response in, respectively, primary and secondary locations, as well as on time and spatial constraints (Figure 2A-1).

The TarGOST® investigation was conducted according to the SI SAP, except as noted below:

- DNAPL samples collected from monitoring wells DW-04, DW-05, DW-07 and MW-18, and a LNAPL sample collected from MW-09 were submitted to Dakota for evaluation of NAPL response to the laser-induced fluorescence (LIF) technology.
- Additional TarGOST[®] explorations near MW-18 were completed to further investigate NAPL observed in the well during the monitoring well survey.
- Additional TarGOST[®] explorations were completed along the eastern shoreline to compare LIF responses with NAPL observations from the Eastern Shoreline study in 2007 (AECOM 2008).
- An additional round of step-out TarGOST[®] explorations was advanced, noted as offset TarGOST[®] locations in Figure 2A-1. The need for offset/step-out explorations was determined from the observed degree of TarGOST[®] response in the primary and secondary TarGOST[®] explorations.
- Two pairs of collocated TarGOST[®] explorations were completed to evaluate response variability. TG-12R/46 and TG-42R were located adjacent to TG-12 and TG-42, respectively.
- Electrical conductivity (EC) was measured and recorded using TarGOST[®] at 19 explorations. The objective was to determine whether EC data correlated with geology and NAPL occurrence. Acceptable EC data are found in the logs for explorations TG-03 to TG-13, TG-17 to TG-18B and TG-33 to TG-37.
- Six confirmation borings were completed next to TarGOST® explorations. Selected interval depths were submitted to Dakota for signal (%RE) analysis, enabling comparison of fluorescence of individual soil samples with that of in-situ cores.
- Two locations (TG-18B and TG-32B) had to be re-drilled near the locations specified in the SI SAP because the first attempts met shallow refusal.
- Some depth intervals within certain TarGOST[®] borings had unreliable %RE responses, due to either pre-probing or broken fibers in the probe tip. These intervals, which have been excluded from the NAPL data set, include the following: TG-18B (15 to 15.6 feet), TG-33 (0 to 4.5 feet), TG-41 (0 to 10 feet), TG-18 (8 feet to total depth), TG-32B (0 to 10 feet), and TG-34 (0 to 2 feet).



2.5. Environmental Soil Borings

Fifteen environmental borings (GEI-1 to GEI-15) were completed from March 27 through April 2, 2013. Soil borings were drilled at the locations shown on Figure 2A-1. Boring logs are included in Attachment 2A-3. Photographs of the soil cores are included in Attachment 2A-4.

The general sampling strategy presented in Section 2.1.3 was followed for the GEI locations. In addition, for TarGOST[®] confirmation samples, soil borings were performed adjacent to TarGOST[®] explorations where various low and high %RE values were observed in order to evaluate TarGOST[®] response with respect to NAPL presence. The depth interval was specified to match a distinct TarGOST[®] response. Tests conducted on the soil samples are summarized in Table 2A-1. Analytical results are presented in Section 3.

The environmental soil borings were completed according to the SI SAP.

2.6. Shoreline Monitoring Well Installation

Monitoring wells were installed between March 25 and April 12, 2013 along the shore of the GWPS. This activity was undertaken to evaluate upland-to-sediment pathways, complete the monitoring well network along the entire shoreline and obtain additional information regarding groundwater conditions.

2.6.1. Monitoring Well Construction

Twelve shoreline monitoring wells were installed (MW-32S to MW-40S, MW-32D, MW-36D, and MW-39D) (Figure 2A-1). Three well pairs were installed, as shallow (MW-32S, MW-36S, and MW-39S) and adjacent deep (MW-32D, MW-36D, and MW-39D) wells. Well construction details for the newly installed monitoring wells are presented in Table 2A-2. Wells logs are included in Attachment 2A-3. Photographs of the soil cores are included in Attachment 2A-4.

In addition to the general soil sampling strategy presented in Section 2.1.3, emphasis was placed on targeting the saturated zone. Soil samples were collected at depths corresponding to the screen interval of each monitoring well. Composite soil samples representing the entire length of the screen interval were collected for grain size analysis.

The monitoring wells were constructed with 2-inch-diameter, Schedule 40 threaded polyvinyl chloride (PVC) riser and machine-slotted well screens. Shallow well screens have 0.010-inch-wide slots. Deep well screens have 0.020-inch-wide slots. PVC end caps were installed on the bottom ends of the well screens. Wells monitoring the groundwater table were constructed with screens 3 to 10 feet long. Shallow wells were constructed with 20/40 silica sand filter to limit entry of fine-grained particulates from the surrounding formation into the wells. Deep wells were constructed with 10/20 silica sand filter. In monitoring wells MW-32D and MW-39D, 20/40 silica sand was installed near the top of the sand filter to prevent bentonite intrusion into the sand filter. The sand filter extends from the bottom of the well screen to at least 1 foot above the top of the well screen. Annular seals consist of a minimum 1-foot-thick layer of hydrated bentonite pellets or chips installed between the filter pack and the concrete surface seal. Wells were completed using flush-mounted monuments installed in a concrete surface seal to prevent surface water from infiltrating the well. Each monitoring well was secured with an expandable well cap (J-plug) and corrosion-resistant lock.



Deep wells were drilled through the Fill unit into underlying glacial deposits using conductor casing to avoid cross-contamination, as noted on the deep well logs. The temporary conductor casing was installed no deeper than 1 foot above the depth of the deep well screen.

A summary of the SI wells installed is presented in Table 2A-2. Analytical results for soil samples collected are presented in Section 3.

2.6.2. Well Development

The new monitoring wells were developed 24 hours or more after installation, using a combination of surging and purging until at least five well casing volumes of water were removed from each well and turbidity was stabilized at less than the target of approximately 10 nephelometric turbidity units (NTU). Water quality parameters (e.g., temperature, pH, conductivity, turbidity) were measured and recorded during well development.

2.6.3. Deviations from Work Plan

Shoreline monitoring wells were completed and developed using the procedures in the SI SAP. There were no deviations from the work plan.

2.7. Kite Hill Geotechnical Investigation

Geotechnical drilling at Kite Hill was performed on April 11 and 12, 2013, to evaluate slope stability in anticipation of placing an engineered, vegetated soil cover on this portion of the AOI.

Three geotechnical borings (MW-32D/GEO-1, GEO-2, and GEO-3) were drilled. Boring logs are included in Attachment 2A-3. Photographs of the soil cores are included in Attachment 2A-4. Soil samples from three borings were collected and submitted to ARI for geotechnical testing. The laboratory tests completed included grain-size distribution (ASTM D422) and percent fine content (ASTM D1140). The laboratory report is included in Attachment 2A-5.

As discussed in Section 2.6, soil samples for chemical analyses were obtained from boring MW-32D/GEO-1. Boring MW-32D/GEO-1 was also completed as a shoreline monitoring well.

2.7.1. Deviations from Work Plan

The geotechnical investigation was completed according to the SI SAP, except for the following:

- Geotechnical borings were drilled using hollow-stem augers rather than mud rotary as planned. Mud rotary was proposed for installation of these wells because of concerns regarding heaving sands identified in previous borings drilled nearby; however, the mud rotary rig was heavy and concerns were raised regarding possible damage to the Park's turf. In addition, mud was lost down-hole. These borings were completed successfully using hollow-stem augers. Soil sampling with a split-barrel sampler was performed as planned in the SI work plan.
- Atterberg limits testing was not performed because the samples collected were not sufficiently fine-grained. Soil samples for geotechnical testing were submitted to ARI for testing because of potential chemical contamination in the samples.



2.8. Petrophysical Investigation

The presence of NAPL in the AOI upland was evaluated during the SI in a petrophysical investigation on April 17 through 19, 2013. Four petrophysical borings (PT-01, PT-01B, PT-02, and PT-03) were completed (Figure 2A-1). Boring logs are included in Attachment 2A-3.

PT-01B was drilled because of poor recovery in PT-01. PT-02 was located on the eastern shoreline where NAPL was observed in SI explorations MW-36S, MW-36D, and TG-42R. PT-03 was located near the shoreline of Harbor Patrol where NAPL was observed in SI explorations GEI-14 and TG-20.

Undisturbed soil cores for petrophysical testing collected from the soil borings (in 4-inch-diameter polycarbonate Lexan[™] sleeves) were immediately placed on dry ice and stored vertically. Cores were cut to 2.5-foot lengths, packed with dry ice and in large coolers and shipped to the lab. Cores were submitted for core photography (ASTM D5079) and free product mobility testing (ASTM D425M, Dean Stark). Petrophysical soil tests performed are summarized in Table 2A-3. Analytical results are presented in Section 3. Petrophysical laboratory reports are provided in Attachment 2A-6.

2.8.1. Deviations from Work Plan

The petrophysical investigation was completed according to the SI SAP, with one exception. Petrophysical borings were advanced using sonic drilling instead of hollow-stem augers. Samples were collected using a decontaminated split-spoon sampler. The sampling device was 5 feet long, with an inner diameter of 3.5 inches, an outer diameter of 3.75 inches and a clear polycarbonate Lexan[™] tube liner.

2.9. Groundwater Monitoring

Two groundwater monitoring events were completed with a threefold purpose:

- Measure groundwater depths and evaluate groundwater elevations and gradients,
- Measure NAPL depths and thicknesses in wells where present, and
- Collect groundwater analytical data to evaluate the vertical and lateral extent of chemicals of concern at the shoreline and to estimate flux at the Lake Union shoreline.

Monitored wells are mapped on Figure 2A-1.

2.9.1. Groundwater and NAPL Measurements

Before the spring (April 22, 2013) and fall (October 14, 2013) groundwater monitoring events, depth-to-water measurements were recorded within a single 12-hour period from usable monitoring wells located in upland. After wells were opened to vent, depth to groundwater and total monitoring well depth were measured to the nearest 0.01-foot using a decontaminated interface probe. Groundwater elevations were used as the basis for groundwater contour figures in the RI. Depth to groundwater was not measured at MLS locations.

Wells from the adjacent Metro site also were measured and sampled in coordination with the SI (Arcadis 2013a, b). Depth-to-water measurements from monitoring wells MLU-1, MW-4 and MW-7 on the Metro site were incorporated in the RI evaluations. Water level measurements are included in Table 2A-6.



The depth and thickness of NAPL were measured and recorded during both groundwater monitoring events (April and October 2013). Results are presented in Table 2A-5.

2.9.2. Groundwater Sampling – Spring

The spring groundwater monitoring event occurred April 15 through 25, 2013. Monitoring wells and multilevel samplers included in the monitoring activities and analyses performed are listed in Table 2A-7. Depthto-water measurements and groundwater elevations are presented in Table 2A-6. Analytical results are included in Attachment 2A-9. In summary:

- Excluding monitoring wells with NAPL, all other usable wells were sampled, for a total of 54 wells.
- Six of the total wells sampled are MLS wells, each consisting of three to five individual sampling ports targeting different depths.
- Groundwater samples were collected from 67 wells and ports.

Groundwater samples were obtained using the techniques outlined in the SIWP SAP. The samples were placed into a cooler with ice and logged on the chain-of-custody. Samples were submitted for analyses of BTEX and PAHs.

Groundwater analytical results are discussed in Section 3.

2.9.3. NAPL Sampling- Spring

Bulk NAPL samples were collected in April 2013. A summary of NAPL tests conducted is included in Table 2A-4. NAPL physical testing included density, specific gravity and kinematic viscosity using methods API RP40, ASTM D1481 and ASTM D445. Chemical analyses included expanded PAH analysis (43 alkyl-PAHs using SW-846 8270 with selective ion monitoring [SIM]) and volatile organic compounds (VOCs) using EPA 8260C.

2.9.4. Groundwater Sampling – Fall

The fall groundwater monitoring event occurred October 14 through 18, 2013. Monitoring wells and multilevel samplers included in the monitoring activities and analyses performed are presented in Table 2A-7. Depth-to-water measurements and groundwater elevations are presented in Table 2A-6. In summary:

- Shoreline monitoring wells plus two inland wells were sampled, for a total of 24 wells.
- One MLS well with three ports was sampled.
- Field-filtered and non-filtered samples were collected at all the shoreline wells and ports, and analyzed for PAHs, arsenic, BTEX or a combination thereof.

Shallow and deep shoreline monitoring wells were sampled to evaluated upland flux to Lake Union. Field-filtered samples were collected at MW-03 and MW-03D and analyzed for arsenic. This information was used to provide information regarding background concentrations of arsenic.

In addition to field-filtering, sample collection procedures were the same as those used in the spring groundwater sampling event. Unfiltered samples were submitted for analyses of BTEX and PAHs. Field-filtered samples were submitted for analysis of PAHs and dissolved arsenic (Table 2A-7). Groundwater analytical results are discussed in Section 3.



2.9.5. Deviations from Work Plan

Groundwater sampling was completed according to the SI SAP, except as noted below:

- Four of the spring groundwater samples were filtered in the laboratory using a 0.7-micron borosilicate glass fiber filter before being analyzed for PAHs, as outlined in Table 2A-7. This procedure was a last-minute addition to the regular unfiltered PAH analysis for all wells, with the goal of deciphering the effect of filtering on PAH concentrations.
- Fall groundwater sampling included collection of field-filtered groundwater samples for PAHs. PAH samples were also collected using traditional (non-filtered) methods. This change was verbally approved by Ecology in September 2013.
- Fall groundwater samples were analyzed for dissolved arsenic, elevated concentrations of arsenic having been measured in soil collected the prior spring. This change was verbally approved by Ecology prior to sampling in October 2013.

2.10. NAPL Baildown Testing

The presence of NAPL in the AOI upland was evaluated during the SI using NAPL baildown testing between April 29 and October 14, 2013.

A baildown test was performed in monitoring well MW-09, which contained a layer of LNAPL greater than 1-foot-thick. The LNAPL baildown test was completed using a decontaminated disposable polycarbonate bailer to remove as much product as possible, taking care to minimize the volume of water removed from the monitoring well. After LNAPL was removed from the monitoring well to the maximum extent practicable, an oil-water interphase probe was used to measure the depth to water and thickness of product until at least 80 percent of the initial thickness of LNAPL was recovered. Initial measurement intervals were within minutes. Eventually, measurement intervals were extended to 3 weeks because recovery was slow. A data logger placed in the well was programmed to record hydrostatic submergence pressure 8 times per second, supplementing the manual interface probe readings.

There were two deviations from the work plan:

- Although thicknesses of NAPL greater than 1 foot were encountered in at least five wells, NAPL baildown tests were performed only in MW-9. The test could not be performed in the other four wells for at least one of the following reasons: the DNAPL was too viscous, the DNAPL was not thick enough or the screen was clogged.
- A data logger was placed in the well to supplement the manual interface probe readings. It was programmed to record hydrostatic submergence pressure 8 times per second.

2.11. Slug Testing

Slug tests were performed on seven monitoring wells near the shoreline on April 24 and 25, 2013, to evaluate hydraulic conductivity (K) of the water-bearing units. The monitoring wells tested and estimated hydraulic conductivity values are presented in Attachment 2A-7.

The slug tests were consistent with the procedures in the SI work plan, with the following exceptions:



Falling head tests were performed on some monitoring wells whose screened interval was partly above the water table. For wells with screened intervals spanning the water table, falling-head test data are not representative of aquifer response because some of the displaced water drains into the unsaturated zone above the water table. Data from these wells were not used in analysis.

2.12. Professional Survey

All SI explorations (including locations where refusal was encountered or multiple attempts were made) were surveyed on April 25, 2013 by the Washington-licensed professional land surveyor True North Land Surveying of Seattle Washington. All existing monitoring wells were surveyed by True North on April 29, 2013.

Locations were surveyed for X-Y-Z coordinates (Z for monitoring wells included both monument rim elevation as ground surface and top-of-casing/PVC). The horizontal accuracy of the wells and soil borings was 0.1 feet. The vertical accuracy of the soil borings was 0.1 feet. Vertical accuracy of the monitoring wells was 0.01 feet.

Elevations were referenced to U. S. Army Corps of Engineers (USACE) (Locks) datum and North American Vertical Datum of 1988 (NAVD88). Horizontal coordinates were referenced to the NAD 83, Washington State Plane North coordinate system. Survey results are included on boring and well logs (Attachment 2A-3).

Procedures for professional surveying outlined in the SAP were followed, except that the vertical accuracy of the soil borings was 0.1 foot, not 0.01 foot as specified in the SAP.

3.0 RESULTS

This section presents results from the 2013 SI. Because the data have been integrated into the main RI, the results are not discussed in detail in this appendix.

3.1. Monitoring Well Conditions Survey/Well Repair/Lock Replacement

The following observations were made during the monitoring well conditions survey and ensuing activities:

- The monument for monitoring well MW-17 was damaged, potentially allowing surface water infiltration. The monument was replaced during the SI.
- The casing for monitoring well MW-28 was too high and prevented the monument from closing properly when secured with a J-plug and lock. During the SI, the casing elevation was reduced from 34.35 feet to 34.24 feet relative to USACE datum.
- Monitoring well PZ-4 was considered unusable because of a broken monument rim and clogged casing. It was not sampled, developed, or gauged.
- J-plug type caps were placed on all existing wells at the site, where possible.
- Locks were replaced on all existing wells at the site, with keyed-alike padlocks.

Overall, 42 existing monitoring wells and seven MLS wells were considered usable. Well gauging information from the well survey is included in Table 2A-6. Wells considered usable are depicted on Figure 2A-1. Measured groundwater elevations and NAPL thicknesses in existing wells are included in Tables 2A-5 and 2A-6.

3.2. Geophysical Results

The draft geophysical report is presented in Attachment 2A-1. Although large anomalies indicative of buried tanks or structures were not found, anomalies A through J (Figure 2A-2) were identified as locations for further sampling or drilling. The anomalies can be divided into four categories:

- High conductivity soils,
- Magnetic anomalies,
- EM anomalies indicative of scattered metallic debris, and
- Linear anomalies indicative of pipe, cables, or other utilities.

An extended geophysical interpretation overlaying former MGP structures is presented in Figure 2A-2. Appendix 1B to the RI reviews geophysical anomalies in conjunction with historical documents.

3.3. TarGOST® Results

Six confirmation borings were completed next to TarGOST[®] explorations. Comparison figures including NAPL observations from the confirmation borings alongside the nearby TarGOST[®] logs are presented in Attachment 2A-2 Figures A2-1 to A2-7. Several types of TarGOST[®] data were generated during and after the SI:

- LIF responses to NAPL samples
- TarGOST[®] logs (consistent scale)
- TarGOST[®] logs depicting mirror images of the primary TarGOST[®] exploration and collocated exploration (referred to as butterfly logs)
- Table showing electrical conductivity measurement success, per log
- LIF responses to soil samples
- Classification plots for TarGOST[®] logs, soil samples and NAPL samples
- Non-negative least squares (NNLS) waveform analysis for TarGOST[®] logs and soil samples

The data are included and discussed in Attachment 2A-2. The results are also discussed in the main body of the RI and in the "NAPL Evaluation" (RI Appendix 5F).

3.4. Geotechnical Testing Results

Geotechnical laboratory tests were performed by ARI, located in Tukwila, Washington. Selected soil samples were tested for grain size (ASTM Method D422) and percent fines (greater than U.S. No. 200 sieve; Method ASTM D1140). Geotechnical laboratory reports are included in Attachment 2A-5.



3.5. Petrophysical Results

Petrophysical and NAPL physical laboratory tests were performed by PTS Laboratories Inc., located in Santa Fe Springs, California. Soil cores were tested for free product mobility using ASTM Method D425M, Dean-Stark. NAPL samples from monitoring wells were tested for kinematic viscosity and density by Methods ASTM D445, ASTM D1481 and API RP40.

Petrophysical and NAPL test results are summarized in Tables 2A-3 and 2A-4, respectively. The laboratory reports are included in Attachment 2A-6. Petrophysical results are discussed in the main body of the RI and in Appendix 5F.

3.6. NAPL Baildown Testing Results

NAPL recovery rates were low and the methods developed by Huntley (2000) and Kirkman (2012) to interpret the NAPL baildown measurements and calculate NAPL transmissivity could not be used. LNAPL transmissivity is a measure of the potential flux of LNAPL per unit drawdown, or the volume of LNAPL travelling through a unit width of an aquifer per unit time per unit drawdown (units of length squared per time). NAPL baildown results and interpretation are presented in Attachment 2A-8 and in Appendix 5F of the RI.

3.7. Slug Testing Results

Slug test results are presented in Attachment 2A-7. Plots of the slug test response and type curves analyzed are presented in Figures A7-1 through A7-7. Table A7-1 shows interpreted hydraulic conductivity values. Slug test results are discussed in Section 5 of Appendix 3E.

3.8. Chemical Results

Selected soil, groundwater and NAPL samples were submitted for chemical and physical analyses. This section presents a summary of analyses and tests performed. Laboratory reports and chain-of-custody reports are available in Attachments 2A-9 and 2A-6, respectively. Chemical results are discussed in more detail in Section 8 of the RI.

3.8.1. Soil

Chemical analyses on selected soil samples were performed by ARI for the following chemical constituents:

- BTEX by EPA Method 8260 (low level),
- PAHs by EPA Method 8270 SIM (low level),
- Arsenic by EPA Method 200.8, and
- Polychlorinated biphenyls (PCBs) by EPA Method 8082 (low level).

The analyses performed on soil samples are listed in Table 2A-1. The laboratory reports are shown in Attachment 2A-9. Soil results are discussed in the main body of the RI.



3.8.2. Groundwater

Chemical analyses of selected groundwater samples collected during the 2013 spring and fall groundwater monitoring events were performed by ARI. As noted in Section 2.9.5, some of the samples were filtered in the laboratory; others had been filtered in the field. The samples were submitted for the following analyses:

- Spring
 - BTEX by EPA Method 8260 (low level) and
 - PAHs by EPA Method 8270 SIM (low level), including the subset of samples that were lab-filtered.

Fall

- BTEX by EPA Method 8260 (low level),
- PAHs by EPA Method 8270 SIM (low level), including the subset of samples that were field-filtered, and
- Arsenic by EPA Method 200.8.

Analyses performed are listed in Table 2A-7. The laboratory reports are included in Attachment 2A-9. Results are discussed in the main body of the RI.

3.8.3. NAPL

Chemical analyses of NAPL were performed by ARI. NAPL samples from monitoring wells were submitted for the following analyses:

- PAHs and alkylated PAHs by EPA Method 8270 SIM,
- BTEX by EPA Method 8260 (low level), and
- VOCs and semivolatile organic compounds (SVOCs) by EPA Method 8260 (low level).

NAPL analyses performed are listed in Table 2A-4. The laboratory reports are included in Attachment 2A-9. NAPL results are discussed in the main body of the RI.

4.0 DECONTAMINATION PROCEDURES AND INVESTIGATION DERIVED WASTE

Decontamination was performed using procedures outlined in the SIWP SAP, with a minor modification: if residual NAPL was present or had been encountered, equipment was pre-cleaned with acetone or isopropyl alcohol and rinsed with hexane followed by the detergent wash and rinse.

IDW, including soil cuttings, groundwater, decontamination water, disposable sampling supplies and disposable personal protective equipment, was placed in labeled 55-gallon steel drums. The drums were sealed, chained to each other and stored several feet from structures within the Cracking Towers fenced area during the SI field activities. Composite drum samples were collected and analyzed for waste profile purposes.



Forty-nine drums of IDW were generated during the 2013 SI. On June 17, 2013, Kleen Environmental removed 47 drums for disposal at an approved offsite disposal facility. On November 25, 2013, Kleen Environmental removed the remaining two drums for disposal at an approved offsite disposal facility.

5.0 REFERENCES

- Arcadis. 2013a. Groundwater Monitoring Report 2013, Former Chevron Bulk Plant No. 100-1327, Facilities North/King County (METRO), Seattle, Washington.
- Arcadis. 2013b. Person communication (email from Samuel Miles, Arcadis, to Maura O'Brien, Washington State Department of Ecology, regarding up-to-date gauging data for KC Metro project [three tables]).
- Electric Power Research Institute and Puget Sound Energy. 1998. Fate and Transport Assessment of Polycyclic Aromatic Hydrocarbons from Tar. Gas Works Park MGP Site.
- GeoEngineers, Inc. 2013. Supplemental Investigation Work Plan, Gas Works Park Site, Seattle, Washington.
- Huntley. 2000. "Analytic Determination of Hydrocarbon Transmissivity from Baildown Tests, Ground Water." 38 (1).
- Kirkman. 2012. Refinement of Bouwer-Rice Baildown Test Analysis, Ground Water Monitoring & Remediation.
- Washington Department of Ecology. 2005. Agreed Order DE 2008–Gas Works Park Sediment Site issued to the City of Seattle and Puget Sound Energy. State of Washington Superior Court.
- Washington Department of Ecology. 2013. Approval of Request to Amend Agreed Order DE 2008--Gas Works Park Sediment Site.



Supplemental Investigation Soil Testing Summary

Gas Works Park Site

Seattle, Washington

Sample ID	Sample Depth	Date	PAHs	Alkylated PAHs	BTEX	Arsenic	PCBs	Grain Size	Percent Fines
	(feet bgs)		EPA Method 8270 SIM	EPA 8270 SIM	EPA Method 8260 (Low level)	EPA 200.8	EPA 8082 (low level)	ASTM D422	ASTM D1140
GEI-1	0 to 3	4/01/13					Х		
GEI-1	7 to 7.5	4/01/13		<u>_</u>			Х		
GEI-1	12 to 12.5	4/01/13	Х				Х		
GEI-1	16.5 to 17	4/01/13	Х		Х		Х		
GEI-1	17 to 17.5	4/01/13					Х		
GEI-1	23 to 24	4/01/13	Х		Х		Х		
GEI-2	0 to 3	4/01/13	X		X				
GEI-2	16 to 17	4/01/13	Х		Х				
GEI-2	5 to 6	4/01/13	Х		Х				
GEI-3	11.5 to 12	3/27/13		Х	Х	Х			
GEI-3	16 to 17	3/27/13		Х	Х	Х			
GEI-3	2 to 3	3/27/13				Х			
GEI-3	22 to 23	3/27/13		Х	Х	Х			
GEI-3	27 to 28	3/27/13	Х		Х				
GEI-3	8 to 9	3/27/13				Х			
GEI-4	.5 to 1.5	3/27/13				Х			
GEI-4	10 to 11	3/27/13				Х			
GEI-4	15 to 16	3/27/13	Х		Х	Х			
GEI-4	20 to 21	3/27/13				Х			
GEI-4	30 to 31	3/27/13	Х		Х				
GEI-4	5.5 to 7	3/27/13	Х		Х	Х			
GEI-5	1.5 to 2	3/28/13				Х			
GEI-5	15 to 16	3/28/13	Х		Х				
GEI-5	5 to 7	3/28/13	Х		Х	Х			
GEI-5	10 to 10.5	3/28/13				Х			
GEI-5	22 to 23	3/28/13				Х			
GEI-6	10 to 12.5	3/28/13	Х		Х				
GEI-6	20 to 21	3/28/13	Х		Х				
GEI-6	25 to 26	3/28/13	Х		Х				
GEI-6	5.5 to 6	3/28/13				Х			
GEI-7	12 to 14	3/28/13	Х		Х				
GEI-7	20 to 21	3/28/13	Х		Х				
GEI-8	4 to 4.5	4/01/13	Х		Х				
GEI-8	5 to 6	4/01/13	Х		Х				
GEI-8	8.5 to 9.5	4/01/13	Х		Х				
GEI-9	11 to 11.5	4/01/13	Х		Х				
GEI-9	16 to 17	4/01/13	Х		Х				
GEI-10	2 to 3	3/29/13	Х		Х				
GEI-10	6.5 to 7.5	3/29/13	Х		Х				
GEI-11	16 to 17	3/29/13	Х		Х				
GEI-11	21.5 to 22.5	3/29/13	Х		Х				
GEI-11	26 to 26.5	3/29/13	Х		Х				
GEI-12	11 to 15	3/29/13	Х		Х				
GEI-12	15 to 17	3/29/13	Х		Х				
GEI-12	25 to 26	3/29/13	Х						
GEI-12	5 to 7	3/29/13	Х		Х				
GEI-13	13 to 16	4/01/13		Х	Х				
GEI-13	23.5 to 24.5	4/01/13		Х	Х				
GEI-13	25 to 25.5	4/01/13	Х		X				
GEI-13	8 to 9.5	4/01/13		Х	Х				
GEI-14	14.5 to 15.5	4/02/13		Х	Х				
GEI-14	27 to 28	4/02/13		Х	Х				
GEI-14	37 to 38	4/02/13	Х		Х				
GEI-14	8 to 9	4/02/13		Х	Х				
GEI-15	0 to 2	4/02/13	Х		Х				
GEI-15	12.5 to 13.5	4/02/13	Х		Х				



Sample ID	Sample Depth	Date	PAHs	Alkylated PAHs	BTEX	Arsenic	PCBs	Grain Size	Percent Fines
Sample ID	(feet bgs)	Date	EPA Method 8270 SIM	EPA 8270 SIM	EPA Method 8260 (Low level)	EPA 200.8	EPA 8082 (low level)	ASTM D422	ASTM D1140
GEI-15	6.5 to 7	4/02/13	Х		Х				
GEO-2	14 to 16	4/11/13						Х	
GEO-2	19 to 20.5	4/11/13							Х
GEO-2	24 to 26	4/11/13						Х	
GEO-2	34 to 36	4/11/13						Х	
GEO-2	39 to 40.5	4/11/13						Х	
GEO-2	44 to 44.5	4/11/13						Х	
GEO-2	9 to 10.5	4/11/13						Х	
GEO-3	15 to 17	4/12/13						Х	
GEO-3	20 to 21.5	4/12/13						Х	
MW-32D/GE0-1	10.5 to 12.5	4/10/13						Х	
MW-32D/GE0-1	16.5 to 18	4/10/13						Х	
MW-32D/GE0-1	18.5 to 20.5	4/10/13						Х	
MW-32D/GE0-1	20.5 to 22.5	4/10/13						Х	
MW-32D/GE0-1	22.5 to 24	4/10/13							Х
MW-32D/GE0-1	26.5 to 28	4/10/13							Х
MW-32D/GE0-1	28.5 to 30.5	4/10/13						Х	
MW-32D/GE0-1	35.5 to 37	4/10/13						Х	
MW-32D/GE0-1	42 to 43	4/10/13							Х
MW-32D/GE0-1	8.5 to 10.5	4/10/13							Х
MW-32D/GE0-1	43.5 to 44.5	4/12/13	Х		X	Х		Х	
MW-32S	29 to 30	4/12/13	Х		X	Х		Х	
MW-33S	12 to 22	3/28/13						Х	
MW-33S	13 to 14	3/28/13	Х		X				
MW-33S	17 to 17.5	3/28/13	Х		X	Х			
MW-34S	5 to 10	3/27/13						X	
MW-34S	7 to 8	3/27/13	X		X	X			
MW-35S	4.5 to 5	3/27/13				X			
MW-35S	4 to 7	3/27/13						X	
WW-355	5 t0 6	3/27/13	X		X				
MW-36D	23 to 24	3/28/13	X		X			v	
MW-36D	29 to 33	3/29/13	v		Y	X		X	
WW-36D	31 to 32	3/29/13	×		X	× ×			
WW-365	14 (0 15	3/29/13	^		^	×			
WW 265	22.5 to 23	3/29/13				X		v	
WW 275	14 to 21	3/29/13				v		^	
MW-375	.5 to 20	3/20/13				^		Y	
MW-375	7.5 to 8	3/26/13				Y		~	
MW-375	7.5 to 6	3/26/13	x		x	~			
MW-375	13 5-14 5	3/26/13	~		~	×			
MW-38S	3.5 to 13.5	3/25/13				~			
MW-38S	.5 to 1	3/26/13				х			
MW-38S	10 to 11	3/26/13				X			
MW-38S	5 to 15	3/26/13						Х	
MW-38S	8 to 9	3/26/13	Х		x				1
MW-39D	.5 to 1.5	3/25/13				Х			
MW-39D	8 to 10	3/25/13	Х		х	Х			
MW-39D	16 to 19	3/26/13						х	
MW-39D	17 to 18	3/26/13	Х		х	Х			
MW-39S	3.5 to 13.5	3/25/13						Х	
MW-40S	17.5 to 18	4/01/13	Х		Х				
MW-40S	5 to 10	4/01/13				1	1	Х	
MW-40S	5 to 6	4/01/13	Х		Х	Х			

Table 2A-2 Supplemental Investigation Monitoring Well Construction Details Gas Works Park Site Seattle, Washington

Screen Interval Depth Well Location Installation Diameter Screen slot size **Ground Surface** Current TOC Total Depth (feet, bgs) Geologic Unit of Well ID Date (inches) (inches) Elevation Elevation (feet, TOC) Screen Interval^a Northing Easting Тор Bottom MW-32D 4/12/2013 2 0.02 238868.03 1269843.30 29.9 29.4 47.0 42.0 47.0 Qva **MW-32S** 4/12/2013 0.01 238864.97 1269847.34 29.8 31.5 16.5 31.0 2 29.3 Fill MW-33S 3/28/2013 1270318.67 22.1 2 0.01 238748.97 38.7 38.3 13.0 22.0 Fill MW-34S 9.8 5.0 Fill 3/27/2013 2 0.01 238734.93 1270501.78 28.4 28.0 9.8 MW-35S 3/27/2013 2 0.01 238807.89 1270634.86 24.7 24.1 7.0 4.0 6.8 Fill MW-36D 3/28/2013 2 0.02 239091.49 1270785.63 30.0 29.6 33.7 29.3 33.8 Qvr MW-36S 3/29/2013 0.01 239086.77 1270783.61 30.1 29.6 12.9 8.0 22.8 Fill 2 MW-37S 3/26/2013 2 0.01 239231.18 1270816.75 27.1 26.9 14.8 5.1 14.8 Fill MW-38S 3/26/2013 2 0.01 239318.10 1270820.88 25.9 25.4 16.9 7.1 16.6 Fill MW-39D 3/25/2013 2 0.02 1270814.56 27.0 26.7 22.5 17.0 21.8 239391.05 Qva/Qpgt 0.01 26.9 14.1 3.9 14.1 Fill MW-39S 3/25/2013 2 239397.29 1270814.09 26.6 10.9 4.0 10.9 Fill MW-40S 4/1/2013 2 0.01 239491.03 1270790.39 25.7 25.2

Notes:

Elevation based on:

Horizontal Datum: NAD83 WA State Plane North.

Vertical Datum: US Army Corps of Engineers.

^a Some screen intervals cross more than one geologic unit. Units listed here are the same as those assigned by Aspect in their groundwater modeling report, with the exception of MW-9, which was formerly interpreted as being screened across Qpgt (Aspect 2012).

Qpgt: Pre-Fraser Till

Qva: Vashon Advance Outwash

Qvr: Vashon Recessional Outwash

TOC: top of casing

Supplemental Investigation Petrophysical Testing Summary Gas Works Park Site Seattle, Washington

Boring/	Sample ID	UV Photography Core	Within Core Sample	Field Observation	Shoon	Free Product Mobility Test (ASTM D425M)			
Location	Sample ID	Sample Depth (ft bgs)	Depth (ft bgs)		Jieen	(Under Air/ "Drainage")	(Under Water/"Imbibition")		
PT01B	PT01B-11-13.2A	11-13.2	12.9	"NAPL present, strong naphthalene-like odor" "HS PID 14.2 ppm"; "HS PID 93 ppm <mark>" Heavy sheen with NAPL</mark>	HS	x			
PT01	PT01-21.1-22B	21.1-22	21.2	"MS PID 15.3 ppm" "Sheen in small florets on outside of sample core" <mark>Slight to moderate sheen</mark>	SS-MS		x		
DTOO	PT02-10-13B	10-13	11.8	"coated in NAPL, with naphthalene-like odor" "HS PID 1.0 ppm"; "completely coated with NAPL" "HS PID 133 ppm"; "Rainbow color sheen appears in blobs, naphthalene-like odor" "HS 100% PID 61 ppm" Heavy sheen with NAPL	HS		x		
P102	PT02-20-23	20-23	21.45	"coated in NAPL, but with no free NAPL, strong naphthalene-like odor" " HS PID 180 ppm"; "staining does not coat all pieces, small amount of NAPL observed" "HS PID 75 ppm"; "HS PID 62 ppm"; "heavily coated with free NAPL" "HS PID 88 ppm" Heavy sheen with NAPL	HS		X		
	PT03-8-10A	8-10	8.55	"HS 70% PID 24 ppm" Sheen has "Florets"; "NAPL impact; the NAPL is black very strong hydrocarbon odor, shake test: 1 mm NAPL on surface, stained and streaked on sides of jar" "HS 70% PID 89.9 ppm" Sheen has "Florets"; "stained black, black NAPL blebs" "HS PID <1 ppm" Sheen has "Florets" Heavy sheen with NAPL	HS	X			
РТ03	PT03-10-13B	10-13	10.85	"HS 70% PID 24 ppm" Sheen has "Florets"; "NAPL impact; the NAPL is black very strong hydrocarbon odor, shake test: 1 mm NAPL on surface, stained and streaked on sides of jar" "HS 70% PID 89.9 ppm" Sheen has "Florets"; "stained black, black NAPL blebs" "HS PID <1 ppm" Sheen has "Florets" Heavy sheen with NAPL	HS		X		
	PT03-28-30B	28-30	29.7	"NAPL observed in 1/2 inch band"; "NAPL within pore space stained copper color" "HS PID <1 ppm"; "DNAPL to HS throughout" "HS PID 60 ppm"; "1/2 inch NAPL staining" "NS PID 42.3 ppm"; "1 inch NAPL staining" "HS PID <1 ppm" Heavy sheen with NAPL	HS		X		

Notes

NS = no sheen

SS = slight sheen

MS = moderate sheen

HS = heavy sheen

ppm = parts per million

Field screening NAPL category



Supplemental Investigation NAPL Testing Summary

Gas Works Park Site

Seattle, Washington

				NAPL Sampling	
Well Name	NAPL Phase	Sample Date	Alkylated PAHs	VOCs	Kinematic Viscosity/Density
			EPA Method 8270SIM	EPA Method 8260C	ASTM D1481; ASTM D445
DW-04	DNAPL	4/15/2013			
DW-05	DNAPL	4/15/2013	Х	х	Х
DW-07	DNAPL	4/15/2013	Х	х	Х
MW-09	LNAPL	4/15/2013	Х	Х	Х
MW-09	DNAPL	4/15/2013	Х	Х	Х
MW-18	DNAPL	4/15/13; 4/22/13	Х	Х	Х
PZ-03	DNAPL	4/17/2013	Х	Х	



Supplemental Investigation NAPL Thickness Data Gas Works Park Site Seattle, Washington

	Geological Unit	Date Measured				Measured N	APL Data			Corre	cted/Equivalent Elev	ations
Well	of Screen Interval		Top of Casing Elev. (ft USACE)	LNAPL Depth (ft TOC)	DTW (ft TOC)	DNAPL Depth (ft TOC)	Total Depth (ft TOC)	LNAPL Thickness	DNAPL Thickness	LNAPL Elevation (ft USACE)	Groundwater Elevation (ft USACE)	DNAPL Elevation (ft USACE)
DW-04	Till	2/27/2013	25.33		7.21	33.94	37.00		3.06		see Note 1	-8.62
DW-04	Till	4/15/2013	25.33		7.33	34.62	37.02		2.40		see Note 1	-9.30
DW-04	Till	4/22/2013	25.33		16.31	34.87	37.02		2.15		see Note 1	-9.55
DW-04	Till	4/29/2013	25.33		16.11	34.10	37.02		2.92		see Note 1	-8.78
DW-04	Till	10/14/2013	25.33		16.20	35.13	37.02		1.89		see Note 1	-9.81
DW-05	Qva	2/27/2013	25.12		4.31	26.70	29.38		2.68		20.81	-1.58
DW-05	Qva	4/15/2013	25.12		3.39	25.89	29.29		3.40		21.73	-0.77
DW-05	Qva	4/22/2013	25.12		3.21	28.50	29.38		0.88		21.91	-3.38
DW-05	Qva	10/14/2013	25.12		4.15	28.88	29.38		0.50		20.97	-3.76
DW-07	Qva	2/27/2013	24.99		4.30	40.36	42.50		2.14		20.69	-15.38
DW-07	Qva	4/15/2013	24.99		3.15	40.11	42.30		2.19		21.84	-15.13
DW-07	Qva	4/22/2013	24.99		3.18	41.96	42.30		0.34		21.81	-16.98
DW-07	Qva	10/14/2013	24.99		4.08	41.90	42.30		0.40		20.91	-16.92
MW-09	Till	2/27/2013	33.97	8.89	10.50		20.50	1.61		25.08	24.95	
MW-09	Till	4/15/2013	33.97	6.69	9.83	16.20	20.52	3.14	4.32	27.28	27.03	17.77
MW-09	Till	4/22/2013	33.97	6.43	8.29		20.52	1.86		27.54	27.39	
MW-09	Till	4/29/2013	33.97	6.52	8.07		20.52	1.55		27.45	27.32	
MW-09	Till	10/14/2013	33.97	8.95	9.86	18.51	20.52	0.91	2.01	25.02	24.94	15.46
MW-18		2/27/2013	38.21		16.41	32.15	33.57		1.42		21.80	6.06
MW-18		4/15/2013	38.21		15.87	33.04	33.59		0.55		22.34	5.17
MW-18		4/22/2013	38.21		15.40	32.51	33.57		1.06		22.81	5.70
MW-18		10/14/2013	38.21		16.63	32.25	33.57		1.32		21.58	5.96
PZ-03	Qvr	3/1/2013	34.52		12.97	14.49	15.38				21.55	
PZ-03	Qvr	4/15/2013	34.52		12.06	Trace	14.49		Trace		22.46	
PZ-03	Qvr	4/17/2013	34.52		12.05	Trace			Trace		22.47	
PZ-03	Qvr	4/22/2013	34.52		12.24	Trace	14.49		Trace		22.28	
PZ-03	Qvr	10/14/2013	34.52		13.41	Trace	14.49		Trace		21.11	

Notes:

1. Depth to water below lake level. Well damage suspected. Corrected Groundwater Elevation was not calculated.

LNAPL specific gravity, PTS result for MW09-130415-LNAPL (see Attachment A-6). Specific gravity of MW-09 LNAPL = 0.9212.

NM = not measured

Qva = Vashon Advance Outwash

Qvr = Vashon Recessional Outwash

Till = Qpgt = Pre-Fraser Till

TOC = top of casing

DTW = depth to water



Supplemental Investigation Groundwater Elevations Gas Works Park Site

	Well L	ocation													
Well ID	Northing	Easting	Well Diameter (in)	Ground Surface (ft USAC	Elevation CE)	Top of Casing Elevation (ft USACE)	Screen Inte Time of I (ft	rval Depth at nstallation bgs)	Geologic Unit of Screen Interval ^a	Depth to Groundwater (ft TOC)	Groundwater Elevation (ft USACE)	Depth to Groundwater (ft TOC)	Groundwater Elevation (ft USACE)	Depth to Groundwater (ft TOC)	Groundwater Elevation (ft USACE)
				When Installed	Current		Тор	Bottom		2/27/13	2/27/13 or 3/1/2013		2/2013	10/14/2013	
Gas Works Parl	k Property	•		4											
TDW-1	239245	1269574	2	24.90	24.86	24.57	37.5	42.5	Qva	3.85	20.72	2.71	21.86	3.59	20.98
TSW-1	239252	1269586	2	25.77	25.74	25.40	5.3	10.3	Fill	4.73	20.67	3.59	21.81	4.49	20.91
TDW-2	238940	1269755	2	24.84	25.00	25.11	34.5	39.5	Qva	3.93	21.18	2.85	22.26	3.72	21.39
TSW-2	238955	1269763	2	27.53	27.52	28.14	7.0	12.0	Fill	6.55	21.59	5.42	22.72	6.28	21.86
TDW-3	238770	1269998	2	27.13	26.88	26.46	34.5	39.5	Qva	5.92	20.54	4.83	21.63	5.70	20.76
TSW-3	238776	1270000	2	27.53	27.50	27.82	6.0	11.0	Fill	6.45	21.37	5.35	22.47	6.23	21.59
MW-03	239454	1270269	2	38.69	38.64	38.23	1.6	10.6	Qpgt	8.17	30.06	4.81	33.42	7.05	31.18
MW-03D	239459	1270280	2	38.93	38.86	38.42	54.6	57.6	Qpgt	13.95	24.47	14.29	24.13	15.19	23.23
MW-09 ^{b, c}	239136	1270551	2	34.35	34.41	33.97	10.8	20.8	Qva	10.5	23.47	8.29	27.39	9.86	24.11
MW-10	238982	1270112	2	32.42	32.31	32.99	5.3	15.3	Fill	9.84	23.15	8.42	24.57	10.10	22.89
MW-13	238836	1269903	2	32.86	32.48	32.72	7.3	17.3	Fill	11.49	21.23	10.35	22.37	11.26	21.46
MW-14	238795	1270188	2	27.22	26.93	27.53	2.5	9.5	Fill	5.46	22.07	4.59	22.94	5.62	21.91
MW-15	238857	1270255	2	38.07	37.65	38.25	9.5	19.5	Fill	16.23	22.02	14.90	23.35	16.17	22.08
MW-17	239089	1269812	2	33.07	33.08	32.66	6.5	16.5	Fill	12.21	20.45	10.83	21.83	11.78	20.88
MW-18	239327	1269776	2	38.51	38.48	38.21	unknown	unknown	unknown	16.41	21.80	15.40	22.81	16.63	21.58
MW-19	239212	1269916	2	39.39	39.34	39.14	unknown	unknown	unknown	16.43	22.71	16.06	23.08	17.41	21.73
MW-22	238721	1270122	2	24.69	24.30	25.07	24.0	34.0	Qva	3.31	21.76	2.21	22.86	3.10	21.97
MW-23	238718	1270190	2	23.79	23.60	23.92	22.0	32.0	Qpgt	2.38	21.54	1.27	22.65	2.16	21.76
MW-24	238719	1270125	2	24.64	24.28	24.87	5.0	15.0	Qvr	3.25	21.62	2.13	22.74	3.01	21.86
MW-25	238713	1270192	2	23.69	23.30	23.39	5.0	15.0	Qvr	2.28	21.11	1.20	22.19	2.05	21.34
MW-26	239414	1270609	2	32.94	33.55	32.81	9.0	12.6	Qpgt	7.78	25.03	7.69	25.12	9.49	23.32
MW-27	239268	1270426	2	35.42	35.48	35.26	12.0	15.0	Qpgt	6.19	29.07	5.51	29.75	8.59	26.67
MW-28 ^d	238800	1270458	2	37.60	37.60	37.49	17.0	27.0	Qpgt	15.38	22.22	14.62	22.98	15.49	22.00
MW-29	238995	1270119	2	31.53	31.55	32.30	13.0	23.0	Qpgt	8.99	23.31	7.73	24.57	9.43	22.87
MW-30	238986	1270115	4	31.91	31.93	32.95	12.0	22.0	Qpgt	9.19	23.76	8.20	24.75	9.87	23.08
MW-31	239409	1269783	4	41.33	41.36	40.90	35.0	45.5	Qpgt	14.58	26.32	15.90	25.00	13.77	27.13
MW-32D	238868	1269843	2	29.92	29.92	31.35	42.0	47.0	Qva			7.54	23.81	8.40	22.95
MW-32S	238865	1269847	2	29.83	29.83	31.12	16.5	31.0	Fill			7.68	23.44	8.51	22.61
MW-33S	238749	1270319	2	38.70	38.70	39.08	13.0	22.0	Fill			16.45	22.63	17.31	21.77
MW-34S	238735	1270502	2	28.44	28.44	28.05	5.0	9.8	Fill			6.25	21.80	6.94	21.11
MW-35S	238808	1270635	2	24.69	24.69	24.15	4.0	6.8	Fill			2.38	21.77	3.24	20.91
MW-36D	239091	1270786	2	29.99	29.99	29.55	29.3	33.8	Qvr			7.82	21.73	8.70	20.85
MW-36S	239087	1270784	2	30.13	30.13	29.62	8.0	22.8	Fill			7.88	21.74	8.72	20.90
MW-37S	239231	1270817	2	27.14	27.14	26.85	5.1	14.8	Fill			5.11	21.74	5.98	20.87
MW-38S	239318	1270821	2	25.94	25.94	25.42	7.1	16.6	Fill			3.70	21.72	4.55	20.87
MW-39D	239391	1270815	2	26.99	26.99	26.74	17.0	21.8	Qva/Qpgt			5.00	21.74	5.85	20.89
MW-39S	239397	1270814	2	26.89	26.89	26.61	3.9	14.1	Fill			4.86	21.75	5.74	20.87
MW-40S	239491	1270790	2	25.69	25.69	25.18	4.0	10.9	Fill			3.48	21.70	4.31	20.87
PZ-03	239232	1269811	1	34.81	34.81	34.52	5	20	Qvr	12.97	21.55	12.24	22.28	13.41	21.11
PZ-09	239322	1269844	2	36.76	39.26	38.81	12.5	22.5	Qvr	16.1	22.71	14.55	24.26	16.03	22.78
PZ-10	239315	1269814	2	36.97	38.84	38.48	12.5	22.5	Qvr	16.1	22.38	14.09	24.39	16.20	22.28
RW-01	239317	1269857	4	36.91	39.56	39.02	12.5	22.5	Qvr	16.31	22.71	15.01	24.01	16.60	22.42
UBS-1	238946	1270752	2	23.13	23.11	23.59	2	11.7	Fill	3	20.59	1.88	21.71	2.73	20.86



	Well L	ocation													
Well ID	Northing	Easting	Well Diameter (in)	Ground Surface (ft USA)	e Elevation CE)	Top of Casing Elevation (ft USACE)	Screen Inte Time of I (ft	rval Depth at nstallation bgs)	Geologic Unit of Screen Interval ^a	Depth to Groundwater (ft TOC)	Groundwater Elevation (ft USACE)	Depth to Groundwater (ft TOC)	Groundwater Elevation (ft USACE)	Depth to Groundwater (ft TOC)	Groundwater Elevation (ft USACE)
				When Installed	Current		Тор	Bottom		2/27/13	or 3/1/2013	4/22	2/2013	10/14	/2013
OBS-2	238962	1270739	2	26.46	26.52	26.21	2	11.7	Qpgt	5.71	20.50	4.57	21.64	5.44	20.77
OBS-3	238984	1270678	2	29.60	29.61	29.39	2	11.7	Fill	7.17	22.22	6.34	23.05	7.34	22.05
Harbor Patrol P	roperty														
CMP-01	239055	1269720	2	25.24	25.20	24.97	6.5	21.5	Fill	4.32	20.65	3.19	21.78	4.04	20.93
DW-04	239159	1269736	2	25.86	25.86	25.33	32.0	37.0	Qpgt	7.21	18.12	16.31	9.02	16.20	9.13
DW-05	239141	1269718	2	25.44	25.45	25.12	24.0	29.0	Qva	4.31	20.81	3.21	21.91	4.15	20.97
DW-06	239095	1269675	2	25.04	25.00	24.67	37.0	42.0	Qva	3.86	20.81	2.83	21.84	3.62	21.05
DW-07	239055	1269726	2	25.35	25.43	24.99	37.5	42.5	Qva	4.3	20.69	3.18	21.81	4.08	20.91
PZ-01	239204	1269609	1	25.62	25.70	25.09	3.0	13.0	Qvr	4.46	20.63	3.20	21.89	4.17	20.92
PZ-05	239013	1269781	1	27.74	28.05	27.83	3.0	18.0	Fill	7.23	20.60	6.07	21.76	6.94	20.89
PZ-06	239074	1269764	1	27.16	27.69	27.13	5.0	20.0	Fill	6.53	20.60	5.50	21.63	6.22	20.91
PZ-08	239157	1269715	1	25.66	25.66	25.30	5.0	20.0	Qvr	4.51	20.79	3.38	21.92	4.32	20.98
Metro Property	(South Yard)				-				-	-					
AGI-2	239488	1269432	unknown	21.60		33.93	8	23	Fill	NM	NM	11.96	21.97	12.94	20.99
MLU-1	239376	1269561	unknown	36.13	36.13	36.15	10	20	Qvr	NM	NM	14.14	22.01	15.5	20.65
MW-04	239365	1269468	unknown	21.40	21.40	27.95	9.7	19.4	Qvr	NM	NM	15.18	12.77	16.26	11.69
MW-07	239423	1269511	unknown	21.70		34.38	6.5	16.5	Fill	NM	NM	12.40	21.98	13.37	21.01
MW-8A	239469	1269368	unknown	33.96	33.96	33.56	unknown	unknown	Fill	NM	NM	11.70	21.86	12.65	20.91
MW-25	239445	1269400	4	33.19	33.19	34.16	5	20	Qvr	NM	NM	12.30	21.86	13.22	20.94
MW-26	239410	1269440	4	33.22	33.22	33.87	5	20	Fill	NM	NM	11.90	21.97	12.89	20.98
MW-27 ^e	239751	1269439	unknown	37.66	37.66	37.26	4.5	19.5	Fill	NM	NM	7.34	29.93	10.16	27.10
SMPN-01	239748	1269435	unknown	37.43	37.43	37.03	unknown	unknown	unknown	NM	NM	8.75	28.28	10.49	26.54
SMPN-02	239746	1269439	unknown	37.50	37.50	37.10	unknown	unknown	unknown	NM	NM	7.88	29.22	10.50	26.60
SMPN-03	239740	1269434	unknown	37.46	37.46	37.06	unknown	unknown	unknown	NM	NM	8.30	28.76	10.52	26.54
Near Metro Pro	perty (In/Next to	Roads)													
MW-09 ^e	239767	1269388	unknown	27.30		39.71	11.9	21.9	Qva	NM	NM	11.07	29.18	14.10	25.70
MW-11	239705	1269431	unknown	23.90		103.86	6.0	15.5	unknown	NM	NM			11.04	92.82
MW-19	239721	1269253	unknown	34.52	34.52	34.12	9	19	Fill	NM	NM	12.18	21.94	13.10	21.02
MW-20	239651	1269334	unknown	35.14	35.14	34.74	13	23	unknown	NM	NM	12.80	21.94	13.72	21.02
MW-21	239539	1269546	unknown	34.91	34.91	34.51	5	23	Fill	NM	NM	12.47	22.04		
Lake Union Elev	/ation										20.52		21.65		20.75

Notes:

^a Some screen intervals cross more than one geologic unit. Units listed here are the same as those assigned by Aspect in their groundwater modeling report, with the exception of MW-9 which was formerly interpreted as being screened across Qpgt (Aspect 2012).

 $^{\rm b}$ Well contains LNAPL. Water elevation corrected based on a LNAPL specific gravity of 0.9212.

^c LNAPL specific gravity, PTS result for MW09-130415-LNAPL. Specific gravity of MW-09 LNAPL = 0.9212.

^d TOC elevation changed from 37.597 to 37.494 feet USACE after 4/25/2013 survey.

^e Well contains LNAPL. Water elevation corrected based on a LNAPL specific gravity of 0.80.

Gray shading indicates uncertainty or unable to verify/populate.

Horizontal Datum: NAD83 WA State Plane North.

Vertical Datum: US Army Corps of Engineers (USACE).

NM = not measured

Qvr = Vashon Recessional Outwash

Qva = Vashon Advance Outwash

Qpgt = Pre-Fraser Till

-- = well not in existence at the time

Metro Ground Surface and Measuring Point Elevations: measurement elevation from May 2011 survey (Arcadis) unless otherwise noted. TOC = top of casing



Supplemental Investigation Groundwater Testing Summary Gas Works Park Site Seattle, Washington

			Ana	lysis		
		PAHs		BTEX	Dissolved Arsenic	
Well Name	EPA M (ethod 8270 s (Low level)	SIM	EPA Method 8260 (Low level)	EPA Method 200.8	Geologic Unit of Screen Interval
	Unfiltered	Lab Filtered	Field Filtered	Unfiltered	Field Filtered	
CMP-01	S,F	S	F	S,F	F	Fill
DW-06	S			S		Qva
MLS-1-1	S			S		Till
MLS-1-2	S			S		Qvr
MLS-1-3	S			S		Qvr
MLS-2-1	S			S		Qva
MLS-4-2	S			S		Qva
MLS-4-3	S			S		Qva
MLS-4-5	S			S		Fill
MLS-5-1	S			S		Qva
MLS-5-2	S			S		Qva
MLS-5-3	S			S		Qvr
MLS-5-4	S			S		Qvr
MLS-5-5	S			S		Fill
MLS-6-1	S,F		F	S,F	F	Qva
MLS-6-2	S,F		F	S,F	F	Qvr
MLS-6-4	S,F		F	S,F	F	Fill
MLS-7-1	S			S		Qva
MLS-7-2	S			S		Qvr
MLS-7-4	S			S		Fill
MW-03	S			S	F	Till
MW-03D	S			S	F	Till
MW-10	S			S		Fill
MW-13	S			S		Fill
MW-14	S			S		Fill
MW-15	S			S		Fill
MW-17	S			S		Fill
MW-19	S			S		
MW-22	S,F		F	S,F	F	Qva
MW-23	S,F		F	S,F	F	Till
MW-24	S,F		F	S,F	F	Qvr
MW-25	S,F		F	S,F	F	Qvr
MW-26	S			S		Till
MW-27	S			S		Till
MW-28	S			S		Till
MW-29	S			S		Till
MW-30	S			S		Till
MW-31	S	1		s		Till

	Analysis					
	PAHs EPA Method 8270 SIM (Low level)			BTEX EPA Method 8260 (Low level)	Dissolved Arsenic EPA Method 200.8	Geologic Unit of Screen Interval
Well Name						
	Unfiltered	Lab Filtered	Field Filtered	Unfiltered	Field Filtered	
MW-32D	S,F		F	S,F	F	Qva
MW-32S	S,F		F	S,F	F	Fill
MW-33S	S,F		F	S,F	F	Fill
MW-34S	S,F		F	S,F	F	Fill
MW-35S	S,F	S	F	S,F	F	Fill
MW-36D	S,F	S	F	S,F	F	Qvr
MW-36S	S,F		F	S,F	F	Fill
MW-37S	S,F		F	S,F	F	Fill
MW-38S	S,F		F	S,F	F	Fill
MW-39D	S,F		F	S,F	F	Qva/Till
MW-39S	S,F	S	F	S,F	F	Fill
MW-40S	S,F		F	S,F	F	Fill
OBS-1	S,F		F	S,F	F	Fill
OBS-2	S			S		Till
OBS-3	S			S		Fill
PZ-01	S,F		F	S,F	F	Qvr
PZ-05	S			S		Fill
PZ-06	S			S		Fill
PZ-08	S			S		Qvr
PZ-09	S			S		Qvr
PZ-10	S			S		Qvr
RW-01	S			S		Qvr
TDW-1	S			S		Qva
TDW-2	S,F		F	S,F	F	Qva
TDW-3	S,F		F	S,F	F	Qva
TSW-1	S			S		Fill
TSW-2	S,F		F	S,F	F	Fill
TSW-3	S,F		F	S,F	F	Fill

Notes:

S = Sampled and Analyzed in Spring (April 2013) event

F = Sampled and Analyzed in Fall (October 2013) event

Qvr = Vashon Recessional Outwash

Qva = Vashon Advance Outwash

Till = Pre-Fraser Till (Qpgt)







Legend

- Area of Investigation (AOI)
- Historical Railroad Features
- -- Interpreted Pipe or Utility
- Magnetic Anomalies
- EM Anomaly (Metallic Objects)
- High Conductivity Area (Conductive Soil)
- Geophysical Survey Limits

Notes:

Notes: 1. Geophysical Site Investigation, Gas Works Park by Zone 2013. 2. Historical structures provided by Floyd[Snider, 2012. 3. Site structures delineated as shown in the General Plan, Lake Station, Seatte Gas Company, April 1949, revised in June 1953, the 1950 Oil Lines, Seattle Gas Co. Map, and a 1956 aerial photograph. 4. Historical railroad features shown as delineated in General Plan, Lake Station, Seattle Gas Co., June 1938. 5. Structure labels shown in '() indicate previous MGP operational uses (pre-1946). 6. Data Source: 2005 USGS aerial photograph. Does not show current conditions.

DISCLAIMER: This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. The locations of all features are approximate. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.



Gas Works Park Site Seattle, Washington



ATTACHMENT 2A-1

Zonge Geophysical Site Investigation Report Gas Works Park April 2013



GEOPHYSICAL SITE INVESTIGATION GAS WORKS PARK SEATTLE, WASHINGTON



Photo: City of Seattle: http://www.seattle.gov/tour/images/gasworks8.jpg

Prepared for:

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April 2013

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- Figure A2 Total Magnetic Field
- Figure A3 Apparent Conductivity
- Figure A4 In-Phase Response

Appendix B – Technical Note: Geophysical Detection of Buried Objects



1.0 INTRODUCTION

Zonge International, Inc. (Zonge) conducted a geophysical site investigation at the Gas Works Park, Seattle, Washington. The investigation was conducted for GeoEngineers, Inc. as part of their supplemental investigation for Puget Sound Energy. This report describes the techniques and procedures used as well as presenting our results and interpretation.

The site, shown in Figure 1, was formerly a manufactured gas facility, manufacturing natural gas from coal and oil. Those operations ceased in 1956. The site also has a history of site alterations and decommissioning, removing structures, moving soils and debris. Soils are heterogeneous fill, often containing bricks, slag, and other construction and industrial materials. The site is currently a grass covered park with several areas of above ground vessels, towers, and piping remaining from the gas production facility.

The objective of the study was to identify buried objects, piping, tanks and other materials which may remain from the former operations on that site within the geophysical survey limits shown on Figure 1.

The geophysical investigation included:

- A magnetic (MAG) survey utilizing a Geometrics G858G magnetometer/gradiometer.
- An electromagnetic (EM) survey utilizing the Geonics EM31 terrain conductivity meter.
- A ground penetrating radar (GPR) survey utilizing a Geophysical Survey Systems Inc. SIR3000 control unit with a 400 MHz antenna.

Results of this geophysical investigation are summarized in Figures 2, *Primary Geophysical Targets*, and Figure 3, *Extended Geophysical Interpretation*, and discussed below in the Section 4, *Results and Interpretation*. Basic principles of these techniques are described in Appendix B, *Geophysical Detection of Buried Objects*.


2.0 FIELD SURVEY

Field work was conducted March 5, 6, & 7, 2013, by a senior geophysicist and a staff geophysicist from Zonge.

2.1 Magnetic Data Acquisition

The MAG survey was conducted using a Geometrics G858G cesium magnetometer/gradiometer. This instrument was run in the "continuous" sampling mode, recording the magnetic field at 0.1 second intervals (approximately 0.5 feet). Two magnetic sensors spaced 0.5 meters apart, one above the other, were used to obtain the vertical magnetic gradient. Line spacing for the MAG survey was 10 feet. Magnetic survey lines are shown on Figure 1 and the magnetometer data plots are provided in Appendix A.

2.2 EM Data Acquisition

EM data were acquired using a Geonics EM-31 terrain conductivity meter. Both quadraturephase (apparent conductivity) and in-phase data were recorded. Data were recorded at a 0.2 second interval, corresponding to a distance of approximately 1 foot. Data were recorded on an Allegro handheld ruggedized field computer (Windows CE/DOS) running DAT31 MK2 software from Geomar of Mississauga, Ontario. EM survey lines are shown on Figure 1 and the EM data plots are provided in Appendix A..

2.3 GPR Data Acquisition

GPR was conducted in areas where cultural interference limited the resolution of the MAG and EM techniques. The GPR survey utilized a Geophysical Survey Systems, Inc. (GSSI) SIR3000 control unit and a 400 MHz antenna mounted within a survey cart. Figure 1 shows GPR profile locations. GPR data were acquired in areas where cultural interference limited the resolution on MAG and EM techniques.

2.4 Survey Positioning and Mapping

For the MAG and EM surveys, location data were acquired simultaneously with the geophysical data using Differential Global Positioning Systems (DGPS). MAG data were acquired using a Trimble Ag132 DGPS system. That system provides visual feedback to the operator to assure that he is "on line" and that the survey area is covered uniformly. For the EM31 survey a Trimble GeoExplorer 6000 XH was used. A grid was established with pin flags placed at the ends of, and at intermediate locations along the lines. Each system is a real time differential GPS unit with "submeter" accuracy; hence positions are generally good to $\pm 1-2$ feet, but may be off by 2-3 feet.



3.0 DATA PRESENTATION & ANALYSIS

Magnetic (MAG) and electromagnetic (EM) data were gridded and contoured using the Geosoft Oasis montaj data processing and analysis software system. Color contour data plots are included in Appendix A.

3.1 Magnetic Data

Magnetic data are displayed on two figures, one plot of the analytic signal (Figure A1) and the total magnetic signal (Figure A2). The analytic signal is our preferred presentation as it provides a simplified signature and better resolution of the anomalous areas than unprocessed field data. A high in the analytic signal occurs directly over the magnetic "source." The total magnetic field plot shows the data from the top sensor of the G858, which was also used to calculate the analytic signal.

The observed magnetic field responds strongly to steel objects. Depth of exploration depends on the mass of steel in the object. Generally, the larger the mass and the shallower the object the stronger the response. Typically a drum size object can be detected at a depth of 5-10 feet. Shape and orientation of elongated objects also influence the magnetic response.

3.2 Electromagnetic Data

Both quadrature-phase (apparent conductivity) and in-phase EM31 data were recorded in the field. Appendix B includes a discussion of these two measured parameters of the EM response. Plots of both data sets are included in Appendix A.

The EM31 responds both to soil (terrain) conductivity and to metallic or electrically conductive objects (tanks, pipelines, communication lines, fences, reinforcing steel, etc.). The EM31 in-phase signal responds strongly to metallic conductors and is less sensitive to soil conductivity than the quadrature response. The unit of measurement for the in-phase response is the ratio in parts per thousand of the secondary field to the primary EM field (ppt). The EM31 quadrature-phase signal is proportional to the soil conductivity and is reported in units of conductivity, millisiemen/meter (mS/m). The EM31 was set to clip the signal at 208 mS/m so no conductivity variation was recorded above that threshold. The measured apparent conductivity is a weighted average of soil conductivity over the depth of exploration (15-20 feet) with the stronger weighting on the near surface. The quadrature signal also responds to metallic objects and will not reflect the soil conductivity in areas where metallic objects are present.

The EM31 is designed to measure soil conductivities to depths of 10-15 feet. It can often detect strong metallic conductors at somewhat greater depth.



3.3 Ground Penetrating Radar Data

Ground penetrating radar records electromagnetic wave reflections from objects with contrasting dielectric properties. Metal objects are very good reflectors. Plastic objects and voids are also good reflectors.

GPR data profiles were analyzed for reflections consistent with subsurface tanks, pipes or other buried materials. Depth of investigation of the GPR is limited by the conductivity of the soil. Clays and conductive soils attenuate the signal rapidly. At this site, depth of investigation was generally limited to 2-3 feet.



4.0 RESULTS AND INTERPRETATIONS

4.1 General Comments

Preliminary results were conveyed to GeoEngineers on March 12, 2013. Those preliminary results included eleven (11) "Primary Geophysical Targets" shown on Figure 2. Those preliminary targets were conveyed to GeoEngineers as possible locations for further sampling or drilling. Throughout this report, we have kept that original designation for as "Primary Geophysical Targets" for those preliminary targets.

More extensive data analyses lead to our Extended Geophysical Interpretation which is presented in Figure 3. The extended interpretation includes additional general areas of anomalous response identified with letters A-J.

While many anomalous areas were identified, we did not find any large anomalies which would be indicative of massive vessels or structures which might contain several tons of steel.

Geophysical data color contour plots are included in Appendix A. These include Magnetic Analytic Signal, Total Magnetic Field, EM31 Apparent Conductivity, and EM31 In-Phase Response. In-phase response background levels are represented by green and light blue tones in Figure A4. Red (strongly positive) and dark blue (strongly negative) tones indicate potential EM anomalies. The EM31 response to a buried metallic object may be positive or negative (or some combination of both) based on the orientation of the transmitter and receiver coils relative to the target.

4.2 Primary Geophysical Targets

Preliminary, "Primary Geophysical Targets" as well as associated ArcGIS files, were conveyed to GeoEngineers after completion of the geophysical survey and a preliminary examination of the data plots. These results were provided in order to guide GeoEngineers in their intrusive field investigations. These targets, shown on Figure 2, are characterized by both MAG and EM anomalies and are judged as the anomalies most likely to represent buried steel objects such as underground tanks.

4.3 MAG Anomalies

In Figure 3 we have identified several magnetic anomalies where steel objects are likely present in the subsurface. Most of these areas show a clutter of anomalies, indicative of a collection of objects with no single object dominating the response.



4.4 EM Anomalies

In Figure 3, areas identified as **High Conductivity Areas** exhibited apparent conductivities above 200 mS/m. This is possibly an area of ash or slag and/or very conductive pore water (ionic solutions) in the soils. Extensive clays might also produce the observed response.

Areas identified as **EM Anomalies** exhibit a chaotic rapidly varying EM response typical of scattered metallic debris. Depths are likely less than 15 feet as the EM31 sensitivity is strongly reduced below 12-18 feet. The EM31 responds to conductive materials (steel, aluminum or copper), either linear conductors such as pipes and cables, and/or metallic objects such as tanks or machinery.

Anomalies designated as **Interpreted Pipe or Utility** are EM anomalies indicative of long linear conductors such as metallic pipes, underground power cables, and communication cables.

Petrochemicals and non-aqueous phase liquids (NAPL) have little effect on the EM response unless they have a thickness of a few feet.

4.5 GPR Results

No ground penetrating radar (GPR) anomalies indicative of large underground objects or collection of objects were noted on any of the profiles. A few small "point reflectors", shallow utilities, and or tree roots were noted on some sections but we have not mapped those minor features. GPR depth of investigation was typically 2-3 feet and occasionally 4 feet. Shallow excavation features could be seen on some of the profiles around the large above ground tanks.

4.6 Discussion of Anomalies

Anomalies A through J are identified on Figure 3, *Extended Geophysical Interpretation*. These anomalous areas have been identified after a more complete data examination than the preliminary Primary Geophysical Targets. To a large degree, those primary targets are included within these anomalous areas.

Anomaly A

Anomaly A has a magnetic signature indicative of scattered buried steel objects. One of the stronger magnetic features was selected as a Primary Target. There is an area of high soil conductivity overlapping the southern portion of the MAG anomaly.

Anomaly B

Anomaly B includes two areas of chaotic MAG and EM response indicative of a collection of metallic materials. Two locations have been selected as Primary Targets.



Anomaly C

Anomaly C is an area with high magnetic response as well as an in-phase EM response, indicative of buried metallic objects. This is a broad feature with no single peak to identify as a primary target.

Anomaly D

Anomaly D is a broad area of MAG anomalies with an overlaying conductivity high. This is indicative of abandoned infrastructure, possibly pipes and other objects. One strong MAG anomaly has been selected as a Primary Target.

Anomaly E

Anomaly E is a broad EM and MAG anomaly, although the two do not appear entirely coincident. The EM anomaly may be due in part to a linear conductor, pipe or utility, possibly associated with additional metallic objects producing the MAG anomaly. No Primary Target was associated with this anomaly as it is more indicative of linear conductors and/or debris without a single strong anomalous target.

Anomaly F

Anomaly F is a strong, localized MAG anomaly near the concrete trestle structures. The monopole MAG response is indicative of the end of a pipe or vertical well casing. This anomaly was included as a Primary Target.

Anomaly G

Anomaly G includes an extensive area of strong and chaotic MAG and EM response. This is indicative of shallow buried materials. Four strong MAG anomalies that also included strong in-phase response were included as Primary Targets.

Anomaly H

Anomaly H is a linear trend of MAG anomalies, mostly coincident with linear EM anomalies. This feature is indicative of a steel pipe or series on pipes. As with Anomaly E, no Primary Target was associated with this anomaly as it is more indicative of a series of linear conductors without a single strong anomalous target.

Anomaly I

Anomaly I is a strong localized magnetic monopole within an area of high conductivity. This anomaly is indicative of a vertical pipe or well casing or perhaps moderate size steel object. It was selected as a Primary Geophysical Target.



Anomaly J

Anomaly J is a strong local MAG anomaly within an area of high conductivity. This is indicative of a buried object. We have assigned this as a Primary Geophysical Target. Its close proximity to the landscape structures (The Prow) and utility lines suggest that it may be associated with current infrastructure, irrigation or electrical.



5.0 SUMMARY AND CONCLUSIONS

The Gas Works Park is a busy site in terms of geophysical response and possible buried materials, as one would expect after 50 years of industrial operations and redevelopment/cleanup activities. We have outlined extensive anomalous areas indicative of scattered buried objects and several linear features indicative of buried pipes or utilities. Within those areas, we have highlighted several of the strongest anomalies, Primary Geophysical Targets, which could be indicative of buried tanks or other steel objects. We did not observe any large anomalies that might be associated with several tons of steel, e.g. large underground vessels or pieces of machinery.



6.0 CLOSURE

Zonge International, Inc. (Zonge) has performed this work in a manner consistent with the level of skill ordinarily exercised by members of the profession currently practicing under similar conditions. No warranty, express or implied, beyond exercise of reasonable care and professional diligence, is made. This report is intended for use only in accordance with the purposes of the study described within.

Geophysical surveys performed as part of this survey may or may not successfully detect or delineate any or all subsurface objects or features present. Locations, depths and scale of buried objects or subsurface features mapped as a result of this survey are a result of geophysical interpretation only, and should be considered as confirmed, actual, or accurate only where recovered by excavation or drilling.

We appreciate the opportunity to perform this geophysical investigation. Should you require further information concerning the field investigation, or this report, please contact us at your convenience.

Respectfully Submitted,

Zonge International, Inc.

Rowland B. French, Ph.D., L.G. Senior Geophysicist

Attachments: Figures 1 - 3 Appendix A - Geophysical Data Plots Appendix B - Geophysical Detection of Buried Objects

FILE: Zonge Gas Works Geophysics r12.docx REVISION: 2013-12-05 PROJECT: 13024













GEOPHYSICAL SITE INVESTIGATION GAS WORKS PARK SEATTLE, WASHINGTON

APPENDIX A

GEOPHYSICAL DATA PLOTS

- Figure A1 Magnetic Analytic Signal
- Figure A2 Total Magnetic Field
- Figure A3 Apparent Conductivity
- Figure A4 In-Phase Response



Agency Review Draft



Agency Review Draft





Agency Review Draft





Agency Review Draft





GEOPHYSICAL SITE INVESTIGATION GAS WORKS PARK SEATTLE, WASHINGTON

APPENDIX B

TECHNICAL NOTE:

GEOPHYSICAL DETECTION OF BURIED OBJECTS



Zonge Project 13024



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Photo 1-EM61



Photo 2-GPR



Photo 3-Magnetometer

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GEOPHYSICAL DETECTION OF BURIED OBJECTS

INTRODUCTION

Several geophysical techniques are used for locating buried objects such as underground storage tanks, pipes, utilities, drums and other debris. These techniques are used routinely, and are often recommended or required by state agencies, funding institutions and/or the EPA, particularly on sites where underground burial of steel drums or other debris may have occurred or where underground storage tanks are suspected.

Geophysics is generally used in the early reconnaissance phase of these investigations as a guide to sampling, excavation and/or placement of monitoring wells. In this paper we describe three of the most common geophysical techniques, electromagnetics (EM), magnetics (MAG) and ground penetrating radar (GPR).



Photo 4-EM31



Page 2

UTILITY OF GEOPHYSICS:

First, a few words about "geophysics" as used for environmental and geotechnical engineering applications. Surface geophysical techniques probe subsurface materials (soils and rock) using surface instruments. This is done by measuring physical signals which have interacted with the earth materials. These signals may be electrical, magnetic, acoustic (seismic) or electromagnetic.

Surface geophysics offers several advantages over other exploration techniques:

1) Surface geophysical methods are *Hon-intrusive* 'in that they do not disturb the ground surface, or stir up any contaminants which might be in the soil.

2) Geophysical methods *measure earth properties over a large volume*. Whereas drilling only samples the earth at the point of the borehole, the measured geophysical response is affected by earth materials several feet, or tens of feet, away from the instrument sensor. This allows broad areas to be effectively "screened" with a series of surface measurements.

3) Most geophysical equipment used in environmental and geotechnical applications *can be hand carried*. Geophysical surveys do not require vehicular access, but only a walking path, clear of brush and obstacles.

4) Geophysical surveys are relatively *inexpensive* and can be performed quickly.

TYPICAL OBJECTIVES:

Geophysics may be used in either a reconnaissance mode, or in a detailed survey mode. In the reconnaissance mode, geophysics is used to "screen" large areas to determine the presence or absence of buried objects. In more detailed surveys, the location and extent of the object is mapped in greater detail. This facilitates the efficient excavation of tanks or debris, aids the effective placement of monitoring wells, or improves the design of a sampling program. The techniques discussed here are also useful for objectives other than identifying buried objects. Electromagnetic induction (EM) is especially useful in mapping changes in soil (e.g. sand or gravel channels), mapping clay aquitards, and mapping contaminant leachate plumes in groundwater. GPR can be used to map shallow stratigraphy or to map zones of disturbed soils.

GEOPHYSICAL METHODS:

Three geophysical methods are commonly used in the search for buried objects: 1) electromagnetic induction (EM), 2) magnetics (MAG), and 3) ground penetrating radar (GPR). EM and magnetics are complementary methods, most effective in the reconnaissance mode but also useful for more detailed work. GPR is most effective for detailed work, but may also be used in reconnaissance surveys.

Electromagnetic Methods:

The electromagnetic induction (EM) technique measures the electrical conductivity of the earth by inducing a time varying electric current in the earth. This is shown schematically in Figure 1. The EM technique was developed to measure natural soil conductivity to aid in identifying soil types and to measure rock conductivity in order to identify zones of conductive mineralization.

Man-made metallic objects are generally orders of magnitude more conductive than natural soils. Thus, the electric currents induced in the ground by EM instruments will be dramatically affected by the presence of any man made metallic object. Examples include pipes, tanks, cables, concrete reinforcing steel, or steel drums. By looking for anomalous signals which cannot be attributed to natural soils, buried metallic objects can readily be identified.

Frequency-domain EM – EM31

Frequency-domain EM systems transmit a sinusoidal waveform at a fixed frequency, or at



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multiple frequencies. The resulting secondary magnetic field may be phase shifted, depending on the nature of the target. Both the in-phase component (in phase with the primary magnetic field) and the quadrature phase component (shifted 90° from the primary field) can be measured to provide the phase shift information.

The Geonics EM31 is a common frequency domain EM instrument, often used for buried object detection. The cover photo 4 shows the EM31 in a field situation. Figure 1 is a schematic showing the principles of operation. A transmitter coil is in one end of the boom and a receiver coil in the other end. Depth of investigation for the EM-31 is generally 10-15 feet, but it may detect large metal objects at a somewhat greater distance. The instrument can quickly cover a wide area, mapping anomalous areas (metallic object locations) as well as changes in the soil character.

Figure 2 shows some sample data over a disposal site where 55 gallon steel drums had been dumped in a field and then covered with soil. The noisy and/or negative "apparent" conductivity is a clear indicator of metallic objects. The EM31 also records an "in-phase response" which aids in identifying metallic conductors. Data in Figure 2 indicate the zone of burial covers most of the northwest expanse of the site.

Time-domain EM – EM61

Time-domain EM systems transmit a magnetic pulse, with a duration in the order of tens of microseconds (μ s). That magnetic pulse induces electric currents in the ground as well as in any metallic object which is buried (or on the surface) within its range of influence. Currents induced in metallic conductors decay at a much slower rate than currents induced in the ground. Hence, metallic conductors can be easily identified.

The EM61-MK2a (cover photo 1) is a timedomain metal detector manufactured by Geonics, Ltd., of Toronto, Canada. The EM61-MK2a instrument consists of two horizontal air cored coils, 1.0

FIGURE 1 PRINCIPLES OF ELECTROMAGNETIC INDUCTION



meter by 0.5 meters in size. The bottom coil acts as a receiver and transmitter and the top coil as a receiver. The instrument weighs about 75 lbs. and is pulled by one operator.

The Geonics EM61-MK2a has 4 time gates, to measure the rate of decay of the signal, and two receiver coils, to measure the field gradient. The rate of decay is dependant on the size, shape, and orientation of the metallic object. Generally, the EM61 is used to estimate gross target parameters, but can be used for more detailed discrimination of targets, particularly in identifying unexploded ord-nance (UXO) materials.

The two receiver coils are very helpful in the differentiating between near surface objects and deeper objects. Since the amplitude of the response is highly dependent on the distance between the coil assembly and target, small near surface targets often produce a response orders of magnitude larger than targets having greater size at deeper depths. This masking effect from the near surface materials



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is drastically reduced by processing output of the two coils, essentially subtracting a portion of the bottom coil response from the top coil response. This is referred to as the differential mode or the differential signal.

Figure 3 shows some sample data over a 55 gallon steel drum partially buried, essentially flush with the surface of the ground. The response from the top and bottom coils is indicative of a substantial metallic presence. The relatively weak differential response is indicative of a shallow target.



A) EM31 Apparent Conductivity



B) EM31 In-Phase Response





E) Vertical Magnetic Gradient





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Magnetic Methods:

Magnetic methods measure disturbances in the earth's natural magnetic field. These disturbances are caused by magnetic materials, either magnetic rocks, or man made objects containing iron or steel. This is shown schematically in Figure 4. Most soils have negligible magnetization (both induced and remnant). Thus, most magnetic disturbances from shallow sources can be attributed to iron or steel objects which have been placed there by man's activities.

Magnetometers used for buried object detection usually measure the gradient of the magnetic field. This is done by measuring the difference between the magnetic field at two sensors separated vertically by two or three feet. This configuration is more sensitive to nearby disturbances, and is less effected by disturbances caused by distant objects or shallow bedrock.

Photo 3 on the cover shows a magnetometer/ gradiometer. This instrument can also cover wide areas quickly, providing complementary data to EM. Figure 2 includes total magnetic field data, gradiometer data, and magnetic analytic signal data over the barrel disposal area. The large deviations in both total field and gradient are indicative of steel objects in close proximity.





Ground Penetrating Radar:

Ground penetrating radar (GPR), like other radar techniques, sends out an electromagnetic pulse (radio wave or microwave) which is reflected off a "target" and returns to the receiver. GPR operates at lower frequencies (80-1500 MHz) than other radar to obtain better penetration in the earth materials. The antenna is pulled slowly along the ground surface to produce a continuous subsurface profile.

Photo 2 on the cover shows a GPR unit in operation. The 400 MHz antenna shown is being pushed in its cart. The control and recording unit is carried on the cart enabling one person operation.

Figure 5 is an example GPR profile over a shallow vault. The vertical scale is a time scale, giving the time for the radar pulse to travel down to the reflector and return to the receiver. Knowing the pulse velocity in the soils, we can convert this to depth. The horizontal scale corresponds to distance along the surface. Fiducial time marks on the record are placed at four foot intervals. The vault



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lid reflector shown appears as a hyperbola on the record. The vault lid produces a strong reflection with a characteristic ringing of the electronics, which appears as a dark red or blue band below the first arrival from the vault lid.

GPR is a tool for looking at selected areas in detail. Its continuous subsurface profiles give a graphic portrayal of subsurface conditions, and often provide an excellent means of accurately locating pipes and tanks. However, the GPR depth of exploration is strongly dependent on soil conductivity and subsurface conditions. In dry, sandy soils useful data may be obtained from depths down to 15 feet, whereas in conductive clay soils, typical of the Willamette valley, investigation depth is often limited to 2 or 3 feet.

FIGURE 5 SAMPLE GPR PROFILE



DISCUSSION:

As we have stressed, EM and magnetics are effective in screening large areas quickly to identify areas where buried objects may be present. Often these techniques can provide a rough estimate of the size and depth of the object causing the anomalous readings. The choice of frequency domain EM (i.e. EM31) versus time-domain EM (i.e. EM61) depends on the objectives and the site. The EM61 is very effective at identifying small pieces of metal (e.g. unexploded ordnance), and offers some depth and discrimination capability. It is also less sensitive to cultural noise (e.g. buildings, vehicles, etc.) than the EM31. The EM61 can often resolve anomalies which are close together, where the EM31 does not. However, the EM61 requires a tight line spacing, typically 1 meter, to assure the area is covered. Also, the wheeled cart is difficult or impossible to operate on some sites (the EM61 can also be carried on a shoulder harness but is very awkward).

The EM31 is favored over the EM61 on more open sites where the objective is to locate underground tanks, drums, or collections of debris. The broader sphere of influence of the EM31 allows it to be run on a coarser line spacing, typically 5-20 feet depending on the target.

A major limitation of both EM and MAG is their sensitivity to cultural noise. Buildings, fences, metallic surface debris, and vehicles all create cultural noise. The EM and magnetic instruments respond to any metallic objects, whether buried or in plain view above ground. Thus, areas within 20 to 40 feet of buildings, vehicles or pipelines will be masked by the strong response from those objects. EM and magnetics will not be able to definitively identify other buried objects within that masked zone.

GPR on the other hand is fairly immune to those forms of cultural noise. The radar signal is confined to a broad beam, spreading at roughly a 45° angle, beneath the antenna. Most antennas are well shielded with little upward propagation of the pulse. Thus GPR can be run next to buildings, fences and parked vehicles. GPR may be run inside buildings and even over reinforced concrete.

Because the GPR beam is directional, it does not have the same utility as a reconnaissance tool



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as the EM and MAG techniques. Whereas the latter techniques would readily detect a large tank 10 or 20 feet off the survey line, GPR would not detect the tank unless the survey line passed directly over it.

CONCLUSIONS

No geophysical technique should be used without some form of "ground truth" provided by drilling, excavation, or some other form of sampling. The geophysical signature of an underground storage tank may be very similar to that of a buried automobile. However, geophysics can eliminate random drilling or extensive excavation when searching for underground tanks or other materials.

To conclude, EM, magnetic, and GPR methods are effective, complimentary techniques used in the detection and delineation of subsurface metallic objects. The choice of technique or techniques depends very much on both site conditions and the survey objective.

FURTHER READING:

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DISCUSSION OF GEOPHYSICAL

TECHNIQUES

GEOPHYSICAL DETECTION OF BURIED

OBJECTS

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ATTACHMENT 2A-2 TarGOST® Data Processing

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ATTACHMENT 2A-2 TARGOST® DATA PROCESSING

1.0 INTRODUCTION

This attachment is intended to provide a summary of the Tar-Specific Green Optical Screening Tool (TarGOST[®]) investigation and related data generated during the 2013 Supplemental Investigation at the Gas Works Parks Site (GWPS, Site). TarGOST[®] is a laser-induced fluorescence (LIF) screening tool designed to delineate nonaqueous phase liquid (NAPL) in the subsurface, generating in-situ real-time data. TarGOST[®] guidance is included as Sub-attachment 2A-2.6 (TarGOST[®] Guide). TarGOST[®] technology was developed by Dakota Technologies, Inc. (Dakota).

TarGOST[®] is deployed with direct push drilling. At the Site, Dakota's fiber optic cables were strung through the driller's rods; the TarGOST[®] tip along with the rods were advanced into the ground with the rig. The procedure works as follows:

- A shock-protected optical chamber (SPOC) drill bit is connected to fiber optic cables strung through drilling rods.
- A TarGOST[®] drilling probe is sent vertically into the subsurface, attached to a GeoProbe.
- Most of the laser light emitted by the optical window is reflected by the soil. In the presence of oil-like material (OLM) and tar-like material (TLM), polycyclic aromatic hydrocarbons (PAHs) in the NAPL absorb the light and move to an excited state.
- When the PAHs are restored to ground state, the return wavelength generated is longer than that of the laser light. This fluorescence behavior is captured by the optical fibers and a spectrometer within the TarGOST[®] system.
- The returning fluorescence is divided into four wavelength channels plotted on charts referred to as waveforms (energy [milli- or pico-volts] vs. time [nanoseconds]).
 - The first channel is reflection from soil, referred to as scatter and abbreviated as "%Sctr" (percent scatter).
 - The remaining three channels are fluorescence response of soil, referred to as %Fluor.
 - The %Fluor is normalized by the scatter, yielding an output known as Signal %RE.
 - %RE stands for %Reference Emitter (% is to the calibrated value determined using gray paint).
 - %Fluor and Signal (%RE) are graphed versus depth on the TarGOST[®] logs.
- The %RE and %Fluor are color-coded to help alert to shifts in NAPL types, for example from light NAPL (LNAPL) to dense NAPL (DNAPL).

The following sections describe TarGOST® field methodology, TarGOST® data types generated during and following the 2013 Supplemental Investigation, and TarGOST® data reduction. Appendix 5F (NAPL Evaluation) to the main RI includes additional discussion related to TarGOST® and NAPL at the GWPS.



2.0 TARGOST® FIELD METHODOLOGY

Forty-five TarGOST® explorations (TG-1 to TG-45) and two co-located explorations (TG-12R/46 and TG-42R) were advanced during the Supplemental Investigation (SI) between March 18 and March 26, 2013. Dakota provided TarGOST® equipment, and Cascade Drilling provided direct push drilling equipment. Two locations (TG-18B and TG-32B) had to be re-drilled near the original attempted locations because the first attempts met shallow refusal.

The TarGOST® system was outfitted onto a utility vehicle comprising a generator, computer, rod-rack, fiber optic cables and TarGOST® probe tips. The TarGOST® tip has a sapphire optical window emitting pulses of 523-nanometers (nm; green) laser light through the fiber optic cables from the TarGOST® system (generator, computer and LIF source) (Sub-attachment 2A-2.6 – TarGOST® Guide). The sapphire optical window on the TarGOST® tip was calibrated before each TarGOST® location with a standard reference emitter (100 percent frequency), a unique gray paint used at all sites (Dakota 2013).

3.0 TARGOST® DATA TYPES

Several types of TarGOST[®] data were generated during and after the 2013 Supplemental Investigation: NAPL LIF responses, TarGOST[®] logs and associated electrical conductivity (EC) data, TarGOST[®] soil confirmation samples, Dakota three-dimensional (3D) modeling, classification plots, the Dakota site report, and non-negative least squares (NNLS) waveform analysis. These data are discussed in the following subsections.

3.1. NAPL Sample LIF Responses

LIF responses from five NAPL samples collected at the Site are included as Sub-attachment 2A-2.2.1. Small product samples were collected at the very beginning of the 2013 Supplemental Investigation from any well that had NAPL in it. DNAPL samples were collected from DW-4, DW-5, DW-7 and MW-18. An LNAPL sample was collected from MW-9. Samples were sent to Dakota in advance of the TarGOST[®] drilling work to verify that the LIF equipment could respond to the different types of NAPL at the Site. DNAPL samples submitted to Dakota for LIF response produced signal %RE with orange tone and shorter lifetime/"skinny" waveform bases (plotted on the x-axis of the waveform callouts); the LNAPL sample produced signal %RE with yellow tone and longer lifetime/thicker waveform bases.

3.2. TarGOST[®] Logs and EC Data

TarGOST[®] logs for all 49 TG- probes are available in Sub-attachment 2A-2.2 (TarGOST[®] Logs and EC Data). The scale on the logs is consistent (0 to 40 feet deep and 0 to 600 %RE).

TarGOST[®] logs present %RE signal versus depth. Color-coding of signal %RE is generated by taking the normalized average of scatter and additional fluorescence channels. The call-out waveforms on the left of the log plot the channels. The waveforms plot signal in millivolts (mV) on the y-axis and time on the x-axis. Longer waveform bases also referred to as ski-slopes are indicative of solvated NAPL or petroleum products compared to skinny peaks indicative of "tar" (Dakota 2013). Fluorescence %RE is also presented on the logs. Because fluorescence removes scatter it is often more useful than waveforms in distinguishing different NAPLs. Scatter responds to soil type, with lighter soil resulting in higher scatter. When both the scatter and fluorescence go up, it is probably a false positive response due to geology (lighter soil). Examples include TG-25 at 9 feet, TG-31 at 12 feet and TG-41 at 20 feet, which range from 7 to 8 %RE. Therefore background response due to geology is at least 8 %RE.



EC readings were attempted at TarGOST[®] locations. However, difficult probing conditions resulted in sporadic EC data collection, with quality data collected at about 40 percent of the holes. For this reason, not all EC data depicted on the TarGOST[®] logs are accurate: a table summarizing accuracy of EC readings per log is included in Sub-attachment 2A-2.2.

3.3. TarGOST® Confirmation Samples

Six GeoEngineers' (GEI-) confirmation borings were completed next to TG- TarGOST[®] explorations. Soil impact observations and geology were logged. Twelve soil samples were collected from selected intervals within the six borings and split into two. One split sample was submitted to Analytical Resources, Inc. (ARI) for PAH analysis, and one split was submitted to Dakota for LIF %RE analysis. The TarGOST[®] responses from the soil samples are included in Sub-attachment 2A-2.3. Analytical concentrations for the split soil samples are included in Attachment 2A-9 to Appendix 2A. TarGOST[®] logs and classification plots were used in the process. Side-by-side comparison including analytical results, field screening and geologic units are presented in Figures 2A-2-1 to 2A-2-7.

Zones selected for sampling had a TG signal that was fairly uniform (not spikey) over a thickness of 6 inches or more. The selected zones included high, med and low TG responses.

Before splitting, soil samples were well-homogenized in a stainless steel bowl with a stainless steel spoon. The bowl was washed with alcohol between samples.

Each sample is represented as a separate log in Sub-attachment 2A-2.3. The naming convention for the soil splits on the logs is as follows: GEI_12_25_26 represents the split soil sample from GEI-12 from 25 to 26 feet deep. Dakota placed three different aliquots of each soil sample on the optical window for a preset amount of time (represented as feet on the log). Results indicate the heterogeneity within each sample. Then Dakota averaged the signals of the three aliquots to yield the best possible TG value for that sample.

3.4. Dakota 3D Modeling

Dakota completed 3D model of TarGOST[®] data collected at the GWPS. The model does not take into account analytical results, historic and recent field observations, geology or hydrogeology¹. To assist with model development, GeoEngineers provided some guidance to Dakota regarding general NAPL trends observed at the GWPS.

The model reflects a recombination of three stand-alone "subdomains." In general, they are Harbor Patrol area and north and west; Cracking Tower area and south; and MW-09 area, eastern/southeastern portion of upland and the northeast corner.

The model shows rainbow-colored sticks for each TG probe in 3D, with a range of colors that represents %RE. Dakota modeled five shells: one each at 15 %RE, 25 %RE, 50 %RE, 75 %RE and 100 %RE. The model also shows radial cross-section views through Harbor Patrol area, west of Cracking Tower area, just south of the Play Barn, and the northeast corner.

¹A separate 3D model developed by GeoEngineers for the GWPS includes geology, hydrogeology, chemistry and storm drain network information not included in Dakota's TarGOST® 3D Site-specific model.

3.5. Classification Plots

Dakota provided NAPL classification plots for TarGOST[®] logs, soil split samples, and NAPL samples (Sub-attachment 2A-2.4). NAPL Classification plots are derived from the waveforms, including scatter, average lifetime (tau) of the peaks on the y-axis and wavelength on the x-axis. Fill colors correspond to signal %RE from the TarGOST[®] logs. NAPL classification logs were used to distinguish NAPL types (i.e. LNAPL vs. DNAPL vs. mixes). Blue-shifted (left quadrant) and long-lived clusters are indicative of solvated² NAPL or petroleum products; red-shifted (right quadrant) short-lived clusters are indicative of heavier NAPL.

3.6. Dakota Report

The TarGOST[®] Investigation report by Dakota is available in Sub-attachment 2A-2.5 (TarGOST[®] Report). It includes detailed field notes, a calibration discussion, false positives/interference, a waveform discussion, and a table of production and observations.

3.7. NNLS Waveform Analysis

Waveforms provide insight into different types of NAPL. For example if TarGOST[®] response is observed on NAPL, longer waveform bases (ski-slopes) will appear in solvated NAPL or petroleum products compared to skinny peaks indicative of tar (Dakota 2013).

Dakota performed NNLS waveform analysis on all logs (Sub-attachment 2A-2.7). NNLS analysis separates the %RE LIF response to different NAPL types, called components, and a background component. Each component has a signature waveform. Software compares the component waveforms to the entire set of waveforms that make up a TarGOST[®] log. The log is broken into the matching components or NAPL types. Deviation or residual is also plotted on the left.

A "basis set" for the NNLS analysis (comprising distinct waveforms from a given depth range within a TarGOST[®] log) was chosen based on five lines of evidence: (1) samples that represented the greatest spatial coverage of the Site, (2) geographic clustering and classification plot clustering, (3) depth intervals that were "clean enough" to be harvested (i.e., not several NAPL types intermixed), (4) depth intervals that were located next to soil analytical samples and (5) discussion with Dakota.

The following four "basis set" components were selected:

- Dense 1 DNAPL from the MGP (harvested from TG-15 northeast of the Cracking Towers, 27.31 to 28.68 feet below ground surface [bgs]),
- Dense 2 DNAPL from Harbor Patrol and the former tar refinery (harvested from TG-21 at Harbor Patrol, 22.15 to 25.58 feet bgs),
- Light1 Petroleum-like LNAPL from the gully (harvested from TG-39, 11.37 to 13.32 feet bgs) and
- Light 2 MW-09-like LNAPL (harvested from TG-12 around 8.87 to 10.73 feet bgs).

² A solvated compound is one formed from the interaction of a solvent and a solute.

The entire set of TarGOST[®] logs was run with all four components so as to identify a "best fit" for all %RE³. Each log had its own background waveform analysis assigned by Dakota. On a few logs, there were signals Dakota was confident were not NAPL; for these logs, Dakota created temporary Basis Waveforms to eliminate the spurious (non-NAPL) results.

Dakota also performed NNLS analysis on the soil split confirmation samples. Because of a bug in the program, Dakota was unable to run NNLS analysis on the NAPL samples.

4.0 DATA REDUCTION

The TarGOST[®] data reduction process entailed the following: omitting data not representative of current conditions, deciding what to use for background, and creating an all-encompassing table showing interpreted NAPL intervals by depth for each TarGOST[®] boring. A discussion of TarGOST[®] data interpretation and TarGOST[®] correlation to NAPL field observations is included in Appendix 5F (NAPL Evaluation) to the RI report.

4.1. Data Exclusions

As discussed in the TarGOST[®] investigation report in Sub-attachment 2A-2.5, some depth intervals within certain TarGOST[®] borings had unreliable %RE responses, due to either pre-probing or broken fibers in the probe tip. As Dakota mentions (Sub-attachment 2A-2.5),

"... at many probing locations, the 0 to 3' interval was hand augered to look for the park irrigation system, then backfilled with the same material to provide lateral stability to the advancing the TarGOST[®] probe. Some locations were pre-probed with a dummy probe to 4.5' or deeper to get past rubble or obstructions. Locations that were hand augered or pre-probed do not provide reliable TarGOST[®] data in the disturbed interval. When looking at TarGOST[®] logs, keep in mind that the data in the upper interval may not represent subsurface contaminant distribution or concentration levels."

The following intervals were excluded from the TarGOST[®] data set:

- TG-18, 8 feet bgs to total depth (8.98 feet bgs) Inaccurate response identified by Dakota either on log or in report.
- TG-18B, 15.5 feet bgs to total depth (15.6 feet bgs) Inaccurate response identified by Dakota either on log or in report. TarGOST[®] probe was broken and bent at this interval, resulting in a false positive. Because there are inaccurate responses on this log, the classification plot for TG-18B omits outliers.
- **TG-32B**, 0 to 10 feet bgs Inaccurate response identified by Dakota either on log or in report.
- TG-33, 0 to 4.5 feet bgs Inaccurate response identified by Dakota either on log or in report. This interval was pre-probed. This response may not be representative. This omits outliers on its classification plot. Because there are inaccurate responses on this log, the classification plot for TG-33 omits outliers.

³ Note: scales are not consistent from log to log for the waveform analysis.

- TG-34, omit 0 to 2 feet bgs Inaccurate response identified by Dakota either on log or in report. This interval was pre-cleared. This response may not be representative. This omits outliers on its classification plot. Because there are inaccurate responses on this log, the classification plot for TG-34 omits outliers.
- TG-37, omit 2 to 26.05 feet bgs Inaccurate response identified by Dakota either on log or in report.
 Dakota report indicates the probe window was shifted. There is a clear elevated background signal with NNLS.
- **TG-41**, omit 0 to 10 feet bgs Inaccurate response identified by Dakota either on log or in report.

During waveform analysis, Dakota identified an additional interval whose response was likely a result of "paint" or "grass: TG-02, omit 0 to 5.8 feet bgs.

4.2. Background %RE Determination/Inferred NAPL Presence

Background response due to geology is thought to be at least 8% RE (see Section 3.2). The TarGOST[®] %RE cutoff value to distinguish between the presence and absence of NAPL at GWPS is conservatively 10%RE; the rationale for this cutoff is described in Appendix 0 of the RI report.

4.3. TarGOST® "Picks" Table

Interpreted NAPL intervals by depth for each TarGOST[®] boring were tabulated for use in the conceptual site model (CSM) and remedial investigation (RI). Depth intervals for each TarGOST[®] boring were assigned one of the following categories:

- No data (see Section 4.1 for more detail)
 - Depth interval identified as inaccurate by Dakota on log or in report because, for example, fibers broke, probe rod broke or probe window shifted.
- No impacts
 - <10 %RE depth intervals that had consistent %RE values of <10 %RE were considered to be "no impacts" or "background"
 - >10% %RE, but response was identified as grass or paint by Dakota during waveform analysis (e.g., TG-02, 0 to 5.8 feet bgs), or response had predominant waveform match to background basis set (TG-42, 0 to 8 feet bgs).
- NAPL impacts
 - LNAPL
 - LIGHT1 depth intervals whose predominant waveforms match⁴ LIGHT1 basis set
 - \circ LIGHT2 depth intervals whose predominant waveforms match LIGHT2 basis set
 - DNAPL
 - DENSE1 depth intervals whose predominant waveforms match DENSE1 basis set
 - o DENSE2 depth intervals whose predominant waveforms match DENSE2 basis set

⁴ Professional judgment was used in determining predominant waveform match for a given depth interval.

Correlation of TarGOST[®] picks to NAPL field observation picks is discussed further in Appendix 5F (NAPL Evaluation) of the RI report.

5.0 REFERENCES

Dakota. 2013. Personal communication (telephone call from Randy St. Germain, Dakota, to GeoEngineers).



Notes:

1. Refer to Attachment A-2 TarGOST Data Processing. Classification plots graph lifetime on vertical-axis and wavelength on horizontal-axis.

2. NAPL includes categories 'heavy sheen with NAPL' and 'tar or tar impacted interval' NAPL impact designation.

3. Geologic units: Af = fill; Qvr = Vashon recessional outwash; Qva = Vashon advanced outwash; Qpgt = pre-Fraser till.

4. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.





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Notes:

1. Refer to Attachment A-2 TarGOST Data Processing. Classification plots graph lifetime on vertical-axis and wavelength on horizontal-axis.

2. NAPL includes categories 'heavy sheen with NAPL' and 'tar or tar impacted interval' NAPL impact designation.

3. Geologic units: Af = fill; Qvr = Vashon recessional outwash; Qva = Vashon advanced outwash; Qpgt = pre-Fraser till.

4. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Class	fication Plots
	GEI-8 at 5-6 ft bgs
	3.00





Notes:

1. Refer to Attachment A-2 TarGOST Data Processing. Classification plots graph lifetime on vertical-axis and wavelength on horizontal-axis.

2. NAPL includes categories 'heavy sheen with NAPL' and 'tar or tar impacted interval' NAPL impact designation.

3. Geologic units: Af = fill; Qvr = Vashon recessional outwash; Qva = Vashon advanced outwash; Qpgt = pre-Fraser till.

4. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.





1. Refer to Attachment A-2 TarGOST Data Processing. Classification plots graph lifetime on vertical-axis and wavelength on horizontal-axis.

2. NAPL includes categories 'heavy sheen with NAPL' and 'tar or tar impacted interval' NAPL impact designation.

3. Geologic units: Af = fill; Qvr = Vashon recessional outwash; Qva = Vashon advanced outwash; Qpgt = pre-Fraser till.

4. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Soil Confirmation TarGOST Screening

No GEI-10 soil sample analyzed with TarGOST"

Classification Plots

No GEI-10 soil sample analyzed with TarGOST"





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1. Refer to Attachment A-2 TarGOST Data Processing. Classification plots graph lifetime on vertical-axis and wavelength on horizontal-axis.

2. NAPL includes categories 'heavy sheen with NAPL' and 'tar or tar impacted interval' NAPL impact designation.

3. Geologic units: Af = fill; Qvr = Vashon recessional outwash; Qva = Vashon advanced outwash; Qpgt = pre-Fraser till.

4. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document. GeoEngineers, Inc. cannot guarantee the accuracy and content of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.



SUB-ATTACHMENT 2A-2.1 TarGOST® NAPL Responses Logs



SUB-ATTACHMENT 2A-2.2 TarGOST[®] Logs and Electrical Conductivity Data

SUB-ATTACHMENT 2A-2.2.1 TarGOST® Logs



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	-35.0								
	-30.0								
	-25.0								



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	Site: Gas Work	ks Park		Y Coor 239463	d.(Lat-N) 3.6624 /	/ System:	Final dep 11.78 ft	oth:	
	GWP_	TG-0)2				TarGO	ST By C)akota
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	30.0								
Fluor Only Color is 41 parts not used 85 parts Red 89 parts Orange 55 parts Blue	-25.0								
							+		



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	Site: Gas Works Park	Y Coord.(Lat-N) / System: 239400.5248 /	Final depth: 16.01 ft
	GWP_TG-06		TarGOST By Dakota www.DakotaTechnologies.com
	-35.0 -40.0 0 100 200 300	400 500 5.0E3	
2 1 9.85 ft 8.6 %RE	30.0		
4 3	25.0		
59.0 %RE			I I I I I



FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator / Unit: SDA / TG1004	Elevation: 32.4 ft	Date & Time: 2013-03-19 13:12 PDT
DAKOTA	Client / Job: GeoEngineers /	X Coord.(Lng-E) / Fix: 1270715.347 /	Max signal: 9.9 %RE @ 12.17 ft
	Site: Gas Works Park	Y Coord.(Lat-N) / System: 239357.9123 /	Final depth: 21.60 ft
	GWP_TG-07		TarGOST By Dakota www.DakotaTechnologies.com
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	25.0		
9.9 %RE		- I I I I I I I I I I I I I I I I I I I	$\overline{+}$



FARGO, ND 701.237.4908 www.DakotaTechnologies.com	Operator SDA / TG	/ Unit: 51004			Eleva 32.7	ation: ft			Date & Tir 2013-03-1	ne: 9 14:35	PDT	
DAKOTA	Client / Jo GeoEngi	ob: ineers	1	-	X Co 1270	ord.(Lng 747.424	g-E) / Fix: 1 /	-	Max signa 33.4 %RE	/: @ 12.4	9 ft	
	Site: Gas Wor	ks Par	k		Y Co 2393	ord.(Lat 58.1004	-N) / Syst I /	em:	Final dept 22.16 ft	h:		
	GWP	_TG	-08						TarGOS www.DakotaTeo	Chnologies.	Dal	kota
	-40.0	100	200	300	400	500		5.0E3	50	5.	0	5.0
	-35.0											
2 1 1 13.06 ft 26.1 %RE	30.0											
4	-25.0											



TECHNOLOGIES	GeoEngi	neers /		12707 Elevat	82.064 /		18 Da	8.3 %	RE (@ 13.4	8 ft	-
	Site: Gas World Client / Jo	ks Park		Y Coo 23933 X Coo	rd.(Lat-N) 0.837 I rd.(Lng-E,	/ System:	Fil 19 M	nal c .89 ax si	lepth <mark>ft</mark> ignal.	:		
	GWP	_TG-0	9				Ta	w.Dako	OS otaTech	T By nologies.	Dak	ota
13.48 ft 18.3 %RE	-35.0	100 200) 300	400	500	5.0E3		20	40	2.0		1.0
4 3 2 1 1 2 49 ft	-25.0 -30.0											



FARGO, ND 701.237.4908 www.DakotaTechnologies.com	Operator / Unit: SDA / TG1004	Elevation: 33.0 ft		Date & Time 2013-03-19	: 16:38	PDT
DAKOTA	Client / Job: GeoEngineers /	X Coord.(Lng-E) / Fix 1270620.876 /		Max signal: 14.5 %RE @	0.41 f	t
	Site: Gas Works Park	Y Coord.(Lat-N) / Sys 239392.9768 /	stem:	Final depth: 13.04 ft		
	GWP_TG-10			TarGOST www.DakotaTechn	By I	Dakota
	40.0	0 400 500	5.0E3	50	5.0	1.0 2.0
	-35.0				-	
	30.0					
	25.0				-	







FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator / Unit: SDA / TG1004	Elevation: 35.1 ft	Date & Time: 2013-03-20 11:31 PDT
DAKOTA	Client / Job: GeoEngineers /	X Coord.(Lng-E) / Fix: 1270514.067 /	Max signal: 7.8 %RE @ 6.74 ft
	Site: Gas Works Park	Y Coord.(Lat-N) / System: 239083.0432 /	Final depth: 17.83 ft
	GWP_TG-13		TarGOST By Dakota www.DakotaTechnologies.com
	40.0 0 100 200 300	400 500 5.0E3	50 1.0 2.0
	35.0		
	30.0		
	25.0		







31.1 %RE	25.0				1 - 1 - 1 - 1 - 1 - 1 - 1		M.M.M.M.M.		AMAN AMAN ANA ANA ANA ANA ANA ANA ANA AN
4 2 23.00 ft 18.1 %RE	30.0								
	35.0								
	40.0	100	200 300	400	500	200	50 TarGOS	5 5	2.0 Dakota
	GVVP Site: Gas Wo	rks Park	.10	Y Co 2392	ord.(Lat-N 10.6132 /) / System:	www.DakotaTe Final dept 25.89 ft	chnologies h:	.com
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Client / J GeoEng Operator SDA / TO	lob: jineers r / Unit: G1004		X Co 1270 Eleva 37.3	ord.(Lng-E 423.502 ation: ft	=) / Fix:	Max signa 33.9 %RE Date & Til 2013-03-2	al: @ 15.6 me: 20 15:4	3 PDT



82.8 %RE	-25.0						L. M. M. W.		when the test of the second		Martin Mr. Manna Martin Martin Martin	
18.54 ft 45.6 %RE	-30.0					-		+			+	
	-35.0											
	40.0	100	200	300	400	500	10		50	10	2.0	
	GWF	'_TC	3-17						TarGOST By Dakota www.DakotaTechnologies.com			
	Site: Gas Works Park Client / Job: GeoEngineers /				Y Coord.(Lat-N) / System: 239329.5381 / X Coord.(Lng-E) / Fix: 1269790.288 /				Final depth: 28.57 ft Max signal: 82.8 %RE @ 16.96 ft			
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM												
	Operato SDA / T	or / Unit G1004			Elevation: 38.8 ft				Date & Time: 2013-03-21 08:13 PDT			



TECHNOLOGIES FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	GeoEngineers / Operator / Unit: SDA / TG1004	1269797.87 Elevation: 39.9 ft	Max signal: 27.0 %RE @ 8.91 ft Date & Time: 2013-03-21 09:32 PDT			
DAKOTA	Client / Job:	X Coord.(Lng-E) / Fix:				
	Site: Gas Works Park	Y Coord.(Lat-N) / System: 239376.3738 /	Final depth: 8.98 ft			
	GWP_TG-18		TarGOST By Dakota www.DakotaTechnologies.com			
	40.0 0 100 200 300	400 500 5.0E3	50 2.0 4.0 2.0			
	-35.0					
	30.0					
	25.0					



Callouts	Depth (ft) Signal (%RE)	Sctr 570 620 670 Cond (mS/m)	Sctr (%RE)	Fluor (%RE) Rate (in/s)
			1 2	
			+ -	
	5.0			
			IZ	
			1 7	Marrow Marrow
	10.0		1 2	
			+ ~	
			+ -	
			t t	
			I Z	
	15.0		+ 5	
			- + +	
			+ m	
			+ Mr	
			1 2	
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	25.0		+ ~~	
			Ī	Ī
			-	
			1	± ±
		—	+	
	-30.0		+	
			+	
			+	
		IIIIII	Ī	I I I I
	-35.0		+	
		Ţ	-	‡ ‡
			+	+ +
		1	+	‡ ‡
			+	Ŧ Ŧ
	40.0	400 500 50	50	
	OWD TO 40	400 500 5.0	TarGO	ST By Dakota
	GWP_1G-19		www.Dakota	Technologies.com
	Site:	Y Coord.(Lat-N) / System:	Final de	oth:
	Gas Works Park	239355.5459/ X Coord (I ng E) / Eive	24.95 ft	aal:
DAKOTA	GeoEngineers /	1269744.526 /	3.5 %RF	@ 4.07 ft
TECHNOLOGIES ARGO, ND 701.237.4908	Operator / Unit:	Elevation:	Date & 7	Time:
WWW.DAKOTATECHNOLOGIES.COM	SDA / TG1004	38.0 ft	2013-03	-21 17:09 PDT



7.3.9 70INE	-25.0									MMMM	
	30.0										
	-35.0										
	40.0	100	200	300	400	500	5.0	50	10	1.0 2.0	
	GWP	_T0	j-20					TarGOST By Dakota www.DakotaTechnologies.com			
DAKOTA	Site: Gas Wo	rks Pa	rk		Y Coord.(Lat-N) / System: 238996.0276 /			Final depth: 25.99 ft			
	Client / Job: GeoEngineers /				X Co 1269	ord.(Lng 764.259	-E) / Fix: I	Max sigr	Max signal: 75.9 %RE @ 14.87 ft		
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator	r / Unit. G1004			Elevation: 27.6 ft			Date & Time: 2013-03-21 12:18 PDT			





	25.0							-	+ + + +	enther first		marchil	-
	-30.0								-				
	-35.0												
	40.0	100	200	300	400	500		5.0	50)	2.0 4	.0	2.0
	GWP	_тс	3-22						TarC www.Da	GOS kotaTeo	ST By chnologies	Da	kota
	Site: Gas Wo	rks Pa	ırk		Y Co 2391	ord.(L 74.34	at-N) / Sysi 72 I	tem:	Final 24.04	dept ft	h:		
DAKOTA	Client / J GeoEng	lob: ineers	s /		X Co 1269	ord.(L 674.4	ng-E) / Fix: 6 I		Max : 8.6 %	signa	al: @ 8.86	ft	
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator	r / Unit G1004			Eleva 25.8	ation: ft			Date 2013	& Tir -03-2	ne: 21 14:2	1 PD	Ť



	-25.0							+ + + + + + + + + + + + + + + + + + +	Muldan	ANNA ANNA I I I I I	
	-30.0										
	-35.0										
	40.0	100	200	300	400	500	5.0	50	2.0	2.0 4.0	
	GW	P_TC	G-23					TarGOST By Dakota www.DakotaTechnologies.com			
	Site: Gas Works Park Client / Job: GeoEngineers /				Y Co 2392	ord.(La	t-N) / System: 4 I	Final depth: 24.52 ft Max signal: 9.2 %RE @ 0.70 ft			
DAKOTA					X Co 1269	ord.(Lr	g-E) / Fix: 6 /				
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator / Unit: SDA / TG1004				Elevation: 26.1 ft			Date & Time: 2013-03-21 15:00 PDT			





25.0 30.0 <td< th=""><th rowspan="3">FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM</th><th colspan="4" rowspan="2">Client / Job: GeoEngineers / Operator / Unit: SDA / TG1004</th><th>Eleva 30.0</th><th>ation: ft</th><th></th><th colspan="4" rowspan="2">Max signal: 8.0 %RE @ 9.16 ft Date & Time: 2013-03-22 08:29 PDT</th></td<>	FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Client / Job: GeoEngineers / Operator / Unit: SDA / TG1004				Eleva 30.0	ation: ft		Max signal: 8.0 %RE @ 9.16 ft Date & Time: 2013-03-22 08:29 PDT			
25.0 30.0 30.0 30.0 35.0 35.0 40.0 0 100 200 200 300 40.0 0 100 200 30.0 5.0 5.0 1.0 1.0 </th <th>X Co 1270</th> <th>ord.(Lng- 583.609 I</th> <th>E) / Fix:</th>						X Co 1270	ord.(Lng- 583.609 I	E) / Fix:				
25.0 30.0 35.0 40.0 0 100 200 300 400 500 5.0 50 1.0 1.0 GWP_TG-25 TarGOST By Dakota www.Dakota Technologies.com		Site: Gas Wor	ks Par	rk		Y Co 2388	ord.(Lat-N 55.4575	V) / System:	Final depth: 17.22 ft			
		GWP	_TG	-25					TarGOST By Dakota www.DakotaTechnologies.com			
25.0		40.0	100	200	300	400	500	5.0	50	1.0	1.0	
		-35.0								+		
		-30.0								+		
		-25.0								+		



TECHNOLOGIES FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operato SDA / T	r / Unit G1004	:		Eleva 26.5	ation: ft		Date & Time: 2013-03-22 09:19 PDT			
DAKOTA	Client / Job:				X Coord.(Lng-E) / Fix:			Max signa	1: @ 7 94 ft		
	Site: Gas Works Park				Y Coord.(Lat-N) / System: 238839.5312 /			Final depth: 20.88 ft			
	GWP	_тс	6-26					TarGOST By Dakota www.DakotaTechnologies.com			
	40.0	100	200	300	400	500	5.0	20 40	2.0	2.0	
	-35.0										
	30.0										
	-25.0					-					


	-25.0									
	-30.0									
	-35.0									
	40.0	100	200	300	400	500	5.0	50	1.0	2.0
	GWP Site: Gas Wo	_TG	3-27 rk		Y Co 2388	ord.(Lat-N 07.8902 /) / System:	Final dept	chnologies.c	om
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Client / J GeoEng Operato SDA / T	lob: ineers r / Unit. G1004	s /		X Co 1270 Eleva 25.3	ord.(Lng-E 599.03 I ation: ft	E) / Fix:	Max signa 7.0 %RE (Date & Til 2013-03-2	al: @ 5.56 ff ne: 22 10:22	PDT



	25.0							Mary Mary		
	-30.0									
	-35.0								-	
	-40.0	100	200	300	400	500	5.0	50	0.5	2.0
	GWP	_те	<u>)-28</u>			_		TarGC www.Dakota	ST By Technologies	Dakota
	Site: Gas Wor	rks Pa	rk		Y Co 2387	ord.(Lat- 82.1149	N) / System:	Final de 26.43 ft	pth:	
DAKOTA	Client / J GeoEng	lob: ineers	s /		X Co 1270	ord.(Lng 496.78	-E) / Fix:	Max sig	nal: @ 9.17	ft
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator SDA / TO	r / Unit G1004			Eleva 32.3	ation: ft		Date & 2013-03	Time: -22 11:29	PDT

Callouts	Depth (ft) Signal	(%RE) Sctr 570 620	670 Cond (mS/m)	Sctr (%RE)	Fluor (%RE) Rate (in/s)
				N	MMM	R
				Mar		Mars
				t the		
	5.0			+8	K. A.	- And
					MAN	
	10.0			+ ~	E .	The second
					Man	
				T T	M.M.	
				the state		
	15.0			t + + +	5	
				- M	1 Allandar	and
4 1 3 1						
2	20.0			- 2		
1				+	Land Land	Mr. Marte
14.34 ft						1 million
3.5 %RE				t t t	14 HAVAN	they have
	25.0			- And	AN AN	MAN AND
				ANN		M
				Month and	- Charles	- Annald
				+ <		***
	-30.0			+	-	+
			Ţ	-	-	Ţ
			+	+		1
	35.0			-	+	+
	-35.0		-	-	Ŧ	7
				+	Ţ	1
			1	+		+
	40.0					+ + + + + + + + + + + + + + + + + + + +
	GWP TG-20	g 300 400 500	5.0	TarGO	ST By	Dakota
	Site:	Y Coord.(L	at-N) / System:	www.Dakota	Technologies.c	com
	Gas Works Park	238793.71	56 /	28.65 ft		
DAKOTA	GeoEngineers /	1270422.3	75 I	4.8 %RE	@ 14.23	ft
FARGO, ND 701.237.490 WWW.DAKOTATECHNOLOGIES.CD	B Operator / Unit:	Elevation:		Date & T	ime:	DDT
	SDA/ IG1004	38.3 TT		2013-03	-22 13:30	

Callouts	Depth (ft)	Signal (%RE)	Sctr 570	620 670	Cond (mS/m)	Sctr (%RE)	Fluor (%RE) Rate (in/s)
							- In		W Manual
	5.0						Mary		ANNAN ANAN
	-10.0					-			-
	-15.0								
	-20.0								
	-25.0								+
	30.0								
	-35.0								
	40.0	00 200 300	400	500	5.0		20	0.5	1.0
	GWP_ Site:	TG-30	Y Cool	rd.(Lat-	-N) / Syste	m:	TarGC www.Dakota Final de	ST By Technologies.c	Dako
FARGO, ND 701.237.4908	Client / Job GeoEngine Operator / C	eers I	X Cool 12703	rd.(Lng 39.165	I-E) / Fix:		Max sign 4.3 %RE Date & T	nal: : @ 0.16 ft Time:	t



FARGO, ND 701.237.4908 www.DakotaTechnologies.com	Operator SDA / TO	r / Unit: G1004			Eleva 38.3	ation: ft		Date & Tin 2013-03-2	ne: 2 15:48	PDT	_
DAKOTA	Client / J GeoEng	lob: ineers	1		X Co 1270	ord.(Ln 253.22	g-E) / Fix: 5 I	Max signa 34.3 %RE	l: @ 6.74	ft	
	Site: Gas Wor	rks Pa	rk		Y Co 2387	ord.(La 88.071	t-N) / System: 2 I	Final depti 38.04 ft	h:		
	GWP	_TG	i-31	- 67	1			TarGOS www.DakotaTec	T By hnologies.c	Dak	ota
	-40.0 0	100	200	300	400	500	5.0	50	5.0	2	2.0
	-35.0							The state the state of the stat		Mr. Mr. Mar May	
	-30.0							and a state of the state of the state		April of My May Wall was a second	
	25.0							- + + + + + + + + + + + + + + + + + + +		Winny Marken Mark	
TT.S JOINE								T		What who	



FARGO, ND 701.237.4908 www.DakotaTechnologies.com	SDA / TG	1004		37.3	ft		Date & 1. 2013-03-	me: 22 17:11	PDT
DAKOTA	Client / Jo GeoEngi	neers /		X Con 1270	ord.(Lng-E 252.611 /	E) / Fix:	Max sign 4.0 %RE	al: @ 2.40 f	t
	Site: Gas Worl	ks Park		Y Co.	ord.(Lat-N 65.1085 /	l) / System:	Final dep 6.87 ft	th:	
	GWP_	TG-3	2				TarGO www.DakotaT	ST By echnologies.c	Dakot
	-40.0	100 200	300	400	500	5.0	50	1.0	1.0
	35.0								
	-30.0								
	25.0								

allouts	Depth (ft) Signal (%RE)	Sctr 570 620 670 Cond (mS/m)	Sctr (%RE)	Fluor (%RE) Rate (in/s)
reprobed to 10' bgs				A A A A A A A A A A A A A A A A A A A
	5.0			MMM MMM
	10.0		M m m	Munited and the second
	-15.0		M Manna	American American American American
2.26 ft 5.3 %RE	20.0			Manual Marine Marine
	25.0			Water of Mary Mary and Mary
.01 ft 0 %RE	30.0			man Min Mun Mun
	-35.0			
	40.0 100 200 300	400 500 5.0	50	5.0 2.0
	GWP_TG-32B		TarGC	ST By Dakota
	Site: Gas Works Park	Y Coord.(Lat-N) / System: 238860.1566 / X Coord (Lng. E) / Eiv:	Final de 33.42 ft	pth:
DAKOTA TECHNOLOGIES	GeoEngineers /	1270251.303 /	15.3 %R	E @ 22.26 ft



	25.0								
	30.0								
	-35.0								
	40.0	100 20	0 300	400	500	20	20 4	0 5.0) 1.0
	GWP_ Site:	TG-3	33	Y Co	ord.(Lat-N) / System:	Final de	aTechnologies	Dakota s.com
DAKOTA TECHNOLOGIES FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Client / Jol GeoEngin Operator /	b: leers I Unit:		X Co 1270 Eleva	ord.(Lng-E 234.667 I ation:	E) / Fix:	Max sig 57.4 %F Date &	nal: RE @ 3.0 Time:	4 ft



	25.0										And Market	
	30.0										-	
	-35.0										-	
	40.0	100	200	300	400	500	5.0E3	50		10 By		1.0 kota
	GVVP_ Site: Gas Work	s Pa	i-34 rk		Y Co 2387	ord.(Lat- 32.2498	-N) / System:	www.Dakot Final de 25.07 f	aTechno e <i>pth:</i> t	logies.c	om	Nota
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Client / Jo GeoEngin Operator / SDA / TG	b: neers / Unit: 1004			X Co 1270 Eleva 24.4	ord.(Lng 172.794 ation: ft	g-E) / Fix: I	Max sig 60.8 % Date & 2013-0	nal: RE @ Time 3-25	0.90	ft PD1	r



TECHNOLOGIES FARGO, ND 701.237.4908	GWP Site: Gas Wo Client / J GeoEng Operato	rks Pa Job: gineers	3-35 rk		Y Co 2387 X Co 1270 Eleva	ord.(La 74.639 ord.(Li 178.38 ation:	at-N)/S 18/ ng-E)/F 13/	ystem:	Ta www Fill 25 Ma 37 Da	nal de 19 ft ax sig .7 %F	DST aTechnolo epth: t nal: RE @ 7 Time:	By I	Dak	ota
	-35.0	100	200	300	400	500		200		20 40		50		
	-25.0									monton	1 1 1 1 1 1 1 1 1 1 1		When have	



FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator / Unit: SDA / TG1004	Elevation: 28.2 ft	Date & Time: 2013-03-25 13:49 PDT
DAKOTA TECHNOLOGIES	Client / Job: GeoEngineers /	X Coord.(Lng-E) / Fix: 1270180.147 /	Max signal: 357.5 %RE @ 8.62 ft
	Site: Gas Works Park	Y Coord.(Lat-N) / System: 238869.2682 /	Final depth: 18.17 ft
	GWP_TG-36		TarGOST By Dakota www.DakotaTechnologies.com
	40.0 0 100 200 300	400 500 20	20 50 1.0
	35.0		
	-30.0		
	25.0		
04.3 %INE		-	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII



1576.7 %RE	-25.0								white a start
20 10 17.62 ft 125.2 %RE	30.0								
	-35.0								
	-40.0	100 20	0 300	400	500	5.0E3	50	200	1.0
	GWP	_TG-3	37				TarGOS www.DakotaTeo	Chnologies.com	Dakota
	Site: Gas Wor	rks Park		Y Co	ord.(Lat-N) 64.4415 /	/ System:	Final dept	h:	
DAKOTA	Client / J GeoEna	lob: ineers /		X Co	ord.(Lng-E) 213.893 /	/ Fix:	Max signa	l: RE @ 13.3	36 ft
TECHNOLOGIES FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator SDA / TO	r / Unit: G1004		Eleva 36.5	ation: ft		Date & Tir 2013-03-2	ne: 25 14:53 F	PDT



FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator / Unit: SDA / TG1004		Eleva 30.8	ation: ft			Date 8	& Tim 03-25	e: 16:17	PDT
DAKOTA	Client / Job: GeoEngineers /		X Coord.(Lng-E) / Fix: 1270158.344 /				Max signal: 220.5 % RE @ 9.85 ft			
	Site: Gas Works Park		Y Coord.(Lat-N) / System: 238985.015 /				Final depth: 16.19 ft			
	GWP_TG-38	B					TarGOST By Dakota www.DakotaTechnologies.com			
	40.0 100 200	300	400	500	5	10	50 1	00	50	
	-35.0									
40 20 11.64 ft 212.7 %RE	30.0									
80 60	25.0							+		





Callouts	Depth (ft)	Signal (%RE)	Sctr 570 620 670	Cond (mS/m)	Sctr (%RE)	Fluor (%RE)	Rate (in/s)
Preprobed to 10' bgs. Signal within this zone may not accurately represent signal depth or intensity				MMMM	www.	Mar Mar Mar	MMMM
	5.0					AN AND AND A	NWMM
				MANAM		may and the party	MMMM
	-10.0			MMMMMMM	Jan Mann	- Mar A	MMMM
55 ft 5.9 %RE	15.0			MMMMM	What have		MMMMM
				Any William	Summer of M	MANA AND	Mary Mary
	20.0			WWWWWWWWW	Anna Anna	And Why have	In Mart Martin
	25.0			WWW WWWWWWWWWWWWWW		Warner Hander Hanner	maly marsh man Mul
				M. M. M.	1 1 1 1 1 1 1 1	and the former of the second sec	Anything to a second
.52 ft 0 %RE	-30.0						
	-35.0					-	
	40.0	00 200 300	400 500	20	20 40	20	10
	GWP	TG-41		20	TarGC	ST By	Dako
	Site: Gas Works	s Park	Y Coord.(Lat- 238760.1086	Final depth: 28.05 ft			
TECHNOLOGIES	GeoEngin Operator /	: eers / Unit:	X Coord.(Lng- 1270315.196 Elevation:	Max signal: 15.9 %RE @ 9.55 ft Date & Time:			
FARGO, ND 701.237.490 www.DakotaTechnologies.co	B Operator / SDA / TG1	004	Blevation: 38.8 ft		Date & 1	-26 09:00	PDT



TECHNOLOGIES FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	GeoEngineers / Operator / Unit: SDA / TG1004	1270790.097 / Elevation: 29.5 ft	59.4 %RE @ 11.29 ft Date & Time: 2013-03-26 10:19 PDT		
DAKOTA	Site: Gas Works Park Client / Job:	Y Coord.(Lat-N) / System: 239108.2314 / X Coord.(Lng-E) / Fix:	Final depth: 31.04 ft Max signal:		
	GWP_TG-42		TarGOST By Dakota www.DakotaTechnologies.com		
	35.0 40.0 0 100 200 300	400 500 5 10			
3 2 1 22.45 ft 20.9 %RE	30.0		Multimeter and the second seco		
5	25.0		All		



FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	SDA / TO	G1004	_		29.8	ation: ft		_	Date & Til 2013-03-2	me: 26 11:21	PDT	
DAKOTA	Client / Jo GeoEngi	ob: ineers	51		X Co 1270	ord.(Lng 788.311	I-E) / Fix:		Max signa 39.4 %RE	a/: @ 10.0	0 ft	
	Site: Gas Works Park				Y Coord.(Lat-N) / System: 239101.9129 /				Final depth: 31.22 ft			
	GWP_TG-42r								TarGOST By Dakota www.DakotaTechnologies.com			
	-40.0	100	200	300	400	500	-	20	20	2.0	1.0	
	-35.0											
	-30.0							Monthly Manufart Manufart	I I I I I I I I I I I I I I I I I I I	a su three a discover to the therether to	WWWWWWWWWWWWWWWWWWWWW	
20.4 %KE	-25.0						-	MMMMMMM	A share a shar		MM MM MM	



687.4 %RE	25.0	HAMMANN MAR	The second secon
2 1 1 19.41 ft 6.4 %RE	30.0		
	35.0		
	40.0 0 100 200 300	400 500 20	20 40 50 1.0
	GWP_TG-43		TarGOST By Dakota www.DakotaTechnologies.com
	Site: Gas Works Park	Y Coord.(Lat-N) / System: 239226.8316 /	Final depth: 26.41 ft
DAKOTA	Client / Job: GeoEngineers /	X Coord.(Lng-E) / Fix: 1270802.295 /	Max signal: 687.4 %RE @ 8.96 ft
FARGO, ND 701.237.4908 WWW.DAKOTATECHNOLOGIES.COM	Operator / Unit: SDA / TG1004	Elevation: 28.5 ft	Date & Time: 2013-03-26 13:12 PDT



FARGO, ND 701.237.4908 www.DakotaTechnologies.com	Operator / U SDA / TG10	04		Eleva 34.3	ation: ft		Date & T. 2013-03-	me: 26 14:16 F	TDY
DAKOTA	Client / Job: GeoEngine		X Coord.(Lng-E) / Fix: 1270521.787 I			Max signal: 87.5 %RE @ 7.73 ft			
	Site: Gas Works		Y Coord.(Lat-N) / System: 239249.0687 /			Final depth: 12.10 ft			
	GWP_1	G-44					TarGOST By Dakota www.DakotaTechnologies.com		
	40.0	0 200	300	400	500	20	20	5.0	1.0
	-35.0								
4 2 8.39 ft 53.4 %RE	-30.0								
6	-25.0								



FARGO, ND 701.237.4908 www.DakotaTechnologies.com	Operator / Unit: SDA / TG1004	Elevation: 35.5 ft	Date & Time: 2013-03-26 14:56 PDT		
DAKOTA	Client / Job: GeoEngineers /	X Coord.(Lng-E) / Fix: 1270514.446 /	Max signal: 41.4 %RE @ 8.78 ft		
	Site: Gas Works Park	Y Coord.(Lat-N) / System: 239230.2581 /	Final depth: 18.82 ft		
	GWP_TG-45		TarGOST By Dakota www.DakotaTechnologies.com		
	35.0 40.0 0 100 200 300	400 500 20			
2 8.93 ft 23.5 %RE	30.0				
6	25.0				



SUB-ATTACHMENT 2A-2.2.2 TarGOST® Butterfly Log Plots





SUB-ATTACHMENT 2A-2.2.3 TarGOST® Electrical Conductivity Data

File	Date/Time	Final Depth	Max Signal	Max Signal	RE Area	EC Good	EC Bad	EC NC*
GWP_TG-01	3/18/2013 14:33	7.2	14.4	1.5	1920.29			Х
GWP_TG-02	3/18/2013 15:56	11.8	336.3	8.1	1923.46			Х
GWP_TG-03	3/19/2013 8:14	14.9	8.1	1.3	1886.83	Х		
GWP_TG-04	3/19/2013 9:19	9.6	43.6	4.2	1901.04	Х		
GWP_TG-05	3/19/2013 10:10	24.3	196.5	24.3	1944.2	Х		
GWP_TG-06	3/19/2013 11:10	16.0	59.6	9.0	1982.31	Х		
GWP_TG-07	3/19/2013 13:12	21.6	9.9	12.2	1956.09	Х		
GWP_TG-08	3/19/2013 14:35	22.2	33.4	12.5	1829.71	Х		
GWP_TG-09	3/19/2013 15:26	19.9	18.3	13.5	1881.34	Х		
GWP_TG-10	3/19/2013 16:38	13.0	14.5	0.4	1801.6	Х		
GWP_TG-11	3/20/2013 8:31	24.6	198.0	15.6	1834.92	Х		
GWP_TG-12	3/20/2013 10:07	29.4	466.6	28.2	1734.39	Х		
GWP_TG-13	3/20/2013 11:31	17.8	7.8	6.7	1807.76	Х		
GWP_TG-14	3/20/2013 13:14	22.2	152.4	14.2	1776.78		Х	
GWP_TG-15	3/20/2013 14:16	28.8	669.2	28.5	1938.38		Х	
GWP_TG-16	3/20/2013 15:43	25.9	33.9	15.6	1774.79		Х	
GWP TG-17	3/21/2013 8:13	28.6	82.8	17.0	1887.68	Х		
GWP TG-18	3/21/2013 9:32	9.0	27.0	8.9	1811.81	Х		
GWP_TG-18B	3/21/2013 10:06	15.6	340.1	15.6	1749.96	X		
GWP TG-19	3/21/2013 17:09	24.9	3.5	4.1	2077.19			Х
GWP TG-20	3/21/2013 12:18	26.0	75.8	14.9	2056.59			Х
GWP TG-21	3/21/2013 13:16	25.9	323.3	19.3	1971.11			Х
GWP TG-22	3/21/2013 14:21	24.0	8.6	8.9	2030.76			Х
GWP TG-23	3/21/2013 15:00	24.5	9.2	0.7	1996.97			Х
GWP TG-24	3/21/2013 15:47	28.0	229.4	21.6	2086.22			X
GWP TG-25	3/22/2013 8:29	17.2	8.0	9.2	1839.87			X
GWP TG-26	3/22/2013 9:19	20.9	28.7	7.8	1820.67			X
GWP TG-27	3/22/2013 10:22	17.0	7.0	5.6	1794.48			X
GWP TG-28	3/22/2013 11:29	26.4	5.9	9.2	1879.7			X
GWP TG-29	3/22/2013 13:30	28.6	4.8	14.2	1889.64			X
GWP TG-30	3/22/2013 15:00	5.0	4.3	0.2	1818.87			X
GWP TG-31	3/22/2013 15:48	38.0	34.3	6.7	1801.83			X
GWP TG-32	3/22/2013 17:11	6.9	4.0	2.4	1886 48			X
GWP_TG-32B	3/22/2013 17:35	33.4	15.3	22.3	1803.47			X
GWP TG-33	3/25/2013 9:39	22.1	57.4	3.0	1858	х		
GWP TG-34	3/25/2013 10:45	25.1	60.8	0.9	1857.76	X		
GWP TG-35	3/25/2013 11:36	25.2	37.7	7 1	1813 13	X		
GWP TG-36	3/25/2013 13:49	18.2	357.5	86	1954 42	X		
GWP TG-37	3/25/2013 14:53	26.0	1624.4	13.4	1830.24	X		
GWP TG-38	3/25/2013 16:17	16.2	220.5	9.8	1658 19		х	
GWP TG-39	3/25/2013 17:09	26.0	454.6	15.6	1732 76		x	
GWP TG-40	3/26/2013 8:06	21.3	1396.6	9.0	1808.95		~	х
GWP TG-41	3/26/2013 9:00	28.0	15.9	9.5	1846 64			X
GWP TG-42	3/26/2013 10:19	20.0	59.3	11 3	1878 98			X
GWP TG-42r	3/26/2013 11:21	31.0	20.4	10.0	1880.06			x
GWP TG-43	3/26/2013 11.21	26.4	687.3	۵.0 م ۸	1754 07			X
GWP TG-44	3/26/2013 13.12	10.4	87 5	5.0 7 7	1794 74			X
GWP TG-45	3/26/2013 14.10	12.1	Δ1 Λ	7.7 2.2	1876 00			X
GWP TG-46	3/26/2013 15:44	24 6	340 6	0.0 8 A	1741 52			x
<u> </u>	0/20/2010 10.44	27.0	0-0-0	0.0	1771.52			~ ~

[STATS] File Count=49 Total Depth=1061.8 Max Depth=38.0 Max Signal=1624.4

* Not Recorded

SUB-ATTACHMENT 2A-2.3 TarGOST[®] Confirmation Sample Logs





DAKOTATECHNOLOGIES.COM	Client / Job: GeoEngineers / Operator / Unit: SDA / TG1004			Elevation: Unavailable	Date & Time: 2013-04-29 10:21 PDT				
				X Coord.(Lng Unavailable	-E) / Fix: / NA	Max signal: 8.4 %RE @ 4.30 ft			
	Site: Gas Works Park			Y Coord.(Lat- Unavailable	Final depth: 9.90 ft				
	GEI_7	_12_14	4				TarGOST By Dakot www.DakotaTechnologies.com		
	-14.0-							10	
	-12.0								
Black sand and gravel, no MGP odor	-10.0								
and a second						<u></u>	1		


















SUB-ATTACHMENT 2A-2.4 TarGOST® Classification Plots

SUB-ATTACHMENT 2A-2.4.1 Classification Plots for NAPL Responses



SUB-ATTACHMENT 2A-2.4.2 Classification Plots for TarGOST® Logs







































GWP_TG-19	
and as	







GWP_TG-23					
				-	
Party of					







GWP_TG-27				
· interest			0	

GWP_TG-28	1				
a initi	÷.				
	A CO				
GWP_TG-29					
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20.				0	-

GWP_TG-30	



GWP_TG-32						
		0			0	

































SUB-ATTACHMENT 2A-2.4.3 Classification Plots for Confirmation Samples























SUB-ATTACHMENT 2A-2.5 Dakota TarGOST® Investigation Report Gas Works Park July 2013

TarGOST[®] Investigation

Gas Works Park Seattle, Washington

Report Date: July 18, 2013

Prepared for: GeoEngineers Project Manager: Zanna A. Satterwhite, LG

Prepared by: Steve Adamek, P.G. & Randy St. Germain Dakota Technologies, Inc. 2201-A 12th St. N. Fargo, ND 58102 Phone: (701) 237-4908 Fax: (701) 237-4908 Fax: (701) 237-4926 <u>sadamek@dakotatechnologies.com</u> <u>stgermain@dakotatechnologies.com</u> This report summarizes the field deployment of the Tar-Specific Green Optical Screening Tool (TarGOST®) at the Gas Works Park Site located at 2101 N Northlake Way on the north side of Lake Union in Seattle, WA. It includes a project summary, general field observations, calibration of the TarGOST system, false positive/interference discussion, waveform discussion, and a daily production and observations table.

Project Notes

Sunday, March 17, 2013 – Dakota Technologies Inc. (Dakota) TarGOST operator, Steve Adamek traveled to Seattle, Washington. This was a travel day only, no TarGOST data was collected.

Monday, March 18, 2013 – Steve arrived on-site at 7:45 a.m. GeoEngineers site personnel conducted a site safety meeting and a site walk with all who were present. A secure staging area was setup in the parking lot of the Gas Works Park with a lockable storage container and a lockable fenced in area. A utility vehicle (UTV) from a local rental company arrived and was outfitted with the TarGOST system, a weather enclosure, generator and a rod rack. The Geoprobe rig and operator arrived about noon. It was discovered that the rods provided by Boart Longyear to push the TarGOST probe, were in very poor condition. Time was spent selecting the best rods, repairing many to make them useable, and then stringing the TarGOST fiber optical cable through them.

Data collection began at 1:30 p.m. at location number GWP-TG-01. We encountered rubble and the TarGOST probe broke off at 7' bgs. Steve was unable to remove the broken off probe and had to pull the fiber cable until it broke to recover the majority of the cable. The UTV and TarGOST system were taken back to the staging area to install a new probe and optical fiber cable.

Most locations were hand-augered to 3' bgs by Boart Longyear personnel to prevent damage to the park's irrigation system. Nearly all locations required the use of plywood pads to prevent damage to the grass. Considerable time was spent moving plywood to get to boring locations. GWP-TG-02 was started about 3 p.m. and reached a total depth of 12' bgs when refusal was encountered. Electrical conductivity (EC) data was inadvertently not recorded for either of the day's TarGOST locations. Holes were grouted and plywood pads moved to new locations. Crew left the site at 5:45 p.m.

Tuesday, March 19, 2013 – Dakota's TarGOST operator was on-site at 6:50 a.m. for a 7 a.m. requested start. The generator was fueled up and the TarGOST system started. GWP-TG-03 was started at 8:15 after preclearing to 3'. The probe was pushed to refusal at 14.89' bgs. Good TarGOST data was collected and the EC was working properly. GWP-TG-04, 05 and 06 were done before lunch. After lunch, work was resumed at location GWP-TG-07. The hole was pre-probed to 4.5' to get past some rubble before starting the TarGOST logging. GWP-TG-08, 09 and 10 were also advanced before ending work for the day. New probe rods had arrived so at the end of the day Steve removed the worn out rods and restrung with new rods. He left the site at 5:45 p.m.

Wednesday, March 20, 2013 – Steve was on-site at 7 a.m. He started logging at 8:32 a.m. and pushed GWP-TG-11 to refusal at 24.64' (encountered some rubble at the surface). GWP-TG-12 was started at 10:08 and after preprobing to 4.5' bgs GWP-TG-13 was started at 11:33 and pushed to refusal at 17.83'. The TarGOST data looked good. The crew took a lunch break started at 12:15. Location GWP-TG-14 was started at 11:15 p.m. The TarGOST data looked normal but the EC data seemed noisy. After completing the boring the EC wires were examined and cleaned. There appeared to be a break in the wire somewhere inside the cable. It was decided not to take the time to repair the break because it would probably take an hour or more to restring cables and put on new down-hole tooling. The crew began logging location GWP-TG-15 at 2:17 pm but the direct push rig was having electrical problems. We began location GWP-TG-16 at 3:42 p.m. and pushed to 25.89' bgs. The direct push rig had problems again after this hole so Steve took the TarGOST system back to the staging area to

replace the TarGOST probe and EC dipole. Steve was able to get everything ready for Thursday. Steve left the site at 6:45 p.m.

Thursday, March 21, 2013 – Dakota personnel were on-site at 7 a.m. Started location GWP-TG-17 at 8:15 and pushed to 28.57'. GWP-TG-18 was pushed to 9'bgs and got hard refusal. The crew tried to probe through the obstruction with a dummy point with no success. They changed location and pre-probed to 12' bgs and then pushed location GWP-TG-18B through the pre-probed hole to refusal at 15.06'bgs. The probe broke off and bent first rod 10:28 a.m. Steve went back to the staging area to string up a new cable and attach a new TarGOST probe. Dakota had no fiber cables left on-site that have EC wires. TarGOST system was operational again at 11:43 a.m. The crew began probing GWP-TG-20 at 12:20 p.m. The location was pre-probed to 4.5'bgs and pushed to 25.99'. No EC data was collected at this location. GWP-TG-21, 22, 23 and 24 were done by 4:20 p.m. The crew started GWP-TG-19 at 4:50 p.m. but got refusal at 3.5', so overwrote TarGOST file and moved slightly. The new GWP-TG-19 was pushed to 24.95'. Steve left the site at 6 p.m.

Friday, March 22, 2013 – Crew was on-site at 7 a.m and started location GWP-TG-25 at 8:30 a.m. (pushed to refusal at 17.22' bgs). They also logged GWP-TG-26, 27 and 28 before lunch. GWP-TG-29 was started at 1:30 and was pushed to 28.65' bgs. Probe rig was having electrical problems again. Set up at location GWP-TG-30 but got refusal at 5' repeatedly. We started GWP-TG-31 about 4 p.m. and pushed to 38.04'. GWP-TG-32 was pre-probed to 4.5' but got refusal at 6.87' bgs. GWP-TG-32B was pre-probed to 10'bgs and started logging at 5:37 p.m. The log was terminated at 33.42'. TarGOST data was transferred to the client, and operator was off site by 6:30 p.m.

Saturday, March 23, 2013 – No field work (park is too busy on weekends) Sunday, March 24, 2013 – No field work

Monday, March 25, 2013 – Dakota was on-site at 7:05 a.m. While Boart Longyear workers laid out mats for the first locations, Steve removed the fiber cable and installed one that had functional EC wires. The TarGOST system was ready to go about 9 a.m. Location GWP-TG-33 was pre-probed to 4.5' then logging began at 9:40 a.m. The probe was pushed to 22.08', TarGOST and EC data looked good. GWP-TG-34 and 35 were done before lunch. A lot of mats had to be moved to get to the next probe location. GWP-TG-36 was pre-probed to 4.5' and logging started at 1:51 p.m.; refusal was reached at 18.17' bgs. Log GWP-TG-37 was started at 2:55 p.m. The background of the TarGOST log was elevated for much of the log, very much different from other logs in the area. After recovering the rods and probe, the RE and background was checked to identify the problem. The RE was not much different than the original measurement made at the beginning of the push but the background was very high. After disassembly it was found that the parabolic mirror in the probe had (atypically) shifted position, resulting in the high background. Large signals were unaffected by the problem, small signals would have been buried in the high background however. The repair was done quickly while the rig was being moved to the next location. GWP-TG-38 and 39 were logged but the EC was not working properly. Work for the day was completed at 5:30; operator was off site at 6 p.m.

Tuesday, March 26, 2012 – Dakota was on-site at 7 a.m. EC was not operational because no more cables were available with intact EC wires. GWP-TG-40 was started at 8:07 a.m. and was pushed to 21.30' bgs. GWP-TG-41 was pre-probed to 10' bgs, started logging at 9 a.m. and pushed to 28.08'. GWP-TG-42 was located at the shore on the east edge of site. Crew began logging at 10:20 a.m. and penetrated some very loose cinder material, pushed to 31.04'bgs. It was decided to do a duplicate log here to get a feel for subsurface homogeneity. GWP-TG-42r was located 6.5' south of TG-42. Started log at 11:24 a.m. and pushed to 31.22'. After lunch GWP-TG-43, 44, 45 and 46 were logged. GWP-TG-46 was a duplicate log for location GWP-TG-12. Logging for the project was completed at 4:15 pm. Equipment was taken back to the staging area and
disassembled for shipment back to Dakota. All digital TarGOST data was given to the client. Operator left site at 7 pm.

Wednesday, March 27, 2013 - Travel day

General Observations/Notes of Interest

Breakdowns/Standby: Production was below average for this TarGOST project. Several factors contributed to the slower than normal data collection rate. Site-related production restrictions included hand-augering to look for irrigation, site related rubble, and the need for plywood padding to drive on the grass. Work related production restrictions included TarGOST equipment failures do to difficult probing conditions (EC and mirror problems), grouting and probe machine break downs. Two probe break-offs and several cable changes resulted in approximately 4 hours of down-time. It should be noted that where possible, TarGOST related hardware was repaired or replaced before of after normal daily work.

Safety Incidents: NA

Validation/Sampling by Dakota: Soil samples collected by GeoEngineers during and after the TarGOST study generally correlated well with the *in-situ* logs.

General comments: As stated, the daily production was poor compared to historical averages but reasonable given the challenging subsurface and surface circumstances. The TarGOST data collected at this site was of high quality and the few anomalies in the data have been noted. EC data collection was somewhat sporadic with quality data collected at about 40% of the holes.

At many probing locations, the 0 to 3' interval was hand augered to look for the park irrigation system, then backfilled with the same material to provide lateral stability to the advancing the TarGOST probe. Some locations were pre-probed with a dummy probe to 4.5' or deeper to get past rubble or obstructions. Locations that were hand augered or pre-probed do not provide reliable TarGOST data in the disturbed interval. When looking at TarGOST logs, keep in mind that the data in the upper interval may not represent subsurface contaminant distribution or concentration levels.

Calibration of the TarGOST

Prior to conducting each log, two measurements (RE and Background) are recorded.

Reference Emitter (RE): The RE is a standard substance that is used to calibrate the TarGOST instrument prior to every log. It reflects and fluoresces at known and consistent levels. It serves two main purposes:

1) **Qualitative examination the performance of the instrument -** RE needs to be the correct shape so it is confirmed that all four channels (filters, etc.) are intact and functioning. A bad or misshapen RE waveform indicates potential damage of the detection system optics.

2) **Quantitatively "calibrate" the instrument -** RE is used to achieve the proper signal intensity (by adjusting laser energy). An RE in the proper range keeps the instrument in the optimum range for the fluorescence detector and electronics. The RE is a calibration for the response of the system to a known fluorescence signature, not a method of converting fluorescence to a known concentration. All downhole measurements are normalized to a percentage of the RE. A 100% RE reading simply means that a measured material has a

fluorescence/scatter signal that is identical to that of RE. A 200% RE means a substance has a fluorescence/scatter signal twice that of RE, and so forth.

RE range: RE area's typically fall between 1,600 and 2,000 pVs for TarGOST (picovolt-seconds, a measure of waveform area). Precise RE intensity 'tuning' by adjusting the laser excitation light to achieve an exact value is unnecessary because all signals are reported as a percent of this signal (%RE).

Background: The background is a measure of the optical cleanliness of the light path (e.g. fiber optics, mirror, window, filters). Sources of signal in the background include foreign material on fiber faces, filter auto-fluorescence, mirror and window fluorescence, and reflection/scatter from scratched/worn windows. The background waveform is not applied to the data collected (i.e. it is not subtracted as a background) and is taken only as a general data quality measure and is employed by the operator to insure that there are no significant defects that could raise the system background - making it more difficult to discern low NAPL saturation (staining) responses.

Background range: Background values can vary widely (in terms of relative percent difference) from 0.1% of the RE signal to 10%. In terms of area, the values can range from 0 to 50 pVs. As the background increases beyond 10% for TarGOST, a new window and a re-assembly of the probe may be needed. However, there is no hard cut-off value and a balance must be struck between site needs and available time.

False Positives / Interference

In some cases TarGOST will respond to naturally fluorescent minerals, biogenic minerals (shells) and organic matter like peat. Most often this response shows a sufficiently different signature or waveform and is of relatively low response compared to LNAPL and DNAPL, with relatively fresh rotting wood being a major exception in that it can fluoresce as intensely as tar/creosote. Questionable signals (fill colors and waveforms that differ from known NAPL responses) will most often be flagged by the operator and should be sampled to provide an understanding of the materials present and the resulting fluorescence signals. Feel free to call Dakota to discuss co-sampling locations or interpretation of the co-sampling results.

Waveform Discussion

Careful co-sampling, examination, and analysis of soil cores are required to determine what benefit waveforms (three-dimensional fluorescence signatures) may or may not provide toward the site conceptual model. A relatively wide variety of waveforms were observed at this site, indicating relatively high heterogeneity of fluorescing materials. In complex fluorescent data sets like this (as opposed to sites with just one or two waveform types) it is not beneficial to write up descriptions in text, but rather provide graphics that assist visually – in a "picture is worth a thousand words" sense. A recently developed classification analysis method is the fastest method we have found to quickly survey for differences in waveforms between differing logs or differing response horizons within a single log (attached in a PDF). All the waveforms from each sounding are plotted on a single graphic – allowing a spatial method of matching or spotting unique fluorescence signatures. Below is a description of the classification plots and examples of how to employ them.

X-Axis: Wavelength

The "center of gravity" of the four peaks of the waveform determines the x-axis position. For example, a clean waveform dominated by the blue (laser scatter peak) plots to the left – while a waveform plotted heavily toward the orange and red peaks will plot further to the right. Imagine placing a fulcrum under the waveform and determining the center of balance on the time axis of the waveform.

Y-Axis: Lifetime

The average lifetime of the 4 peaks determines the position on the y-axis. Short lifetimes (near zero) are plotted very low. The longer the lifetimes get the higher on the y-axis the waveform's oval data point is plotted. Laser scatter (blue channel) domination causes baseline data points to be plotted near the bottom while LNAPLs have longer lifetimes and plot three to four units high on the y-axis.

Color

The fill colors used in the log's fill of the Signal (%RE) on the standard TarGOST logs are also used to fill the ovals that represent each waveform. Use the fill color to find the depth along the TarGOST log where certain ovals originated. For instance, if the fill color of some plotted classification ovals are pink, look for where in the log (feet) the Signal (%RE) was filled with pink. This allows you to target where on the log to make further examination of the waveform to locate sampling depths or otherwise investigate your TarGOST data more fully.

Interesting classification plots to consider as examples include:



All "clean soils" (no fluorescence) are plotted in the lower left corner – this is because only the scatter provides significant contribution to both the x- and y-axis of the data set. Notice the blue data points match the blue fill

of the baseline's low Signal (%RE) of the log. Example waveforms from TG-01 are shown next to the classification plot above so that you can get a "feel" for why the data is plotting where it is on the classification chart.



Log TG-02 had fluorescence waveforms with some long lifetimes amidst modestly long lifetimes and ranged from left-of-center to center on the lower left quadrant of the classification plot. Look at the two waveform types that were observed to understand why those colored ovals were plotted where they were on the classification chart. Remember to look at the fill colors (upper right in the waveform plot) to find the matching fill colors also used to fill the ovals in the classification plot. There is a modest amount of heterogeneity in this log's classification plot. That is readily apparent because there are ovals spread quite broadly about in the lower left quadrant. This indicates there is heterogeneity of the fluorescent materials, either due to differing NAPL qualities - or even the presence of false positives.



Opposite in behavior is this plot, which shows an example of very red-shifted and short-lived waveforms. Notice that this chart's data ovals are tightly grouped indicating only a single type of waveform or "class", indicating very homogeneous chemistry with depth. So even though the NAPL deposits spanned across many feet in this log, the fluorescence did not vary – and it's likely that chemistry then didn't vary to any significant degree. The plot "streams" out and away from the blue cluster because as the size/intensity of the fluorescence channels grow they get large enough to dominate their weighting on the chart. The ovals are strung along a line due to the data generated while entering and leaving the NAPL body. In other words, had we only logged NAPL-saturated and clean soils, there would simply be a blue cluster (clean) and an orange cluster (NAPL saturated) separated from each other. In this plot there are ovals connecting them in between (pink) which represent staining (lighter contamination).



Finally we have this chart which shows a high degree of heterogeneity and three fairly distinct clusters. The yellow/green ovals at upper left are quite likely LNAPL (blue-shifted fluorescence along with long lifetimes), while the lower right maroon "stream" is likely classic tar (orange dominated and very short lifetimes). The middle group between the extremes may indicate a mix of those two, just a differently weathered tar, tar released from a different point in the waste stream, or even a false positive. The only sure way to know is multiple lines of evidence (sampling, site layout/history, previous findings, or NAPL presence in nearby wells for instance).

You can also use these classification charts to find similarities or differences from log to log as well. For instance, TG-24 and TG-21 are very similar to each other, as are TG-39 and TG-40, but the first pair is very different from the second pair. If you flip back/forth to each of them in the PDF you can see for yourself.

Table of Production and Observations

File	Date/Time	Final	Max	Max	EC	Observations		
		Depth	Signal	Signal	Data			
		(ft)	(%RE)	Depth				
GWP TG-01	3/18/2013 14.33	72	14	(ft) 15		Rubble present broke off TarGOST probe		
GWP TG-02	3/18/2013 15:56	11.8	336	8.1		FC not recorded		
GWP TG-03	3/19/2013 8:14	14.9	8	13	X	precleared with hand auger to 3' bos		
GWP TG-04	3/10/2013 0:14	9.6	11	1.0	X	precleared with hand auger to 3 bgs		
GWP TG-05	3/19/2013 10:10	2/ 3	107	24.3	X	precleared with hand adger to 5 bgs		
GWP TG-06	3/19/2013 10:10	16	60	24.5	X			
	3/19/2013 11:10	21.6	10	12.2		pro probad to 4.5'		
GWP_TG-08	3/19/2013 13.12	21.0	10	12.2		pre-probed to 4.5		
GWP_IG-00	3/19/2013 14.33	22.2	33 10	12.0		precleared with hand auger to 5 bgs		
GWP_IG-09	3/19/2013 15.20	19.9	10	13.5		precied to 2		
GWP_IG-10	3/19/2013 10.30	13	10	0.4	~ 			
GWP_IG-II	3/20/2013 8.31	24.0	190	0.01	X			
GWP_IG-12	3/20/2013 10:07	29.4	467	28.2	X			
GWP_IG-13	3/20/2013 11:31	17.8	8	6.7	X	pre-probed to 4.5		
GWP_IG-14	3/20/2013 13:14	22.2	152	14.2				
GWP_IG-15	3/20/2013 14:16	28.8	669	28.5		EC dead		
GWP_TG-16	3/20/2013 15:43	25.9	34	15.6		Probe rig problems		
GWP_TG-17	3/21/2013 8:13	28.6	83	17	Х			
GWP_TG-18	3/21/2013 9:32	9	27	8.9	Х	shallow refusal many times		
GWP_TG-18B	3/21/2013 10:06	15.6	340	15.6	Х	broke off TarGOST probe and bent first rod		
GWP_TG-19	3/21/2013 17:09	24.9	4	4.1		very shallow refusal first time, pre-probed to 4.5'		
GWP_TG-20	3/21/2013 12:18	26	76	14.9		pre-probed to 4.5', odor and sheen		
GWP_TG-21	3/21/2013 13:16	25.9	323	19.3		pre-probed to 4.5'		
GWP_TG-22	3/21/2013 14:21	24	9	8.9		pre-probed to 4.5'		
GWP_TG-23	3/21/2013 15:00	24.5	9	0.7		pre-probed to 4.5'		
GWP_TG-24	3/21/2013 15:47	28	229	21.6		precleared to 2'		
GWP_TG-25	3/22/2013 8:29	17.2	8	9.2				
GWP_TG-26	3/22/2013 9:19	20.9	29	7.8				
GWP_TG-27	3/22/2013 10:22	17	7	5.6				
GWP_TG-28	3/22/2013 11:29	26.4	6	9.2				
GWP_TG-29	3/22/2013 13:30	28.6	5	14.2		rig problems again		
GWP_TG-30	3/22/2013 15:00	5	4	0.2		many refusals at 5' bgs		
GWP_TG-31	3/22/2013 15:48	38	34	6.7		pushed all rods available		
GWP_TG-32	3/22/2013 17:11	6.9	4	2.4		shallow refusal		
GWP_TG-32B	3/22/2013 17:35	33.4	15	22.3		pre-probed to 10' bgs		
GWP TG-33	3/25/2013 9:39	22.1	57	3	Х	New EC cable. Preprobed to 4.5'		
GWP_TG-34	3/25/2013 10:45	25.1	61	0.9	Х	precleared to 2'		
GWP_TG-35	3/25/2013 11:36	25.2	38	7.1	Х	precleared to 2'		
GWP_TG-36	3/25/2013 13:49	18.2	358	8.6	Х	pre-probed to 4.5'		
GWP_TG-37	3/25/2013 14:53	26	1624	13.4	Х	precleared to 2', elevated background signal		
GWP_TG-38	3/25/2013 16:17	16.2	221	9.8		EC quit working, broken wires		
GWP_TG-39	3/25/2013 17:09	26	455	15.6		pre-probed to 4.5', multi product log		

File	Date/Time	Final Depth (ft)	Max Signal (%RE)	Max Signal Depth (ft)	EC Data	Observations
GWP_TG-40	3/26/2013 8:06	21.3	1397	9		precleared to 2'
GWP_TG-41	3/26/2013 9:00	28	16	9.5		pre-probed to 10' bgs
GWP_TG-42	3/26/2013 10:19	31	59	11.3		precleared to 2', very soft slag, visible NAPL
GWP_TG-42r	3/26/2013 11:21	31.2	39	10		precleared to 2', duplicate 6.5' from previous
GWP_TG-43	3/26/2013 13:12	26.4	687	9		
GWP_TG-44	3/26/2013 14:16	12.1	88	7.7		
GWP_TG-45	3/26/2013 14:56	18.8	41	8.8		pre-probed to 4.5'
GWP_TG-46	3/26/2013 15:44	24.6	341	8.6		pre-probed to 4.5'

SUB-ATTACHMENT 2A-2.6 Dakota Technologies TarGOST® Guide



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A Introduction

The Tar-specific Green Optical Screening Tool (TarGOST®) is a laser-induced fluorescence (LIF) screening tool that is specifically designed to detect non-aqueous phase liquid (NAPL) in the subsurface. It responds almost exclusively to NAPLs found at former manufactured gas plants (MGPs) and wood-treating (creosote/pentachlorophenol) sites. It does this by sensing the fluorescence of polycyclic aromatic hydrocarbons (PAHs) and any other fluorescent molecules found in MGP and creosote LNAPLs and DNAPLs. TarGOST is a modified version of Ultra-Violet Optical Screening Tool (UVOST®). Dakota developed the UVOST early in the 1990's with U.S. Air Force funding. The UVOST platform is a mature technology that has been applied at hundreds of petroleum, oil, and lubricant (POL) contaminated sites in the U.S., Europe, and Japan since 1994. TarGOST has been in commercial use since March 2003.



B Principles of Operation

B.1 Components

The following gives an introduction to the basic components of the system.

• Laser

The laser is up-hole and produces concentrated light of one narrow range of wavelengths. For TarGOST, the laser produces short (5 billionths of a second) pulses green light, as opposed to Dakota's UVOST system that uses an ultra-violet laser for excitation.

• Fiber-Optic Cable

The fiber-optic cable is a robust plastic coated metal conduit that houses two fiber optic cables and the wires for the conductivity measurement. This cable is strung through the probe rods prior to field activities. One fiber carries the laser down to the probe while the other returns scattered laser and fluorescent light.

• Shock Protected Optical Chamber (SPOC)

The distal end of the fiber optic cable attaches to the SPOC. The SPOC houses a mirror that turns the light and a sapphire window. Light passes through the window and strikes the soil in immediate contact with the window. The resulting scattered and fluorescent light is sent up-hole for measurement. The SPOC has channels that allow the conductivity wiring to pass through to the dipole tip at the bottom of the assembly.

• Spectrometer

The TarGOST's custom spectrometer divides the returning light into four distinct wavelength (or color) bands and converts the light into a corresponding electrical current where the current amplitude is proportional to the light amplitude.

• Analog to Digital Converter

The A/D converter produces an averaged digital signal from the current provided by spectrometer that can be read by the computer software.

Conductivity

The electrical conductivity of the soil can be logged simultaneously with the LIF information.

• Depth Meter and Hammer Rate

Depth is tracked by a string potentiometer system on the direct push equipment to insure that the optical data is tagged with its proper depth. Data density is generally less than one inch. We can also track our Hammer Rate when using a percussion delivery platform.

• Computer and Software

All data is logged using Dakota's proprietary Optical Screening Tool (OST) software running on a Windows platform. We use ruggedized field laptops.

B.2 Laser-Induced Fluorescence

The TarGOST system is, in its simplest sense, a front-face fluorometer that is coupled via fiber optics to a sapphire-windowed probe that is advanced into the ground.

A front-face fluorometer is a device that shines excitation light onto, and collects emission from, the same surface. This is different from conventional fluorometers, which operate with the excitation and emission beams at 90° and usually involve clear liquid analytes.

The TarGOST system makes continuous measurements of the soil matrix as the windowed probe is pushed slowly into the subsurface.

The measurements are made hundreds of times each second. Each individual measurement begins with a pulse of laser excitation light being launched into one of two optical fibers that are strung through the drill/push rod string. As the rod is advanced into the subsurface, the very fast pulses of laser light (nanoseconds in duration) are directed out the sapphire window and onto the soil surface that is pressed very firmly against the outside of the window.

Pulses of laser light strike whatever is present just outside the surface of the window. Most of the laser light is simply reflected by the soil matrix. However, if oil-like material (OLM) or tar-like material (TLM) containing PAHs (or other fluorescent molecules) are present, the PAHs that exist in these NAPLs absorb some of the light and are driven into an electronically excited state. When these PAHs eventually return to the ground state (this typically takes less than 10 ns), a portion of the PAHs emit red-shifted light (longer wavelength light than the excitation laser). Some of this fluorescence, along with a portion of the reflected excitation laser light, are collected by the SPOC's mirror and focused into the collection optical fiber for return to the TarGOST instrument for detection.

The light returning from the windowed probe is directed into a spectrometer located inside the TarGOST system, yielding a waveform.

The TarGOST's custom spectrometer divides the returning light into four distinct wavelength (or color) bands and converts the light into a corresponding electrical current pulse where the current amplitude is proportional to the light amplitude. This current pulse is wired into a fast digital storage oscilloscope where it is converted into a transient voltage signal, is digitized, and recorded. This digitized transient is called a waveform.

Figure 1 shows an example waveform. Each peak (or channel) represents a different wavelength band. The laser light that is being reflected from the soil matrix is monitored in the first channel (blue, left-most) and the three fluorescence bands are observed in the three right-most channels (green, orange, and red).



Figure 1. Example TarGOST Waveform

B.3 Scatter Correction

Due to complicated processes such as energy transfer, photon cycling, and other phenomena that "quench" the fluorescence in high NAPL concentration soils, fluorescence often does not scale linearly with concentration. To correct for this inherent property, the TarGOST system scatter corrects the data.

In calculating the TarGOST total signal, the fluorescence area is divided by the area under the laser scatter channel. This is referred to as scatter-correction or normalization. This is necessary because at very high concentrations the fluorescence does not continue to scale with concentration. The uncorrected TLM curve in Figure 2 illustrates the problem.

The addition of more and more NAPL to a soil sample should (if there were no quenching phenomenon) result in increasing fluorescence, but it only increases up to a certain point where the fluorescence response flattens out or begins to fall.

This poor type of response is called non-monotonic behavior and is obviously undesirable behavior for a screening tool. The laser scatter correction system is designed to prevent this "roll-over" affect. The scatter correction keeps this from occurring at the high end of concentrations (where soil is heavily contaminated or even saturated with NAPL). The scatter-corrected curves in Figure 2 illustrate the desired effect of scatter correction.

The laser scatter intensity is usually minimal until NAPL concentrations reach the tens or hundreds of thousands PPM level, where the quenching or saturation (non-linearity of fluorescence response) is most pronounced. Laser scatter correction generally doesn't "kick in" until high concentrations are being measured, where fluorescence response flattens out or rolls over. In this way, the scatter corrected fluorescence readings scale relatively well across a wide range of concentrations, from the typical limit of detection (LOD) of 250-500 ppm, to the almost neat NAPL encountered in soil saturated with free product. Remember that TarGOST is designed to respond only to the NAPL impacted soils, not the PAHs attached in "dry" form to soot or dissolved phase PAHs. This makes it ideal for delineating source term areas of mobile MGP NAPL.



Figure 2. Variability of TarGOST Repsonse

The scatter correction works well, but it isn't perfect.

The TarGOST system is not an analytical instrument like a laboratory GC that sits in a clean, stable environment and only gets fed ultra-clean matrix-isolated analytes. Instead, it is asked to respond faithfully to an analyte that exists in a thousand different forms in an endless number of environments.

At high NAPL concentrations, even small variations in the laser scatter greatly influences the total signal, especially when the laser scatter gets close to zero.

For instance, let's imagine that with neat NAPL in front of the window, the fluorescence channels are averaging around 10,000 pico-Volt seconds (pVs) in area with each pulse of the laser. The laser scatter may be fluctuating between 400 and 800 pVs, because the scattered light is dim from being absorbed by the PAHs. Now, even if the fluorescence stays almost constant at 10,000 pVs every measurement, the relatively large variation in the tiny laser scatter that occurs will create a two or three-fold increase/decrease in total signal, even with the same NAPL sitting on the window. That's why very high readings (>500) often look unstable and jagged – because the laser scatter signal is so weak it "jitters" a lot compared to the fluorescence, causing large variations in signal, even though the fluorescence portion of the waveform is relatively stable. For this reason, any wide swings in large signals should "be taken with a grain of salt".

At low signals (0-100 %RE), it is often helpful to use the Fluor (%RE) or "Fluorescence Only" column of data. At low concentrations the change in scatter from the formation itself might actually "mess with" the Signal, causing it to change for reasons other that NAPL content. The Fluor column is the most reliable indicator of NAPL at near limits of detection quantities.

B.4 Calibration and Signal Calculation

The waveform shapes (the relative amount of signal in each channel or band and the decay time on the right side of each peak) tell us quite a bit about the qualitative nature of what's happening outside the window. But what interests people most is the amount of NAPL that is present vs. depth. We do this by portraying the signal vs. depth in a continuous log format, where the signal is relative to a known fluorescence reference emitter (RE).

To accomplish this we must reduce the waveform to a single quantitative number. We also need to normalize for any energy drift of the laser and optical alignment changes, so it is necessary to calibrate the system prior to each

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sounding and plot the down-hole data. The RE is a stable and known material that can be applied to the window and measured just prior to each sounding. The signal of the down-hole sample is then plotted as a function of depth and a percent of the RE.

Figure 3 graphically illustrates the calibration waveform and its use in the determination of an example %RE.

The RE both reflects some of the laser light and fluoresces at levels that are in the same general range as soils that are moderately to heavily contaminated with MGP NAPL. The Reference Emitter waveform shown in the figure is an actual RE waveform taken with the TarGOST. By definition the RE will always have a %RE value of 100%. The example waveform on the right is a real waveform of impacted soil; notice the low scatter in the example and its impact on the total signal level of 219%.

To calculate the %RE, the area under the three fluorescence channels of the waveform is determined. As discussed in the previous section on scatter correction, the fluorescence area is divided by the laser scatter area. This fluorescence over scatter value is divided by the corresponding RE value and reported as a percent.

Once the RE is measured, all subsequent measurements can be normalized by this RE waveform, providing an apples-to-apples presentation of the data regardless of laser energy drift or other changes that would cause a difference in raw signal amplitude over time. It may be useful to think of the RE waveform as the equivalent of the single-point 100ppm isobutylene calibration used for hand-held photo-ionization detectors.



Figure 3. Example %RE Calculation

B.5 Signal vs. Depth Plotting

To better appreciate the qualitative information that TarGOST provides, the logs are color-coded by "filling in" the log's x-axis (%RE) with colors generated from the waveform at each and every depth. The color is determined by the amount of signal present in each of the four wavelength channels. See Figure 4 for an example.

This makes the interpretation of the logs easier to see "at-a-glance" as opposed to relying solely on the few selected waveforms to understand the qualitative nature of the data vs. depth. Color-coding alerts the observer to shifts in NAPL types and can also help identify weak interfering minerals like calcite and organic matter, both of which can sometimes (rarely) be mistaken for MGP waste.



Figure 4. Depth vs %RE and Callouts

B.6 Variability and Preferential Response

NAPLs vary in fluoresce intensity and spectral distribution (color), even NAPLs found at the same site.

Figure 2 illustrates conceptually that TarGOST often responds with varying sensitivity toward different NAPLs, depending on their origin and/or variances in the conditions under which they've been exposed in the decades they've spent in the subsurface. For instance, a thick asphaltine TLM will typically fluoresce much less intensely than a less viscous "runny" OLM. This may well be due to the relative abundance of solvent in one matrix vs. the other. The more solvent available (i.e. the less viscous the NAPL), the higher the likelihood of PAHs being able to emit photons (fluoresce) before a non-radiative mechanism allows the PAH to come back down to the ground state without emitting a photon (quenching).

The preferential sensitivity of TarGOST toward the less viscous (more mobile) OLMs is welcomed by most users, since TarGOST seems to accentuate the presence of the more mobile NAPLs.

It is these more mobile NAPLs that are of the highest regulatory/compliance concern. There is an abundance of anecdotal evidence that suggests that some NAPLs may fractionate in the subsurface into OLM and TLM or even DNAPL and LNAPL. Dakota has participated in a number of investigations where a single NAPL body seems to have 'split' into two distinct NAPLs, with both NAPLs having similar but distinct waveform shapes as we moved away from the suspected release point and they appear to form two separate horizons (a "high" and "low" layer). Although there has been plenty of speculation, the exact mechanism for this phenomenon (if it actually occurs) is not known.

TarGOST uses a green laser to excite the larger (4 -5 rings and higher) PAHs that exist almost exclusively in NAPL form, as opposed to smaller (2-3 ring) PAHs that can more readily partition into the groundwater due to

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their much higher solubilities in water. UVOST on the other hand employs ultra-violet (UV) light which can and does excite the smaller 2-3 ring aqueous phase PAHs and sometimes detects (marginally) high concentrations dissolved phase PAHs such as naphthalenes in the groundwater. When this behavior is combined with UVOST's non-monotonic response for many NAPLs, extremely complicated logs are generated that need to be computer analyzed to separate the NAPL fluorescence contribution from that of the dissolved phase. The dissolved phase signals can even surpass NAPL signals, making confident NAPL delineation almost impossible at many sites. This is especially true for those sites with sand/gravel, where pockets of NAPL are perched in or amongst slow-moving or stagnant groundwater.

It should also be mentioned that TarGOST was designed to exclusively detect high concentration PAH NAPLs ("heavies"). TarGOST has, by design, a very limited response (if any) to lighter fuels. While this is often desirable, there are some cases where TarGOST "missing" lighter fuels is undesirable, but this is a limitation of the TarGOST technology.

C Results

Dakota has years of experience using TarGOST. The system has both been fully tested in the lab and in the field.

C.1 Laboratory Testing

Figure 5 illustrates waveforms that are typical of those generated with TarGOST.

If the soil is free of NAPL, the laser scatter channel (leftmost) is far more intense than the three fluorescence channels. The Clean Sand waveform in the figure illustrates what clean (or very low NAPL) soil typically looks like on the TarGOST system. If NAPL is present, the fluorescence channels begin to grow in comparison to the laser channel. The 1,000ppm and 10,000ppm waveforms in the figure illustrate such a condition. Finally, with pure NAPL on the window, the increase in the fluorescence channels is minimal, but there has been significant loss of signal in the laser reflectance channel, due to absorbance by the PAH-laden NAPL.



Figure 5. Example TarGOST Waveforms

Lab studies with MGP NAPL on moist Fisher[®] sea sand (and other soils) consistently demonstrate that TarGOST is capable of linear response vs. NAPL concentration over useful ranges, but some NAPLS are simply better behaved (more/less fluorescent) than others. Figure 6 shows examples of the range we see in TarGOST response for a variety of MGP NAPL on soils.



Figure 6. TarGOST response to a variety of MGP NAPLs

C.2 Real-World Data

Dakota has over twenty miles of vertical logging experience using TarGOST. Below are just a few logs of interest gathered over those years.





Figure 7. Example Log with EC

Figure 8. Example data including EC and Hammer Rate (red fill in right panel)



Figure 9. Example data with very high signal (low scatter)

D Theory and Results Summary

The following bulleted list is meant as a quick reference once the underlying principles of operation and results have been examined.

- TarGOST specifically targets the PAHs found in former MGP and creosote NAPLs and DNAPLs. There are most certainly other fluorescent molecular structures beside PAHs that contribute, but the PAHs dominate in most NAPLs
- TarGOST does detect moderate staining and residual levels of NAPL as well as free phase
- TarGOST is completely "blind" to aqueous (dissolved phase) PAHs
- TarGOST is not able to reliably detect "dry" PAHs (dry in the organic solvent sense) that are sorbed to soot, wood chips, and ash. They can generate a small signal but it is often weak and not easily teased out of the background. Many times we're left wondering whether a small signal is caused by very high concentrations of "dry" PAHs on purifier chips or ash/soot or very low (100s of ppm) residual NAPL levels.
- TarGOST's typical lab-determined LOD for NAPL on site soil is 100-500 ppm (weight of NAPL/weight of soil matrix). The more the NAPL fluoresces, the lower the LOD. Note that this is not the same as weight of Total PAHs /weight of soil matrix, since not all of a NAPL is PAHs
- TarGOST does, on occasion, respond to mineral or organic matter enough to be a nuisance. False positives include crushed limestone gravel fill, buried rotting wood/brush debris (the result of major flooding on a gravelly river), sea shells (shell hash), sawdust, quick lime, and some "mystery" solids/soils that were not identifiable
- TarGOST has been observed to significantly respond to peat material, but most peats fluoresce weakly often there is NAPL in the peat so it's difficult to know for sure whether it's been the peat or NPAL staining that's causing the fluorescence
- TarGOST does not respond to typical lighter end fuels like gasoline or kerosene (diesel can/has been detected) unless they contain MGP waste or creosote that they are co-mingled in them (pentachlorophenol an obvious example)
- TarGOST is single-point calibrated with a reference emitter (RE) immediately prior to each sounding and the results are always plotted relative to RE (%RE)
- TarGOST calibration/setup isn't perfect and the response for an identical NAPL can vary with optical platform and from lab to field. However, once set up on site, the response remains stable over time and from log-to-log. Changes to the spectrometer and mirror alignment/collimation SOP in 2007 made significant improvements to the consistency of the response
- NAPLs can vary greatly in their fluorescence response even NAPLs found on the same site from the same source
- Thinner, less viscous NAPLs typically fluoresce much more (x10) than the more viscous TLMs. Asphalt-like TLMs which are solid/plastic fluoresce very poorly
- Scatter-correction is applied to TarGOST data to reduce/eliminate "response rollover" at high concentrations but at low concentration (<100% RE) the Fluor (%RE) data column is better for judging "hits"
- Color-coding is determined by the relative waveform areas in each channel and provides "at-a-glance" recognition of waveform consistency or changes
- The waveforms contain both quantitative and qualitative information



E On-Site Fundamentals

E.1 Delivery Platform

Dakota has used its TarGOST systems in conjunction with nearly all commonly available directpush (CPT and percussion) systems on land, ice, and on the water (barge).

• Dakota's Probe Rig

Dakota owns a Geoprobe® 5400 direct-push probe mounted on a Ford F-550 truck. When we operate our own system (TarGOST and Geoprobe) we generally send two experienced Dakota technicians.

• Third Party Rig

Dakota can rent a probe (for example a track rig) or our customers can hire a third party for the drilling activities. This third party option is generally a good idea when Dakota's mobilization fees are cost prohibitive or a special drilling license is required by the state.

• Barge

Dakota has extensive experience working from barges while providing TarGOST services. Barge sizes have ranged from 16' to 150' and we have worked in water depths of a couple of feet to 50'.

E.2 Pre-Planning

• Free Sample Check

Dakota will gladly look at your sample and let you know if TarGOST is the right choice for you. If your NAPL doesn't respond well with TarGOST, we'll also test your sample with UVOST to see if it is the better solution. Contact us for details, but it generally involves you sending us jars (from 5 to 40 ml) of your test NAPLs in an unrefrigerated shipping container, along with information regarding your site and contact information. In just a few days we'll let you know the results.

• Probe Rig

Arrange for Dakota to probe your site with our self-contained system or hire an outside drilling contractor. Dakota will need to communicate with your potential contractor to determine if they are capable of pushing direct sensing equipment. We have integrated with most Geoprobe models, many AMS probe machines, Marl rigs, homemade probe machines, CME drill rigs, mini CPT skids, tracked CPT machines and several brands of 40 ton CPT trucks.

• Utility Clearance

Dakota personnel have been instructed NOT TO PROCEED until underground utilities have been identified. Please communicate with Dakota to ensure that this is completed.

Site Access

If any special security, permits or safety clearance is needed for Dakota's personnel or equipment is needed, alert Dakota prior to us showing up on-site.

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• Transport

The main components of the TarGOST system are housed in a shock-protected enclosure measuring roughly 2x2x2 feet and weighing approximately 100 pounds. In addition to this enclosure, there is a rod-rack with generally four-foot rods, a computer, fiber cables, a generator, tools, spare probes and various peripheral items. When we ship the system, everything fits in a 4x4x4 foot enclosed pallet. A fork lift and secure storage should be arranged near the work site.



Figure 10. TarGOST and all peripherals in an enclosed palette being loaded for transport

• Hole Locations

Some customers like to pre-plan the hole locations, mark the site accordingly, and record all relevant x-y and elevation data. A plan of bounding the contamination based on results determined on-site is also viable. Regardless if the hole placement follows a grid or bounding procedure, Dakota strongly prefers to start the job in what is believed to be "the heart" of the contamination. This gives everyone involved a feel for how well the NAPL is going to respond to TarGOST delineation.

• Sampling

Dakota recommends discrete sampling at 10% of the hole locations if semi-quantitative values are to be assigned to the LIF signals. Soil sampling can be reduced to approximately 5% of hole locations as a ground-truthing exercise. If an extensive sampling program is planned the client should consider hiring a more cost effective driller. Remember to build sampling time into you scope of work. Do consider getting TarGOST responses to homogenized splits of your samples. If your site has heterogeneous lithology (very typical), the chance of you sampling soils/NAPL that are representative of that which the TarGOST probe passed through are near zero. If heterogeneity exists, and you try to compare lab results to TarGOST %RE of adjacent logs rather than TarGOST %RE of those same samples, the correlation will be terrible (the expected result).

E.3 Daily Production

Footage

TarGOST productivity can range anywhere from 200 to over 500 ft/day. If the pushes are fairly deep (>30 ft), and the obstructions rubble are minimal, then the average is on the higher end because spend a lot more time actually probing, not moving around from location to location and/or trying multiple times to get holes started through rubble. Other factors affecting production are grouting requirements, surface pavement, surface topography and vegetation. We typically can log between 10 and 20 locations a



• Start-Up Time

When the system first arrives on site, it is powered up and tested

proper function. If it is in Dakota's Geoprobe, the TarGOST is simply powered up and we're ready to begin probing after a very short warm-up. If a CPT or other direct-push machine is used, the TarGOST system is integrated into the delivery platform, rods are strung with the Dakota's optical fiber cable and proper depth measuring connections are made (about a 2 to 3 hour procedure).

• Decontamination

Typically Dakota uses a rubber rod wiper to "squeegee" any contaminated mud from the probe. If additional decontamination is required, production rates will be impacted accordingly.

• Sampling

If Dakota is contracted to collect soil samples, it will be prudent to do all the sampling at one time, preferably at the end of the job. Using LIF data, impacted zones can be identified and targeted for sampling, eliminating the need for continuous cores.

• Barge Productivity

TarGOST operations on a barge usually limit daily production to 50 - 200' of logged depth. Additional factors affecting barge productivity are; location accuracy needed, subsurface conditions, water depth and presence of current or tide.

E.4 Deliverables

• JPEG Images

Once a log is completed our TarGOST operators can immediately generate an image of the log. Callouts are used to show the waveform from areas of interest. Along with the %RE versus depth plot, the scatter and the fluorescence levels as a function of depth are provided. Secondary data such as the rate of probe advancement, the amount of hammering required to advance the probe with percussion systems, and conductivity may also be available. At the bottom of the log is the pertinent info for the data such as site name and location as well as basic stats such as total depth. These images can be printed on site.

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• Data in Text Format

Along with the log image, our customers are given the data in ASCII tab delimited format. No string header is provided for the columns (to make importing into other programs easier). Each row is a unique depth reading. The columns are:

1	2	3	4	5	6	7	8	9	10	11
Depth	Total Signal (%RE)	Ch1 (%RE Sctr)	Ch2 (%RE Fluor),	Ch3 (%RE Fluor),	Ch4 (%RE Fluor),	Push Rate	Cond. Depth	Cond. Signal	Hammer Depth	Hammer Rate

TarGOST data collected with a CPT rig will not include the CPT data as that is an independent acquisition system. Dakota is only responsible for providing the LIF data.

E.5 Post-Investigation

• Customer Care

Dakota prides itself on going the extra mile from our customers. Whether it is providing detailed information such as this document, or walking the customer through the data on the phone long after we have left the site, we are committed to our customers being well informed and pleased with our service.

Hole Locations

Once Dakota leaves, our customers may wish to survey all the TarGOST locations if it wasn't done prior to the job. Getting good positional information, including elevation, is key to any future CAD and visualization efforts.

Conceptual Site Model Visualization

Dakota now provides the capability to view TarGOST/UVOST/ROST site characterization data in static or dynamic format with unparalleled resolution. Dakota can also overlay the site with aerial photographs or building CAD models over GIS terrain data to provide an accurate overall picture of the site with relevant subsurface features.

- » 2-D (fence or cross section) and 3-D models such as Plume and Stick provide a variety of methods to best represent the log data
- » Capable of vertical resolution less than 1 inch
- » Log interpolation between direct push locations using a highly accurate modeling algorithm
- » Choose a variety of display formats including static graphics and dynamic video
- » Overlay site aerial photographs or satellite images onto the model
- » Integrate Dakota's visual models with client's existing AutoCAD drawings

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Figure 11. Geology slice and LIF data



Figure 12. 2D overlay of UVOST data and site photo

SUB-ATTACHMENT 2A-2.7 TarGOST® NNLS Waveform Analysis

SUB-ATTACHMENT 2A-2.7.1 NNLS Basis Set Components




































Signal (%RE)



SUB-ATTACHMENT 2A-2.7.2 NNLS TarGOST® Logs

















































Signal (%RE)



















































































































Signal (%RE)













Signal (%RE)





Signal (%RE)



















LIGHT1
























SUB-ATTACHMENT 2A-2.7.3 NNLS Confirmation Samples



























Background

LIGHT2

200

200

Time (ns)

DENSE2





























ATTACHMENT 2A-3 SI Boring and Well Logs

ATTACHMENT 2A-3 SI Boring and Well Logs

	SO	IL CLASSIF		ON CH	ART	ADDITION	AL MATERIAL SYMB			
М	AJOR DIVIS	IONS	SYME GRAPH		TYPICAL DESCRIPTIONS	SYMBOLS GRAPH LET	TYPICAL			
	GRAVEL	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES	A	C Asphalt Concrete			
	AND GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES		C Cement Concrete			
COARSE GRAINED SOILS	MORE THAN 50% OF COARSE ERACTION	GRAVELS WITH FINES		GM SILTY GRAVELS, GRAVEL - SAND		CI	R Crushed Rock/			
	RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES		S Topsoil/			
MORE THAN 50%	SAND	CLEAN SANDS		SW	WELL-GRADED SANDS, GRAVELLY SANDS		Forest Duff/Sod			
RETAINED ON NO. 200 SIEVE	AND SANDY SOILS	(LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND	Meas	sured groundwater level i			
	MORE THAN 50% OF COARSE ERACTION	SANDS WITH FINES		SM	SILTY SANDS, SAND - SILT MIXTURES	explo Meas	ploration, well, or piezomet asured free product in well			
	PASSING NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		SC	CLAYEY SANDS, SAND - CLAY MIXTURES	_⊻_ piezo	piezometer			
				ML	INORGANIC SILTS, ROCK FLOUR, CLAYEY SILTS WITH SLIGHT PLASTICITY	Disti	Distinct contact between soil			
FINE	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS	geol Appr chan	geologic units Approximate location of soil s change within a geologic soil			
SOILS	ULATO		-	OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	Mate	erial Description Co			
MORE THAN 50% PASSING NO. 200 SIEVE				мн	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS SILTY SOILS	Disti	Distinct contact between soil			
0LVL	SILTS AND	LIQUID LIMIT GREATER THAN 50	////	СН	INORGANIC CLAYS OF HIGH PLASTICITY	geol Appr	ogic units oximate location of soil s			
	ULATO		Anh	он	ORGANIC CLAYS AND SILTS OF MEDIUM TO HIGH PLASTICITY	chan	ge within a geologic soil			
н	GHLY ORGANIC S	SOILS		РТ	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS					
NOTE: Multiple	e symbols are u	sed to indicate bo	rderline or o	dual soil c	lassifications	Lab	oratory / Field Tests			
Blow of blo dista	Sai 2.4 2.4 Sta She Pis Dire Count is reco ows required nce noted).	npler Symb -inch I.D. split ndard Penetra elby tube ton ect-Push k or grab prded for drive to advance sa See exploratio	n sample ampler 12	(SPT) (SPT) ers as th 2 inches hamme	e number (or r weight	AL Atter CA Cher CP Labo CS Cons DS Dired HA Hydr MC Mois OC Orga PM Perm PI Plas PP Pock PPM Parts SA Siev TX Triax UC Uncc VS Vane	rberg limits mical analysis pratory compaction test solidation test ct shear cometer analysis sture content mic content neability or hydraulic con ticity index set penetrometer s per million e analysis cial compression onfined compression e shear en Classification			
and c A "P' drill r	drop. ' indicates sa 'ig.	ampler pushec	l using th	ne weigh	it of the	NS No V SS Sligh MS Mode HS Heav NT Not 1	isible Sheen ht Sheen erate Sheen ry Sheen Fested			
NOTE: Th conditions not warrar	ne reader mus s. Description nted to be rep	t refer to the dis s on the logs a presentative of s	scussion i oply only a subsurface	in the rep at the sp e condition	port text and the logs of exp ecific exploration locations ons at other locations or tim	olorations for a prop and at the time the nes.	er understanding of subsur explorations were made; the			

IAL MATERIAL SYMBOLS

SYM	BOLS	TYPICAL						
GRAPH	LETTER	DESCRIPTIONS						
	AC	Asphalt Concrete						
	сс	Cement Concrete						
	CR	Crushed Rock/ Quarry Spalls						
	тs	Topsoil/ Forest Duff/Sod						

oundwater Contact

- asured groundwater level in loration, well, or piezometer
- asured free product in well or zometer

aphic Log Contact

- tinct contact between soil strata or ologic units
- proximate location of soil strata inge within a geologic soil unit

terial Description Contact

- tinct contact between soil strata or logic units
- proximate location of soil strata nge within a geologic soil unit

δF	Percent fines
L	Atterberg limits
Α	Chemical analysis
P	Laboratory compaction test
S	Consolidation test
S	Direct shear
Α	Hydrometer analysis
IC	Moisture content
ID	Moisture content and dry density
C	Organic content
M	Permeability or hydraulic conductivity
1	Plasticity index
Р	Pocket penetrometer
РМ	Parts per million
Α	Sieve analysis
Х	Triaxial compression
C	Unconfined compression

een Classification

- Visible Sheen
- ht Sheen
- derate Sheen
- vy Sheen Tested

per understanding of subsurface e explorations were made; they are



	Drilled	4/10	<u>Start</u>)/2013	4/	<u>End</u> 12/2013	Total Depth	h (ft)	4	7		Logged By PDR Checked ByZAS/TB	Dri	_{iller} Boart Longyear			Drilling Mud Method (cont	Rotar inuou	ry/Sonic us core)
	Hammer Auto Drill Data 140 (Ibs) / 30 (in) Drop Equ									Dril Eau	ling CME-850 upment Track-Mour	Tra	acked Rig; Rubber	4 2 (in)	2 (in) well was installed on 4/12/2013 to a depth of 47			
	Surface	e Elev	ation	ft)		29.92				Top	o of Casing		29.43	(ft).	wotor			
	Easting	J Datu g (X)	m		USA 12	69843.3	:кs) }			Но	rizontal	Date Me	asured	Depth to <u>Water (ft)</u>		Elevation (ft)		
	Norming (Y) 238868.03 Dat									Dat	um NAD83 WA State Plane North 4/				4/22/2013 7.5 22.4			
	47 feet. Temporary conductor casing (10-ii										Linch diameter) used	l fro	m 0 to 41 feet bgs with	bentor	nite se	al from 38 to 4	1 fee	et bgs.
				FII	ELD D	ATA										WE	LL	LOG
	n (feet	feet)			d Samp	Name	evel	: Log	-	cation	M/ DES	ATE CR	ERIAL		ace ppm)			Steel surface
	levatio	Jepth (i	Iterval		collecte	ample	Vater L	Braphic	Broup	Jassifi		011		sheen	leadsp 'apor (j		$ \leq $	monument
	ш	0-		4	0	0)	>		SN	и И	Brown silty fine to m	ediu	m sand with occasional	0	1>		R	
	-	-	X								-	irgan	iics (topson) -	-				-Concrete surface
	-	-	\square						M	<u>г</u>	Gray/brown silt with gravel	fine	sand and occasional			2.0'		
	-	_		0 1	5	1					Brown silty fine to m (loose to medium	ediu n der	m sand with fine gravel nse, moist)				2% 2%	
	_													NS	<1			
	-5D	-		0 4		2							-					-2-inch Schedule 40 PVC well casing
ľ	_12	5 —							SF	<u>р</u>	No recovery, coarse washed cuttings	san	d and fine gravel from					
	-	-											-	-				
	-	-		3 5		3					Brown fine to coarse	e san	nd with fine	-		8% 8%	%% %%	
	-	-					⊥				angular/subround wet)	ded (gravel (loose, moist to -	NS	<1		1200 1200 1200	
	_	_		6 4		4 %F					Groundwater encour (%F = 4)	ntere	ed at 7.7 feet	_		88 88 88		
ELL	<i>.</i> 0																	
ENTAL_W		10 —		2 0	2 9 5	5				GP	Brown fine to coarse gravel (loose, we (SA: %F = 6)		id with fine to coarse					-Bentonite seal
VIRONME	-	-		2 9	SA					_ (SA; %F = 6)		-	-		8% 8%	%% %%		
GEI8_EN	-	-							GF	P M	 Black low density/fria Light brown silty fine 		gravel (loose, wet)	NS	<1			
S8.GDT/	-	-		6 6		6			- Ch	•	occasional fine g	rave	el (loose, wet)	-		88 88 88	202 202 202	
NGINEER	-	-						GP - GP - Gray/black fine gravel with fine to coarse sand,								190 190 190		
te:GEOE	_ ⁽⁵⁾	15 —		6 6		7			SN	M	agglomerate, wo shoe, concrete p	od d iece: et. bl	lebris (processed) in s in sample (loose, wet) lack coating on gravel	SS <10%		22 20 20 20	XX XX XX	
.ibTempla											particles (has she Brown silty fine to co	een) barse	e sand with fine to				20 2020	
emplate/L	-	-		6 6		<u>8</u> SA					 coarse, angular i blackening of gra guickly, no odor 	multi ains, (loos	-colored gravel, slight - sheen dissipates se. wet)			88 88 88		
SPJ DBT	-	-									- (SA; %F = 20)	(-	NS	<1			
8684601.0	-	-		6 9		<u>9</u> SA			5P-3	51VI	- and silt, multi-col gravel with occas	barse lor gr siona	e sand with fine gravel rains, angular and flat – al wood chips (loose,	-		88 88 88		
KTOP/01	-	-							SF	<u>р</u>	wet) (SA; %F = 8)			-			2020 2020 2020	
ASHIDES	_10	20 —									Gray coarse sand wind and occasional fi	ith fir ine to	ne subrounded gravel o medium sand (loose, —	NS	<1	88 88	2 2/2/	
SERS/TN.	Not	e: Ple	ase se	e Figu	re A-1 fo	or explana	ation	of syr	nbols	8								
Path:C:\U	\geq								.00		f Monitorina V	We	ell MW-32D/GFC)-1				
te:5/14/13						2 1		-	<u> </u>	,	Project:		Puget Sound Energy	gy No	orth La	ake Union		
attle: Dai	G	E	ЪE	N	SIN	EER	S	0	1		Project Locatio	n:	Gas Works Park, S	Seattle	e, Wa	ashington		Figure A-2
Se	19						-				Project Numbe	r:	0186-846-01					Sheet 1 of 3

FIELD DATA						D D	ATA							WELL I	OG
Ĭ	Elevation (feet)	엉 Depth (feet) 	Interval	Recovered (in)	Blows/foot	Collected Sample	Sample Name	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)		
-		-		6	7		<u>10</u> SA			SP-SM	wet) Brown fine to coarse sand with silt (ground - agglomerate) (loose, wet) (SA; %F = 11)	NS NS	<1 <1		-Bentonite seal
-		-		6	8		<u>11</u> %F			SP-SM	 Thin band black coated particles from 22 to 22.5 feet Black coarse sand with silt and fine to coarse gravel, angular, friable, vesicular material, particles stained (loose wet) 	ss ss	<1 <1		
_ %		- 25 —] o	6						- (%F = 8) -				
-		-		12	8		12				Black silty fine to coarse sand with occasional			00000000000000000000000000000000000000	
-		-		12	32		13			— <u>—</u> — - SP	(milled), some thin metal chips and ceramic pieces (loose, wet) (%F = 20) Black fine to coarse sand with ceramic pieces, metal pieces, wood debris, slight odor.	MS	<1	2020 2020 2020 2020 2020 2020 2020 202	-10-inch diameter borehole to 41 feet; 6-inch diameter borehole to 47 feet
		30 -		20	56		14			GP	angular (non-agglomerate) (dense, wet) (SA; %F = 3) Gray fine to coarse angular gravel with occasional medium to coarse sand (not agglomerate) (very dense, wet)	NS	<1		
-		-		18	58		15			GP SP	Fine to medium sand lense (very dense, wet) Gray fine to coarse gravel with fine to coarse sand, trace silt (very dense, wet) Gray fine to medium sand with trace silt and lenses of coarse sand with occasional fine to	NS	<1	ADACACACACACACACACACACACACACACACACAC	
/ELL *		-		18	98		16				coarse gravel (very dense, wet)	NS	<1		
		35 —		18	64		<u>17</u> SA				(SA; %F = 3)	NS	<1		
		-		12	78		18						~1		
	Ó	- 40 —		18	52		19			SP-SM	- Gray fine to medium sand with silt (very dense, 			40 E	
		-		_							Occasional coarse sand and fine gravel			40.5 P 4 41.0 - 0 0 42.0 - 0 0	-20/40 sand backfill -10/20 sand backfill
KI UP/U18084001.GF		-	X	12			20;MW-32D (43.5-44.5)				Becomes finer	NS	<1		-2-inch Schedule 40 PVC screen, 0.020-inch slot width
	Note: Please see Figure A-1 for explanation of symbols														
							Lo	bg	of	Moni	toring Well MW-32D/GEO-1 (co	ntin	ued)	
Seame: Date:0/14/	Log of Monitoring Well MW-32D/GEO-1 (continued) GEOENGINEERS Project: Puget Sound Energy North Lake Union Project Location: Gas Works Park, Seattle, Washington Project Number: 0186-846-01														

ſ			FIELD DATA										WELL	LOG	
	Elevation (feet)	5 Depth (feet) 	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name	Water Level	Graphic Log	Group Classification	MATI DESCF	ERIAL RIPTION	Sheen	Headspace Vapor (ppm)	P. 11	
-		F2 -	12	81		21			SM	Gray silty fine to coarse – gravel (very dense, r	sand with fine to coarse noist) -	NS	<1		—2-inch slip cap
														47.0'	
VTAL_WELL															
/GEI8_ENVIRONMER															
JENGINEERS8.GDT															
ate/LibTemplate:GEC															
1601.GPJ DBTempla															
HUDESKTOP/018684															
C:USERS/TNAS	Not	te: Plea	ase see	Figure	A-1 for	explana	tion	of syr	nbols						
4/13 Path						Lo	og	of	Moni	toring Well MW	-32D/GEO-1 (co	ntin	ued)		
Seattle: Date:5/1	C	BE	DE	١G	INE	ER	S	0	1	Project: Project Location: Project Number:	Puget Sound Energ Gas Works Park, S 0186-846-01	gy No Seattle	erth La e, Wa	ake Union shington	Figure A-2 Sheet 3 of 3

Figure A-2 Sheet 3 of 3

ſ	StartEndTotal49.5Drilled4/11/20134/11/2013Depth (ft)C									5	Logo Chec	ged By ARJ ked ByZAS/TB	Driller Boart L	ongyear			Drilling Method Hollow-stem Auger			
;	Surfac Vertic	ce Elev al Dat	vation	ı (ft)		3 USAC	0.17 E (Locł	(S)		Ha Da	ammer ata	140	Autohammer (lbs) / 30 (in) Dr	rop	Drillin Equip	g ment	CME-850 Tracked Rig			
1	Eastir Northi Notes	ig (X) ng (Y) s: Han	d-dug	g wit	h post	1269 238 thole di)972.23 3799.4 gger fro	3 m 0 to	2 fee	Sy Da	ystem atum	stem tum NAD83 WA State Plane North			<u>Grour</u> Date N	ndwate leasure	PT Depth to ed Water (ft) Elevation (ft)			
										- J										
	Elevation (feet) Depth (feet) Interval Recovered (in) Blows/foot Blows/foot Blows/foot Collected Sample Blows/foot Collected Sample Blows/foot Collected Sample Collected Sample Sample Collected						MATERIAL DESCRIPTION				Headspace Vapor (ppm)	REMARKS								
-	¢	0— - - 5— -	-	10	22		1			SM	- Bri - Bla - Rc	own silty fine to r occasional fine asphalt fragmen ack at 5.5 feet ock and crushed one piece of tar	nedium sand with gravel, trace brich ts (loose, moist) concrete from 5.5 n friable agglomer	h k and 5 to 6 feet, ate	NS	<1	Concrete and rock in base of sampler Hard drilling			
TANDARD	Ъ	- - 10 —		17	6		2 SA				- - w - - -	ith white soft silt avelly fine sand fragments and	(bentonite like) with mostly decay glass shards	red wood	- - NS	<1	Groundwater encountered at 8 feet SA (%F = 17) Bentonite layer, pea gravel layer (1-inch thick), geomembrane at 10 feet			
emplate:GEOENGINEERS8.GDT/GEI8_ENVIRONMENTAL_S	<i>\</i> \$	- - 15 —		22	7	3	<u>:GEO-2</u> 14-16 SA		on 1997	SP-SM	- - - - -	ack fine to coars; gravel is agglor occasional glas fragments, occa mostly decayed with filigree (loc	e sand with gravel nerate red, white, s fragments and r asional fine gravel wood, one ceram se, wet)	l and silt; friable, rubber I, trace nic piece	- - - - - - - - - - -	<1	SA (%F = 7)			
010186846/01/GINT/018684601.GPJ_DBTemplate/LibT	Nc	- - 20 — te: Ple	ease s	9 see	10 Figure	€ A-1 fo	4 %F r explan	ation of	f sym	SP-SM	- 	ack fine to mediu white, brown, fragments?, occ thin metal highl fragments highl white ceramic v	m sand; sand par iable agglomerate casional rubber, o y corroded, trace y decayed, one pi vith filigree (mediu	ticles tan, , shell ne piece wood iece of um dense,	- - - NS	<1	%F = 11			
3 Path:P://												Log of Bo	oring GEO	-2						
seattle: Date:7/30/1	GEOENGINEERS A Project: Puget Sound Energy North Lake Union Project Location: Gas Works Park, Seattle, Washington Figure A-3																			

Project Number:

0186-846-01

Figure A-3 Sheet 1 of 3


Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample C	Sample Name Testing	Water Level Granhic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS		
- - - -	- 45 — - - -	5	50/5"		9 SA 10		o 	Gray silty fine to medium sand with gravel (very dense, wet) (till) - -	NS	<1	SA (%F = 2)		
				1		1 11-1	- 11	1	L	<u>I</u>	1		
	Note: Please see Figure A-1 for explanation of symbols												



Project:Puget Sound Energy North Lake UnionProject Location:Gas Works Park, Seattle, WashingtonProject Number:0186-846-01

e, Washington Sheet 3 of 3





Log of Boring GEO-3 (continued)



Project: Project Location: Project Number:

Puget Sound Energy North Lake Union on: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-4 Sheet 2 of 2





0186-846-01

GEOENGINEERS8.GDT/GEI8_ENVIRONMENTAL_WELL DBTer ERS/TNASH/DESKTOP/018684601.GPJ attle: Date:5/14/1:

Figure A-5 Sheet 2 of 2

Dr	rilled	3/2	<u>Star</u> 7/20) 13	<u>En</u> 3/27	<u>d</u> /2013	Total Depth	ı (ft)	1	8		Logged By PDR Checked By ZAS	Dri	iller Boart Longy	year			Drilling Method Sonic (continuous core)
Su Ve	rface	e Elev I Datu	atio m	า (ft)		3 USAC	7.96 E (Locl	ks)			Har Dat	mmer ta				Drilling Equipr	l nent	Rubber Track-Mounted Spider 3 Sonic Drill Rig
Ea	sting	g (X)				1270	307.96	6			Sys	stem	۰ ۸۸	State Plane Nor	th	Ground	dwater	Depth to
No	otes:	Han	d-du	g wit	h posti or well	hole dig	ger from	n 0 to	o 2 fe	et bgs	s. Hi	lit pipe at 18 feet bgs; a	band	oned hole. See		Date M	easure	d <u>Water (ft)</u> <u>Elevation (ft)</u>
\geq				(4)	FIFI	D DA	ТА											
Elevation (feet)		⊃ Depth (feet) 	Interval	Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Water Level	Graphic Log	Group	Classification	M DES	ATE SCR	ERIAL RIPTION		Sheen	Headspace Vapor (ppm)	REMARKS
		Ū	М	24						SN	N	Brown silty fine to n (roots)	nediu	m sand with organic	CS			
-		-	Å	60						SN	И	Black silty fine to co fine to coarse g -	oarse ravel	sand with occasion (loose, moist)	al	-		
	5 —									GN SN	И	Black fine to coarse to coarse sand Brown silty fine to n coarse gravel, v (approximately)	e grav and s nediu vith oo 3 inch	el agglomerate with ilt (hard, angular) m sand with fine to ccasional silty interb nes)	beds	- NS	<1	
- - 										SM	И	- Gray silty fine to me - fine to coarse g	edium ravel	a sand with occasior	nal	- - - - -	<1	Perched groundwater encountered at 7 feet
										SP-S	SM	Gray fine to coarse — fine gravel, occ: material, low de gravel –	sand asiona nsity,	with silt and occasi al black vesicular small percentage o	ional - of	-		
		-		36						SP	-	Red-orange fine to grains are low d agglomerate Becomes black	coars lensity	se sand with trace si y, weathered	ilt,	-	-1	
ate/Lib lemplate:GEOEivoi		15 -										Becomes black Becomes black No recovery from 1 Steel pipe piece	5 to 1	7 feet		-		
4601.GPJ DBTempl		-		12						SN	Л	- Gray silty fine to co gravel	arses	sand with fine to coa	arse			
USERSVINASHIDESKI OP/018684	Not	e: Ple	ase	see	Figure	A-1 for	explana	tion	of sy	mbols	5							
13 Path:C.										L	og	of Monitorin	۱g ۱	Well MW-3	3S(a)		
Seattle: Date:5/14,	G											Project: Project Locatic Project Numbe	on: er:	Puget Sound Gas Works F 0186-846-01	d Enei Park, s	gy N Seatt	orth Ie, W	Lake Union /ashington Sheet 1 of 1





Log of Monitoring Well MW-33S(b) (continued)



Project: F Project Location: G Project Number: 0

Puget Sound Energy North Lake Union ation: Gas Works Park, Seattle, Washington ber: 0186-846-01

Figure A-7 Sheet 2 of 2



0186-846-01

ERS8.GDT/GEI8 ENVIRONMENTAL DBT GР Date:5/14/1

Figure A-8 Sheet 1 of 1



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Figure A-9 Sheet 1 of 1



\frown		\square		FIE			—				T		WELLING
Elevation (feet)	Jepth (feet)	nterval	Recovered (in)	3lows/foot	Collected Sample	Sample Name	Nater Level	Graphic Log	Broup Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	
	20 —		60	<u> </u>	+		f		SP	Black fine to medium sand lense			
-	-					- MW-36D (23-24)			GP	Black coarse gravel with coarse sand, - multi-colored agglomerate with larger debris (brick)	-		
- -	- 25 -					(20-2-7) +DUP			SM	Gray to black silty fine to coarse sand with fine to coarse gravel	- - - MS	31	10-inch diameter borehole to 28 feet, 6-inch diameter borehole to 35 feet
-	-		60						SP-SM	Gray medium to coarse sand with silt and fine to coarse gravel, some silt lenses -	- - - ss	10.1	
-	-					MW-36D (29-33 composite)			SM	- Silty fine to medium sand with occasional fine _ gravel (wet)	-		28.0'
_0	30 —		60						.		MS	33.5	PVC screen, 0.020-inch slot width
-	-					MW-36D (31-32)			SM	Gray silty fine to medium sand with fine to coarse gravel (dense, moist)	- SS 	10	10/20 sand backfill
-	-										NS	8.0	33.8' - 4-inch slip cap
	lote: Pl¢	ease		Figur	e A-1	for explana	ation	of sy	mbols				35.0
		=	_	_	_			 Loز	g of N	Ionitoring Well MW-36D (conti	nued	I)	
eattle: Date of	Cog of Monitoring Well MW-36D (continued) Project: Puget Sound Energy North Lake Union Project Location: Gas Works Park, Seattle, Washington												ake Union Ishington Figure A-10

0186-846-01

Figure A-10 Sheet 2 of 2



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Figure A-11 Sheet 1 of 2

\square		FIEL	D DA	٩ΤΑ							WELL LOG
² Elevation (feet) § Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	
	- 48			MW-36S (22.5-23)			SM	Black coarse gravel (1/2"), smaller pieces are broken up agglomerate, heavily coated with free NAPL Silty fine to medium sand with occasional fine gravel	HS HS SS	62 88 13	22.8'- 23.0' 23.5'-

Log of Monitoring Well MW-36S (continued)



Project: P Project Location: G Project Number: 0

Puget Sound Energy North Lake Union tion: Gas Works Park, Seattle, Washington ber: 0186-846-01

Figure A-11 Sheet 2 of 2



ſ		FIELD DATA													WE	ELL LC	G
	Elevation (feet)	Depth (feet)	Interval	Recovered (in)	Blows/foot	Collected Sample	Sample Name	Water Level	Graphic Log	Group Classification	MATE DESCF	ERIAL IPTION	Sheen	Headspace Vapor (ppm)			
		20 —		24						SM	Gray silty fine to mediun fine to coarse rounde -	sand with occasional d gravel (dense, wet) -			22 (1)	1000 1000 1000 1000 1000 1000 1000 100	
DB1emplate/Lb1emplate/GEOENGINEERS8.GD1/GEI8_ENVIRONMENTAL_WELL																	
USERS/TNASH/DESKTOP/018684601	Not	e: Plea	ase s	see F	-igure :	A-1 for	explana	tion	of syr	nbols							
13 Path:C:								L	_00	g of M	Ionitoring Well	MW-37S (contin	ued)			
ate:5/14/							0.1	J.			Project:	Puget Sound Energ	jy No	rth La	ake Union		
Seattle: D	Ċ	E	DE		IG	INE	ER	S			Project Location: Project Number:	Gas Works Park, S 0186-846-01	eattle	e, Wa	shington	Fig SI	ure A-12 neet 2 of 2



0186-846-01

Date:5/14

NFI N

ENVIRONMENTAL

/GFI8

Figure A-13 Sheet 1 of 1

ſ	Drilled	3/25	<u>Starl</u> 5/20 [,]	13	<u>Er</u> 3/26	<u>nd</u> /2013	Total Depth	n (ft)	2	22		Logged By PDR Checked By ZAS	Driller Boart Lor	ngyear			Drilling Method	Sonic (c	ontinuous cor	e)
F C	-lamm Data	er									Dril Equ	lling Rubber Tr uipment S	ack-Mounted Spic	der 3	A 2 (in)	well wa	s installed c	on 3/26/20 <i>°</i>	3 to a depth of 2	2.1
s	Surfac /ertica	e Elev al Datu	atior Im	ו (ft)		USA	26.99 CE (Loci	ks)			Top Ele	o of Casing vation (ft)	26.74		(ft). <u>Ground</u>	water	De	oth to		
E	Easting Northir	g (X) 1g (Y)				12 23	70814.56 39391.05	5			Hor Dat	rizontal tum NAD83 W	/A State Plane No	orth	Date Mea 4/22/20	asured 013	<u>Wa</u>	ater (ft) 5.0	Elevation 22.0	<u>(ft)</u>
	Notes	:	Ha	nd-o	dug w	ith p	osthole d	ligg	jer fr	om C) to	2 feet bgs. Tempora	ry conductor casi	ing (10-ir	nch diam	neter)	used from	n 0 to 15	feet	
ſ				3, 99	FIEL	D D)ATA				1.0							WELL	LOG	\equiv
	(feet)	et)		d (in)	t	Sample	ame	el	l 60		tion	MA	ATERIAL			a Ê			Steel surfac	•
	evation	pth (fe	erval	covere	ws/foo	llected	mple N	ater Lev	aphic L	dno	assifica	DES	CRIPTION		een	adspac por (pp		/	monument	5
	Ele	o De		е́Я 24	Blo	8	Sai	Ma	5 1111	5 SI	B M	Black silty fine to coa	arse sand with organ	nics (tree	ů	- Aa Va			\mathbb{R}	
-		-	M			T	MW-39D (0.5-1.5)					roots), some brid odor	ck fragments, no stair	ning, no	NS	<1			Concrete surfa	ice
_1	ŕ	_	\square	26		+						Cradeo to inorrogood	I madium ta asaraa a	and			2.0'—		sear 2-inch Schedu	le 40
		_		30								Grades to increased	i medium to coarse s	sanu					PVC well casir	ıg
										SP-	SM	Brown to black medi occasional black vesicular materia	um to coarse sand w , low density, angular al, fines portion very f	vith silt, r fine	55	<1				
		_										(possible cinders	3)		NS	<1				
		5-		60															borehole to 15 6-inch diamete	er feet, r 1
-	0	-										Groundwater encour	ntered at 6.1 feet		-				feet.	
_1	20	-								S	P	Brown to black medi silt, larger more	um to coarse sand w common black, low d	vith trace lensity,	NS	<1			0	
-		-				T	MW-39D (8-10)					angular vesicular agglomerate ligh	r material, occasiona t brown to orange co	al blor	-				Bentonite seal	
-		-										-			-					
TAL_WEL		10 —		60		+						Brown to black medi	um to coarse sand w	vith trace	NS	<1				
IRONMEN		-										material with vitr pieces of friable	eous luster, occasion light colored agglome	nal small erate,	-					
GEI8_ENV	\$	-								•			brown to red color		-					
RS8.GDT/(-										Drilling becomes ha	rder at 13 feet		_					
ENGINEEF		-				I	MW-39D		T	SI	M	Gray silty fine to coa coarse gravel	arse sand with occasi	ional	- NS	<1				
late:GEOI		15 —		60			(14-15)			SP-	SM	Grav fine to coarse	sand with silt and fine				15.0'—		0000	
e/LibTemp		_					MW 20D				0	coarse rounded odor, gravel colo	gravel, gravel to 1.5", r is white to orange	', no		<i>c</i> 1	16.0'-		20/40 sand ba	ckfill
DB Templat	0	-					(16-19 composite)					_					17 11	0 0 0 0	10/20 sand ba	ckfill
01.GPJ D							MW-39D (17-18)										17.1		5.	
P\0186846																		◦		
1/DESKTO		-								SI	М	Gray silty fine to me fine to coarse ro	dium sand with occas unded gravel, dense,	sional , no odor	NS	<1			PVC screen, 0.020-inch slot	e 40
RS\TNASH I	Not	20 — te: Ple	ase	see l	Figure	۱ A-1 f	or explana	tion	of sy	mbols	s	L_				I	ı ł	λ. ∿ γ —1λ. ΄	. y would	
					-						-	,								\dashv
:5/14/13 Pa			_								LO	og of Monitori	Puget Sou			orth I	ake I Ini	on		
attle: Date	C	E	ol	ĒN	NG	IN	EER	S	1	J		Project Locatio	n: Gas Work	s Park,	Seattle	e, Wa	ashingto	n	Figure Δ ₋ 1	4
Se		-	1					-	-	-		Project Numbe	r [.] 0186_846_	.01					Shoot 1 of	່

0186-846-01

Figure A-14 Sheet 1 of 2

	[F	FIEL	D DA	ATA								WE	LL LOG
	n (feet)	eer)			ot	d Sample	Name	evel	Log	ation	MATI			ace pm)		
	Elevation	neptn (16	Interval	Kecover	Blows/fo	Collected	Sample	Water Le	Graphic	Group Classific	DESCR	RIP HON	Sheen	Headspa Vapor (p		
	2	:0 —	2	24											¢	0
															21.8'	0 1.5-inch slip cap
															22.1'	
ΞĽ																
1EN I AL_WE																
8.GU1/GE18																
INGINEERS																
nplate:GEUE																
plate/Lib l en																
er ublem																
018684601.0																
UESKI OPV																
SEKSVINASH	Note:	Plea	se se	ee Fi	igure /	A-1 for	explana	ition	of syr	nbols						
13 Path:C:\U\									Log	j of N	lonitoring Well	MW-39D (contir	nued)		
Date:5/14/.	0		, r						/		Project:	Puget Sound Energy	gy No	orth La	ake Union	
Seattle:	G	EC)E	N	IG	INE	ER	S			Project Location: Project Number:	Gas Works Park, S 0186-846-01	seattle	e, wa	isnington	Figure A-14 Sheet 2 of 2



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ile: Date:5/14/13 Path:C:USERSITNASHDESKTOP/018884601.GPJ DBTemplate/LibTemplate:GEOENGINEERS8.GDT/GEI8_ENVIRONMENTAI

Figure A-15 Sheet 1 of 1



Log of Monitoring Well MW-40S

Project:



Date:5/1

Puget Sound Energy North Lake Union Project Location: Gas Works Park, Seattle, Washington Project Number: 0186-846-01

Figure A-16 Sheet 1 of 1

	Drilled	Start End Total 2 lled 4/1/2013 4/1/2013 Depth (ft) 2 face Elevation (ft) 35.42 USACE (Locks)								27		Logged By A Checked By Z	ARJ ZAS ^{DI}	_{iller} Boart Longyear			Drilling Method	Direct Push	
S V	urface ertical	e Eleva I Datui	atior n	า (ft)		USA	35.42 CE (Lock	(S)			H D	ammer ata			Drilling Equipi) ment		Geoprobe 662	20 DT
E	asting	g (X) a (Y)				127	70720.37 39526.8	,			S	ystem NA	AD83 WA	State Plane North	Groun	dwate	<u>r</u>	Depth to	
•	Notes:	9(1)				20	0020.0						1000 11/1		Date N	easure	<u>d</u>	<u>Water (ft)</u>	<u>Elevation (ft)</u>
ř					FIEL	D D	ATA												
:	eet)			(in)		mple	le	_	6		E		ΜΔΤΙ	ΞΡΙΔΙ					
	ation (f	h (feet	val	overed	s/foot	cted Sa	ple Na Ing	er Leve	hic Lo	đ	sificatio		DESCF	RIPTION		space r (ppm)		REMAR	ŚŚ
li	Eleva	o Dept	Inter	Reco	Blow	Colle	<u>Sam</u> Testi	Wate	Grap	Grou	Clas				Sheel	Head			
	þ	-		30			GEI-1 (0-3)			S	М	Brown silty fir gravel, br (rootlets) black (me	ne to mediu rick fragmer one black a edium dense	Im sand with occasional hts, trace organics aspheltic gravel, fused e, moist)	_ NS	<1			
		_								S	М	Dark brown s	silty fine to r al gravel (m	nedium sand with edium dense, moist)		<1 <1			
-															NS	<1			
-												Grades to bla	ack						
-		_										-			-				
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	þ	5 —		30								-			-				
		_										Grades to bro	own		NS -	<1			
-		- GEI-1									014			1	_				
-		GEI-1 (7-7.5)									SM	Black stained and fine g	gravel (med	to medium sand with silt ium dense, moist)	NS	<1			
-												Ī							
- -		_								- s	P	Brown, tan, y	vellow, black	coarse sand with gravel; e, fused, low density,	·				
	ò	10 —		36								low densit	, tan, brown ity vesicular	, yellow and black fused , metallic luster (loose,	-				
		_										_			NS -	<1			
		_				+	GEL1					_			_				
1999 -						Ļ	(12-12.5)												
												Becomes bla	ick stained		<5%	<1	Grou	indwater encounter	red at 13 feet
		_											- <u>-</u>		-				
are:GEO	ò	15 —		42						G	iP	Gray gravel v — red, black material a	with sand; g <, tan, fusec and black. v	ravel is agglomerate, I low density, vesicular esicular. low density.	-				
VLID I EMP		_										metallic lu	uster (mediu	um dense, wet)	_				
		_				Ţ	GEI-1 (16.5-17)		0 0 0 0			Tar-like blebs	s within grai	n space artially decayed	HS	<1		Tar-like, raint	woo
						<b>↓</b>	(17-17.5)		•	S	P	Gray medium gravel (de	n to coarse ense, wet)	sand with occasional					
1808400		_													NS	<1			
		-										-			-				
NASHUL		20 —										L							
IDSERSI	Note	e: Plea	ase	see l	igure	A-1 fo	or explanat	ion	of sy	mbol	s								
												Log o	of Bori	ng GEI-1					
Jate:5/14/				_	53		C. 1	L.	1			Project:		Puget Sound Ene	ergy N	orth	Lake L	Jnion	
Deame: L	G	E		= N	١G	IN	EER:	S		1		Project Lo	cation:	Gas Works Park,	Seat	le, V	Vashing	gton Fi	igure A-17
1												FIDJECT NL	innber:	0100-040-01					Sneet 1 of 2

Sheen	Headspace Vapor (ppm)	REMARKS
NS	<1	
- NS	<1	
NS	<1	
_		
 _ NS	<1	
-	NS NS NS NS	Alport (ppm) - NS - 1 -

# Log of Boring GEI-1 (continued)



Project: Project Location: Project Number:

Puget Sound Energy North Lake Union on: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-17 Sheet 2 of 2

Drille	ed 4/1	<u>Start</u> 1/201	3	<u>Enc</u> 4/1/2	<u>1</u> 2013	Total Depth	(ft)	2	0		Logged By ARJ Checked By ZAS	Driller Boart Longy	year			Drilling Method Direct Push
Surfa Vertic	ice Eleva cal Datu	ation m	(ft)	ι	3 JSAC	7.87 E (Loci	(s)			Ha Da	ammer ata			Drilling Equipn	nent	Geoprobe 6620 DT
Eastin North	ng (X) hing (Y)				127( 238	)319.96 899.51	6			Sy Da	vstem atum NAD83 \	VA State Plane Nor	th	Ground Date Me	dwater easure	Depth to <u>Water (ft)</u> <u>Elevation (ft)</u>
Note	IS:															
Elevation (feet)	⊃ Depth (feet)	Interval	Recovered (in)	Blows/foot	- Collected Sample O	Testing UT	Water Level	Graphic Log	Group	Classification	M/ DES	ATERIAL CRIPTION		Sheen	Headspace Vapor (ppm)	REMARKS
- - _%	-		24			(0-3)			SM SP	<u>A</u>	Approximately 2 inc Brown silty fine sand fine sand at 0.25 Black stained mediu (medium dense,	tes asphalt concrete I with gravel, grades to t feet m to coarse sand with g moist)	tan gravel	- NS - <5% - NS -	<1 <1 <1	Gray, blocky
-	5 48 GEL-2 (5-6) GEL-2 (5-6) GEL-2 (5-6) Gray to black fine to coarse gravel with sand medium dense, moist) NS <1															
	, - , - , - , - , - , - , - , - , - , -										- - Slight naphthalene-I	ke odor		- NS - NS - SS <15% -	<1 <1 <1	White, blocky
			10					0	SP SP	<u> </u>	Tan medium to coai dense, moist) Red-brown 1-inch ir Red-brown fine to co Brown medium to co	se sand with gravel (me terbedded silt and fine s barse sand with gravel parse sand (dense, mois	edium sand st)	NS NS	<1	Groundwater encountered at 14.5 feet
	_		40		Ť	GEI-2 (16-17)			SP-S	δM	Brown gray mottled – gravel and silt (c	medium to coarse sand ense, wet)	l with	- NS	<1	
	- - 20				<b>.</b>				SM	1	Gray silty fine to coa wet) -	rse sand with gravel (de	ense,	NS -	<1	
N	ote: Plea	ase s	see F	igure A	A-1 for	explanat	tion	of syr	nbols							
											Loa of Ba	oring GEI-2				
	Geo	DE	ĒN	IGI	NE	ER	S	0	1		Project: Project Locatio	Puget Sound n: Gas Works F	d Ene Park,	rgy No Seatt	orth Ie, V	Lake Union /ashington Figure A-18

0186-846-01

Figure A-18 Sheet 1 of 1

	Drilled	<u>S</u> 3/27	t <u>art</u> 7/20	13	<u>En</u> 3/27	<u>nd</u> 7/2013	Total Depth	(ft)	2	9		Logged By ARJ Checked By ZAS	Driller Boart Longyea	ır			Drilling Method Direct Push
s v	urface 'ertical	Eleva Datur	ntior n	n (ft)		USAC	34.07 CE (Loci	(s)			Ha Da	immer ita	1		Drilling Equipn	nent	Geoprobe 6620 DT
E N 1	asting lorthing	(X) g (Y)				127 239	0730.52 9136.77	2			Sy Da	rstem atum NAD83	WA State Plane North		Ground Date Me	dwater easure	Depth to <u>d Water (ft)</u> <u>Elevation (ft)</u>
							Λ <b>Τ</b> Λ										
	Elevation (feet)	bepth (feet)	Interval	Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Water Level	Graphic Log	Group Classification	Classification	M DES	ATERIAL SCRIPTION		Sheen	Headspace Vapor (ppm)	REMARKS
-		- 0		30						Brick SP SM	:k 5	Approximately 1-inc Brown fine to mediu (paver sand) Dark gray silty fine occasional gray	ch thick brick paver um sand (dry to moist) (fill) to medium sand with el (silt 30% gravel 15%)	 	- SS - 5% - MS	<1	Blocky, metallic
-		_					GEI-3 (2-3)					moderate hydro	carbon odor		40%	1.5	Florets
0	9	_								- sm	1 -	Brown to dark brow occasional grav	n silty fine sand with el, trace organics (mulch)		~5%		
-												-			NS	1.3	
- - -	Ś	- SI - GEI-3 (8-9)										Black medium to cc - soot, gravel red agglomerate, lo irregular, angula - medium to coar moderate napht	aarse sand with gravel and , tan, black, yellow w density fused and vesicula ar, sand black soot stained, se fragments, agglomerate, halene-like odor	ar,	MS 30%	3.7	Florets, streaks
		10 —		24								Black, tan, red med occasional grav fragments and o agglomerate, lo metallic	lium to coarse sand with el, sand agglomerate cinders, fused, irregular grav w density, angular, vesicular	/el	мз	5.6	Florets, streaks
		_					GEI-3 (11.5-12)			GP	<u> </u>	Olive green gravel strong naphthal fused, vesicular	with sand, NAPL present, ene-like odor, agglomerate, , angular to subrounded (we	 et)	HS -	14.2	Groundwater encountered at 12 feet
	ò	- 15 —		18								-		-	HS	93	
		-					GEI-3 (16-17)			\$00 \$00	DT DT	Green gray to dark Dark gray to black s decayed light br naphthalene-like	gray soot-like material soot-like material with partial own wood fragments, strong e odor (wet)	lly J	NS HS	123	Strong naphthalene-like odor
	ó	-								— <u>—</u> —		Gray elastic silt with	n trace organics (rootlets)		-		Respirator used
	Note	20 e: Plea	ise	see F	igure	A-1 fo	r explana	tion	of syr	nbols		_					
												Log of B	oring GEI-3				
ocarile. Date:01-	G											Project: Project Locatio Project Numbe	Puget Sound E on: Gas Works Pa er: 0186-846-01	iner rk, S	gy No Seatt	orth le, V	Lake Union Vashington Sheet 1 of 2



### Log of Boring GEI-3 (continued)



Project: Project Location: Project Number:

Puget Sound Energy North Lake Union tion: Gas Works Park, Seattle, Washington ber: 0186-846-01

Figure A-19 Sheet 2 of 2

Dril	lled	<u>St</u> 3/27/	<u>art</u> 2013	E 3/2	<u>End</u> 27/2013	Total Depth	(ft)	3	51	Logged By ARJ Checked By ZAS	Driller Boart Longyear				Drilling Method Direct Push
Sur Ver	face E tical D	ilevat atum	ion (ft	)	USA	28.53 CE (Locl	(s)		H D	ammer ata		Dril Equ	ling Jipm	nent	Geoprobe 6620 DT
Eas Nor	ting (λ thing (	() (Y)			12 [.] 23	70767.86	6		S D	ystem Jatum NAD83 V	VA State Plane North	Gro	ound	lwater	Depth to
Not	tes:													asurec	
				FIE	LD D	ATA									
(feet)	(ter	cr)	(in) be	ot	Sample	<u>lame</u>	vel	-og	ation	MA				a (F	REMARKS
levatior	enth (fe		ecovere	lows/foo	ollected	ample h esting	ater Le	raphic I	roup lassifica	DES	CRIPTION		leen	eadspac apor (ppi	-
Ξ	Ċ	<u>י</u> 	18		ŭ	ЮĻ	3	0 I I I	D D AC	Approximately 2 inch	nes asphalt concrete	č	מֹ	Ϊ»	
-		-			Î	GEI-4 (0.5-1.5)			SM	Dark brown to black occasional fine g asphalt fragment	silty fine sand with ravel, trace brick fragments, s (loose, dry to moist)	-		<1	Organic sheen
-		_			+					-		_		<1	Very loose, almost no hammer action
-		_													
_ ¹ 2									SP	Black to brown fine t (red, tan, brown agglomerate, low	o medium sand with gravel fine to coarse gravel, / density, fused) (black fine				
-										grained, low den (loose, moist)	sity, metallic luster, vesicular)				
_	Ę	5 —	24			GEI-4			GP	Grav to black fine to	coarse gravel with sand	- N 60 N	1S 0% 1S	18	Florets Florets, olive stained gloves
_										<ul> <li>gravel is black me to gravel is black aq angular, fused; s</li> </ul>	and is black, tan to red	_ 15	5%		Groundwater encountered at 6 feet
	- b c agglomerate, low density, subrounded to														
-		_						ວັດ ວິດ		-		_			
_ <u>^</u>		_						ວິດ ວິດ		_		_			
								$\circ$							
	10	) — (	9			GEI-4 (10-11)				_		S	SS %	2.8	Streaks
		-			*					-		- 0			
		-						0 0 0 0		-		-			
		-								-		_			
		_						$\hat{\mathbf{a}}$		-		_			
	15	5 —								_		_			Mathe ell libre a des
		-	12			(15-16)				Sand has soot coate	d grains, tan, red, black,	S 5	ss %	5.0	
		_			_			ວັດ ວິດ		- angular to round	ea, iow density (wet)	_			
		-						ວິດ ວິດ		-		-			
20004001.C		-								-		-			
		-							SP-SM	Black to dark gray fi	ne sand with gravel and silt;				
	20	)								possibly stained wet)	(medium dense to dense,				
	Note: I	Pleas	e see	Figur	e A-1 fo	or explana	tion	of syr	mbols						
										Log of Bo	oring GEI-4				
Jate of 14/	~	A	-			S. 1.	J.	1		Project:	Puget Sound Ene	ergy	No	orth	Lake Union
Seame	GI	EO	E	NG	iIN	EER	S			Project Locatio	n: Gas Works Park, r: 0186-846-01	Sea	attl	e, W	/ashington Figure A-20

$\square$			FIEL	D D	ATA							
Elevation (feet)	े Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
-	20 —	42		Î	GEI-4 (20-21)					NS	5.0	Moderate mothball-like odor
-	-			<b>.</b>					- Grades to gray -	-		
<u>م</u>	_									NS	2.3	
-	-							SM	Gray silty fine to medium sand with occasional gravel (dense, wet)			
-	25 —	48										Slight mothball-like odor
-										NS	1.8	
-												
	_			Ţ	GEI-4 (28.5-29)			SP-SM	<ul> <li>Dark gray fine sand with silt and occasional fine</li> <li>gravel (stained plastic sampler olive color)</li> <li>(very dense, wet)</li> </ul>	HS 80%	1.1	Slight mothball-like odor Rainbow
-	30 —	12		Ì	GEI-4 (30-31)					SS <5%	1.5	White streaks

tatte: Date:5/14/13 Path:C:USERSITNASHIDESKTOP/018684601.GPJ DBTemplate/LibTemplate/SEOENGINEERS8.GDT/GEI8_ENVIRONMENTAL_STANDARD

Note: Please see Figure A-1 for explanation of symbols

### Log of Boring GEI-4 (continued)



Project: Project Location: Project Number:

Puget Sound Energy North Lake Union Gas Works Park, Seattle, Washington 0186-846-01

Figure A-20 Sheet 2 of 2

Drilled 3/28/2013 3/28/2013 Total Depth (ft) 24								24	Logged By ARJ Checked By ZAS Driller Boart Longyear				Drilling Direct Push		
Surface Vertica	e Eleva al Datu	ation (ft) m	)	USA	25.87 CE (Locl	(s)		H	lammer Data				Drilling Equipr	) ment	Geoprobe 6620 DT
Easting Northin	g (X) ng (Y) : Hand	l-dug wi	th post	127 239 hole di	70823.98 9274.93 igger from	3 n 0 to	o 2 fe	s E et bgs.	System Datum NAD83 WA State Plane North			<u>Groun</u> Date M	dwate leasure	r Depth to <u>Elevation (ft)</u>	
$\geq$	FIELD DATA														
Elevation (feet)	⊃ Depth (feet) 	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Water Level	Graphic Log	Group Classification		M/ DES	ATERIA SCRIPTI	L ON	Sheen	Headspace Vapor (ppm)	REMARKS
_^^^ _	-	24		T	GEI-5 (1.5-2)			SM	Dark brov organi _ roots)	vn silty fine ics (rootlet (loose, mo	e to medium ts, wood frag oist) (topsoil	sand with gments from tree )	NS	<1	
-	-	34		*				SP	Tan, red, 1-inch sof Sand mac friable Gravel is small	gray fine t ft partially de of angu e; tan, red ag vesicles (la	to coarse sa decayed wo ilar, low dens gglomerate, oose, moist)	nd with gravel; od chip sity, agglomerate, low density, fused	NS NS	<1	
- _^P	5 —	34			GEI-5 (5-7)			SP	Gray to ta gravel Sand is p agglor red-br luster;	an fine to c I (medium redominar merate, fria rown fused	coarse sand dense, wet) htly angular, able, coarse d agglomerat	with occasional ; low density sand includes te with vitreous	– – NS		Groundwater encountered at 5 feet
-	-			•					Gravel is vitreou – low de	red-brown us luster, t ensity, sligl	i fused agglo black agglon ht odor	omerate with nerate, vesicular,	NS NS	9.6	
		30		Ţ	GEI-5 (10-10.5)			GP GP	- Black, tan - coarse Gravel is agglor - low de Sand is a friable	h, brown cc e sand (me black, tan, merate, an ensity, vitre ngular, low e, slight ode	parse gravel edium dense , red, brown gular to sma eous luster; v density, ag or	with medium to e, wet); fused all to no vesicles, nglomerate,	- - NS - NS	3.5 8.5	
- ~		30		<b>•</b>	GEI-5 (15-16)			SM	- Gray silty - subroi 1/2-ind - Increasing -	medium to unded to n ch mediun g silt	o coarse sar ounded grav n sand lense	nd with gravel, vel, occasional e (dense, wet)	- NS - NS - NS	1.8	Rock in sampler shoe
- Not	- 20	ase see	Figure	A-1 fo	or explana	tion	of sy	SM	Gray silty round	fine to coa	arse sand wi (very dense,	ith coarse wet)	_		
									Log	of Bo	oring G	GEI-5			
Ċ	GEOENGINEERS Pro										Project:       Puget Sound Energy North Lake Union         Project Location:       Gas Works Park, Seattle, Washington         Project Number:       0186-846-01				

$\square$			FIEL	D D	ATA							
Elevation (feet)	성 Depth (feet)	Interval Recovered (in)	Blows/foot	<b>Collected Sample</b>	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
6	20	48								NS	4.5	
	-			Ì	GEI-5 (22-23)					NS	1.2	

# Log of Boring GEI-5 (continued)



Project: Project Location: Project Number:

Puget Sound Energy North Lake Union on: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-21 Sheet 2 of 2



$\square$			FIEL	D D	ATA							
Elevation (feet)	3 Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
-	20 -	24		1	GEI-6 (20-21)				Black stained fine to coarse gravel with coarse sand; gravel black vesicular agglomerate; sand stained, fused agglomerate, tan, red, brown, platey	HS 60%	90.5	Metallic
-	-						0	SM	Dark gray to black silty fine sand with rounded to subrounded gravel (dense, wet)	SS		Streaks
- %	- 25 —	- 48		+	GEI-6					ня	122	
-	-	40		Ļ	(25-26)				- Grades to gray	- SS 5%	15.1	Milky streaks
-	-								Grades to very dense	NS		
- 0	-							- <u>-</u>	- Gray silty fine sand with gravel	NS	10	
-	30 —	12		Ì	GEI-6 (30-31)					NS	22.8	

### Log of Boring GEI-6 (continued)



Project: Project Location: Project Number:

Puget Sound Energy North Lake Union a: Gas Works Park, Seattle, Washington b: 0186-846-01

Figure A-22 Sheet 2 of 2



$\square$			FIEL	D D	ATA							
Elevation (feet)	s Depth (feet)	Interval Recovered (in)	Blows/foot	<b>Collected Sample</b>	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
- -  -		48			GEI-7 (20-21)					NS	<1	

### Log of Boring GEI-7 (continued)



Project: Project Location: Project Number:

Puget Sound Energy North Lake Union on: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-23 Sheet 2 of 2

Start         End         Total         15         Logged By         ARJ         Driller         Boart Long           Drilled         4/1/2013         4/1/2013         Total         15         Checked By         ZAS         Driller         Boart Long												Driller Boart Longyear			Drilling Method Direct Push
Surfac Vertica	e Elev al Dati	/atio	n (ft)		USA	25.32 CE (Loc	ks)			Hammer Data	I		Drillin Equip	g ment	Geoprobe 6620 DT
Eastin Northin Notes	g (X) ng (Y) : Har	nd-du	ıg wit	h post	127 23	70602.79 8807.66 igger fron	9 6 n 0 to	o 2 fe	et bgs.	System Datum NAD83 WA State Plane North			Grour Date N	idwatei leasure	Depth to d Water (ft) Elevation (ft)
$\geq$	FIELD DATA														
Elevation (feet)	o Depth (feet)	Interval	Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Water Level	Graphic Log	Group Classification		MA DES(	TERIAL CRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
	30       GEL8       SP       Red, brown, black fine to medium sand with gravel (medium dens, wet)         48       GEL8       SP       Red, brown, black fine to medium sand with gravel (medium dens, wet)         5       48       GEL8       SP       Red, brown, black fine to medium sand with gravel (medium dens, wet)         6       GEL8       SP       Dark brown to black silty fine sand with gravel (medium dens, wet)         10       50       SP/SM       Gray medium sand and silty sand interber (dense, wet)         10       50       SP/SM       Gray medium sand and silty sand interber (dense, wet)         10       50       SP/SM       Gray silty fine to medium sand with grave         10       50       SP/SM       Gray silty fine to medium sand with grave         10       50       SP/SM       Gray silty fine to medium sand with grave         10       50       SP/SM       Gray silty fine to medium sand with grave         10       50       SP/SM       Gray silty fine to medium sand with grave         10       50       SP/SM       Gray silty fine to medium sand with grave         10       50       SP/SM       Gray silty fine to medium sand with grave         10       50       SP/SM       Gray silty fine to medium sand with grave         10									d silty fine sand with i, one fine gravel piece of e, vesicular, metallic luster agglomerate, red to brown iable gravel is black erate with metallic luster; alene-like odor (moist to silty fine sand with gravel; lack agglomerate, vesicular, edium dense, wet) gravel (medium dense, wet) h occasional thin sandy silt organics (rootlets) (soft, wet) ind silty sand interbedded fium sand with gravel	- NS - SS 10% / NS / NS - NS - NS - NS - NS - NS 	<ul> <li>&lt;1</li> <li>&lt;1</li> <li>&lt;1</li> <li>&lt;1</li> <li>&lt;1</li> <li>&lt;1</li> </ul>	White streaks Groundwater encountered at 4.5 feet White streaks Moderate odor		
No	te: Ple	ease	see	Figure	A-1 fc	or explana	ition	of sy	mbols						
										Log o	f Bo	ring GEI-8			
C	<b>BE</b>	ol	En	١G	IN	EER	S	0	J	Project: Project Loc	catior	Puget Sound Ene Gas Works Park,	ergy N Seat	lorth tle, V	Lake Union Vashington Figure A-24

seatie: Date:5/14/13 Path.C:USERS\TNASHDESKTOP018884601.GPJ DBTemplateLlibTemplate.GEOENGINEERS8.GDT/GEI8_ENVRONMENTAL_STANDARD

Figure A-24 Sheet 1 of 1

0186-846-01


$\square$		FIEL	D D	ATA							
Elevation (feet) 3 Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
- 20	46							Gray silty fine to medium sand with gravel (dense, wet)	NS	<1	
-	-								NS		
_%									NS	<1	
- 25	_										

Note: Please see Figure A-1 for explanation of symbols

#### Log of Boring GEI-9 (continued)

![](_page_433_Picture_4.jpeg)

Project: Project Location: Project Number:

Puget Sound Energy North Lake Union on: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-25 Sheet 2 of 2

Dr	illed	<u>5</u> 3/2	<u>Start</u> 9/20	13	<u>En</u> 3/29	<u>nd</u> //2013	Total Depth	(ft)	2	20		Logged By Checked By	ARJ ZAS	Driller Bo	oart Longyear			Drilling Method	Direct Pu	ısh
Su Ve	rface rtical	Eleva Datu	ation n	(ft)		USA	23.92 CE (Loci	(s)			Har Dat	mmer ta				Drilling Equipr	) nent		Geoprobe	e 6620 DT
Ea: No	sting rthing	(X) g (Y)				12 23	70238.07	7			Sys Dat	stem tum	NAD83	WA State F	Plane North	<u>Groun</u>	dwate	<u>r</u>	Depth to	
No	otes:															Date IVI	easure	<u>:0</u>	<u>vvater (π)</u>	<u>Elevation (it)</u>
					FIEL	D D	ATA													
feet)		£		(in)		ample	ime		p	5	5		M	ATERIAI	_					
ation (		th (fee	val	overed	vs/foot	ected S	ing	er Leve	ohic Lo	up sificati	ssincau		DES	CRIPTIC	ON NC	u	dspace or (ppm)		REM	ARKS
Elev		o Dep	Inter	Rec	Blov	Colle	<u>San</u> Test	Wat	G G U	C C	Ca	Dia La		Caralland		Shee	Head			
				48						SIVI	1	Black to t	ional grav	el (loose, moi	im sand with ist)					
		_										_				NS	<1			
		_				Ì	GEI-10 (2-3)		0 0	GP-G	θM	Black gra wet);	vel with sil gravel is b	t and sand (n lack agglome	nedium dense, rate, metallic	MS	2.5	Gro	undwater enc	ountered at 2.5 feet
F		_				┢			0	SM	1	luster the sa	, vitreous, ame, mod	sand is small erate hydroca with gravel ()	ler particles of arbon odor	- 90%	2.0		Flat me	tallic, faint
<u>_1</u> 0		-										_ wet)	ine sand	with graver (i	neulum dense,	- NS	<1			
-		5 —		30						SP	, -	Gray meo grave	dium to coa	arse sand wit	h fine to coarse	_				
		_														NS	<1			
						Ť	GEI-10 (6.5-7.5)					Increasing	g gravel							
		_				<b>↓</b>						-				NS	<1			
Ē		-										_				-				
_%		_										-				-				
I		10 —		30								_								
		_								<u> </u>			to modium			NS	<1			
										55		grave	l (dense, v	vet)	he to coarse					
GEI8_EN																NS	<1			
-		_										_				_				
		_										-				-				
ate.ce.01		15 —		48								Fine to m	edium sar	ıd						
		_										-				NS	<1			
		_										Medium t	o coarse s	and with coa	rse gravel	NS	<1			
10-10-1																				
01000400		-										-				-				
S S		_										_				-				
		20 —																		
- IDSERS	Note	e: Plea	ases	see F	igure	A-1 fo	or explanat	tion	of sy	mbols										
													of Bo	ring Cl	=1 10					

# Project: GEOENGINEERS

ieattle: Date:5/14/13

#### =1-10 LOG OT Doring C

Puget Sound Energy North Lake Union Project Location: Gas Works Park, Seattle, Washington Project Number: 0186-846-01

Figure A-26 Sheet 1 of 1

Drille	d 3/2	<u>Start</u> 9/2013	<u>En</u> 3/29	<u>nd</u> //2013	Total Depth	(ft)	3	30	Logged By Checked By	ARJ ZAS	Drille	_r Boart Lo	ngyear			Drilling Method	Direct Push	
Surfac Vertic	ce Elev al Datu	ation (ft)		3 USAC	37.21 E (Loci	(s)		H	lammer Data					Drilling Equipr	) ment		Geoprobe 6	620 DT
Eastir North	ng (X) ing (Y) s: Han	d-dug wi	th postl	127 238 hole dig	70251.2 3857.14 gger from	n 0 to	o 2 fe	S D eet bgs.	System Datum	NAD83 V	WA St	ate Plane N	lorth	<u>Groun</u> Date M	dwate leasure	<u>r</u> d	Depth to <u>Water (ft)</u>	Elevation (ft)
$\geq$		-						-										$ \longrightarrow$
Elevation (feet)	o Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Water Level	Graphic Log	Group Classification		MA DES	ATEF CRIF	RIAL PTION		Sheen	Headspace Vapor (ppm)		REMAR	RKS
	0				GEI-11			SM GP-GM SP-SM	Dark brow occas Black silty gravel Dark gray Dark gray Dark gray and o dense Dark gray Sand o dense Mottled ta sand o Gray fine Gray fine	vn silty fine ional grave r fine to me l, brick frag r silty fine to ccasional b e, moist) vn fine grav tan, fused, agglomerat um dense, own and grav with fine grav an, brown a with fine to to medium ck fine to m	edium s gment o mediu prick fra vel with , friable tte, vesi wet) ray silty avel (m and gray	and with occa and and with agglomerate, icular, metallic medium to co and and on se and of the occa and occase y silty fine to oc a gravel (dense with silt (dense sand	h asional gravel ium ; and cluster parse e, moist) coarse e, moist)		<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1<	Perched	groundwater end	countered at 6.5 feet
	- - 20 — 20 =	ase see	Figure	A-1 for	(16-17)	tion	of sv	SP SP	Brown me - (dense -	e, wet)	oarse sa	and with fine (	gravel	- NS 	<1			
									Log	of Bo	ring	GEI-11				·		
	GEO	οEι	NG	INE	EER	S	0	J	Project: Project Project	Location Number	H in: C ir: C	Juget Sou Gas Work )186-846-	ind Ene s Park, 01	srgy N Seatt	orth Ie, V	Lаке U Vashin	gton	Figure A-27 Sheet 1 of 2

$\square$	FIEL	D D	ATA							
Elevation (feet)	Interval Recovered (in) Blows/foot	<b>Collected Sample</b>	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
	36	•	GEI-11 (21.5-22.5)				Grades to gray Tar-like material between grains at 21.75 feet Gray medium to coarse sand with coarse gravel interbedded with gray medium to coarse sand 2-inch thick band of gray fine to medium sand with tar-like globules	SS 5% NS	2.0 <1	Milky
	36	Ţ	GEI-11 (26-26.5) GEI-11 (27.5-28)			SM	2-inch black medium to coarse sand with gravel, stained Silty gray fine to medium sand with rounded fine gravel (very dense, wet)	NS	1.4	

tattie. Date:5/14/13 Path:C:USERSITNASHIDESKTOP/018684601.GPJ DBTemplate/LibTemplate/CEOENGINEERS8.GDT/GEI8_ENVIRONMENTAL_STANDARC

Note: Please see Figure A-1 for explanation of symbols

#### Log of Boring GEI-11 (continued)

![](_page_436_Picture_4.jpeg)

Project: Project Location: Project Number:

Puget Sound Energy North Lake Union tion: Gas Works Park, Seattle, Washington ber: 0186-846-01

Figure A-27 Sheet 2 of 2

Drille	ed 3/2	<u>Start</u> 9/2013	3/	<u>End</u> /29/2013	Total Depth	(ft)	2	:6	Logged By Checked By	ARJ ZAS	Drille	er Boart Lo	ngyear			Drilling Method Direct Push
Surfa Verti	ace Eleva cal Datu	ation (f m	t)	USA	35.41 CE (Lock	s)		Ha Da	ammer ata					Drilling Equipi	g ment	Geoprobe 6620 DT
Easti North Note	ing (X) ning (Y) es: Hand	d-dug v	vith po	127 23 osthole d	70195.16 39046.6 igger from	0 to	o 2 fe	S D et bgs.	ystem atum	NAD83 V	WA St	tate Plane N	lorth	<u>Groun</u> Date N	idwate leasure	27 Depth to ad Water (ft) Elevation (ft)
$\leq$			FI	ELD D	ATA											
Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification		M/ DES	ATEF SCRIF	rial Ption		Sheen	Headspace Vapor (ppm)	REMARKS
_^^^ -	-	36						SM SP SM BRICK	Dark brow organi Grades to Gray med Black silty Crushed r	vn silty fine ics (rootlets black stain lium sand ( sand with red brick	e to mee ts) (moi ined wit (moist) n fine gr	dium sand wit ist) th gravel ravel (slight oc	h trace		<1 <1 <1	
-	-							SP SP	Stained b (moist Black to d brick f	lack to darl i) (strong o lark gray fin fragments	rk gray i odor) ine to m	fine to mediur	n sand	– HS 100% -	187	Metallic, thick
-	5-	48			GEI-12 (5-7)			ML/SM SP	Interbedd sand I	ed gray to lenses	dark br	rown silt to silt	y fine	HS 100%	245	Rainbow, staining brown to PID bag
- -	-								With coar With occa	rse gravel asional 2 m	nm silt k	lenses		- SS <5%	1.7	Milky
	10 —	54			GEI-12 (11-15)			<u>SM</u> SP	Gray to da Black silty Gray med	ark gray / medium s dium sand (	sand wi (mediu	ith brick fragm m dense, wet	ents	HS >95%	, D	Rainbow Groundwater encountered at 11.5 feet
	-								- With fine -	to coarse g	gravel			- HS ->95%	214	Metallic
								SP	NAPL coa Shake tes coppe sampl	ated grains at at 14 fee r colored N ler, gloves	s et: NAP NAPL, s stained	L surface glob stained plastic d olive color	oules,	- HS 100%	251	Globules
	-	30		↓ ↓	GEI-12 (15-17)				Gray med gravel Tar-like b Shake tes globul floatin	lium to coa l (medium o lack materi y between st at 16 fee es at base g	arse sai dense, rial from grains et: tar-lil e of wate	nd with fine to wet) 1 15.5 to 16.5 ke substance er small globu	coarse feet, in les	HS 70% -	30.5	Metallic
	- 20 —		Figure					SP-SM	Gray fine	sand with	silt (de	nse, wet)		_		
		200 500	, iyu		n exhiqi iqr		or syl	GIUUI								
									Log	of Bo	oring	g GEI-12				
	Geo	σE	N	GIN	EERS	5	0	J	Project: Project Project	Locatio Numbe	F on: ( er: (	⊢uget Soι Gas Work 0186-846-	inα Ene s Park, 01	ergy N Seatt	iorth tle, V	Lake Union Washington Figure A-28 Sheet 1 of 2

Sheet 1 of 2

$\bigcap$			FIEL	D D	ATA							
Elevation (feet)	కి Depth (feet)	Interval Recovered (in)	Blows/foot	<b>Collected Sample</b>	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
	20 — - - 25 —	34			GEI-12 (5-26)				- With gravel - Gray medium to coarse sand with fine to coarse	NS	<1	
	_									HS	12.4	

tattie. Date:5/14/13 Path:C:USERSITNASHIDESKTOP/018684601.GPJ DBTemplate/LibTemplate/CEOENGINEERS8.GDT/GEI8_ENVIRONMENTAL_STANDARC

Note: Please see Figure A-1 for explanation of symbols

#### Log of Boring GEI-12 (continued)

![](_page_438_Picture_4.jpeg)

Project: Project Location: Project Number:

Puget Sound Energy North Lake Union on: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-28 Sheet 2 of 2

Dri	lled	Start 4/1/2013         End 4/1/2013         Total Depth (ft)         2           Elevation (ft)         35.17         USACE (Locks)										Logged By Checked By	ARJ ZAS	Driller Boar	t Longyear			Drilling Method Direct Push
Sur Ver	face tical l	Eleva Datur	ntior n	n (ft)	I	3 JSAC	5.17 E (Locł	(s)			Ha	ammer ata				Drilling Equipr	) ment	Geoprobe 6620 DT
Eas Noi No	sting ( thing tes:	(X) (Y)				1270 239	)525.65 143.21	;			S	/stem atum ♪	NAD83 V	VA State Pla	ne North	Groun	dwate leasure	T Depth to ad Water (ft) Elevation (ft)
					FIEL	D DA	TA											
^b Elevation (feet)	. : . :	<ul> <li>Depth (feet)</li> </ul>	Interval	Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group	Classification		MA DES	TERIAL CRIPTION	I	Sheen	Headspace Vapor (ppm)	REMARKS
		0-		54						SF	Ρ	Brown fine moist)	sand with (topsoil)	trace silt (med	ium dense,			
F		_										-				NS	<1	
-		-								SF	P	Black to gr sand w	ay sooty s ith gravel	tained medium (medium dense	to coarse e, moist)	NS	<1	
		5										With occas agglom	sional red, nerate, coa	tan vesicular fu irse sand to fine	used e gravel sized	- NS	<1	
_		-										Gray silt wi	ith occasio	onal fine gravel	(soft, wet)	- ss	<1	Groundwater encountered at 6 feet
	- - - - - - - - - - - - - -										P L	Dark gray f occasic fragme Shake test Gray silt wi – (soft, w	to brown f onal grave nts, mostl from 8 to ith trace o <i>i</i> et)	ne to medium s l and trace orga y decayed) 9.5: trace NAP rganics (wood f	sand with anics (wood L on surface ragments)	- HS 95% - NS	25.8	Rainbow
		_										-				ss	14	Metallic streaks
		-				<b>•</b>	GEI-13 (13-16)					– Occasiona –	l 2 mm sa	ndy silt lenses (	(slight odor)	-		
		-							//	SP-8	sМ	Gray fine s (moder	and with state odor)	silt and gravel (	dense, wet)	- MS 40%	25	Rainbow streaks
		15 — - -		30		<u> </u>				- <u>-</u> SF		Gray fine s present very str gloves, mm of wet)	and with o t as dark l rong odor, PID bag NAPL on	occasional grav prown within poi hydrocarbon si copper color, sh surface copper	el, NAPL re space, taining on nake test 1 color (dense,		102	Blebs semi-circular, brown
		-										-				HS HS		
		20 —																
OEROLINA	Note:	Plea	ise	see f	igure	A-1 for	explanat	ion	of syr	nbols	6							
												Loa	of Bo	ring GEI	-13			
Uate:5/14/1	6			-			. I.	J.	/			Project:		Puget	Sound Ene	ergy N	orth	Lake Union
Seame	G	EOENGINEERS										Project L Project N	Location	n: Gas W 1: 0186-8	orks Park, 846-01	Seatt	ie, V	Vashington Figure A-29 Sheet 1 of 2

Figure A-29 Sheet 1 of 2

$\square$			FIEI	LD D	DATA							
Elevation (feet)	Cepth (feet)	Interval	Blows/foot	<b>Collected Sample</b>	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
_~\$^ -	20 — -	6	D					SP	Gray fine to medium sand with trace silt and occasional gravel, less NAPL saturation (dense, wet) NAPL observed	HS 90% HS SS		Rainbow
-	-			Ì	GEI-13 (23.5-24.5)			SM	NAPL observed NAPL observed Grav silty fine to medium sand with gravel (very	HS SS HS SS	480	
_%	25 —		5		GEI-13 (25-25.5)			SW	- dense, wet) -	SS		

Note: Please see Figure A-1 for explanation of symbols

#### Log of Boring GEI-13 (continued)

![](_page_440_Picture_4.jpeg)

Project: Project Location: Project Number:

Puget Sound Energy North Lake Union ion: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-29 Sheet 2 of 2

![](_page_441_Figure_0.jpeg)

![](_page_442_Figure_0.jpeg)

Project Number:

0186-846-01

Figure A-30 Sheet 2 of 2

Drille	ed 4	<u>Star</u> /2/20	<u>t</u> )13	<u>Er</u> 4/2/	<u>nd</u> /2013	Total Depth	(ft)	1	5	Logged By ARJ Checked By ZAS	Driller Boart Longyear			Drilling Method	Direct Push	
Surfa Vertio	ice Ele cal Dat	vatio um	on (ft)		USA	26.17 CE (Loci	(s)		H	Hammer Data		Drillir Equi	ng oment		Geoprobe 662	20 DT
Easti North	ng (X) hing (Y	)		th nost	127 23	70797.85 9445.61	5	2 fe	S E	System Datum NAD83 V	VA State Plane North	<u>Grou</u> Date	ndwate Measur	ed	Depth to <u>Water (ft)</u>	Elevation (ft)
	5. Tiai	nu-uu	ug wi	in posi					et bys.	1						
Elevation (feet)	Depth (feet)	Interval	Recovered (in)	Blows/foot	Collected Sample	ATA Sample Name Testing	Water Level	Graphic Log	Group Classification	MA DES(	TERIAL CRIPTION	Sheen	Headspace Vanor (nom)	X	REMARI	KS
ERS8. GDT/GEI8_ENVIRONMENTAL_STANDARD	0- 5-		24 24 30			GEI-15 (0-2) GEI-15 (6.5-7) GEI-15 (12.5-13.5)				Brown to black silty fi trace organics (r asphaltic grains ( Coarse sand with gra yellow agglomera fused; and black finely vesicular, n Brown, tan, yellow, b with coarse sand brown, tan, yellow, b smaller pieces of Black coarse sand w Black coarse sand w Black coarse sand w Gravel with sand Gray medium to coar	ine sand with gravel and jots and rootlets), trace loose, moist) haltic grains (hardened tar?) avel; black, tan, brown, te, low density, vesicular, agglomerate, low density, netallic luster lack fine to coarse gravel , gravel is agglomerate, v fused vesicular, low luster; and black, low , metallic luster, sand is above ith gravel dium to coarse sand with an yellow agglomerate y, vesicular, and black density, vesicular, metallic halter particles of above. 	- NS - NS - NS - NS - NS - SS 109 - NS - NS - NS - NS - NS - NS - NS	< <1	Grou	undwater encounte	red at 4.5 feet aks
	15 -	-			Ţ	GEI-15 (14-14.5) + DUP			SM	<ul> <li>(dense, wet)</li> <li>Gray silty fine to meen dense, wet)</li> </ul>	lium sand with gravel (very		<1			
C.USERSITNASHIDESKTOP016884601.GPJ DBTemplate/LibTemplate.	15       Image: Comparison of symbols         16       Image: Comparison of symbols															
V13 Path:C										Log of Bo	ring GEI-15					
eattle: Date:5/14	Ge	0	En	NG	IN	EER	S	0	1	Project: Project Location	Puget Sound Ene Gas Works Park,	ergy I Sea	North ttle, V	Lake l Nashin	Jnion gton F	igure A-31

Project Number:

0186-846-01

Figure A-31 Sheet 1 of 1

Drille	ed 4/*	<u>Start</u> 17/20	13	<u>En</u> 4/17/	<u>d</u> 2013	Total Depth	(ft)	2	25		Logged By PDR Checked By ZAS Driller Boart Longyear				Drilling Method Sonic (continuous core)
Surfa Vertio	ace Elev cal Datu	atior/	n (ft)	l	3 JSAC	3.98 E (Lock	(s)		ł	Ha Da	nmer a	Di	rilling quipn	nent	Rubber Track-Mounted Spider 3 Sonic Drill Rig
Easti North Note	ng (X) hing (Y) es: San	npling	g met	hod: 5	1270 239 by 3½	0731.54 138.15 " ID split	spc	on w	ith lexa	Sy Da	tem um NAD83 WA State Plane North ore sleeves.	<u>G</u> 	round ate Me	dwater easured	Depth to <u>d Water (ft)</u> <u>Elevation (ft)</u>
$\geq$							-								
Elevation (feet)	⊃ Depth (feet) I	Interval	Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Water Level	Graphic Log	Group Classification	CIASSIIICAUUI	MATERIAL DESCRIPTION		Sheen	Headspace Vapor (ppm)	REMARKS
- - -	-	-									Lithology not logged; see GEI-3	-			
- - -	5		60								Test sample 5 to 10 feet with 100% recovery				
											<ul> <li>15 inch recovery on 1st attempt, try 2nd to observe recovery, very poor recovery of mostly water and NAPL</li> <li>Black colored water with strong hydrocarbon odor (will re-drill for this sample in PT-01B)</li> </ul>	-	HS	<1	
	15 — - -										-	_			
	20 – 20 –	ase	see F	igure	A-1 for	explanat	tion	of sy	mbols		-				
											Log of Boring PT-01				
	Ge	ol	EN	IG	NE	ER	S	0	J		Project: Puget Sound En Project Location: Gas Works Park Project Number: 0186-846-01	erg , Se	y No eatt	orth Ie, W	Lake Union /ashington Sheet 1 of 2

$\square$		FIEL	D D	DATA							
Elevation (feet)	Interval Recovered (in)	Blows/foot	<b>Collected Sample</b>	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Sheen	Headspace Vapor (ppm)	REMARKS
- · ·	-			P1-01 (20-21.1A); PT-01 (21.1-22B); PT-01 (22-25D)				Water and sediment in sampler (approximately 2 inches water in top of sampler), strong hydrocarbon odor	-		

Note: Please see Figure A-1 for explanation of symbols

### Log of Boring PT-01 (continued)

![](_page_445_Picture_4.jpeg)

Project: Project Location: Project Number:

Puget Sound Energy North Lake Union on: Gas Works Park, Seattle, Washington er: 0186-846-01

Figure A-32 Sheet 2 of 2

	Drilled	<u>5</u> 4/17	<u>tart</u> 7/2013	<u>Er</u> 4/17	<u>nd</u> 7/2013	Total Depth	(ft)	1	6	Li Cł	ogged By PDR necked By ZAS	Driller Boart Longyear				Drilling Method Sonic (cor	ntinuous core)
S V	urface ertica	e Eleva I Datur	ation (ft)	)	USA	33.97 CE (Locł	(S)			Hamm Data	her		Drill Equ	ling lipm	ent	Rubber Track-Mo Sonic D	ounted Spider 3 rill Rig
E	asting orthin	g (X) a (Y)			127	70731.21				Syster Datun	m n NAD83 W	A State Plane North	Gro	und	water	Depth to	
N	lotes:	Sam	oling me	ethod: {	5' by 3	1/2" ID split	spo	on w	ith lexa	an core	e sleeves.		_ <u>Date</u>	<u>e Me</u>	asure	<u>d Water (ft)</u>	<u>Elevation (ft)</u>
ř				FIEL	D D	ATA											
	eet)		(in)		umple	me	_	g	5	Ę	MQ.	τεριδι					
	ation (†	h (feet)	/al wered	s/foot	cted Sa	<u>ole Nai</u> ng	er Leve	hic Lo	p sificatio	אוורמות	DESC	RIPTION		_	space (ppm)	REMA	ARKS
ī	Eleva	<ul> <li>Dept</li> </ul>	Inter Reco	Blow	Colle	<u>Sam</u> Testi	Wate	Grap	Grou				Choo	allee	Head		
		Ū									Lithology not logged;	see GEI-3					
		_								-			-				
-		_								-			-				
-		_								-			-				
<u>_%</u>	2	-								-			-				
-		5 —								_			_				
_		_								_							
L		_															
-		_								-							
_^`	ò	-								-			1				
-		10 —								-			-				
-		_	30			PT-01B (11-13.24)				-			-				
-		_				(				-			_				
-		_								_	No liquid on top of sar recovery from 11 t	npler, 30 inches good o 13.5 feet					
2	Ņ	_															
-		15 —								_							
		T															
2																	
5																	
5																	
	Not	e: Plea	ise see	Figure	A-1 fc	or explanat	tion	of sy	mbols								
$\tilde{\mathbf{G}}$											Log of Bori	ng PT-01B					
			_	13		6.1	J.	/			Project:	Puget Sound Ene	ergy	Nc	orth	Lake Union	
	G	E	E	NG	IN	EER	S		1		Project Location	: Gas Works Park,	Sea	attl	e, V	/ashington	Figure A-33
											-roject number:	0100-040-01					Sheet 1 of 1

Seattle

![](_page_447_Figure_0.jpeg)

ſ		FIELD DATA													
:	Elevation (reet)	Interval	Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group Classification	MATE DESCF	ERIAL	Sheen	Headspace Vapor (ppm)	REM/	ARKS
-	20	-								– Black, strong odor (GP), – NAPL in shoe coatin heavy sheen, some v	- staining, observed g particles of gravel, - water on top of sample	HS			
EKS/INAOHUEONI OF MICO	Note: F	Pleas	e see l	-igure :	A-1 fo	r explana	tion	of syr	nbols						
- Lamo										a of Borina PT.	02 (continued)				
Seattle: Date:5/14/13	G	0	E	IG	IN	EER	S	0	7	Project: Project Location:	Puget Sound Energ Gas Works Park, S	gy N Seatt	orth Ie, V	Lake Union /ashington	Figure A-34

StartEndTotal30Drilled4/18/20134/18/2013Depth (ft)								Logged By PDR Checked By ZAS Driller Boart Longyear							Drilling Method Sonic (continuous core)						
Sur Ver	Jurface Elevation (ft) 27.24 Ha /ertical Datum USACE (Locks) Da							Ha Da	Immer Ita					Drillin Equip	g ment	Rubber Track-Mounted Spider 3 Sonic Drill Rig					
Eas	Easting (X) 1269745.13 Sy Northing (Y) 238975.54 Dr							/stem					Grour	ndwater	[	Depth to					
Notes: Sampling method: 5' by 31/2" ID split spoon with lexan c										ith le>	xan o	pore sleeves.				Date N	leasured	<u>1 \</u>	<u>Vater (ft)</u>	<u>Elevation (ft)</u>	
FIELD DATA																					
Elevation (feet)		o Depth (feet) I	Interval	Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Water Level	Graphic Log	Group	Classification	lithelese	MATERIAL DESCRIPTION				Sheen	Headspace Vapor (ppm)		REMAI	RKS
4SiTNASHDESKTOP01888401.GPJ DBTemplate/LibTemplate/GEOENGINEERS8 GDT/GEI8_ENVIRONMENTAL_STANDARD ・	Note	0       PT-03 (8-10); PT-03 (10-13B)         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0         10       0								mbols		Lithology Lithol	not logged; ated gravel, high sheen le, all soil, h	strong , no flu	g naphthalen uid observed staining on tu	e-like on ube			Ground	100% rec	overy ntered at 9.5 feet
Path:C:US														rin	a DT_0?	2					
te:5/14/131												Project:		<u>, , , , , , , , , , , , , , , , , , , </u>	Puget So	ound Ene	ergy N	lorth	Lake Ur	nion	
									1		Project Location:Gas Works Park, Seattle, WashingtonFigure A-35Project Number:0186-846-01Sheet 1 of 2										

![](_page_450_Figure_0.jpeg)

Note: Please see Figure A-1 for explanation of symbols

#### Log of Boring PT-03 (continued)

![](_page_450_Picture_4.jpeg)

Project:FProject Location:CProject Number:C

Puget Sound Energy North Lake Union n: Gas Works Park, Seattle, Washington r: 0186-846-01

Figure A-35 Sheet 2 of 2

# ATTACHMENT 2A-4 SI Soil Boring Core Field Photos

![](_page_452_Picture_0.jpeg)

GEI-1 0 to 5 feet, 34.5 to 42 inches

![](_page_452_Picture_2.jpeg)

GEI-1 0 to 5 feet, 42 to 49 inches

Gas Works Park Site Seattle, Washington

![](_page_452_Picture_6.jpeg)

![](_page_453_Picture_0.jpeg)

GEI-1 0 to 5 feet, 48 to 55 inches

![](_page_453_Picture_2.jpeg)

GEI-1 5 to 10 feet, 24 to 32 inches

Gas Works Park Site Seattle, Washington

![](_page_453_Picture_6.jpeg)

![](_page_454_Picture_0.jpeg)

GEI-1 5 to 10 feet, 43 to 50.5 inches

SI Soil Boring Core Field Photographs GEI-1

13

16:09

Gas Works Park Site Seattle, Washington

GEOENGINEERS

![](_page_454_Picture_3.jpeg)

0186-846-01 Date Exported: 01/18/19

![](_page_455_Picture_0.jpeg)

GEI-1 15 to 20 feet, inches N/A

![](_page_455_Picture_2.jpeg)

GEI-1 15 to 20 feet, inches N/A

Gas Works Park Site Seattle, Washington

![](_page_455_Picture_6.jpeg)

![](_page_456_Picture_0.jpeg)

GEI-1 15 to 20 feet, 33.5 to 42.5 inches

![](_page_456_Picture_2.jpeg)

GEI-1 15 to 20 feet, 43.5 to 52 inches

Gas Works Park Site Seattle, Washington

![](_page_456_Picture_6.jpeg)

![](_page_457_Picture_0.jpeg)

GEI-1 15 to 20 feet, 32.5 to 42 inches

![](_page_457_Picture_2.jpeg)

GEI-1 15 to 20 feet, inches N/A

Gas Works Park Site Seattle, Washington

![](_page_457_Picture_6.jpeg)

![](_page_458_Picture_0.jpeg)

GEI-1 20 to 25 feet, 29 to 36 inches

![](_page_458_Picture_2.jpeg)

GEI-1 20 to 25 feet, 45.5 to 52 inches

Gas Works Park Site Seattle, Washington

![](_page_458_Picture_6.jpeg)

![](_page_459_Picture_0.jpeg)

GEI-1 25 to 27 feet, 39.5 to 45.6 inches

SI Soil Boring Core Field Photographs GEI-1

Gas Works Park Site Seattle, Washington

![](_page_459_Picture_4.jpeg)

Appendix 2A-4

![](_page_460_Picture_0.jpeg)

GEI-2 0 to 5 feet, 28 to 37 inches

![](_page_460_Picture_2.jpeg)

GEI-2 0 to 5 feet, 36 to 47 inches

SI Soil Boring Core Field Photographs GEI-2

Gas Works Park Site Seattle, Washington

![](_page_460_Picture_6.jpeg)

![](_page_461_Picture_0.jpeg)

GEI-2 0 to 5 feet, 45.5 to 54.5 inches

![](_page_461_Picture_2.jpeg)

GEI-2 5 to 10 feet, 17 to 24.5 inches

SI Soil Boring Core Field Photographs GEI-2

Gas Works Park Site Seattle, Washington

![](_page_461_Picture_6.jpeg)

![](_page_462_Picture_0.jpeg)

GEI-2 5 to 10 feet, 26 to 32 inches

![](_page_462_Picture_2.jpeg)

GEI-2 5 to 10 feet, 38 to 44.5 inches

Gas Works Park Site Seattle, Washington

![](_page_462_Picture_6.jpeg)

![](_page_463_Picture_0.jpeg)

GEI-2 5 to 10 feet, 48 to 54.5 inches

![](_page_463_Picture_2.jpeg)

GEI-2 10 to 15 feet, 8 to 14.5 inches

![](_page_463_Picture_4.jpeg)

Gas Works Park Site Seattle, Washington

![](_page_463_Picture_6.jpeg)

![](_page_464_Picture_0.jpeg)

GEI-2 10 to 15 feet, 21 to 29 inches

![](_page_464_Picture_2.jpeg)

GEI-2 10 to 15 feet, 23 to 35 inches

Gas Works Park Site Seattle, Washington

![](_page_464_Picture_6.jpeg)

![](_page_465_Picture_0.jpeg)

GEI-2 10 to 15 feet, 31 to 40.5 inches

![](_page_465_Picture_2.jpeg)

GEI-2 10 to 15 feet, 44 to 55 inches

Gas Works Park Site Seattle, Washington

![](_page_465_Picture_6.jpeg)

![](_page_466_Picture_0.jpeg)

GEI-2 15 to 20 feet, 18 to 28 inches

![](_page_466_Picture_2.jpeg)

GEI-2 15 to 20 feet, 24 to 33 inches

![](_page_466_Picture_4.jpeg)

Gas Works Park Site Seattle, Washington

![](_page_466_Picture_6.jpeg)

![](_page_467_Picture_0.jpeg)

GEI-2 15 to 20 feet, 30 to 39 inches

![](_page_467_Picture_2.jpeg)

GEI-2 15 to 20 feet, 34.5 to 43.5 inches

SI Soil Boring Core Field Photographs GEI-2

Gas Works Park Site Seattle, Washington

![](_page_467_Picture_6.jpeg)


GEI-3 0 to 5 feet, inches N/A



GEI-3 0 to 5 feet, inches N/A

SI Soil Boring Core Field Photographs GEI-3

Gas Works Park Site Seattle, Washington





GEI-3 0 to 5 feet, inches N/A



GEI-3 0 to 5 feet, inches N/A



Gas Works Park Site Seattle, Washington





GEI-3 0 to 5 feet, inches N/A



GEI-3 0 to 5 feet, inches N/A

SI Soil Boring Core Field Photographs GEI-3

Gas Works Park Site Seattle, Washington





GEI-3 5 to 10 feet, inches  $\ensuremath{\mathsf{N/A}}$ 



GEI-3 5 to 10 feet, inches N/A

SI Soil Boring Core Field Photographs GEI-3

Gas Works Park Site Seattle, Washington





GEI-3 5 to 10 feet, inches  $\ensuremath{\mathsf{N/A}}$ 



GEI-3 5 to 10 feet, inches N/A

SI Soil Boring Core Field Photographs GEI-3

Gas Works Park Site Seattle, Washington





GEI-3 5 to 10 feet, inches N/A



GEI-3 5 to 10 feet, inches N/A

SI Soil Boring Core Field Photographs GEI-3

Gas Works Park Site Seattle, Washington





GEI-3 10 to 15 feet, inches N/A



GEI-3 10 to 15 feet, inches N/A

SI Soil Boring Core Field Photographs GEI-3

Gas Works Park Site Seattle, Washington

