GEOTECHNICAL ENGINEERING REPORT AND TEMPORARY SHORING DESIGN Stillwater Holdings Chevron UST and Soil Removal Interim Action 7 East Rose Street Walla Walla, Washington

Prepared for: Stillwater Holdings, LLC

Project No. AS230442A • February 22, 2024 FINAL





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Executive Summary

Aspect Consulting (Aspect) completed a geotechnical engineering study and temporary shoring design for the Stillwater Holdings Chevron UST and Soil Removal Interim Action (Project) at 7 East Rose Street in Walla Walla, Washington (Site; Figure 1). The Project consists of the removal of three underground storage tanks (USTs) and localized contaminated soil around the tanks. Our services consisted of reviewing existing subsurface exploration data at the Site, completing new subsurface explorations, completing engineering analyses to design temporary shoring, and preparing this report that documents subsurface conditions, the basis of design for the temporary shoring, and recommendations for construction. Our pertinent conclusions and recommendations for the Project are summarized below.

- The Site is underlain by a variable thickness of fill followed by alluvium. The alluvium generally consists of medium dense to dense gravel with silt interbeds and extends to the maximum depth explored (approximately 26.5 feet below the ground surface). Nearby well logs indicate the gravel alluvium extends to depths of at least several hundred feet below the Site area.
- Static groundwater levels measured in the monitoring wells at the Site range between elevation (El) 939 and El 944. The excavation is planned to extend to El 943, and therefore groundwater is expected to be near the base of the excavation. If groundwater is encountered, we anticipate the rate of groundwater flow into the excavation will be up to 10 gallons per minute and can be controlled using a system of sumps and pumps within the excavation. Groundwater will be encountered during shaft excavation for the temporary shoring soldier piles.
- Temporary shoring will be necessary to support the excavation. Aspect has completed design of the temporary shoring system, which consists of cantilever drilled soldier piles with timber lagging. The north shoring wall is designed for additional lateral earth pressure from the footings of the adjacent building and to limit deflections to 0.5 inch or less at the elevation of the adjacent footings. The east, west, and south shoring walls are designed for additional lateral earth pressure from construction equipment (tracked excavator) operating behind the walls and to limit deflections to 1 inch or less.

This Executive Summary should only be used in the context of the whole report.

1 Introduction

Aspect Consulting (Aspect) completed a geotechnical engineering study and temporary shoring design for the Stillwater Holdings Chevron UST and Soil Removal Interim Action at 7 East Rose Stret in Walla Walla, Washington. This report presents our geotechnical engineering conclusions, recommendations, and the basis of temporary shoring design for the Project.

1.1 Project Description

The Project consists of the removal of three steel-reinforced fiberglass underground storage tanks (USTs) and localized contaminated soil around the tanks. Each storage tank is approximately 27 to 29 feet in length and 5 to 7 feet in width. An approximately 12-foot-deep excavation extending to elevation (El) 943¹ will be completed to facilitate UST and soil removal. Once excavation is complete and the USTs are removed, the excavation will be backfilled to existing grade.

¹ Elevations in feet and reference the North American Vertical Datum of 1988 (NAVD88).

2 Site Conditions

This section includes a description of the Site's surface conditions and soil stratigraphy based on the results of our subsurface explorations and review of explorations by others.

2.1 Surface Conditions

The Site consists of a rectangular parcel covering approximately 0.233 acres in Walla Walla, Washington. Its current use is a gasoline service station; a convenience store/mini mart is present in northern portion of the Site, and two canopies covering fuel pumps are present in the northwest and southern portions of the Site. The surface surrounding these features is relatively level and covered with asphalt.

The Site is bordered by a two-story office building to the north (106 North 2nd Avenue), a parking lot and one-story building (21 East Rose Street) to the east, East Rose Street right-of-way (ROW) to the south, and North 2nd Avenue ROW to the west.

2.2 Subsurface Conditions

Our characterization of subsurface conditions at the Site is based on our review of geologic maps, our experience in the Site area, our review of logs of subsurface explorations completed at the Site by Aspect and others.

2.2.1 Geology

Geologic maps indicate the Site is underlain by quaternary alluvium (Derkey et al., 2006; DNR, 2024). The quaternary alluvium deposits consist of discontinuous, unconsolidated deposits of clay, silt, fine sand, and gravel typically found in and adjacent to stream channels and on the floodplain adjacent to streams on the valley floor. The deposits are primarily reworked, locally derived loess and flood deposits.

2.2.2 Subsurface Explorations by Others

We reviewed logs of subsurface explorations completed at the Site and vicinity by others. These include five geotechnical borings (B-1 through B-5) and six monitoring wells (MW-1 through MW-6) completed by GeoEngineers. The approximate locations of these explorations are shown on Figure 2 and the exploration logs are provided in Appendix A.

Additionally, nearby well logs available through the Washington State Well Report Reviewer indicate the alluvium extends to a depth of several hundred feet below the ground surface and is underlain by basalt bedrock (Ecology, 2024).

2.2.3 Subsurface Explorations by Aspect

Aspect completed the following subsurface explorations at the Site:

• Seven monitoring wells, designated AMW-01 through AMW-04 and MW-7 through MW-9, between October 18 and 20, 2023.

• Eight test pits, designated ATP-01 through ATP-08, advanced to depths between 4 and 10.5 feet below ground surface (bgs) on January 9 and 10, 2024.

The locations of the Aspect explorations are also shown on Figure 2. Aspect's exploration logs are provided in Appendix B.

2.2.4 Stratigraphy

Based on our explorations and review of the logs of the explorations by others, we identified two soil units at the Site: fill and alluvium. Descriptions of each of these units, as observed in our explorations and described on the logs of the explorations by others, are presented below. For additional details regarding the composition and distribution of these units, please refer to the exploration logs provided in Appendices A and B.

2.2.4.1 Fill

Fill is present directly beneath the asphalt and typically consists of soft to medium stiff, slightly moist to moist, low plasticity silt with varying amounts of sand and gravel (ML); loose to medium dense, slightly moist, gravel (GP-GM); and loose to medium dense, moist, sand with varying amounts of gravel and cobbles (SM). The thickness of the fill ranges between 3.5 and 8 feet bgs. In some locations the fill is pea gravel, such as around utilities and buried structures.

2.2.4.2 Alluvium

Below the fill, alluvium is present and extends to the maximum depth explored (approximately 26.5 feet bgs). The alluvium typically consists of medium dense to dense, moist to wet, gravel with varying amounts of sand and silt (GP-GM, GM); and medium stiff to hard, wet, low plasticity silt with varying amounts of sand and gravel (ML). While not shown on the final boring logs, we reviewed GeoEngineers' draft boring logs, which contain Standard Penetration Test (SPT) blow counts. The blow counts in the alluvium range between 28 and greater than 100 blows per foot (bpf) for the gravel (most are greater than 50 bpf) and 12 and 51 bpf for the silt. While the boring logs describe the gravel alluvium as dense to very dense, we interpret this unit as typically medium dense to dense and assume the blow counts likely overstated to some degree due to the presence of large gravel, cobbles, and potentially boulders.

2.2.5 Groundwater

Static groundwater levels measured in Aspect's monitoring wells between October 2023 and January 2024 range between approximately El 944 and 936. The static groundwater levels measured in the wells that are closest to the planned excavation range between El 944 and 941.

Groundwater levels at the Site will fluctuate seasonally with changes in precipitation.

2.2.5.1 Slug Testing

We estimated hydraulic conductivity of the soil by performing slug tests at monitoring wells AMW-1, AMW-2, and AMW-4. These estimates were used to inform our analysis of the rate of groundwater flow into the excavation (if groundwater is encountered).

Slug tests involve rapidly changing the water level within a well and then measuring the rate of return to the static water level. The rate of water level recovery is used to calculate the hydraulic conductivity of the water-bearing zone in the vicinity of the well screen using standardized analytical procedures. The slug test results represent a bulk hydraulic conductivity of the soil below groundwater within the screen interval of the wells.

A slug rod (a solid cylinder of known volume) was used to perform the slug tests in each well. During the falling head test, the slug rod was rapidly submerged in the water, causing the water level to rise rapidly before falling back to the static water level over time. Upon completion of the falling head test, a rising head test was performed by rapidly removing the slug rod from the water, causing the water level to rapidly fall before rising back to the static water level over time. In wells where groundwater levels intersected the screen interval or filter pack, only the rising head tests were analyzed.

The water levels in the wells during testing were measured using a vented pressure transducer (certified for 10 meters of submergence) and collected electronically on a data logger set to a nearly continuous time interval (1 second or less). Manual water level measurements were collected using an electronic measuring tape.

From the slug test data, we calculated saturated bulk hydraulic conductivities ranging between 0.7 and 1.4 feet per day (ft/day). The slug test results are included in Appendix C.

3 Temporary Shoring Design

The Project excavation is planned to extend to a depth of 12 feet bgs. Due to the proximity of the USTs to the building footings (between about 2 and 3 feet), an unsupported temporary cut on the north side of the excavation would need to be near-vertical to reach the planned bottom of the excavation. Considering the soil conditions (fill and alluvium, which are prone to caving) through which the excavation will be made, this is not considered feasible and poses high risk for loss of soil/bearing support below the footings and adverse building movement. On the south, east, and west sides of the excavation, the adjacent property lines and fuel pumps also limit the space available for sloped excavations.

Considering these factors, the excavation should be supported using an engineered temporary shoring system. Based on the soil conditions and the planned excavation depth, we consider cantilever soldier piles with timber lagging to be feasible. Soldier piles consist of steel beams (W or HP sections) that are either driven into the ground or placed into concrete-filled drilled shafts. For this Site, the soldier piles will need to be placed into drilled holes. The soldier piles are typically installed at a horizontal spacing of about 6 to 8 feet around the perimeter of the excavation and extend below the base of the excavation. As the excavation is advanced, timber lagging is installed spanning horizontally between soldier piles to form a continuous shoring wall.

3.1 Soldier Pile Design

3.1.1 Assumptions and Recommendations

The sections below describe Aspect's assumptions and recommendations for lateral earth pressures and allowable deflections for the design of the cantilever soldier pile temporary shoring system.

3.1.1.1 Lateral Earth Pressures

The soldier piles are designed using the earth pressures presented on Figure 3. Our assumptions and recommendations related to lateral earth pressures include:

- Level ground conditions exist behind the walls and the walls are free draining through gaps in the timber lagging (buildup of unbalanced hydrostatic pressures behind the walls does not occur).
- The active earth pressure acts over the pile center-to-center spacing above the base of the excavation.
- The allowable passive earth pressure is applied over three shaft diameters (3B) or the pile center-to-center spacing, whichever is less. The allowable passive earth pressure includes a factor of safety of 1.5.
- The active and passive earth pressures below the base of the excavation are appropriate for saturated/submerged soil.

- Seismic lateral earth pressures are excluded because the shoring is assumed to be temporary.
- Additional lateral earth pressure from the footing surcharge of the adjacent building is applied to the north shoring wall. To estimate the surcharge lateral earth pressure on the north shoring wall, we utilized limit equilibrium methods. Based on the foundation plans for the building, the footings below the north wall consist of column footings with interconnected strip footings. The footings are designed for an allowable bearing pressure of 1,500 pounds per square foot (psf) and are embedded 2 to 3 feet below finished grade. The footing that will impose the largest lateral earth pressure on the shoring wall is a 4.5 by 4.5 (length by width, in feet) column footing. The edge of this footing protrudes approximately 2 feet from the wall of the building and is approximately 2.5 feet away from the north shoring wall. Our recommended surcharge lateral earth pressures for the entire north shoring wall are based on this worst-case scenario.
 - The surcharge lateral earth pressure is applied uniformly over the height of the wall located below a 1H:1V (horizontal:vertical) line projected outward and downward from the outside edge of the adjacent building footing.
- An additional lateral earth pressure from construction equipment surcharge (mid-sized tracked excavator) is applied to the east, west, and south shoring walls. We estimate a surcharge lateral earth pressure of 125 psf for a mid-sized excavator (160 size) that is distributed uniformly over the full height of the wall. If the contractor proposes to use heavier equipment or to stockpile soil behind the shoring walls, Aspect should be notified to evaluate the adequacy of the shoring system for the proposed loading.

3.1.1.2 Allowable Deflections

The north shoring wall is designed to limit lateral deflections to less than about 0.5 inches at the footing elevation of the adjacent building to protect the building from potentially damaging ground movements. The east, west, and south shoring walls are designed to limit lateral deflections to less than 1 inch in accordance with industry standard practice where structures and utilities sensitive to movement are not present adjacent to the shoring walls.

3.1.2 Results

Based on the planned excavation geometry and using the lateral earth pressures shown on Figure 3, we evaluated a combination of soldier pile spacing and drilled shaft diameters to determine pile shape and pile embedment requirements using the Shoring Suite computer software program (CivilTech, 2020). Table 1 below summarizes the selected pile shapes, shaft diameters, and pile lengths based on our analyses. The Shoring Suite outputs are provided in Appendix D.

Shoring Wall	Minimum Beam Size	Center-to-Center Spacing (feet-inches)	Concreted Shaft Diameter (inches)	Pile Embedment (feet)	Total Pile Length (feet)
North	W18X130	5'-3.5"	30	22.5	34.5
East	W16X89	6'-3"	30	19.5	31.5
West	W16X89	6'-3"	30	19.5	31.5
South	W16X89	6'-4"	30	19.5	31.5

Table 1. Selected Soldier Pile Properties

3.1.2.1 Timber Lagging Design

Based on the lateral earth pressures and guidance presented in the Federal Highway Administration (FHWA) Geotechnical Engineering Circular No. 4, Table 12— *Recommended Thickness of Temporary Timber Lagging* (FHWA, 1999), 4-inch-thick (nominal) Hem-Fir No. 2 timber lagging will be adequate.

4 Construction Considerations and Recommendations

The following sections present our construction recommendations for the Project.

4.1 Temporary Shoring Construction

4.1.1 Soldier Pile Walls

We provide the following considerations recommendations for construction of the soldier pile walls:

- Due to the proximity of the USTs to the building, the shafts for the north wall soldier piles will be excavated through the USTs, as indicated on the Project plans. Therefore, the contractor should be prepared to encounter the USTs during shaft excavation for the north wall soldier piles. We understand the USTs are steel-reinforced fiberglass.
- Shaft excavation will occur in soil that is primarily gravel, cobbles, and potentially boulders above and below groundwater. Accordingly, we anticipate the need for temporary casing or drilling mud/slurry to prevent caving of the shafts and bottom heave during excavation and to maintain an open hole to allow for steel and concrete placement.
- The bottom of the shafts should be relatively undisturbed and clear of loose/slough soils and debris prior to placing the beams and filling the shafts with concrete.
- If standing water or drilling mud/slurry is present in the shaft at the time of concrete placement, the concrete should be placed with a tremie pipe to displace the water or drilling mud/slurry.
- Due to the relatively close spacing of the soldier piles, sequential shafts should not be excavated on the same working day, and the concrete in a shaft should be allowed to cure at least 12 hours before an adjacent shaft is excavated.
- Excavation for the installation of lagging should be accomplished in 4-foot (maximum) vertical lifts. When the first lift of lagging is complete, the contractor can continue with the excavation in 4-foot lifts until all required lagging has been installed. If caving soils are encountered during excavation, the contractor should be prepared to excavate and install the lagging in shorter lifts. All lagging excavations should be supported by lagging the same working day.
- Any voids that form behind the wall due to caving soils during excavation for lagging should be backfilled with controlled density fill (CDF). Voids should be backfilled the same working day.

4.1.2 Shoring and Adjacent Building Monitoring

The temporary shoring walls and the building should be monitored during construction to verify the shoring is performing as intended by the design and to provide early detection and tracking of deflections before they exceed threshold amounts. Similarly, the adjacent building should be monitored to verify that no significant or adverse movement occurs. Recommended monitoring measures are presented below.

4.1.2.1 Photographic Survey

A pre- and post-construction photographic survey should be completed to document construction conditions at the Site and surrounding areas before the start of and immediately at the end of construction. The photographic surveys should consist of video or photographic documentation of the adjacent streets, buildings, and other improvements, with special attention to cracks and other signs of distress that exist before the start of construction.

4.1.2.2 Optical Survey

An optical survey of the north shoring wall and the adjacent building should be completed during construction. The optical survey should include horizontal and vertical measurements accurate to at least 0.01 feet.

Optical survey points should be located on the top of every other soldier pile on the north shoring wall and on the exterior wall of the adjacent building. A baseline reading of the optical survey points should be completed prior to excavation.

If cumulative horizontal movements exceed 0.25 inches at monitoring points, construction activities should be temporarily stopped to determine the cause of the movement and undertake remedial action(s) as necessary to limit total shoring or building wall movement to 0.5 inches.

The optical survey program should be completed twice a week during excavation and until movements have stabilized. If movements have stabilized by the start of excavation backfill, optical survey of the monitoring points shall be completed at least once a week during backfilling until backfill of the excavation is complete.

4.1.2.3 Crack Monitoring

Prior to construction, the walls and footings (if exposed) of the adjacent building should be inspected for cracks. If cracks are observed, crack gauges should be installed on the cracks and readings taken at least once a week during excavation and backfill.

4.2 Earthwork

4.2.1 General

We expect that earthwork activities can be accomplished with standard construction equipment suited to working in very dense granular soil, such as track hoes equipped with toothed buckets. The contractor should be prepared to encounter and deal with rubble and debris in the fill, and oversized particles, such as boulders in native soil, during excavation.

4.2.2 Temporary Excavation Slopes

In addition to temporary shoring, temporary excavation slopes could be necessary elsewhere during construction. Temporary excavation and slopes should not exceed the limits specified in the local, state, and federal regulations. The stability of temporary excavations and slopes shall be the responsibility of the contractor. For planning purposes, both fill and alluvium typically classify as Type C soil in accordance with the Washington Administrative Code (WAC) 296-155 Part N (WAC, 2016). Temporary excavation slopes in Type C soils are anticipated to stand as steep as 1.5H:1V. The presence of seepage may require that temporary excavation slopes be flattened to remain stable.

We also recommend the following for temporary excavations and slopes:

- Surface water should be diverted away from slopes and excavations.
- Slopes should be protected using plastic sheet, flash coating, or tarps to control erosion and maintain stability, as necessary.
- The duration that excavations or slopes are open should be minimized.
- Traffic, equipment, and material stockpiles should not be allowed near the top of excavations or slopes.
- The conditions of the excavations and slopes should be periodically observed by a competent person who is a representative of the contractor to evaluate safety and stability.

4.2.3 Excavation Backfill

Once the bottom of excavation is reached and tank removal and remedial excavation objectives are met, the excavation will be backfilled up to approximately existing grade and capped with a layer of crushed surfacing to establish a surface until new tanks are installed and the site is repaved at a later date by others. Our recommendations for backfill of the excavation are as follows:

- The excavated materials are not suitable for reuse as backfill and should be exported from the Site.
- Backfill for the excavation should consist of pea gravel meeting the requirements set in the Washington State Department of Transportation's (WSDOT) *Standard Specifications for Road, Bridge and Municipal Construction* (Standard Specifications) 9-03.5 (WSDOT, 2024). We understand pea gravel is desired so that it can be reused as tank backfill when new tanks are installed at a later date.
- The crushed surfacing should consist of at least 4 inches of imported crushed rock or gravel meeting the requirements for Crushed Surfacing Top Course (CTSC) per WSDOT Standard Specification 9-03.9(3). The crushed surfacing should be considered temporary and may require maintenance by the Owner depending on desired serviceability/drivability. A single layer of geotextile meeting the requirements for Separation in Table 3 of WSDOT Standard

Specification 9-33.2(1) should be placed between the crushed surfacing and the pea gravel.

- Backfill should only be placed on a relatively firm and unyielding subgrade.
- The pea gravel should be placed in approximately 2-foot-thick lifts that are tamped in-place using an excavator bucket or similar methods. The CSTC material should be compacted to a relatively firm and unyielding condition to a minimum density of 95 percent of the maximum dry density as determined by ASTM International (ASTM) D1557 (ASTM, 2023).
- Moisture content of the CSTC material should be controlled to within 2 to 3 percent of the optimum moisture. Optimum moisture is the moisture content corresponding to the maximum modified proctor dry density.

4.2.4 Construction Dewatering

The excavation is planned to extend approximately 12 feet below the ground surface to El 943 (base of excavation), which is approximately 1 foot below the highest groundwater levels recorded in the monitoring wells at the Site. Based on this data and the results of our slug testing, and considering the excavation geometry, we estimate the rate of groundwater flow into the excavation will be up to 10 gallons per minute. We anticipate these flows can likely be managed using a system of temporary sumps and pumps.

This estimate is for groundwater flow only and does not include potential stormwater (from precipitation or runoff) directly entering the excavation. Due to the uncertainty concerning the variable nature of hydraulic conductivity across the Site and potential seepage flows in excavations, water management methods should be determined by the contractor based on the conditions encountered during excavation.

5 References

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- Washington State Department of Ecology (Ecology), 2024, https://appswr.ecology.wa.gov/WellConstruction/Map/WCLSWebMap/WellCon structionMapSearch.aspxome.aspx, accessed February 2024.
- Washington State Department of Natural Resources (DNR), 2024, Washington Geologic Information Portal, Accessed February 2024 from https://geologyportal.dnr.wa.gov/.
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- Washington State Legislature, 2016, Washington Administrative Code (WAC), May 20, 2016.

6 Limitations

Work for this project was performed for Stillwater Holdings, LLC (Client), and this report was prepared consistent with recognized standards of professionals in the same locality and involving similar conditions, at the time the work was performed. No other warranty, expressed or implied, is made by Aspect Consulting (Aspect).

Recommendations presented herein are based on our interpretation of site conditions, geotechnical engineering calculations, and judgment in accordance with our mutually agreed-upon scope of work. Our recommendations are unique and specific to the project, site, and Client. Application of this report for any purpose other than the project should be done only after consultation with Aspect.

Variations may exist between the soil and groundwater conditions reported and those actually underlying the site. The nature and extent of such soil variations may change over time and may not be evident before construction begins. If any soil conditions are encountered at the site that are different from those described in this report, Aspect should be notified immediately to review the applicability of our recommendations.

Risks are inherent with any site involving slopes and no recommendations, geologic analysis, or engineering design can assure slope stability. Our observations, findings, and opinions are a means to identify and reduce the inherent risks to the Client.

It is the Client's responsibility to see that all parties to this project, including the designer, contractor, subcontractors, and agents, are made aware of this report in its entirety. At the time of this report, design plans and construction methods have not been finalized, and the recommendations presented herein are based on preliminary project information. If project developments result in changes from the preliminary project information, Aspect should be contacted to determine if our recommendations contained in this report should be revised and/or expanded upon.

The scope of work does not include services related to construction safety precautions. Site safety is typically the responsibility of the contractor, and our recommendations are not intended to direct the contractor's site safety methods, techniques, sequences, or procedures. The scope of our work also does not include the assessment of environmental characteristics, particularly those involving potentially hazardous substances in soil or groundwater.

All reports prepared by Aspect for the Client apply only to the services described in the Agreement(s) with the Client. Any use or reuse by any party other than the Client is at the sole risk of that party, and without liability to Aspect. Aspect's original files/reports shall govern in the event of any dispute regarding the content of electronic documents furnished to others.

Please refer to Appendix E titled "Report Limitations and Guidelines for Use" for additional information governing the use of this report.

We appreciate the opportunity to perform these services. If you have any questions, please call Eric Schellenger, PE, Geotechnical Engineer, at 206-780-7745.

FIGURES



Data source credits: None || Basemap Service Layer Credits: City of Walla Walla, Bureau of Land Management, State of Oregon, State of Oregon DOT, State of Oregon GEO, Esri Canada, Esri, HERE, Garmin, NCREMENT P. USGS, EPA, USDA, Oty of Walla Walla, Oregon State Parks, WA State Parks GIS, Esri, TomTorn, Garmin, FAO, NOAA, USGS, Bureau of Land Management, EPA, NPS, USFWS, Esri, USGS, Esri, HERE, Garmin, USGS, EPA, NPS





Aspect	FEB-2024	DIM / NLK	FIGURE NO.
CONSULTING	PROJECT NO. 230442	REVISED BY: CEB / RAP / HMD	2



- 3. Allowable passive earth pressure includes a factor of safety of 1.5.
- 4. Construction equipment surcharge is appropriate for a 160 size excavator operating directly behind the shoring walls. Aspect should be notified to evaluate additional lateral earth pressures from soil stockpiles, cranes, or other heavy equipment situated behind the shoring.

7 E Rose Street

Walla Walla, Washington

APPENDIX A

Subsurface Exploration Logs (by Others)

	MAJOR DIVIS	IONS	SYME GRAPH	BOLS	
	GRAVEI	CLEAN GRAVELS	000	GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES
	AND GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES
COARSE GRAINED	MORE THAN 50%	GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES
SOILS	OF COARSE FRACTION RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES
MORE THAN 50%	CAND	CLEAN SANDS		sw	WELL-GRADED SANDS, GRAVELLY SANDS
RETAINED ON NO. 200 SIEVE	AND AND SANDY SOILS	(LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND
	MORE THAN 50% OF COARSE	SANDS WITH FINES		SM	SILTY SANDS, SAND - SILT MIXTURES
	ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		SC	CLAYEY SANDS, SAND - CLAY MIXTURES
				ML	INORGANIC SILTS, ROCK FLOUR, CLAYEY SILTS WITH SLIGHT PLASTICITY
FINE	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
SOILS				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
MORE THAN 50% PASSING NO. 200 SIEVE				МН	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS SILTY SOILS
	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		СН	INORGANIC CLAYS OF HIGH PLASTICITY
				он	ORGANIC CLAYS AND SILTS OF MEDIUM TO HIGH PLASTICITY
	HIGHLY ORGANIC	SOILS	m	PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS
	□ 2.4 □ Sta □ She □ Pist	inch I.D. split I ndard Penetra Iby tube	barrel / Da	ames & SPT)	Moore (D&M)
B b S S	Dire Dire Bull Con Con Con Con Con Con Con Con Con Con	ect-Push k or grab htinuous Coring ecorded for dri l to advance sa n log for hamn ampler pusheo	g ven samp ampler 12 ner weight d using the	lers as t inches and dro e weight	he number of (or distance noted). op. : of the drill rig.

TIONAL MATERIAL SYMBOLS

SYM	BOLS	TYPICAL					
GRAPH	LETTER	DESCRIPTIONS					
	AC	Asphalt Concrete					
	СС	Cement Concrete					
	CR	Crushed Rock/ Quarry Spalls					
	SOD	Sod/Forest Duff					
	TS	Topsoil					

Groundwater Contact Measured groundwater level in exploration, well, or piezometer Measured free product in well or piezometer **Graphic Log Contact** Distinct contact between soil strata Approximate contact between soil strata **Material Description Contact** Contact between geologic units Contact between soil of the same geologic unit Laboratory / Field Tests rcent fines rcent gravel terberg limits emical analysis boratory compaction test nsolidation test y density rect shear drometer analysis pisture content pisture content and dry density hs hardness scale ganic content rmeability or hydraulic conductivity asticity index int lead test cket penetrometer eve analysis axial compression confined compression consolidated undrained triaxial compression ne shear **Sheen Classification** Visible Sheen ght Sheen oderate Sheen eavy Sheen

understanding of subsurface conditions. vere made; they are not warranted to be



Drilled	9/2	<u>Start</u> 3/2023	<u> </u> 9/23	<u>End</u> 3/2023	Total Depth	n (ft)	26.5	Logged By Checked By	BKH	Driller	GeoEngineers, Inc.				Drilling Method Hollow-stem Auger
Surface Vertical	e Eleva Datur	ation (ft) m		Unde	etermine	d		Hammer Data	14	0 (lbs) / 3	30 (in) Drop	E	Drilling Equipm	nent	CME-75
Easting Northin	; (X) ig (Y)							System Datum				C	Ground	dwater	not observed at time of exploration
Notes:	Geo analy	Engineer: ysis.	s did no	ot collec	t soil or g	round	lwater sar	nples for chemica	al analysis. (Collected s	soil samples were pro	ovideo	d to Ec	ology	representatives for potential chemical
			FIEI	LD DA	ATA										
Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification		MA DES	ATERIA CRIPTI	L ON		Sheen	Headspace Vapor (ppm)	REMARKS
	0-							Approximate	ly 4 inches	of concret	e (sidewalk)				
	_					H	ML	Occasion Brown silt wit	al cobbles (very densi	e, moist) (fill)				
	_							moist)		000031011	angraver (very stin,	-			
	-							-				-			
	5—	12			B-1(5-6.5)			_				_	NS	22.5	
	-	Ň						-				-			Chatter/gringing from approximately 61% feet
	_					5¢	GM	 Brown silty fin occasion 	ne to coars al cobbles (e gravel w very dens	rith sand and ie, moist)	_			onaller/grinning norn approximately 0721eet
	-							-				-			
	-							_				-		10.0	
	10	10		B	-1(10-11.5)								NS	19.9	
	_							_				-			
	_					6F						_			
	_							Becomes we	et			-			
	15 —	1 12		в	-1(15-16.5)			_				_	NS	0.3	
	-				(,			-				-			
	-					Pa		-				-			
	_							-				-			
	-						1	-				-			
	20 —	7		В	-1(20-21.5)	e (GP-GM	Brown fine to	o coarse gra	ivel with si	ilt, sand and cobbles	6	NS	7.0	
	-					0		_ (very den	ise, wet)			-			
	_					0		Ĺ				-			
	_					0									
	25 —					•	ML	 Brown sandy 	silt with oc	casional g	gravel (stiff, wet)		NS	1.1	
	-			В	-1(25-26.5)			-				_			
		r1	I	-I			1	1					<u> </u>	1	
Not	e: See	e Figure A	-1 for e	xplanat	tion of svr	nbols									
Coo	Coordinates Data Source: Horizontal approximated based on . Vertical approximated based on .														
\bigcap	Log of Boring B-1														
								Drojoot		t Doco	- Ctroot				

Date:10/4/23 Path:\\GeOENGINEERS.COM\WAN\PROJECTS\0\0504202\GINT\050420200.GPJ DBLIbran\/Librany.GEOENGINEERS_DF_STD_US_JUNE_2017.GLB/GEIS_ENVIRONMENTAL_STANDARD_NO_GW

GEOENGINEERS

Figure A-2 Sheet 1 of 1

Project: 6 West Rose Street Project Location: Walla Walla, Washington Project Number: 0504-202-00

ſ	Drilled	9/2	<u>Start</u> 3/2023	[9/23	<u>End</u> 3/2023	Total Depth	(ft)	26.5	Logged By BKH Checked By Driller GeoEngineers, Inc.							Drilling Method Hollow-stem Auger	
	Surface Vertica	e Eleva I Datu	ation (ft) m		Undet	ermined	I		Ha Da	ammer ata	14	0 (lbs) / 3	0 (in) Drop		Drilling Equipn	nent	CME-75
	Easting Northir	g (X) Ig (Y)							Sy Da	stem atum					Ground	dwater	not observed at time of exploration
	Notes:	Geol anal	Engineers ysis.	s did no	t collect :	soil or g	round	water sar	nple	es for chemical	analysis. C	Collected s	oil samples v	vere provid	led to Ec	cology	representatives for potential chemical
ſ				FIEL	_D DA1	Ā											
	Elevation (feet)	o Depth (feet) I	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification			MA DES(TERIA CRIPTIO	L ON		Sheen	Headspace Vapor (ppm)	REMARKS
		-	-				0	AC CSBC	-	Approximately Crushed surfa	6 inches o cing base	of asphalt course (5/	concrete pav /8-inch minus	rement 6)	-		
		-	-					 ML	+ ·	Brown silt with	sand and	l gravel (st	iff, moist)		-		
		-	-						_						-		
		5 —	10		B	2(5-6.5)		GM	 _	Brown silty fin occasiona	e to coarse l cobbles (v	e gravel wi very dense	ith sand and e, moist)		- NS	1.0	Chatter/grinding from 5 feet
RD_N0_GW		-							-						- -	10	
VIRONMENTAL_STANDAI		-			B-2	(10-11.5)	20000		-						-	1.0	
UNE_2017.GLB/GEI8_EN		- 15 — -	10		B-2	(15-16.5)	00000		-	Becomes wet					- NS	0.5	
DENGINEERS_DF_STD_US_							$\sim \sim $		-						- - - NS	0.5	
PJ DBLibrary/Library.GE		-			B-2	(20-21.5)			-						-		
202\GINT\050420200.G		- 25 — -	12		B-2	(25-26.5)		 ML	-	Brown sandy s	 silt with gra	avel (hard,	wet)		- NS	0.3	
0M\WAN\PROJECTS\0\0504																	
IGINEERS.C	Not Coc	e: See ordinat	e Figure A tes Data \$	-1 for e Source:	xplanatic Horizont	on of syn al appro	nbols. oximat	ed based	don	. Vertical appro	ximated b	ased on .					
th://GEOEN		Log of Boring B-2															
Date:10/4/23 Pa	C	E	oEr	NG	INE	ER:	5/	D		Project: Project I Project I	6 West Locatio	t Rose s n: Wall r: 050	Street a Walla, V 4-202-00	Washin	gton		Figure A-3

Project Number: 0504-202-00

Figure A-3 Sheet 1 of 1

Drilled	9/2	<u>Start</u> 4/2023	9/24	<u>End</u> 4/2023	Total Depth	ı (ft)	26	Logged By Checked By	BKH	Driller GeoEngineers, Inc.		Drilling Method Hollow-stem Auger	
Surface Vertical	Eleva Datu	ation (ft) m		Unde	termined	t		Hammer Data	14	0 (lbs) / 30 (in) Drop	Drillir Equip	g ment	CME-75
Easting Northing	(X) g (Y)							System Datum			Grou	ndwate	er not observed at time of exploration
Notes:	Geol anal	Engineers ysis.	s did no	ot collect	soil or g	round	lwater sar	nples for chemica	al analysis. (Collected soil samples were provid	led to	Ecology	representatives for potential chemical
			FIE	LD DA	TA								
Elevation (feet	 Depth (feet) 	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification		MA DES	ATERIAL CRIPTION	Sheen	Headspace Vanor (nnm)	REMARKS
				B	3(5-6.5) 3(10-11.5)		AC CSBC ML ML GP-GM	Approximate Approximate course (5 Brown silt wit (medium Light brown s Brown fine to occasion	ly 4 inches (ly 6 inches (5/8-inch min 5/8-inch min 5/8-inch min th sand and stiff, moist stift with san silt with san coarse gra al cobbles (of asphalt concrete pavement of crushed surfacing base hus) l occasional debris (plastic) (fill) d (soft, moist) vel with silt, sand and very dense, moist)		0.4	Chatter/grinding from 5 feet
		10		B3 B3	3(15-16.5) 3(20-21.5)	$\begin{array}{c} \circ \\ \circ $	GM		- Brown fine to coarse gravel with sand and cobbles (very dense, wet)				
Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Horizontal approximated based on .								- - - on . Vertical appi	roximated b	ased on .	NS	0.3	
	Log of Boring B-3												
G	E	DE	١G	INE	ER	S/	D	Project Project	: 6 Wes Locatio	t Rose Street n: Walla Walla, Washin	gton		Figure A-4

Date:10/4/23 Pttr:\\GEOENGINEERS.COM\WAN\PROJECTS\0\0504202\GINT\050420200.GPJ DBLIbran\Librany.tubrany.gEOENGINEERS_DF_STD_US_JUNE_2017.GLB/GEB_ENVIRONMENTAL_STANDARD_NO_GW

Figure A-4 Sheet 1 of 1

Project Location: Walla Walla, Washington Project Number: 0504-202-00

Drilled	9/2	<u>Start</u> 4/2023	9/24	<u>End</u> 4/2023	Total Depth	n (ft)	26.5	Logged By Checked By	BKH	Driller GeoEngineers, Inc.				Drilling Method Hollow-stem Auger
Surface Vertical I	Eleva Datur	ation (ft) m		Unde	etermine	d		Hammer Data	14	0 (lbs) / 30 (in) Drop	D	rilling quipn	nent	CME-75
Easting (Northing	(X) § (Y)							System Datum			G	round	lwater	r not observed at time of exploration
Notes:	Geol analy	Engineers ysis.	s did no	ot collec	t soil or g	rounc	lwater sar	nples for chemical	l analysis. (Collected soil samples were prov	vided	to Ec	ology	representatives for potential chemical
			FIE	LD DA	TA									
levation (feet	epth (feet)	iterval ecovered (in)	lows/foot	ollected Sample	ample Name esting	raphic Log	roup lassification		MA DES	ATERIAL CRIPTION		neen	eadspace apor (ppm)	REMARKS
ш	0-	- ~	8	ŏ	NF	5	AC		y 4 inches	of asphalt concrete pavement		0 0	Ξÿ	
	_					44	CSBC ML	Crushed surfa	acing base silt with oc	course (5/8-inch minus) casional gravel (stiff, moist)	-			
	-							_			-			
	5 3 B-4(5-6.5)										_	NS	0.1	
	-	3		E	3-4(5-6.5)	ay	GM	Brown silty fin	ne to coars	e gravel with sand and cobbles	_	110	0.1	Chatter/grinding from 6 feet
									se, moist)		_			
											_			
:	10 —	4		B	4(10-11.5)			_			_	NS	0.2	
	_	\square						_			_			
	_							_ Becomes wet	t		-			
	-							_			-	NC	0.2	
	- 15	4		B-	4(15-16.5)			-			_	NO	0.5	
	-							_			-			
	_							-			_			
:	20 —	12		B	4(20-21.5)			_			_	NS	0.4	
	-							_			-			
	_							_			_			
	-							_			-			
	- 25	12		B	4(25-26.5)			-			_	NS	0.3	
N at -		Eighter A	1 for -	volocet	ion of	nhele								
Coor	dinat	es Data S	Source:	xpianat Horizoi	ntal appr	oxima	ted based	l on . Vertical appre	oximated b	ased on .				
	Log of Boring B-4													
G	E	DE	NG	INE	ER	s /	0	Project: Project	6 Wes Locatio	t Rose Street n: Walla Walla, Washi	ingt	on		Figure 4-5

Project Number: 0504-202-00

Date:10/4/23 Path:\\GeOENGINEERS.COM\WAN\PROJECTS\0\0504202(GINT\050420200.GPJ_DBLIbhan/Libhan/Libhan/GEOENGINEERS_DF_STD_LS_JUNE_2017.GLB/GEB_ENVIRONMENTAL_STANDARD_NO_GW

Figure A-5 Sheet 1 of 1

Drilled	9/2	<u>Start</u> 4/2023	<u> </u> 9/24	<u>End</u> 4/2023	Total Depth	ı (ft)	25.75	Logged By Checked By	BKH	Driller	GeoEngineers, Inc.			Drilling Method Hollow-stem Auger	
Surface Vertical	e Eleva Datu	ation (ft) m		Und	etermined	t		Hammer Data	14	40 (lbs) / 30) (in) Drop	D	Drilling Equipn	nent	CME-75
Easting Northin	(X) g (Y)							System Datum				G	around	dwatei	r not observed at time of exploration
Notes:	Geol anal	Engineers ysis.	s did no	ot collec	t soil or g	rounc	lwater sar	mples for chemical	l analysis. (Collected so	il samples were pro	video	d to Ec	cology	representatives for potential chemical
			FIEI	LD DA	ATA										
Elevation (feet)	 Depth (feet) 	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification		M/ DES	ATERIAL CRIPTIC	ŌN		Sheen	Headspace Vapor (ppm)	REMARKS
	- 0	-				b	AC CSBC	Approximately - Crushed surfa	y 4 inches acing base	of asphalt of course (5/	concrete pavement 8-inch minus)	$\sum_{i=1}^{n}$			
	- - 5 —	13			B-5(5-6.5)		ML								
	-					20000	GM	Brown silty fin (medium)	ne to coars dense, mo	e gravel wit bist)	h sand and cobbles				Chatter/grinding from 6½ feet
	10	3		В	-5(10-11.5)	000000		- - -					NS	0.5	
	- 15 — -	7		В	-5(15-16.5)	000000000000000000000000000000000000		-	-			-	NS	0.1	
	- 20 — -	3		В	-5(20-21.5)	() () () () () () () () () () () () () (-				-	NS	0.4	
	- 25 —	10		B	-5(25-26.5)			_					NS	0.3	
Note Coo	Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Horizontal approximated based on . Vertical approximated based on .														
	Log of Boring B-5														
G	E	oEr	١G	INE	EER	S/	D	Project: Project	6 Wes Locatio	t Rose S on: Walla	Street a Walla, Wash	ingt	ton		Figure A-6

Project Number: 0504-202-00

Date:10/4/23 Path:\\GeOENGINEERS.COM\WAN\PROJECTS\0\0504202(GINT\050420200.GPJ_DBLIbhan/Libhan/Libhan/GEOENGINEERS_DF_STD_LS_JUNE_2017.GLB/GEB_ENVIRONMENTAL_STANDARD_NO_GW

Figure A-6 Sheet 1 of 1



Project Number: 0504-202-00

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Figure A-7 Sheet 1 of 1



Project: 6 West Rose Street Project Location: Walla Walla, Washington Project Number: 0504-202-00

GEOENGINEERS

VEL



Project Number: 0504-202-00

UNE 2017.GLB/GEIS ENVIRONMENTAL ğ

GEOENGINEERS

Figure A-9 Sheet 1 of 1



Project: 6 West Rose Street Project Location: Walla Walla, Washington

Project Number: 0504-202-00

Figure A-10 Sheet 1 of 1

GEOENGINEERS

NEL



Project: 6 West Rose Street Project Location: Walla Walla, Washington Project Number: 0504-202-00

GEOENGINEERS

WELI



Project Number: 0504-202-00

Date:104/23 Path:\GEOENGINEERS.COM/WWYPPD.ECTS\0/0504202/GINT/0504202/GINT/0504202/GINT/0EDENGINEERS_DF_STD_LJUNE_2017.GL8/GEB_ENVIPONMENTAI

GEOENGINEERS

Figure A-12 Sheet 1 of 1

APPENDIX B

Aspect Exploration Logs

B. Subsurface Explorations by Aspect

Aspect's field exploration program consisted of seven machine drilled borings with groundwater monitoring well installations and eight test pits. The logs of Aspect's explorations are presented in this appendix and locations of the explorations are shown on Figure 2.

B.1. Drilled Soil Borings

Aspect completed seven drilled borings that were completed as groundwater monitoring wells, designated AMW-01 through AMW-04, and MW-7 through MW-9, between October 18 and 20, 2023. The borings were drilled to depths of 25 feet bgs using sonic methods by a licensed driller (Western States Soil Conservation, Inc.) under subcontract to Aspect. Western States Soil Conservation, Inc. also installed the monitoring wells in each borehole.

An Aspect field representative was continuously present to observe the drilling procedures, screen and collect soil samples, and prepare descriptive logs of each boring. Soils were classified in general accordance with ASTM D2488, *Standard Practice for Description and Identification of Soils (Visual-Manual Procedure)*. The summary exploration log represents our interpretation of the contents of the field logs.

B.2. Test Pits

Aspect completed eight test pits, designated ATP-01 through ATP-08, on January 9 and 10, 2024. The test pits were excavated to depths between 4 and 10 feet bgs using an excavator operated by Able Technologies under subcontract to Aspect.

An Aspect field representative was continuously present to observe the excavation procedures, screen and collect soil samples, and prepare descriptive logs of the explorations. Soils were classified in general accordance with ASTM International (ASTM) D2488, *Standard Practice for Description and Identification of Soils (Visual-Manual Procedure)*. The relative density/consistency of the soils was evaluated qualitatively with a 0.5-inch-diameter steel T-probe and observation of digging effort.

The summary exploration logs represent our interpretation of the contents of the field logs. The stratigraphic contacts shown on the individual summary logs represent the approximate boundaries between soil types; actual transitions may be more gradual. The subsurface conditions depicted are only for the specific date and locations reported and are not necessarily representative of other locations and times.

No. 200 Sieve	an 50% ¹ of Coarse Fraction d on No. 4 Sieve	≤5% Fines		GW	Well-graded GRAVEL Well-graded GRAVEL WITH SAND Poorly-graded GRAVEL Poorly-graded GRAVEL WITH SAND	MC=Natural Moisture Content PSGEOTECHNICAL LAB TESTSPS=Particle Size DistributionGEOTECHNICAL LAB TESTSFC=Fines Content (% < 0.075 mm)GHGH=Hydrometer TestALAL=Atterberg LimitsCC=Consolidation TestStr=Strength TestOC=Organic Content (% Loss by Ignition)Comp=Proctor TestK=Hydraulic Conductivity TestSG=Specific Gravity Test
ined on	Vore tha Retained	6 Fines		GM	SILTY GRAVEL SILTY GRAVEL WITH SAND	Organic Chemicals CHEMICAL LAB TESTS
50%1 Reta	Gravels - I	≥15%		GC	CLAYEY GRAVEL CLAYEY GRAVEL WITH SAND	TPH-Dx Diesel and Oil-Range Petroleum Hydrocarbons TPH-G Gasoline-Range Petroleum Hydrocarbons VOCs Volatile Organic Compounds SVOCs Semi-Volatile Organic Compounds
- More than	e Fraction	Fines		SW	Well-graded SAND Well-graded SAND WITH GRAVEL	PAHs = Polycyclic Aromatic Hydrocarbon Compounds PCBs = Polychlorinated Biphenyls <u>Metals</u> RCRA8 = As, Ba, Cd, Cr, Pb, Hg, Se, Ag, (d = dissolved, t = total)
led Soils	of Coars 4 Sieve	≤5%		SP	Poorly-graded SAND Poorly-graded SAND WITH GRAVEL	MTCA5 = As, Cd, Cr, Hg, Pb (d = dissolved, t = total) PP-13 = Ag, As, Be, Cd, Cr, Cu, Hg, Ni, Pb, Sb, Se, Tl, Zn (d=dissolved, t=total)
Coarse-Grain	50% ¹ or More Passes No.	Fines		SM	SILTY SAND SILTY SAND WITH GRAVEL	PID = Photoionization Detector FIELD TESTS Sheen = Oil Sheen Test SPT ² SPT ² = Standard Penetration Test NSPT = Non-Standard Penetration Test DCPT = Dynamic Cone Penetration Test
	Sands - 5	≥15%		sc	CLAYEY SAND CLAYEY SAND WITH GRAVEL	Descriptive Term Size Range and Sieve Number COMPONENT Boulders = Larger than 12 inches DEFINITIONS Cobbles = 3 inches to 12 inches DEFINITIONS
Sieve	ys San FO%			ML	SILT SANDY or GRAVELLY SILT SILT WITH SAND SILT WITH GRAVEL	Fine Gravel = 3/4 inches to 3/4 inches Fine Gravel = 3/4 inches to No. 4 (4.75 mm) Coarse Sand = No. 4 (4.75 mm) to No. 10 (2.00 mm) Medium Sand = No. 10 (2.00 mm) to No. 40 (0.425 mm) Fine Sand = No. 40 (0.425 mm) to No. 200 (0.075 mm)
s No. 200	s and Cla			CL	LEAN CLAY SANDY or GRAVELLY LEAN CLAY LEAN CLAY WITH SAND LEAN CLAY WITH GRAVEL	Silt and Clay = Smaller than No. 200 (0.075 mm) % by Weight Modifier ESTIMATED ¹ 11 Outbrace 45 to 05 Limits
Nore Passes	Silt			OL	ORGANIC SILT SANDY or GRAVELLY ORGANIC SILT ORGANIC SILT WITH SAND	$\begin{array}{rcl} (1) &= & \text{Subtrace} & 15 \text{ to } 25 &= & \text{Little} & & \text{PERCENTAGE} \\ 1 \text{ to } <5 &= & \text{Trace} & 30 \text{ to } 45 &= & \text{Some} \\ 5 \text{ to } 10 &= & \text{Few} & >50 &= & \text{Mostly} \\ \end{array}$
ls - 50%1 or N	ys Moro			мн	ELASTIC SILT SANDY or GRAVELLY ELASTIC SILT ELASTIC SILT WITH SAND ELASTIC SILT WITH GRAVEL	Slightly Moist = Perceptible moisture CONTENT Moist = Damp but no visible water CONTENT Very Moist = Water visible but not free draining Very below water table
Grained Soi	ilts and Cla			СН	FAT CLAY SANDY or GRAVELLY FAT CLAY FAT CLAY WITH SAND FAT CLAY WITH GRAVEL	Non-Cohesive or Coarse-Grained SoilsRELATIVE DENSITYDensity3SPT2 Blows/FootPenetration with $1/2"$ Diameter RodVery Loose= 0 to 4 $\geq 2'$ Very Loose= 5 to 10 $1/2"$ Diameter Rod
Fine-	S citizi	ridaia		он	ORGANIC CLAY SANDY or GRAVELLY ORGANIC CLAY ORGANIC CLAY WITH SAND ORGANIC CLAY WITH GRAVEL	Loose = 5 to 10 1 to 2 Medium Dense = 11 to 30 3" to 1' Dense = 31 to 50 1" to 3" Very Dense = >50 < 1"
Highlv	Organic Soils			PT	PEAT and other mostly organic soils	Cohesive or Fine-Grained Soils CONSISTENCY Consistency³ SPT² Blows/Foot Manual Test Very Soft = 0 to 1 Penetrated >1" easily by thumb. Extrudes between thumb & fingers. Soft = 2 to 4 Penetrated 1/4" to 1" easily by thumb. Easily molded. Medium Stiff = 5 to 8 Penetrated >1/4" with effort by thumb. Molded with strong pressure
"WITH SIL name; e.g. GRAVEL" r gravel. • "	T" or "WIT⊦ ., SP-SM ● means 15 t Well-grade	I CLA "SILT to 30 d" m	Y" means Y" or "CL % sand a eans app	5 to 15% AYEY" me nd gravel roximatel	 silt and clay, denoted by a "-" in the group tans >15% silt and clay ● "WITH SAND" or "WITH ● "SANDY" or "GRAVELLY" means >30% sand and y equal amounts of fine to coarse grain sizes ● "Poorly 	Stiff= 9 to 15Indented $\sim 1/4"$ with effort by thumb.Very Stiff= 16 to 30Indented easily by thumbnail.Hard= > 30Indented with difficulty by thumbnail.
graded" m contains la Soils were ASTM D24	eans unec ayers of the described 188. Where	ual a two and indi	imounts of soil types identified cated in t	of grain si s; e.g., SM I in the fie he log, sc	Zes • Group names separated by "/" means soil I/ML. Id in general accordance with the methods described in ils were classified using ASTM D2487 or other	Observed and Distinct Observed and Gradual Inferred
laboratory	tests as a	oprop	riate. Ref	fer to the	report accompanying these exploration logs for details.	

Aspect

Estimated or measured percentage by dry weight
 (SPT) Standard Penetration Test (ASTM D1586)
 Determined by SPT, DCPT (ASTM STP399) or other field methods. See report text for details.

Exploration Log Key











NEW STANDARD EXPLORATION LOG TEMPLATE PAGINTW/PROJECTS/230442 - SINGERS CHEVRON.GPJ February 19, 2024



NEW STANDARD EXPLORATION LOG TEMPLATE PAGINTW/PROJECTS/230442 - SINGERS CHEVRON.GPJ February 19, 2024

	٨	maat	Stillwater H	loldings	Chevron UST and	l Soil Removal Interir	nterim Action - 230442 Excavation Log				
	A,	spect			Project Address & S	Site Specific Location			Coordinates (Lat,Lon WGS84)	Exploration Numb	ber
		ONSULTING	Equi	7 E Ros	e St, Walla Wall	a, WA, Chevron Pro	operty		46.0678, -118.3399	ATP-0	3
						Sampling Method	1				
A		Diversion	Exploratio	ouo⊏ n Method	(s)	Work Start/Completion	Dates		934.30 Top of Casing Elev (NAVD88)	Denth to Water (Belo	W GS)
	Jo	sh Kina	Ter	st nit	(0)	1/9/2024	Dutoo		NA	No Water Encour	ntered
Depth (feet)	Elev.	Exploration N	Notes and	Sample	Analytical Sample Number &	Field Tests	Material		Description		Depth
	-	i i i i i i i i i i i i i i i i i i i	with top course		Lab Test(s)		Турс	ASPH	ALT; top course.		(1)
1 -	954	ACCESSION Minor ca	aving observed.			PID=0.2 Sheen=None		GRAV ∖gravel.	EL (GP); very moist; angular t	o round fine	1
2 -	953	Backfille Backfille Backfille	ed with ted material.		TP-03-02 NWTPH-Gx,	PID=57.9 Sheen=Moderate T-probe=3"		SILTY : moist, d	FILL SAND (SM); medium dense to ark gray; fine to medium sand	o dense, slightly l; fine angular	- 2
3 -	952				BETX	PID=0.2 Sheen=None T-probe=6"		∖gravel; ł SILTY	nydrocarbon-like odor. SAND WITH GRAVEL AND	COBBLES (SM);	- 3
4 -	951					PID=0.2 Sheen=None T-probe=1'+		medium medium cobbles	i dense to dense, slightly mois i sand; fine to coarse subroun	at, brown; fine to ded gravel and	- 4
5 -	930 - 949					PID=0.2 Sheen=None		SAND dense, s coarse s	Y SILT WITH GRAVEL (ML); slightly moist, brown; low plas sand; fine to coarse subround	medium dense to ticity; fine to ed gravel and	- 5
6 -	948					Sheen=None			ALLUVIUM		6
7 -	947				TP-03-07 NWTPH-Gx, BETX	Sheen=None		medium coarse s	a dense to dense, slightly mois sand; fine to coarse subround	ed gravel and	- 7
8 -	946					Sheen=None PID=0.2		Becom	nes very moist.		- 8
9 -	945	1552158				Sheen=None		Bottom	of exploration at 9 ft. bgs.		9
10-	944										-10
11-	943										-11
12-	942										-12
13-	941										-13
14-	- 940										+14
<u>6</u> 15-	939										-15
	938										10
18-	937										-18
19-	936										-19
20-	935										-20
21-	934										-21
22-	933										-22
23-	932										-23
24-	931										-24
	930	lond								[
Sample	Leg	jenu			Water Level M oN	ater Encountered		See Expl explanati Logged b Approved	oration Log Key for on of symbols by: DJM d by: Carla Brock	Exploration Log ATP-03 Sheet 1 of 1	on

19. 2024

Managet	Stillwater Holdings	Chevron UST and S	Soil Removal Interin	n Action -	230442	Excavatio	n Log	
Aspect		Project Address & Site	e Specific Location			Coordinates (Lat,Lon WGS84)	Exploration Numb	ber
	7 E Ros Fauinment	e St, Walla Walla,	, WA, Chevron Pro	operty		46.0678, -118.3400 Ground Surface Fley (NAVD88)	ATP-04	4
	CAT 305E		Bucket	,		953 92'		
Operator	Exploration Method	(s)	Work Start/Completion	Dates		Top of Casing Elev. (NAVD88)	Depth to Water (Below	w GS)
Josh Kina	Test pit	1-7	1/9/2024			NA	No Water Encoun	ntered
Depth Elev. Exploration N (feet) (feet) Completion	Notes and Sample Details Type/ID	Analytical Sample Number & Lab Test(s)	Field Tests	Material Type		Description		Depth (ft)
Depth (feet) Elev. (reet) Exploration N Completion	Notes and Details Sample Type/ID with top course SS ad with ed material. te caving dd.	Analytical Sample Number & Lab Test(s) TP-04-05 NWTPH-Gx, BETX TP-04-10.5 NWTPH-Gx, BETX	Field Tests PID=0.2 Sheen=None T-probe=6' PID=0.2 Sheen=None T-probe=6' PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None		ASPHA SILTY S dense, r subroun Pea gra SAND dense, r sand; fir SILTY S medium sand; fir SILTY Medium sand; fir Becom Bottom o Note: Not througho	Description ALT; base course. FILL SAND WITH GRAVEL (SM); r noist, brown; fine to coarse sa ded gravel and cobbles. avel from 1'-2' along North wa Y SILT WITH GRAVEL (ML); r noist, brown; low plasticity; fin te to coarse subrounded grave GRAVEL WITH GRAVEL AND C dense to dense, moist, browr te to coarse sand; fine to coar nd cobbles. res very moist. of exploration at 10.5 ft. bgs. o sheen or hydrocarbon-like or out.	nedium dense to and; fine to coarse II of test pit. medium dense to e to medium el. OBBLES (SM); n; fine to coarse el and cobbles. COBBLES (GM); n; fine to coarse se subrounded dor observed	Depth (ft) - 1 - 2 - 3 - 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 - 15 - 16 - 17 - 18 - 19 - 20 - 21
22-932								-22
23-931								-23
24-930								-24
Sample Type Type		No Wate Cevel Level	er Encountered	L S E L A	See Expl explanation ogged b Approved	oration Log Key for on of symbols by: DJM d by: Carla Brock	Exploration Log ATP-04 Sheet 1 of 1	on

NEW STANDARD EXPLORATION LOG TEMPLATE PAGINTWPROJECTS/230442 - SINGERS CHEVRON.GPJ February 19, 2024

	Acnost	Stillwater Ho	oldings Che	vron UST and S	Soil Removal Interir	n Action	- 230442	Excavatio	n Log	
	Aspect	_	Proj	ect Address & Site	e Specific Location			Coordinates (Lat,Lon WGS84)	Exploration Numb	ber
	Contractor	r Fauir	E Rose St	, walla walla,	Sampling Method	operty		46.0678, -118.3400 Ground Surface Flev (NAVD88)	ATP-0	5
	ble Technologies	CAT	305F		Bucket			954 02'		
	Operator	Exploration	Method(s)		Work Start/Completion	Dates		Top of Casing Elev. (NAVD88)	Depth to Water (Belo	w GS)
	Josh Kina	Tes	t pit		1/9/2024			NA	No Water Encour	ntered
Depth (feet)	Elev. (feet) Exploration N Completion	Notes and Details	Sample Type/ID Sa	Analytical mple Number & Lab Test(s)	Field Tests	Material Type		Description		Depth (ft)
Depth (feet) 1 - 2 - 3 - 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 - 13 - 14 - 15 - 10 - 11 - 17 - 13 - 10 - 11 - 17 - 10 - 10 - 11 - 10 - 10 - 11 - 10 - 10 - 11 - 10 - 10 - 11 - 10 - 1	Elev. (feet) Exploration N Completion 954 •••••• Topped to 3* BC 952 ••••• Backfille excavat 951 ••••• Backfille excavat 951 ••••• Backfille excavat 951 ••••• Backfille excavat 951 ••••• Backfille excavat 940 ••••• Backfille excavat 943 ••••• Backfille excavat 944 ••••• Backfille excavat 943 ••••• ••••• 944 ••••• ••••• 943 ••••• ••••• 944 ••••• ••••• 943 ••••• ••••• 944 ••••• ••••• 943 ••••• •••••• 944 •••••• •••••• 943 •••••••• •••••••• 944 ••••••••••••••••••••••••••••••••••••	Notes and Details with top course SS ad with ed material.	Sample Type/ID Sa	Analytical mple Number & Lab Test(s) TP-05-2.5 IWTPH-GX, BETX TP-05-10 IWTPH-GX, BETX	Field Tests PID=0.2 Sheen=None T-probe=6" PID=0.2 Sheen=None T-probe=1"+ PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None PID=0.2 Sheen=None	Material Type	ASPH/ SILTY S medium sand; fir SAND dense, r coarse s Becom SILTY (medium sand; fir Bottom (Note: No through	Description ALT; base course. FIL SAND WITH GRAVEL AND C dense to dense, moist, brown te to coarse subrounded gravel Y SILT WITH GRAVEL (ML); in moist, brown; low plasticity; fin subrounded gravel. tes fine to medium sand. Cancer to dense, moist, brown BRAVEL WITH SAND AND C dense to dense, moist, brown te to coarse subrounded grave of exploration at 10 ft. bgs. o sheen or hydrocarbon-like o out.	OBBLES (SM); 1; fine to coarse el and cobbles. medium dense to e sand; fine to OBBLES (GM); 1; fine to coarse els and cobbles. dor observed	Depth (ft) - 1 - 2 - 3 - 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 - 15 - 16 - 17
s 18-	936									-18
- 19 -	935									- 19
- 02 Tects/33	934									-20
21-	933									-21
22-	932									-22
23-	931									-23
24-	930									-24
EXPLORA	Legend			No Wate	er Encountered		See Expl	oration Log Key for	Fynloratic	 >P
NEW STANDARU Sample Tvne			Water Level				explanati Logged k Approved	on of symbols by: DJM d by: Carla Brock	Log ATP-05 Sheet 1 of 1	

	Δ	snoct	Stillwater H	loldings	Chevr	on UST and S	Soil Removal Interi	m Actior	n - 230442	Excavatio	n Log	-
			-	7 F Ros	Projec se St ۱	t Address & Site Nalla Walla	e Specific Location WA Chevron Pr	opertv		Coordinates (Lat,Lon WGS84) 46.0679 -118.3401	Exploration Numb	ber
	C	ontractor	Equ	ipment	,, ,		Sampling Metho	d		Ground Surface Elev. (NAVD88)	ATP-00	6
A	ble T	echnologies	CAT	305E			Bucket			953.62'		
	(Dperator	Exploratio	on Method	1(s)	I	Work Start/Completior	n Dates		Top of Casing Elev. (NAVD88)	Depth to Water (Belo	w GS)
	Jo	sh Kina	Те	st pit			1/9/2024 to 1/10/	2024	1	NA	No Water Encour	ntered
Depth (feet)	Elev. (feet)	Exploration N Completion	lotes and Details	Sample Type/ID	Sam L	Analytical ple Number & ab Test(s)	Field Tests	Material Type		Description		Depth (ft)
1 -	953	Contraction of the second s	with top course S				PID=0.2 Sheen=None		ASPH/ fine to c cobbles	ALT; base course, moist; fine oarse subrounded to subangu	to coarse sand; lar gravel and	1
2 -	952		d with				PID=0.2 Sheen=None T-probe=1'		SILTY	FILL SAND WITH GRAVEL AND C dense to dense moist brown	OBBLES (SM);	- 2
3 -	951		eu materiai.				PID=0.2 Sheen=None T-probe=1'+		sand; fir	ne to coarse subrounded grave	and cobbles.	- 3
4 -	950				T NV	⁻ P-06-04 VTPH-Gx,	PID=0.2 Sheen=None T-probe=1'+		SAND dense, r	Y SILT WITH GRAVEL (ML); i moist, brown; low plasticity; fin	medium dense to e sand; fine to	- 4
5 -	949					BETX	PID=0.2 Sheen=None			subloanded graven.		- 5
6 -	947						PID=0.2 Sheen=None PID=0.2	9 Pla		ΔΗΗΛ		- 6
7 -	946						Sheen=None		SILTY (dense to	GRAVEL WITH COBBLES (G o dense, moist, brown; fine to e subrounded gravel and cob	M); medium coarse sand; fine ples	+ 7
8 -	945						PID=0.2 Sheen=None					- 8
10-	944				Т	P-06-10	PID=0.2 Sheen=None		, ,			+10
11-	943					BETX			Note:	o sheen or hydrocarbon-like o	dor observed	-11
12-	942								linougno	Sut.		-12
13-	941											-13
14-	940											-14
- 15 ³⁰	938											- 15
49 16- 165 17	937											-16
	936											-17
- 19-	935											-19
-02 CTS/23044	934											-20
TWPROA	933											-21
ATE P:/GIN	932											-22
Z3-	931											-23
24-	929											-24
XPLO	Leg	jend			r				See Eynl	oration Log Key for	_ •	
EW STANDARD E	- ypd				Water Level	No Wate	er Encountered		explanati Logged k Approved	on of symbols by: DJM d by: Carla Brock	Exploration Log ATP-06 Sheet 1 of 1	on

	٨	mod	Stillwater H	loldings	s Chevro	on UST and S	Soil Removal Interii	n Action	ı - 230442	Excavatio	n Log	
		spect			Project	Address & Sit	e Specific Location			Coordinates (Lat,Lon WGS84)	Exploration Num	nber
		NSULTING	Eau	7 E Ros	se St, V	Valla Walla	, WA, Chevron Pro	operty		46.0679, -118.3399	ATP-0	7
								1				
A			Exploratio	305⊏ n Methor	d(s)		Work Start/Completion	Dates		954.04 Top of Casing Elev. (NAVD88)	Depth to Water (Bel	ow GS)
	lo	sh Kina	Te	st nit			1/9/2024 to 1/10/	2024		NΔ	No Water Encou	ntered
	00		10			nalvtical					No Water Encou	
Depth (feet)	Elev. (feet)	Exploration N Completion	lotes and Details	Sample Type/ID	Samp La	le Number & b Test(s)	Field Tests	Material Type		Description		Depth (ft)
1 -	954 -	to 3" BG	SS					00000	ASPH	ALI; base coarse.		- 1
2 -	953	Moderat observe Backfille	te caving d. d with ed material.				PID=0.8 Sheen=Slight	000000000000000000000000000000000000000	GRAVE gravel.	EL (GP); pea gravel, gray, moi	st; fine rounded	- 2
3 -	952						PID=9.1 Sheen=Slight		SILTY medium sand; fir	SAND WITH GRAVEL AND (dense to dense, moist, gray; ne to coarse subrounded grave	COBBLES (SM); fine to coarse el and cobbles;	- 3
4 -	951					Р-07-04 /ТРН-Gx, ВБТХ	PID=298 Sheen=Moderate		hydroca	irbon-like odor.	,	- 4
5 -	949						PID=102 Sheen=Moderate		SAND` moist, g	Y SILT WITH GRAVEL (ML); ray; low plasticity; fine to coar	medium stiff, se sand; fine to	- 5
6 -	948					P-07-06 /TPH-Gx, BETX	Sheen=Moderate PID=212 Sheen=Moderate		coarse s hydroca Bottom	subrounded gravel and cobble irbon-like odor. of exploration at 6.5 ft bos	s;	
8	947								Note: Hi	ighest PID readings along buil	ding side of test	
9 -	946								5'.	····· b.b ····· 3 b ···· b · ··· - · · ·		- 9
10-	945 -											-10
11-	944											-11
12-	943											-12
13-	942											-13
14-	941 - 940											-14
- 15 13' 30	939											- 15
-16 GEN Lep	938											-16
	937											-18
- 19	936											-19
-02 CTS/23044:	935											-20
	934											-21
22-	933											-22
ZEMPLA	932											-23
501 VOIL	931 - 930											-24
	Leg	jend					I					
EW STANDARD EXI Sample Type					Water Level	No Wat	er Encountered		See Expl explanati Logged b Approved	loration Log Key for ion of symbols by: DJM d by: Carla Brock	Exploration Log ATP-07 Sheet 1 of 2	on

	Λ	sport	Stillwater H	loldings	s Chevi	ron UST and S	oil Removal Interi	m Action	- 230442	Excavatio	n Log	
		sheri	-		Projec	t Address & Site	Specific Location	oportu		Coordinates (Lat,Lon WGS84)	Exploration Numl	ber
–	000	Contractor	Equi	ipment	se 31,	vvalla vvalla,	Sampling Metho	d		Ground Surface Elev. (NAVD88)		8
A	ble T	echnologies	CAT	305E			Bucket			954.69'		
	(Operator	Exploratio	on Metho	d(s)	1	Nork Start/Completion	n Dates		Top of Casing Elev. (NAVD88)	Depth to Water (Belo	w GS)
	Jo	sh Kina	Te	st pit			1/9/2024 to 1/10/	2024		NA	No Water Encour	ntered
Depth (feet)	Elev. (feet)	Exploration N Completion	lotes and Details	Sample Type/ID	Sam	Analytical pple Number & .ab Test(s)	Field Tests	Material Type		Description		Depth (ft)
	954	CONCENTION TOPPED	with top course S				PID=0.2		ASPH	ALT; base coarse. FILL		-
	953	CORO CORO Moderat	e caving d.				PID=0.2		GRAVE	EL (GP); pea gravel.		- 1
	952	excavate	ed with ed material.				PID=0.2		SILTY medium	SAND WITH GRAVEL AND (dense to dense, brown, mois	COBBLES (SM); it; fine to coarse	- 2
3 -	951					TP-08-4	T-probe=1' PID=0.2 Sheen=None		sanu, in	le to coarse subrounded grav	er and cobbles.	- 3
4 -	950				NV	VTPH-Gx, BETX	T-probe=1'		Bottom	of exploration at 4 ft. bgs.	dor obsorived	4
5	949								through	out.		
7	948											
8	947											
9-	946											- 9
10-	945											-10
11-	944											-11
12-	943											-12
13-	942											-13
14-	941											-14
16, 2024	940											-15
1 February	939											-16
ARON GN 17-	938											-17
HO SERS CHE	937											-18
- 810 - 19-	936											-19
-02 JECTS/23(935											-20
21-	934											-21
ATE P:G	933											-22
¹ dw <u>=</u>	932											-23
901 NOL 24 -	931											-24
LORA'	930	lend										
Sample		,			Water Level	No Wate	er Encountered		See Expl explanati Logged k Approved	oration Log Key for on of symbols by: DJM d by: Carla Brock	Exploration Log ATP-08 Sheet 1 of 1	on



P:\GINTW/PROJECTS\230442 - SINGERS CHEVRON.GPJ February 19, 2024 NEW STANDARD EXPLORATION LOG TEMPLATE



P:\GINTW/PROJECTS\230442 - SINGERS CHEVRON.GPJ February 19, 2024 NEW STANDARD EXPLORATION LOG TEMPLATE



NEW STANDARD EXPLORATION LOG TEMPLATE PAGINTWAPROJECTS/230442 - SINGERS CHEVRON.GPJ February 19, 2024

APPENDIX C

Slug Test Results

Table C-1 - Hydraulic Conductivity Estimates from Slug Tests

230442 Singers Chevron, Walla Walla, Washington

Monitoring Well		AMW-01			AMW-02			AMW-04	
Well Depth in Feet		25.0			25.0		25.0		
Screen Length in Feet		15.0			15.0		15.0		
Depth to Screen in Feet		5.0			5.0			5.0	
Depth to Aquitard in Feet		30			30			30	
Depth to Water in Feet		12.03		12.42				11.15	
Depth to Sandpack in Feet		3.0			3.0			3.0	
Slug Displacement (Ho) in Feet	0.35	0.67	0.35	0.31	0.37	0.35	0.18	0.34	0.41
Porosity (n)		0.30			0.30			0.30	
Radius of Casing (rc) in Feet		0.17			0.17			0.17	
Radius of Borehole (rw) in Feet		0.25			0.25			0.25	
Saturated Aquifer Thickness (H) in Feet		18.0			17.6			18.9	
Saturated Well Thickness (Lw) in Feet		8.0			7.6		8.9		
Effective Radius (reff) in Feet		0.195			0.195		0.195		
Effective Screen Length (Le) in Feet		8.0		7.6			8.9		
Slug Size	3' x1"	3' x1"	3' x1"	3' x1"	3' x1"	3' x1"	1.5' x1"	3' x1"	3' x1"
Rising/Falling Head Test	Rising	Rising	Rising	Rising	Rising	Rising	Rising	Rising	Rising
Fully Submerged Sandpack	No	No	No	No	No	No	No	No	No
Transiently Exposed Sandpack	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Transiently Exposed Screen	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Partially Submerged Screen	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Bouwer and Rice Analysis Parameters									
Normalized Head at t1 (y1) in Feet	0.29	0.26	0.38	0.55	0.45	0.49	0.39	0.42	0.35
Time - t1 in Seconds	256	180	155	120	181	190	480	180	118
Normalized Head at t2 (y2) in Feet	0.20	0.16	0.20	0.21	0.23	0.21	0.20	0.23	0.16
Time - t2 in Seconds	391	339	361	606	596	598	917	555	540
Calculated K in cm/sec	4.8E-04	5.2E-04	5.2E-04	3.4E-04	2.9E-04	3.7E-04	2.4E-04	2.5E-04	3.0E-04
Calculated K in ft/day	1.36	1.48	1.46	0.96	0.82	1.05	0.67	0.71	0.86
Geometric Mean K in ft/day		1.4			0.9			0.7	
Geometric Mean K in ft/s		1.66E-05			1.08E-05			8.60E-06	
Screened Interval Soil Type									

Notes:

Data analysis by method of Bouwer and Rice (1976; 1989).

Bold values are entered from field data and other values are calculated.

All depths are below ground surface

^a The Bouwer and Rice A, B, and C coefficients are calculated using regression equations of Van Rooy (1988).

^b Analyzed using methods for oscilatory water level repsonse in Butler, et al (2000).

 c R_e/r_w is the effective radial distance over which y is dissipated, divided by the radial distance of well development.

APPENDIX D

Shoring Suite Outputs



UNITS: Width,Spacing,Diameter,Length,and Depth - ft; Force - kip; Moment - kip-ft Friction,Bearing,and Pressure - ksf; Pres. Slope - kip/ft3; Deflection - in

East & West Shoring Wall East & West Wall Embedment



Licensed to 4324324234 3424343 Date: 2/13/2024 File: S:\Stillwater Holdings Chevron_230442\Geotech\Analysis\Shoring Suite\East-South Wall.sh8

Wall Height=12.0 Pile Diameter=2.5 Pile Spacing=6.2 Wall Type: 2. Soldier Pile, Drilled

PILE LENGTH: Min. Embedment=19.41 Min. Pile Length=31.41 MOMENT IN PILE: Max. Moment=284.71 per Pile Spacing=6.2 at Depth=20.53

PILE SELECTION:

Request Min. Section Modulus = 103.5 in3/pile=1696.56 cm3/pile, Fy= 50 ksi = 345 MPa, Fb/Fy=0.66 W16X89 has Section Modulus = 155.0 in3/pile=2539.99 cm3/pile. It is greater than Min. Requirements! Top Deflection = 0.97(in) based on E (ksi)=29000.00 and I (in4)/pile=1300.0

DRIVING PRESSURES (ACTIVE, WATER, & SURCHARGE):

		`	,			
	Z1	P1	Z2	P2	Slope	
	0	0	12	0.432	0.036000	
	12	0.353	100	1.783	0.01625	
	**Tra					
	0	0.125	12	0.125	0.000000	
PASSIVE PRI	ESSURES	6:				
	Z1	P1	Z2	P2	Slope	
	14	0.322	100	14.16	0.1610	
ACTIVE SPAC	CING:					
	No.		Z depth		Spacing	
	1		0.00		6.22	
	2		12.00		2.50	
PASSIVE SPA	ACING:					
	No.		Z depth		Spacing	
	1		12.00		6.22	

UNITS: Width,Spacing,Diameter,Length,and Depth - ft; Force - kip; Moment - kip-ft Friction,Bearing,and Pressure - ksf; Pres. Slope - kip/ft3; Deflection - in

South Wall South Wall Embedment



UNITS: Width,Spacing,Diameter,Length,and Depth - ft; Force - kip; Moment - kip-ft Friction,Bearing,and Pressure - ksf; Pres. Slope - kip/ft3; Deflection - in

APPENDIX E

Report Limitations and Guidelines for Use

REPORT LIMITATIONS AND GUIDELINES FOR USE

This Report and Project-Specific Factors

Aspect Consulting (Aspect) considered a number of unique, project-specific factors when establishing the Scope of Work for this project and report. You should not rely on this report if it was:

- Not prepared for you
- Not prepared for the specific purpose identified in the Agreement
- Not prepared for the specific real property assessed
- Completed before important changes occurred concerning the subject property, project or governmental regulatory actions

Geoscience Interpretations

The geoscience practices (geotechnical engineering, geology, and environmental science) require interpretation of spatial information that can make them less exact than other engineering and natural science disciplines. It is important to recognize this limitation in evaluating the content of the report. If you are unclear how these "Report Limitations and Use Guidelines" apply to your project or site, you should contact Aspect.

Reliance Conditions for Third Parties

This report was prepared for the exclusive use of the Client. No other party may rely on the product of our services unless we agree in advance to such reliance in writing. This is to provide our firm with reasonable protection against liability claims by third parties with whom there would otherwise be no contractual limitations. Within the limitations of scope, schedule, and budget, our services have been executed in accordance with our Agreement with the Client and recognized geoscience practices in the same locality and involving similar conditions at the time this report was prepared.

Property Conditions Change Over Time

This report is based on conditions that existed at the time the study was performed. The findings and conclusions of this report may be affected by the passage of time, by events such as a change in property use or occupancy, or by natural events, such as floods, earthquakes, slope instability, or groundwater fluctuations. If any of the described events may have occurred following the issuance of the report, you should contact Aspect so that we may evaluate whether changed conditions affect the continued reliability or applicability of our conclusions and recommendations.

Discipline-Specific Reports Are Not Interchangeable

The equipment, techniques, and personnel used to perform a geotechnical or geologic study differ significantly from those used to perform an environmental study and vice versa. For that reason, a geotechnical engineering or geologic report does not usually address any environmental findings, conclusions, or recommendations (e.g., about the likelihood of encountering underground storage tanks or regulated contaminants). Similarly, environmental reports are not used to address geotechnical or geologic concerns regarding the subject property.

We appreciate the opportunity to perform these services. If you have any questions please contact the Aspect Project Manager for this project.