Draft Geotechnical Engineering Report Bellevue Airfield Park Development (Former Eastgate Landfill) Bellevue, Washington

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Prepared for

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1.0 INTRODUCTION

This report summarizes the results of geotechnical engineering services conducted to support design related to the proposed Bellevue Airfield Park (Park) development at the site of the former Eastgate Landfill in Bellevue, Washington as shown on the Vicinity Map on Figure 1. The proposed Park will include two synthetic turf athletic fields, concessions and restroom facilities, play and picnic areas, pedestrian trails, a spray deck, expansion and improvements to existing stormwater management facilities, and lighting and parking improvements.

A portion of the Park site overlies the closed Eastgate Landfill, which has environmental restrictions and ongoing monitoring requirements under the Washington State Department of Ecology (Ecology) Model Toxics Control Act (MTCA) voluntary cleanup program (VCP) and an environmental covenant for the site dated November 12, 2008.

In addition to the geotechnical engineering conclusions and recommendations contained herein, Landau Associates, under subcontract to Walker Macy, is also assisting the design team and the City of Bellevue (City) by providing environmental engineering, permitting support, and landfill cover design services for Phase 1 of the Park development. Evaluations and recommendations related to stormwater management, utilities, civil engineering design, landfill gas management, and air quality monitoring will be provided separately by other members of the Walker Macy design team.

Improvements associated with Phase 1 of the Park development include the Park entry, southern athletic field, concessions and restroom building, stormwater facilities and detention pond, trails, and certain modifications to the groundwater monitoring and landfill gas control systems.

1.1 Site Description

The proposed Bellevue Airfield Park is located adjacent to the I-90 Business Park in Bellevue, Washington (Figure 1). A master plan for the Park, entitled "Bellevue Airfield Park, Eastgate Area Properties Master Plan," was prepared in 2012 for the City of Bellevue Parks & Community Services Department by The Portico Group (The Portico Group 2012). The Eastgate Area Properties are comprised of three parcels totaling 27.9 acres within the Phantom Lake watershed. The City previously purchased portions of these properties from The Boeing Company (Boeing) and the Bellevue School District with the intent of developing an active-use community park. An access road (SE 30th Place, also referred to as the "Shared Entrance Road") has already been constructed along the southern side of the proposed Park as part of the Advanta Office Commons development.

The proposed Park site includes the former Eastgate Landfill, which was operated by King County as a municipal solid waste landfill, and accepted household and demolition wastes from 1951 until it was closed and covered in 1964. The Bellevue Airfield runway was subsequently extended over the former landfill, and operated until 1983. After landfill closure, Cabot, Cabot & Forbes purchased property, including most of the landfill, and developed the I-90 Business Park. Boeing acquired portions of the

former Eastgate Landfill property and adjacent properties in 1980 and 1983. The Boeing-owned property was partially developed by Boeing in the mid to late 1980s; however, no buildings have been constructed directly over the former landfill to date. Closure activities performed at the landfill by King County; Cabot, Cabot & Forbes; the City of Bellevue; or Boeing include landfill capping with a soil cover, groundwater monitoring, stormwater management, leachate collection, and landfill gas migration control (LAI 2000). Leachate is collected on the north side of the landfill in a French drain that discharges to the King County sanitary sewer. Groundwater monitoring wells and landfill gas extraction monitoring wells are located around the perimeter of the landfill. Monitoring well locations, the gas extraction system, the leachate collection system, and the approximate landfill area are shown on Figure 2.

In 2007 to 2008, the Advanta Office Commons development (including three buildings designated buildings A, B, and C, a parking garage, and the shared entrance road) was constructed by Schnitzer Northwest LLC (Schnitzer) adjacent to the southern end of the landfill. This resulted in construction of relatively low-permeability hardscape surfaces (asphalt roadways and parking areas) over a portion of the southern extent of the landfill.

2.0 SCOPE OF SERVICES

Walker Macy retained Landau Associates to provide geotechnical engineering services to support design of the proposed Park improvements, including the new synthetic turf athletic fields, concessions and restroom facilities, parking area and access roads, retaining walls, and associated projects features for each (i.e., underground utilities, etc.). Our scope of services includes the following specific tasks:

- Collecting and reviewing readily available geotechnical and geologic data for the project area
- Obtaining utility clearances prior to performing field explorations
- Performing a Geophysical Survey to estimate the horizontal and vertical limits of the landfill
- Advancing a series of exploratory borings, test pits, and hand auger borings throughout the Park area in the vicinity of proposed improvements and locations needed to identify existing landfill solid waste deposits underlying the site
- Collecting representative soil samples at selected intervals
- Logging the borings, test pits, and hand auger borings and recording pertinent information including soil sample depths, stratigraphy, soil engineering characteristics, groundwater occurrence, and evidence of potential soil or groundwater contamination
- Conducting limited laboratory testing
- Evaluating data from the subsurface investigation and laboratory testing programs and performing certain engineering analyses
- Developing geotechnical engineering conclusions and recommendations to support design of proposed improvements
- Preparing and submitting this written report summarizing our findings and geotechnical engineering conclusions and recommendations. This report includes:
 - a site plan showing the locations of current and previous subsurface explorations, and other pertinent site features.
 - logs of the current and previous borings and other subsurface information.
 - a summary of subsurface soil and groundwater conditions anticipated in the vicinity of the proposed park improvements, as suggested by current and previous exploration data.
 - an evaluation of the settlement-susceptibility of the site soils due to static loads, including estimated settlement magnitudes under the weight of new fill and structures, and recommendations to limit settlements beneath the proposed improvements to within tolerable levels.
 - recommendations for site preparation for the proposed park improvements, including a discussion related to ground improvement techniques (e.g., preloading) that might be necessary to mitigate settlement risks.
 - design recommendations for applicable foundation support type(s) for the proposed park buildings (i.e., spread footings, mat foundations, etc.), including subgrade

preparation, allowable soil bearing pressures, estimates of settlement, and soil parameters for lateral load resistance.

- site factors for use in seismic design of the structures under the 2012 International Building Code (2012 IBC).
- recommendations for subgrade preparation, including reuse of site soil; criteria for selection, placement, and compaction of structural fill; and a discussion of the effects of weather and/or construction equipment on the native soil.
- a discussion related to expected excavation conditions for site utilities.
- recommended design criteria, including earth pressures, for retaining walls. Included is a discussion on approaches to limit settlements beneath the proposed retaining walls to within tolerable levels.
- recommended pavement sections for parking areas and access roads.
- recommendations for monitoring and testing during construction.

2.1 Site Conditions

This section provides a discussion of the general geologic setting of the project area and describes the surface and subsurface conditions observed at the project site at the time of our investigation. Interpretations of the site conditions are based on the results of our review of available information, and the results of our site reconnaissance, subsurface explorations, and laboratory testing.

2.2 General Geologic Conditions

General geologic information for the project site was obtained from the Geologic Map of King County, Washington (Booth, Troost, and Wisher 2006), published by the University of Washington. According to this geologic map, near-surface deposits in the vicinity of the project site consist of alluvial soils, recessional outwash, glacial till, and advance outwash. Soil defined as alluvium is characterized as a loose to medium dense, moderately sorted mixture of gravel and sand with varying amount of silt and clay and silty fine sand with clayey silt interbeds. Recessional outwash soils are typically described as loose to medium dense, stratified sand and gravel deposits and/or well-bedded silty sand and silty clay. Soil defined as glacial till typically consists of a dense to very dense, unsorted mixture of subrounded boulders, cobbles, gravel, and sand in a matrix of silt and clay. Advance outwash deposits typically include dense to very dense well-bedded sand and gravel.

2.3 Surface Conditions

The surface of the existing soil cap layer over the former Eastgate Landfill exhibits a generally hummocky topography with depressions and ridges that appear to promote surface drainage toward the existing stormwater management facilities. Elevations across the upper portions of the soil cap over the landfill range from 335 to about 350 ft (NAVD 1988). Vegetation across the former landfill typically consists of maintained grass and gravel pathways, with asphalt paved surfaces over the southern portion of the landfill associated with the shared entrance road, parking areas, and the former helicopter pad that is

currently used as a basketball court. Along the northern face of the landfill, the site slopes moderately down to the north toward Pond A (the existing three cell stormwater detention pond), with elevations ranging from 340 to about 300 ft. A gravel path circles Pond A, which is located near the bottom of a generally flat north-south trending valley. Moderate to steep slopes covered with heavy vegetation bound the east and west side of the valley where Pond A is located. Existing site topography is illustrated on Figures 3 and 4.

2.4 Subsurface Soil Conditions from Previous Reports

To evaluate the subsurface conditions prior to drilling, we reviewed the following reports and exploration logs:

- Groundwater Investigation, Former Eastgate Landfill, Bellevue, Washington, dated September 26, 2000, prepared by Landau Associates.
- Annual Groundwater Monitoring and Well Construction Detail Report, Former Eastgate Landfill, Bellevue, Washington, dated May 23, 2008, prepared by Landau Associates.
- Groundwater Monitoring Well Logs, dated 2007, prepared by SCS Engineers.
- Gas Probe Monitoring Well Logs, dated 2007, prepared by SCS Engineers.
- Closing Report, Geotechnical Services during Construction, Eastgate Landfill, Landfill Gas Collection System, Bellevue, Washington, dated October 29, 1986, prepared by GeoEngineers.
- Geotechnical and Environmental Studies, Bellevue Airport Site, Bellevue, Washington, dated May 28, 2002, prepared by AMEC Earth & Environmental.
- Report, Site Characterization Study, Portion of Boeing Eastgate Property, Bellevue, Washington, dated December 21, 2004, prepared by Golder Associates.
- Report, Geotechnical Engineering Services, Duct Bank Relocation, Boeing Eastgate Landfill, Bellevue, Washington, dated June 28, 2004, prepared by GeoEngineers.
- Eastgate Landfill Interim Status Report, dated April 22, 1986, prepared by Sweet, Edwards, & Associates.
- Eastgate Landfill Phase II Report, dated June 30, 1986, prepared by Sweet, Edwards, & Associates.
- Eastgate Landfill Summary Report, dated January 17, 1986, prepared by Sweet, Edwards, & Associates.
- Geotechnical Report, Parking Lot Subsidence Investigation, Boeing Computer Center, Bellevue, Washington, dated November 4, 1994, prepared by Converse Consultants NW.

Five geologic units have been previously identified at the site, in addition to the landfill solid waste materials. Previous reports have included borings for a variety of project and site features and have also included figures that show the relative position of the identified units. Approximate locations of selected borings from past studies and site work are shown on Figure 3.

2.5 Other Subsurface Information

Golder Associates (Golder) carried out a geophysical study in 2004 on the southern boundary of the landfill area along the shared entrance road for the Advanta Office Commons development located to the south of the project site (Golder 2004). Golder Associates conducted six induced polarization (IP) surveys and 10 electromagnetic (EM-31) surveys to define the limits of the landfill in this area. The approximate locations of the surveys are shown on Figure 3. Based on the results of their geophysical surveys, Golder reported that the landfill cap in the study area varied in thickness from 2 ft to 15 ft with a typical thickness of about 10 ft. Golder also reported that the landfill deposits extended to depths of up to 40 ft below ground surface (bgs) and provided their interpretation of the landfill boundary along the southern portion of the site. Golder's finding generally confirmed the subsurface soil conditions described in previous reports along the southern portion of the site.

2.6 Subsurface Conditions

Subsurface conditions at the project site were explored by Landau Associates in March 2016. The exploration program consisted of advancing 20 hollow stem auger borings for geotechnical design purposes and determination of the horizontal extent of the landfill solid waste, three test pits for pavement design purposes and 12 test pits to determine the lateral extent of landfill solid waste, and nine hand auger borings for design of pavements and picnic structure foundations in the northwest area at the approximate locations illustrated on Figure 4. A discussion of field exploration procedures, together with edited logs of the exploratory borings, test pits, and hand auger borings, are presented in Appendix A. A discussion of laboratory test procedures, together with the laboratory testing program results, are presented in Appendix B.

Subsurface cross sections indicating the generalized stratigraphy across the project site were developed. The location and orientation of subsurface cross section lines are shown on the Cross Section Alignment Plan (Figure 5), and the subsurface cross sections are presented on Figures 6A through 6F. The extrapolation of subsurface conditions between exploration locations is for illustrative purposes only; actual conditions between explorations may vary from those shown. The exploration logs presented in Appendices A and C provide more detail relative to subsurface conditions observed at specific locations and depths.

Based on the results of the field exploration program and our review of available geologic information and previous geotechnical reports, the site geotechnical condition are summarized below in order of increasing depth from the ground surface.

- Soil Fill Soil fill overlies most of the developed areas of the site and also is present as the soil cap layer over the underlying landfill area. The soil fill generally consists of silty, fine to medium sand with occasional fine gravel. The thickness of the soil fill over the landfill solid waste was typically reported to vary from about 2 to 19 ft across the site.
- Landfill Solid Waste The solid waste fill material below the surficial soil fill generally consists of a mixture of soil and municipal solid waste including brick, timber, asphalt, wood, paper,

metal, plastic, glass and concrete. The solid waste was landfilled between 1951 and 1964 (LAI 2000), so the putrescible portions of the waste would likely be in an advanced state of decay or not present. The solid waste material varies in thickness and was generally encountered to depths of about 2 to 42 ft bgs across the site.

- Alluvium/Recessional outwash Alluvium and recessional outwash underlies the fill materials, and is typically an unconsolidated silty sand with clayey silt interbeds and varying amounts of gravel that underlies the northern area and forms the upper side slopes of the former landfill. The maximum identified thickness of alluvium was 12 ft. The top of the alluvium/recessional outwash is interpreted to be the pre-development ground surface.
- **Glacial Till** The glacial till is typically a very dense, silty sand containing variable amounts of fine to medium gravel and scattered cobbles. Glacial till was observed to be discontinuous at the site, generally below the southern bottom and side slopes of the landfill and, where encountered in borings, ranged from about 9 to 42 ft thick. It was interpreted to be only sporadically present in the vicinity of detention Pond A.
- Advance Outwash Advance outwash encountered below the glacial till and alluvium is typically a dense, slightly silty to silty, fine to medium sand with minor amounts of gravel. Silt lenses were commonly encountered within the advance outwash deposits. The maximum encountered thickness of advance outwash was greater than 37 ft.
- Lacustrine Deposits Lacustrine deposits underlie the advance outwash unit and apparently becomes finer-grained with depth. The upper portion consists of interbedded sand and silt and the lower portion consists of silt interbedded with thinly laminated sand and silty sand. The lower limit of this unit is below the depth of exploratory borings advanced at the site to date.

The specific conditions and some of the proposed park features are discussed in the following paragraphs.

2.6.1 Sport Fields and Main Park Area within the Former Eastgate Landfill Boundary

Borings B-1-16 through B-3-16, B-6-16 through B-11-16, and B-13-16 through B-16-16 were advanced at strategic locations throughout the site of the former Eastgate Landfill. The borings were advanced to depths ranging from 15 to 56.5 feet bgs. Throughout our explorations, we encountered 2 to 15 ft of fill consisting of very loose to medium dense, very silty to silty sand with varying amounts of gravel, organics, and construction debris and dense to very dense silty, sandy gravel with varying amounts of organics and construction debris to depths that we interpreted to be existing landfill cover soil. Below the fill we encountered landfill solid waste deposits consisting of a mixture of soil and municipal solid waste including brick, timber, asphalt, wood, paper, metal, plastic, glass, and concrete to depths ranging from 2 to 36 ft bgs. Glacial till was encountered below the landfill solid waste deposits throughout the remaining depth explored in borings B-1-16, B-3-16, B-8-16, B-9-16, B-13-16, B-14-16, B-15-16, and B-16-16. Glacial till was generally observed to consist of dense to very dense, silty to very silty sand with gravel. Advance outwash was encountered below the landfill solid waste deposits throughout the remaining depth explored in borings B-2-16, B-6-16, B-7-16, and B-11-16. Advance outwash was generally observed to consist of very loose to dense silty sand with gravel.

2.6.2 Northeast Sport Field outside the Former Eastgate Landfill Boundary

Borings B-4-16, B-5-16, B-17-16, and test pit TP-12-16 were advanced at strategic locations outside the boundary of the former Eastgate Landfill in the northeast sport field area. The borings were advanced to depths ranging from 26.5 to 31.5 ft bgs and the test pit to a depth of 9.5 ft bgs. Boring B-4-16 encountered medium dense silty sand with gravel that we interpreted to be fill overlying glacial till comprised of very silty, gravelly sand to the full depth explored. In boring B-5-16, we encountered 1 inch of asphalt pavement overlying fill consisting of medium dense gravelly sand with trace silt to about 7.5 ft bgs overlying very dense, very silty sand with gravel interpreted to be glacial till. Boring B-17-16 encountered advance outwash consisting of dense to very dense, very silty sand with gravel to about 25 ft bgs overlying glacial till consisting of very dense silty sand with gravel. Test pit TP-12-16 encountered 5.5 ft of fill consisting of loose to medium dense silty to gravelly sand with varying amounts of organics, overlying 2.5 ft of advance outwash consisting of medium dense to dense gravelly sand with trace silt and glacial till consisting of very dense silty gravelly sand to the full depth explored.

2.6.3 Parking Areas

Test pits TP-1-16 and TP-2-16 were advanced at strategic locations outside the boundary of the former Eastgate Landfill in the vicinity of the proposed parking area on the east side of the site and borings B-10-16, B-12-16, B-19-16 and B-20-16 were advanced in the vicinity of the proposed parking area on the west side of the site. The test pits were advanced to depths ranging from 4 to 5 ft bgs while the borings were advanced to depths ranging from 6.5 to 31.5 ft bgs.

Test pits TP-1-16 and TP-2-16 advanced in the east side parking area generally encountered 0.6 ft of topsoil overlying 1 to 3.5 ft of fill consisting of loose to medium dense, silty, gravelly sand with varying amounts of construction debris and organics overlying weathered and unweathered glacial till consisting of medium dense to very dense silty gravelly sand to the full depth explored.

Borings B-10-16 and B-12-16 encountered 1.5 to 2.5 ft of medium dense to dense silty sand with gravel and silty, sandy gravel with trace construction debris that we interpreted to be fill. Underlying the fill was glacial till encountered to the full depth explored consisting of very dense, very silty sand with gravel. Boring B-19-16 encountered 5 inches of asphalt overlying loose to very dense silty sand with gravel that we interpreted to be glacial till. Boring B-20-16 encountered dense to very dense very silty sand with gravel that we interpreted to be glacial till that was encountered to the full depth explored.

2.6.4 Pond A Overlooks

Boring B-18-16 was advanced in the vicinity of the proposed pond overlook located on the west side of Pond A. The boring was advanced to a depth of 21.5 ft bgs and generally encountered 7 ft of loose to dense very silty sand with gravel that we interpreted to be fill. Underlying the fill, we encountered soft silt with iron staining and loose, very silty sand with gravel and iron staining that we interpreted to be weathered glacial till to a depth of about 15 ft bgs. Glacial till was encountered underlying the weathered glacial till consisting of very dense, very silty sand with gravel to the full depth explored.

Previous borings EL-103 (LAI 2000) and B-1-83 (Converse Consultants 1983) were advanced in the vicinity of the proposed south overlook along Pond A. These borings encountered fill mixed with some refuse at depth of 5 to 6.5 ft bgs. This layer of fill mixed with some refuse is approximately 4.5 ft thick in Boring EL-103; however, this layer was greater than 9.5 ft thick in Boring B-1-83, extending below the completion depth of that boring. The landfill perimeter test pits on the north side of the landfill area indicate that this layer of fill mixed with some refuse is isolated from the main landfill, and may be remnants of refuse that were relocated and mixed with soil during installation of the storm drain or other past site work in the Pond A area.

2.6.5 Northwest Picnic Structures and Parking Areas

Hand auger borings HA-1-16 through HA-9-16 were advanced at strategic locations outside the boundary of the former Eastgate Landfill in the vicinity of the proposed picnic structures and parking area on the northwest side of the site. The hand auger borings generally encountered about 1 ft of topsoil overlying recessional outwash consisting of medium dense to dense, silty sand with gravel to the full depth explored.

2.6.6 Limits of Landfill Solid Waste

Test pits TP-5-16 through TP-11-16, and TP 12-16 through TP-15-16 were advanced at strategic locations around the perimeter of the former Eastgate Landfill solid waste deposits to further define the boundary as shown on Figure 4. Test pits were completed by initially excavating near the line where the limits of refuse had been approximated by previous investigation using global positioning system equipment, and then extending the trench length horizontally until the actual horizontal limit of refuse was observed in the test pit. The found limit of the landfill refuse was then staked for final survey as shown on Figure 4. Selected photos of the test pits are included in Appendix A.

2.7 Geophysical Study

Global Geophysics (Global) carried out a geophysical study in January and February 2016 across the former Eastgate Landfill site underlying the majority of the proposed Park improvements. Global conducted 11 electrical resistivity tomography (ERT), induced polarization tomography (IPT), EM61 and ground penetration radar (GPR) surveys to help define the limits of the landfill in this area. An explanation of the geophysical survey methods used and results are provided in Appendix D. The approximate locations of the surveys are shown on Figure 4. Based on the results of their geophysical surveys, Global reported that the landfill cap in the study area varied in thickness from 2 ft to 15 ft. Global also reported that the landfill deposits extended to depths of up to 60 ft bgs and provided their interpretation of the landfill boundary. Global's findings generally confirmed the subsurface soil conditions found by the borings and matched well with what was described in previous reports they had prepared for utility installation along the southern portion of the site (Golder Associates 2014).

2.8 Groundwater Levels

Previous investigations at the site identified two aquifers below the site: a shallow perched aquifer and a deeper advance outwash aquifer (LAI 2015a). The shallow perched aquifer is encountered in the solid waste and alluvial materials, and in some locations, the glacial till underlying the fill and alluvial materials. The advance outwash aquifer is encountered below the glacial till layer that underlies most of the landfill area. The existing site monitoring wells and piezometer are screened in the advance outwash. Groundwater elevations calculated using water level measurements collected from each monitoring well and piezometer, and a surface water level measurement at the staff gauge in Pond A, are used to evaluate groundwater flow direction in the advance outwash aquifer. Groundwater elevation contours are plotted for each monitoring event using the measured groundwater elevations. The 2015 groundwater contours are provided in the Landau Associates Project Summary Report dated October 19, 2015 (LAI 2015b). The contours indicate the groundwater within the advance outwash aquifer has a generally easterly flow, which is consistent with flow direction that has been observed at the landfill since Landau Associates began monitoring activities in 2001. This differs from the flow within the perched aquifer (leachate) in the landfill, which generally flows to the north toward the leachate collection trench. Groundwater levels encountered in our borings at the time of drilling ranged from 15.5 to 34 ft bgs (Elevation 304 to 329) and are shown on the borings logs provided in Appendix A.

3.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the results of the field exploration, laboratory testing, and engineering analyses performed, and our understanding of the proposed Park development project, it is our opinion that the improvements proposed as part of Phase 1 of this project can be constructed at the site generally as planned. Design of the proposed improvements will need to consider the presence of compressible landfill deposits under the planned improvements which may require: 1) preloading/surcharging the proposed improvement area to pre-consolidate foundation soils prior to construction, and/or 2) using ground improvement techniques (e.g., drilled shafts, piles, stone columns, Geopiers, etc.) to reduce the settlement potential of the onsite soils. The presence of old landfill deposits will also require limiting contact and excavation of the solid waste materials, and controlling landfill gas (LFG) and leachate that continue to be produced by the landfill. Leachate production will be limited by installing a geomembrane cover over the landfill and upgrading the existing leachate collection trench to continue to discharge to the onsite sanitary sewer system. LFG will be better contained by the geomembrane cover, and will continue to be removed from the landfill area by upgrading the existing LFG extraction wells and venting system.

Conclusions and recommendations related to environmental considerations, health and safety considerations, contaminated soil handling and disposal, seismic considerations, site preparation, fill and compaction, wet weather earthwork, site settlement, preloading, underground utility installation, foundation support, pavement design, and landfill cover system are presented in the following sections.

3.1 Environmental Considerations

Contaminated soils in the form of landfill deposits are present underlying a significant portion of the site (Figures 2 through 5). Concentrations of dissolved iron, dissolved manganese, and 1,4-dichlorobenzene concentrations above screening levels were detected in water samples collected from the onsite leachate collection system. The existing leachate collection system appears to be adequately fulfilling its intended function. Water in the shallow perched aquifer that has been impacted by the landfill refuse is being captured and discharged directly to the onsite sanitary sewer line. The leachate collection system, along with Pond A, is functioning to protect downstream water quality. No exceedances of State surface water standards have been observed downstream of Pond A. Nonetheless, sampling and analysis of surface water from the leachate collection system will continue to be conducted on an annual schedule during the design phase for the Phase 1 Park development.

Further information on the groundwater monitoring and leachate collection systems and MTCA Compliance analysis can be found in LAI's Project Startup Summary Report (LAI 2015b).

3.2 Health and Safety Considerations

Excavations for the proposed improvements will likely be within compacted, clean, granular backfill, the existing cover soils overlying the landfill deposits, and/or native soils consisting of advance outwash and glacial till. However, deeper excavations extending below the existing grade may encounter potentially contaminated materials (landfill deposits) that were not encountered at shallower depths during our site investigation activities. Therefore, site excavations extending into existing site soil should be monitored for the presence of contamination. Monitoring should include visual and odor indications of contamination, as well as health and safety monitoring for LFG using a four gas explosivity and photoionization detector (PID) or similar equipment.

Due to the potential for encountering contaminated soil that was not discovered during previous site investigations, site work contractors should be required to prepare and submit a site-specific health and safety plan meeting applicable regulatory requirements prior to the start of construction. The contractor should also identify a Health and Safety Officer whose responsibility will be health and safety monitoring and oversight.

Current and previous field investigations in and around the Bellevue Airfield park site indicate that landfill deposits are present beneath portions of the site, and methane may be generated as a result of its presence and decomposition. Methane has the potential to accumulate in subsurface structures, voids, and vaults at concentrations that could pose a risk for explosion or oxygen depletion. As a result, development planning and design will need to address the potential presence of methane gas, and if present, accumulation in subsurface structures or voids.

3.3 Contaminated Soil Handling and Disposal

Environmental sampling and testing of the soil excavated and managed onsite should be planned as a part of the proposed project in the form of a soil management plan developed as part of the future Environmental Engineering Design Report (EEDR). Although there is no information suggesting contamination of the existing soil cover material, if soil is encountered during construction that visually appears to be contaminated or exhibits an odor (e.g., soil with oily residue or discoloration, visual landfill refuse, strong petroleum-like odors, groundwater with an oily sheen, etc.), the potentially impacted soil should be segregated, stored on plastic, and covered with plastic pending characterization for disposal. Soil samples should be collected from the potentially impacted soil and analyzed at an accredited laboratory for petroleum hydrocarbons and heavy metals. Additionally, if characterization indicates the presence of petroleum hydrocarbons in the heavy oil range, the soil should also be analyzed for PAHs and PCBs. If the concentration of contaminants in the soil is determined to be below the Model Toxics Control Act (MTCA Method A) concentration for unrestricted land use, the soil may be managed onsite as clean soil. If the contaminant concentrations are determined to be above MTCA Method A levels, the soil should be managed consistent with other contaminated materials identified on the site and removed for disposal at an approved offsite facility. Furthermore, if clearly contaminated soil is encountered during excavation activities, the contractor

should establish appropriate contamination reduction and exclusion zones to help prevent the spread of contaminated materials on the site.

It is important to recognize that current solid waste regulations (WAC 173-350) may significantly restrict the offsite placement of site soil that contains hazardous substances, even if the concentrations are below MTCA cleanup levels. As a result, no existing site soil should be exported from the site, except to a solid waste landfill, without first determining whether the intended use and destination are allowable under Ecology regulations.

3.4 Seismic Considerations

The following sections present our conclusions and recommendations regarding the seismic hazard risk for the site and project, including design ground motions and the results of our liquefaction assessment.

3.4.1 Ground Motions

The Pacific Northwest is seismically active and the project site could be subject to ground shaking from a moderate to major earthquake. Consequently, moderate levels of earthquake shaking should be anticipated during the design life of the proposed Park improvements. In addition, the proposed improvement should be designed to resist earthquake loading using appropriate design methodology. The recommended ground motion design parameters for both design of structures over native soils and for structures over the landfill refuse are provided below.

Earthquake ground motions were estimated using the US Seismic Design Maps from the US Geological Survey (USGS) website (USGS 2015) in accordance with the 2012 IBC. The 2012 IBC accounts for an earthquake ground motion with a 2 percent probability of exceedance in 50 years (or approximately a 2,475-year return period). The seismic parameters in the 2012 IBC are based on maps prepared by the USGS. According to the USGS, the peak horizontal acceleration at the project site is approximately 0.54 times the acceleration due to gravity (0.54g).

3.4.1.1 Structures Over Fill and Native Soils

Based on the average field standard penetration resistance (N), and according to Chapter 20 of ASCE 7, the site classifies as Site Class D. The following parameters are recommended for design of the proposed structures:

- Spectral Acceleration for short periods (S_s): 133% of gravity (1.331g)
- Spectral Acceleration for a 1-second period (S₁): 51% of gravity (0.509g)

The above values can be modified for Site Class D using 1.000 for site coefficient F_a , and 1.500 for site coefficient F_v . The design spectral response acceleration parameters can be taken as two-thirds of the maximum considered earthquake spectral response acceleration presented above. Using the above site class and design adjustments, the following design spectral acceleration parameters can be used:

- S_{DS} = 0.887
- S_{D1} = 0.509

3.4.1.2 Structures Over the Landfill Refuse

Average shear wave velocities for the landfill solid waste deposits are estimated to range between 250 and 600 ft/s (Zekkos 2014). According to Chapter 20 of ASCE 7, the site classifies as Site Class E, based on the estimated shear wave velocities for the site where underlain by landfill refuse. The following parameters are recommended for design of the proposed structures:

- Spectral Acceleration for short periods (S_s): 133% of gravity (1.329g)
- Spectral Acceleration for a 1-second period (S₁): 51% of gravity (0.509g)

The above values can be modified for Site Class E using 0.900 for site coefficient F_a , and 2.400 for site coefficient F_v . The design spectral response acceleration parameters can be taken as two-thirds of the maximum considered earthquake spectral response acceleration presented above. Using the above site class and design adjustments, the following design spectral acceleration parameters can be used:

- S_{DS} = 0.797
- S_{D1} = 0.814

Soil liquefaction is generally limited to granular soils located below the water table that are in a relatively loose, unconsolidated condition at the time of a large, nearby earthquake. The landfill solid waste and dense, glacially consolidated deposits that underlie the project site are anticipated to have a low susceptibility to soil liquefaction. Consequently, it is our opinion that no special liquefaction-related design or construction procedures will be necessary for this project.

3.5 Site Preparation

Site preparation and earthwork will include demolition and removal of some existing structures, existing utilities (including parts of the existing LFG collection system), and asphalt concrete pavement. Site preparation and earthwork will also include stripping vegetation, grading the site with cuts and fills ranging from 2 to 13 ft, respectively, and (if encountered) handling and disposal of potentially contaminated soil. Specific conclusions and recommendations related to the handling and disposal of potentially contaminated soil are provided in Section 3.3.

All existing structures, pavement, vegetation, man-made debris, and other deleterious material should be cleared and stripped from all areas to be occupied by the proposed Park improvements and areas to receive fill. Utility lines and appurtenant structures that will be abandoned under future improvements should be completely removed to a point at least 5 ft (measured horizontally) beyond the foundations of proposed structures. Excavations resulting from the removal of abandoned utilities should be backfilled in accordance with the recommendations presented in Section 3.10.5 of this report. Utility lines that will be abandoned under future buildings may be abandoned in place, provided pipes 12 inches in diameter and larger are completely filled with controlled density fill (CDF). It should be noted that large-diameter utility lines that are abandoned in place could create

obstructions for operations associated with future site development activities (e.g., building construction, site grading, etc.).

Pipes and appurtenant structures abandoned beyond the footprints of future buildings may be abandoned in place, provided pipes 12 inches in diameter and larger are completely filled with CDF. If the existing pipes are abandoned in this manner, structures such as manholes and vaults should be removed to a minimum depth of 3 ft below finish grade and the remaining portion (if any) of the excavation should be backfilled in accordance with the recommendations presented in Section 3.10.5.

Prior to placement of any structural fill to raise site grades in areas that were not previously preloaded, the exposed subgrade should be proof rolled to a dense and unyielding condition. Proof rolling should be accomplished with a fully-loaded dump truck, large self-propelled vibrating roller, or equivalent piece of equipment so that the upper 12 inches of exposed subgrade is compacted to at least 95 percent of its maximum dry density, as determined using test method ASTM International (ASTM) D 1557 (Modified Proctor). The purpose of this effort is to identify possible loose or soft soil deposits and to recompact the soil exposed during site stripping and demolition activities.

Proof rolling should be carefully observed by geotechnical personnel. Areas exhibiting significant deflection, pumping, or weaving that cannot be readily compacted should be overexcavated to firm or dense soil. Overexcavated areas should be backfilled with compacted granular material in accordance with subsequent recommendations for structural fill. During periods of wet weather, proof rolling or compaction could damage exposed subgrades. Under these conditions, a qualified geotechnical engineer should observe subgrade conditions to determine if proof rolling and compaction is feasible.

Construction in wet weather conditions may not allow proper compaction of the subgrade soils. Recommendations for wet weather earthwork are provided in Section 3.7.

3.6 Fill and Compaction

Structural fill used to raise site grades must be properly placed and compacted. In general, any suitable, non-organic, predominately granular soil may be used for fill material, including portions of the existing site fill, provided the material is properly moisture conditioned prior to placement and compaction, and the specified degree of compaction is obtained. If the existing onsite soil is to be reused for structural fill, pieces of wood or other deleterious material should be removed. Excavated site material containing topsoil, wood, trash, organic or fine-grained material, or construction debris will not be suitable for reuse as structural fill and should be placed in nonstructural areas where several inches of post-construction settlement is tolerable. Alternatively, this material could be exported from the site, provided the material is evaluated for contamination prior to removal from the site. If the material contains hazardous substances, disposal at a solid waste landfill would be required.

The suitability of any fine-grained soil excavated from the site or imported for use as compacted structural fill will depend on the gradation and moisture content of the soil when it is placed. As the amount of fines (that portion passing the US Standard No. 200 sieve) increases, the soil becomes increasingly sensitive to small changes in moisture content and adequate compaction becomes more difficult to achieve. Soil containing more than about 5 percent fines cannot consistently be compacted to a dense, non-yielding condition when the water content is greater than optimum. Optimum moisture content is the moisture content at which the greatest compacted dry density can be achieved. The moisture content of the site soil was observed to be variable. In addition, seasonal variation in the moisture content of shallow site soil should be expected.

The near-surface, onsite fill soil consists primarily of very loose to medium dense, very silty to silty sand with varying amounts of gravel and dense to very dense silty, sandy gravel. These soils will be suitable for use as structural fill under most conditions; however, the siltier portions of the fill soils are expected to be moisture sensitive. Furthermore, if the optimum moisture content of the soil is exceeded, moisture conditioning could be required. Moisture conditioning will also be required if onsite soil is obtained from excavations that encounter groundwater. The contractor should be prepared to segregate portions of the fill soils that contain organics and construction debris.

Structural fill soil should be placed in loose, horizontal lifts less than 8 to 10 inches in thickness and thoroughly compacted. All structural fill under future paved areas should be compacted to at least 95 percent of the maximum dry density, as determined using test method ASTM D 1557 (Modified Proctor). Fill placed within landscaped areas should be compacted to a minimum of 85 percent of its maximum dry density to reduce the potential for excessive settlement. Compaction criteria for trench backfill and excavations is presented in Section 3.10.5.

3.7 Wet Weather Earthwork

Some of the near-surface, onsite soil is considered to be moisture sensitive. As a result, it will be difficult to control the moisture content of these materials during periods of wet weather. If construction is accomplished during wet weather, or under wet conditions, exposed subgrades could be easily disturbed by construction equipment. In addition, stockpiles of onsite materials could become saturated and subject to erosion if not properly protected. Site preparation would be facilitated by scheduling such earthwork during the dry summer and early fall months. If fill is to be placed or earthwork is to be performed in wet weather or under wet conditions, the contractor may reduce soil disturbance by:

- Accomplishing earthwork in small sections
- Limiting construction traffic over unprotected soil
- Sloping excavated surfaces to promote runoff
- Limiting the size and type of construction equipment used
- Providing gravel "working mats" over areas of prepared subgrade

- Removing wet surficial soil prior to commencing fill placement each day
- Sealing the exposed ground surface by rolling with a smooth drum compactor or rubber-tired roller at the end of each working day
- Providing upgradient perimeter ditches or low earthen berms and using temporary sumps to collect runoff and prevent water from ponding and damaging exposed subgrades.

It may be necessary to overexcavate loose and wet surficial soil and replace it with clean, well graded sand and gravel or base-course material in paved areas. The depth of overexcavation required will depend on the condition of the soil at the time of construction, but the depth could be on the order of 6 to 12 inches. If the subgrade is particularly loose or disturbed by construction equipment during wet weather, an even thicker subbase layer or the use of a geotextile in combination with a granular base material may be needed to achieve suitable conditions for the proposed pavement sections and future buildings.

3.8 Site Settlement

The results of the current and previous subsurface exploration programs completed at the site indicate that loose fill and compressible municipal solid waste (MSW) underlie a significant portion of the project site. These soils will experience settlement during and after site grades are raised. Consequently, we recommend that any proposed underground utilities be installed after site grades have been raised and the site has been preloaded and/or improved through the use of other ground improvement techniques in order to reduce the magnitude of post-construction settlement.

Static settlement of the ground following placement of the new fill will depend on the height and width of the new fill, as well as the strength and compressibility characteristics of the underlying bearing soil. Ground settlement is anticipated to occur non-uniformly across the site due to the heterogeneous nature and variable thickness of the MSW, the presence of organic material, and the level of compaction the MSW experienced during original placement.

We estimate that the total amount of static ground settlement associated with the loading from the proposed structures in addition to the fill required to bring the site up to grade will be as much as 9 inches over a service life of 50 years. This amount of settlement is expected if no preloading or ground improvement is provided prior to construction of the Park amenities. The actual static settlements will depend on the rate of filling and the specific soil conditions beneath the new fill, which are expected to be variable across the site. Consequently, actual settlements and the time rate of settlement could potentially be greater or less than estimated herein. Preloading, as further described in Section 3.9, is therefore recommended to pre-consolidate the compressible onsite soils and landfill refuse prior to construction, and to reduce total and differential settlements beneath the proposed structures, Park improvements, and utilities to within acceptable levels.

As fill is being placed, installation and monitoring of settlement plates within the fill is recommended in order to identify the end of primary consolidation. Installation of the planned utilities and hardscaping should be deferred until the end of primary consolidation. If constructed in this manner, the majority of the differential settlement should occur prior to the installation of utilities and hardscaping.

3.9 Preloading

Preloading the landfill area of the site with granular fill is recommended to pre-consolidate the underlying compressible refuse and fill soils prior to construction in order to reduce total and differential post-construction settlements beneath the proposed park ball fields and landscape to within tolerable levels (i.e., less than about 1 to 2 inches).

The areas to be preloaded should be cleared and stripped in accordance with the recommendations in Section 3.5 prior to the preload/surcharge fill being placed. The preload/surcharge fill should consist of a predominately granular material such as sand or sand and gravel to facilitate placement and removal.

For schematic design purposes, it can be assumed that preload fill heights of up to 9 ft above proposed finished site grades will be required, with the fill heights varying with the thickness of underlying landfill solid waste deposits. The preloading program will require on the order of about 9 to 20 months to pre-consolidate the underlying soils to the point where about 95 percent of the primary settlement is achieved. For schematic design, a 2H:1V (horizontal:vertical) maximum preload side slopes may be assumed.

The specific design of the landfill preloading program will be provided in the EEDR. Depending on the height(s) of the preload fill selected, surface settlements on the order of about 7 to 8 inches are expected directly beneath the fill in the areas where underlying landfill refuse deposits are located. This expected settlement could affect the existing LFG system. The following measures could be taken to reduce the potential for affecting the operation of the LFG System and groundwater monitoring wells:

- Relocate existing LFG header pipes located beneath or adjacent to preloaded areas prior to the placement of the preload fill.
- Construct strategically placed temporary walls at the edge of the preload to limit its lateral extent and influence, if needed.
- Add well risers and flexible couplings such that the LFG system and groundwater monitoring wells can undergo the expected settlement without sustaining damage.

The preload grading plan based on the underlying refuse thickness will be provided in the EEDR.

3.10 Underground Utility Installation

Underground utilities will consist of piping for plumbing, stormwater, sanitary sewer, and electrical conduits. Underground utilities should only be installed over the landfill areas after preloading has induced 95 percent of the predicted primary settlement. The following sections provide geotechnical recommendations for design and construction of the proposed utility lines.

3.10.1 Dewatering Considerations

Depths to proposed underground utilities are currently unknown; however, they are expected to be constructed in the new structural fill or existing landfill soil cover material. While groundwater was not observed in our explorations at shallower depths in the landfill soil cover material, it is common for isolated pockets of perched groundwater to occur within more granular zones of the landfill soil cover. This type of groundwater typically results in seepage into an excavation for a period of time after it is encountered and often dissipates once the groundwater is allowed to drain into the excavation.

If groundwater is encountered in trench excavations, it is expected that pumping from sumps will be adequate to control the groundwater and remove it from the construction area to maintain a relatively dry excavation. The contractor should be responsible for the design, installation, monitoring, and maintenance of any required dewatering system(s). Prior to discharging water to King County sewer system, a disposal permit will need to be obtained from King County septage disposal program coordinator. Groundwater to be discharged to the King County sewer system must comply with the Industrial Waste Regulations of King County Code (KCC) 28.84.060. Prior to disposal of any groundwater encountered in excavations, the groundwater should be analyzed at a certified analytical laboratory for the compounds required by King County for discharge to the sanitary sewer system.

3.10.2 Trench Excavation

All trenching deeper than 4 feet bgs will require trench safety designed and approved by a professional engineer licensed in the State of Washington. Excavation for utility trenches should be in accordance with the requirements in Section 7-08 of the 2016 Washington State Department of Transportation (WSDOT) Standard Specifications for Road, Bridge and Municipal Construction (Standard Specifications; WSDOT 2016). Small to medium sized conventional construction equipment should be able to excavate the trench to typical utility trench depths. The contractor should be prepared to handle and dispose of oversized material such as cobbles and boulders. Actual trench configurations and maintenance of safe working conditions, including temporary excavation stability, should be the responsibility of the contractor, as discussed in the Site Preparation and Earthwork section of this report.

Trench boxes should provide suitable support for shallow excavations in fill or native soils, provided that settlement-sensitive structures are not situated immediately adjacent to the excavation. Trench

boxes should meet the requirements in Safety Standards for Construction Work, WAC 296-155 Part N and WAC 296-155-657.

Where a trench box is used to support excavations, one or both sides of the trench may cave against the box, especially if loose, granular soil is present. The caving may extend out on either side of the trench for a distance approximately equal to the depth of the trench. Additional bracing or sheeting may be required where the near edge of the trench will be closer than 1.5 times the trench depth to settlement-sensitive utilities or structures. When the trench box is moved, precautions should be taken to minimize disturbance to the pipe, underlying bedding materials, and surrounding soil.

If bracing is needed to support the trench walls, the temporary bracing system should be designed by a structural engineer licensed in the State of Washington, and constructed to support lateral loads exerted by the retained soil mass. It is assumed that temporary shoring would consist of steel plates with internal bracing. Temporary shoring may also be used in conjunction with sloped excavations.

3.10.3 Pipe Foundation Support

Based on conditions observed at the exploration locations and our understanding of the geologic conditions in the area, soil at anticipated trench depths are anticipated to primarily consist of new structural fill or landfill cover soils, and should provide adequate foundation support for the pipes, provided the soil remains in a relatively undisturbed condition and the trench is properly dewatered.

If the trench bottom becomes disturbed due to excavation and/or foot traffic during placement of the pipe, the trench bottom may need to be overexcavated to expose undisturbed foundation soil. Removal and replacement of unsuitable foundation material should be in accordance with Section 7-08.3(1)A of the 2016 WSDOT Standard Specifications. The overexcavation should be backfilled with suitable foundation material to provide a firm trench bottom. Foundation material should meet the requirements for Class B Foundation Material in Section 9-03.12(1)B of the 2016 WSDOT Standard Specifications, and should be thoroughly compacted to provide a firm excavation bottom.

3.10.4 Bedding and Pipe Zone Backfill

To provide uniform support of buried utility pipes, the pipe should be bedded in accordance with Section 7-08.3(1)C of the 2016 WSDOT Standard Specifications. The bedding material should extend 6 inches below the invert of the pipe. Bedding material should extend above the pipe bottom a distance of at least 15 percent of the pipe outside diameter. Pipe zone backfill for rigid pipes should meet the requirements of Section 7.08-3(3) of the 2016 WSDOT Standard Specifications. Pipe zone backfill should extend 6 inches above the crown of the pipe. Pipe bedding material and pipe zone backfill should be brought up evenly around the pipe in relatively horizontal lifts not exceeding 6 inches, and worked under the haunches of the pipe by slicing with a shovel, vibration, or other approved procedures. Pipe zone backfill should be placed in accordance with Section 7-08.3(1)C of the 2016 WSDOT Standard Specifications.

3.10.5 Trench Backfill and Compaction

Most of the subsurface soil exposed in trench excavations is expected to consist of new structural fill or landfill soil cover material. If the excavated soil cannot be used as trench backfill or if additional backfill is needed, an imported material should be used. Imported trench backfill should meet the requirements for Bank Run Gravel for Trench Backfill in Section 9-03.19 of the 2016 WSDOT Standard Specifications. If wet weather construction is anticipated, then the amount of fines should be limited to 5 percent or less based on the fraction of the material passing a US Standard ¾-inch sieve.

Backfilling of trenches should be in accordance with the requirements of Section 7-08.3(3) of the 2016 WSDOT Standard Specifications. Trench backfill should be placed in 6-inch layers and compacted to a relative density of at least 92 or 95 percent maximum dry density, depending on whether the trench is located outside or within structure footprints. Compaction testing should be in accordance with the maximum dry density, as determined using ASTM test method D1557. Flooding and/or jetting of backfill may not be used as a means to consolidate or compact trench backfill. Hand-operated compaction equipment, or other approved methods, should be used to compact the first 18 inches of trench backfill above the pipe. Heavy compaction equipment should not be used for the first 18 inches of backfill above the initial backfill.

3.11 Foundation Support

Although preloading/surcharging the site will effectively force settlement in the underlying landfill refuse prior to construction, methane gas is still being generated by the landfill refuse indicating that decomposition is still occurring, at a very low rate, which could cause future secondary settlement. Foundation support for the proposed bath house structures and water play area underground vault may be provided by a lightly loaded structural slab mat type foundation founded either on existing landfill cover soil or properly placed and compacted structural fill that is underlain by existing landfill cover soils. For foundations that are supported by structural fill, the limits of the overexcavation around the foundation should extend laterally beyond the edge of each side of the footing a distance equal to one-half the depth of the excavation below the base of the structural slab. Alternatively, overexcavation areas could be backfilled to the design footing elevation with CDF or lean concrete, or foundations may be extended to bear on dense to very dense, undisturbed native glacial soils. If CDF or lean concrete is used to backfill the overexcavation, the limits of the overexcavation do not need to extend beyond the width of the footing.

Bearing soil disturbed during foundation excavation should either be properly recompacted or removed. All soil directly below structural slabs should be compacted to at least 95 percent of maximum dry density (ASTM D1557) prior to placement of forms, reinforcing steel, and concrete. The bottom elevation of structural slabs should be founded a minimum of 18 inches below the lowest adjacent final grade.

Assuming the above foundation support criteria are satisfied, structural slab mat type foundations founded directly new structural fill or existing landfill cover soil may be designed using a maximum allowable bearing pressure of 1,500 pounds per square foot (psf) if using a rigid mat method for design, or a maximum modulus of subgrade reaction (k-value) of 125 pounds per cubic inch (pci) if using the flexible method (elastic spring model) for design.

For minor structures such as planned picnic shelters located outside of the landfill area (Figure 4), continuous or isolated spread footings founded directly on medium dense to dense native soils may be proportioned using a maximum net allowable soil bearing pressure of 1,500 psf.

The term "net allowable bearing pressure" refers to the pressure that can be imposed on the soil at foundation level resulting from the total of all dead plus live loads, exclusive of the weight of the footing or any backfill placed above the footing. The net allowable bearing pressures recommended above may be increased by one-third for transient wind or seismic loads.

Passive earth pressures that develop against the sides of building foundations in conjunction with friction developed between the base of the footings and the supporting subgrade, will resist lateral loads transmitted from the structure to its foundation. For design purposes, the passive resistance of well-compacted fill placed against walls or the sides of foundations may be considered equivalent to a fluid with a density of 300 lbs per cubic ft (pcf). The recommended value includes a safety factor of about 1.5 and is based on the assumption that the ground surface adjacent to the structure is level in the direction of movement for a distance equal to or greater than twice the embedment depth. The recommended value also assumes drained conditions that will prevent the buildup of hydrostatic pressure in the compacted fill. In design computations, the upper 12 inches of passive resistance should be neglected if the soil is not covered by floor slabs or pavement. If future plans call for the removal of the soil providing resistance, the passive resistance should not be considered.

An allowable coefficient of friction between concrete and soil of 0.35, applied to vertical dead loads only, may be used to calculate the resistance to sliding at the base of the foundation elements bearing on undisturbed native soil or well-compacted granular fill. However, if passive and frictional resistance are considered together, one-half of the recommended passive soil resistance value should be used because larger strains are required to mobilize the passive soil resistance as compared to frictional resistance. A safety factor of about 1.5 is included in the base friction design value. We do not recommend increasing the coefficient of friction to resist seismic or wind loads.

3.12 Foundation Settlement

Settlement of structural slab mat type foundations depends on foundation size and bearing pressure, as well as the strength and compressibility characteristics of the underlying soil and/or refuse. Assuming construction is accomplished as previously recommended, including preloading/surcharging the site, and for the maximum allowable soil bearing pressures recommended above, we estimate the total settlement of foundations should be less than about 1 inch and differential settlement between two adjacent load-bearing components supported on competent soil should be less than about ½ inch.

Structures that cannot withstand the anticipated settlements or require higher bearing pressures should be supported on deep foundations founded in the underlying till as outlined in Section 3.14. The soil response to applied stresses caused by structural and other loads is expected to be predominately elastic in nature, with most of the settlement occurring during construction as loads are applied.

3.13 Site Drainage

To reduce the potential for groundwater to seep into interior spaces and prevent the buildup of hydrostatic pressure against subsurface walls, we recommend that an exterior footing drain system be constructed around the perimeter of any portion of the building foundations where the interior floor elevation is lower than the exterior grade. The drain should consist of a minimum 4-inch diameter perforated pipe, surrounded by a minimum 12 inches of filtering media and sloped to carry water to a suitable collection and discharge system. The filtering media may consist of open-graded drain rock wrapped by a non-woven geotextile (such as Mirafi 140N, Synthetic Industries 351, or equivalent). The drainage backfill should contain less than 3 percent by weight passing the US Standard No. 200 sieve, based on a wet sieve analysis of that portion passing the US Standard No. 4 sieve. The invert of the footing drain pipe should be placed at approximately the same elevation as the bottom of the footing or 12 inches below the adjacent floor slab grade, whichever is deeper, so that water will not accumulate behind walls or seep through walls or floor slabs. The footing drain should discharge to an approved drain system and include cleanouts to allow periodic maintenance and inspection.

Positive surface gradients should be provided adjacent to the proposed structures to direct surface water away from the foundation and toward suitable discharge facilities. Roof drainage should not be introduced into the perimeter footing drains, but should be discharged directly to the stormwater collection system or other appropriate outlet. Pavement and sidewalk areas should be sloped and drainage gradients should be maintained to carry all surface water away from the building toward the local stormwater collection system. Surface water should not be allowed to pond and soak into the ground surface near the building during or after construction.

3.14 Deep Foundations

Structures that cannot withstand the anticipated settlements or require higher bearing pressures should be supported on deep foundations extending through the landfill deposits and into the underlying glacial till or advance outwash deposits. Deep foundations may include the use of drilled shafts, augercast piles, or driven piles. Under no circumstances should deep foundations tips terminate in the landfill solid waste deposits.

Due to the non-uniform thickness of the landfill solid waste deposits, and if deep foundations are required for the project, Landau Associates will provide specific geotechnical recommendations for deep foundations as structural design details are developed. At a minimum, we require anticipated structural loading requirements, locations of structures and foundation elements, and type of deep foundations to be used.

Installation of drilled shafts or augercast piles can be performed with conventional drill rigs and equipment. Holes advanced for drilled shafts may be susceptible to caving and casing may be required to keep the hole open. In the event that groundwater is encountered, the concrete should be tremied to the bottom of the hole and poured from the bottom up displacing the groundwater out of the top of the hole. Groundwater expelled from the hole will need to be disposed of as described in Section 3.10.1 of this report. Landfill solid waste cuttings generated as a result of drilling operations will need to be disposed of as described in Section 3.3 of this report.

Installation of driven piles using a vibratory hammer will produce ground vibration in the vicinity of the pile installation. While unlikely, ground vibrations associated with installation of driven piles could potentially cause some damage to nearby structures. Ground vibrations could also result in the densification of loose soil and some settlement of the ground surface. Ground vibrations producing densification and settlement are dependent on a complex combination of factors, including energy and amplitude of the vibratory hammer, number of repetitions, soil properties, pile length, location of the water table, type of pile installation, and distance from the pile. The pile foundation axial and lateral capacity can be influenced by the equipment and construction procedures, and the quality of construction is greatly influenced by the experience of the foundation contractor.

3.15 Sport Field Lighting and Luminaire Foundations

According to preliminary plans provided by Walker Macy, luminaires are planned in the parking areas and throughout the Park and along walking areas. Stadium style light standards are planned for illumination of the sports fields.

3.15.1 Luminaire Foundations

Luminaires are planned in the parking areas and throughout the Park and along walking areas. We anticipate that the luminaries will be designed in general accordance with the WSDOT design method. Based on the results of our field exploration, laboratory testing, and engineering analyses, it is our opinion that new luminaries can be supported on drilled shaft foundations. The drilled shafts should be embedded sufficiently to resist lateral forces and the resulting overturning moments.

We anticipate that the luminaire foundations will be founded in properly placed and compacted structural fill overlying existing or recompacted landfill soil cover material. Based on these observations, and assuming the proposed luminaire foundations conform to WSDOT standards for design, we recommend using an allowable lateral bearing stress of 1,500 psf for design of the proposed luminaire standard foundations. Using WSDOT Standard Plan J-28.30-03, we recommend

that a Type B foundation (8-foot long drilled shaft) be used. The WSDOT Standard foundation can be used on level ground and on slopes not exceeding 2H:1V.

Should the luminaries not meet WSDOT standards for design, a special foundation design will be required using the Broms Method as recommended in the 2015 WSDOT Geotechnical Design Manual (WSDOT 2015a) and specified in the 2001 AASHTO Standard Specifications for Structural Support for Highway Signs, Luminaires, and Traffic Signals. An allowable lateral bearing stress of 1,500 psf should be used when applying the Broms method to foundation design for luminaries.

If the bottom of the luminaire foundations encounter landfill solid waste, the foundations should be constructed in accordance with Method 2 as shown on WSDOT Standard Plan J-28.30-03.

3.15.2 Sport Field Lighting Foundations

The sports field light systems are expected to experience relatively high lateral loads requiring deep foundations possibly extending into the underlying landfill solid waste deposits, which exhibit very low lateral resistance. Due to these factors, a special foundation design will be required using the Broms Method as recommended in the 2015 WSDOT Geotechnical Design Manual and specified in the 2001 AASHTO Standard Specifications for Structural Support for Highway Signs, Luminaires, and Traffic Signals. The sport field light standards are planned along the north and south side of Sport Field 1 and on the northwest and southeast sides of Sport Field 2. An allowable lateral bearing stress as shown in the table below should be used when applying the Broms Method to foundation design for sport field lighting foundations. Elevations and thicknesses of the soil layers at the proposed field lighting locations are shown on Figure 6B.

Soil Type	Allowable Lateral Bearing Stress, psf	
New Structural Fill	2,500	
Existing Landfill Cover Soil	1,500	
Landfill Solid Waste	750	
Glacial Till / Advance Outwash	3,000	

Under no circumstances should the sports field light system foundation bottoms be founded in the landfill solid waste deposits underlying the site. We recommend that all sport field lighting foundations extend through the landfill deposits and into the underlying glacial till or advance outwash.

3.16 Retaining Walls

Preliminary plans provided by Walker Macy indicate that retaining walls are planned to consist of gabions or cast in place (CIP) concrete walls. Gabions and CIP walls are considered to be a feasible wall

type for both cut and fill retaining walls planned throughout the park, provided that sufficient space is available to accommodate temporary construction slopes. CIP walls are generally constructed with ready-mix concrete and steel reinforcement placed into removable forms erected on site. Gabions are typically made of stacked stone-filled welded wire baskets. Gabion walls are usually battered (angled back towards the slope), or stepped back with the slope, rather than stacked vertically. The combined weight of the gabions or CIP wall is utilized to resist the lateral earth pressure imposed by the retained soil.

3.16.1.1 Retaining Wall Subgrade Preparation

Based on the results of our explorations and the site topography, CIP concrete retaining walls will likely bear on new structural fill or existing landfill cover soil within the landfill area or loose to medium dense native soils outside the landfill area.

Upon reaching the foundation-bearing surface, the wall subgrade should be checked for the presence of loose to medium dense undocumented fill present over the glacial till. If loose fill or loose native deposits are encountered at the foundation-bearing level, we recommend that the loose soils be removed to a maximum depth of 24 inches from beneath the foundation-bearing surface and be scarified, moisture-conditioned to near optimum moisture, and recompacted in accordance with the recommendations in Sections 3.6. The width of the over-excavation should extend at least 2 ft horizontally beyond the outside edge of the facing units and the length of reinforcement. The excavated unsuitable soil should be replaced with Class B Gravel Backfill for Foundations in accordance scarifications.

If the foundation-bearing soil is composed of new structural fill, medium dense to dense landfill soil cover material, or medium dense to dense native soils, the need for extensive over-excavation, moisture conditioning, and recompaction is not anticipated, although localized subgrade preparation activities may be needed.

All prepared foundation-bearing surfaces should be free of any loose soil and water. Prepared footing subgrades should be observed by a qualified geotechnical or civil engineer to check that suitable bearing soils are present.

3.16.1.2 Retaining Wall Embedment

The minimum embedment depth (distance from the ground surface at the face of the blocks to the top of the leveling pad shall be based on bearing resistance, settlement, and stability requirements. At a minimum, the embedment shall be the maximum of 2 ft or the value provided in the following table.

Slope in Front of Wall	Minimum Embedment Depth (ft)
Horizontal	2
4H:1V	H/10
3H:1V	H/10
2H:1V	H/7
1½H:1V	H/5

Embedment Depth for CIP and Gabion Walls on Slopes

3.16.1.3 Lateral Earth Pressures

The CIP and gabions wall must be designed to resist active lateral earth pressures. The use of active lateral earth pressures assumes that sufficient deformation (0.1 to 0.2 percent of the wall height) of the soil behind the wall could occur to develop an active earth pressure. This lateral deformation is likely to be accompanied by some vertical settlement, which could be up to about 0.05 percent of the wall height.

We recommend that non-restrained (yielding) walls with level backfill under drained conditions be designed for an equivalent fluid density of 35 pcf for active soil conditions. Nonyielding (restrained at the top) walls with level backfill under drained conditions should be designed for an equivalent fluid density of 55 pcf for at-rest conditions. For undrained conditions, yielding walls with level backfill should be designed to resist an equivalent fluid density of 80 pcf. Nonyielding walls with level backfill under undrained conditions should be designed for an equivalent fluid density of 90 pcf. The equivalent fluid densities recommended for use under undrained conditions include hydrostatic pressure.

The above recommendations regarding active and at-rest earth pressures assume that the backfill placed against the below-grade walls will consist of properly compacted structural fill, and no adjacent surcharge loads due to traffic, staging areas, soil stockpiles, etc. If the subsurface walls will be subjected to the influence of surcharge loading within a horizontal distance equal to or less than the height of the walls, the walls should be designed for the additional horizontal pressure. For rigid walls, a uniformly distributed lateral pressure of 0.44 times the surcharge pressure should be included. For walls free to rotate during loading, a uniformly distributed lateral pressure of 0.28 times the surcharge pressure should be included. A minimum surcharge pressure of 250 psf should be assumed when estimating the additional load on retaining walls adjacent to parking areas, traveled paths for maintenance vehicles, and trafficked areas during construction.

Dynamic lateral earth pressures should be included in the design of below grade walls. A lateral pressure distribution of 8H (H is the vertical height of the wall in feet) should be added to the static lateral earth pressures for all non-restrained (yielding) walls with a level backslope. The recommended lateral earth pressure assumes that the wall will be free to rotate and translate during a strong motion

earthquake. A lateral pressure distribution of 17H should be added to the static lateral earth pressures for all restrained (non-yielding) walls with a level backslope. The recommended lateral pressure assumes that the wall is restrained against rotation and translation during a strong motion earthquake.

3.16.1.4 Retaining Wall Allowable Bearing Capacity and Foundation Settlement

Continuous spread footings may be proportioned using an allowable bearing pressure (maximum bearing at the foundation level, which will not lead to a bearing capacity failure, global instability, or excessive settlement) of 1,500 psf, provided the following conditions are met:

- Footings are constructed on new structural fill, medium dense to dense landfill soil cover, or medium dense to dense native soils
- Depth of embedment is equal to at least 2 ft
- Horizontal bench in front of the wall extends at least 4 ft from the toe of the wall.

Settlement of shallow foundations depends on the foundation size and bearing pressure, as well as the strength and compressibility characteristics of the underlying bearing soil. Assuming the foundation for structural earth walls is situated on undisturbed glacially consolidated soils or on a properly prepared subgrade located within existing landfill cover soil or fill, has an effective footing width of 5 ft or less, and has a bearing pressure of 1,500 psf or less, we estimate that the settlement of the retaining wall footings will be less than 1 inch provided the recommendations for the placement and compaction of structural fill and preloading are followed. Differential settlement between two points spaced 100 ft away along the length of the wall will be ½ inch or less. Distortion due to differential settlement along the length of the wall should be less than 1/300 (ft/ft). Most of the settlement will occur during construction. Post-construction settlements should be negligible.

3.16.1.5 Wall Backfill and Drainage Considerations

Free-draining sand and gravel material, meeting the requirements for Gravel Backfill for Geosynthetic Retaining Walls, in Section 9-03.14(4) of the 2016 WSDOT Standard Specifications, should be used as retaining wall backfill. Backfill should be compacted in accordance with Section 3.6. To avoid overstressing of the wall during placement and compaction, backfill placed within 3 ft of the wall face should be compacted to between 90 and 92 percent of the maximum dry density as determined by Section 2-03.3(14)D of the 2016 WSDOT Standard Specifications or by the ASTM D1557 test procedure.

Underdrain pipe for gravity walls should be 6-inch-diameter and conform to Section 9-05.2 of the 2016 WSDOT Standard Specifications. The pipe should be placed with the perforations downward. The pipe should be placed in a minimum 12-inch-thick envelope of gravel meeting the requirements for Gravel Backfill for Drains in Section 9-03.12(4) of the 2016 WSDOT Standard Specifications. The drain gravel should completely surround the perforated drainpipe and be completely surrounded by a non-woven geotextile material with a minimum 12-inch overlap. The geotextile should meet the

requirements for Moderate Survivability in Table 1 and for Class B in Table 2 of Section 9-33 of the 2016 WSDOT Standard Specifications. The top of the perforated pipe should be no higher than the top of the adjacent footing. The drain line should discharge into the storm drainage system, or an approved location.

To reduce the possibility of water ponding and infiltrating into the subsurface behind retaining walls, the adjacent ground surface behind the wall should be sloped to promote runoff away from the top of the wall. Alternatively, a line brow ditch could be constructed along the top of the wall to collect surface water runoff and route it to the storm drain system.

3.17 Pavement Design

The pavement section recommendations provided herein assume that the access roadways and parking lot subgrade will be prepared in accordance with the recommendations provided in Sections 3.5 and 3.6 of this report. The pavement section recommendations are also based on assumed traffic loading for parking lots ranging from about 24 to 54 stalls, the results of our field explorations, and an assumed 20-year performance period. Design pavement sections were determined using the 1993 American Association of State Highway and Transportation Officials (AASHTO) design method and procedures recommended in the WSDOT Pavement Policy dated June 2015.

3.17.1 Roadbed Soil Resilient Modulus

Based on the soils encountered in our borings, test pits, and hand auger explorations, subgrade soils will likely consist of silty sand with gravel comprising existing landfill soil cover materials or native advance outwash deposits. These soils correlate to "average" quality subgrade based on information obtained from the WSDOT Pavement Policy with an average resilient modulus of about 10,000 pounds per square inch (psi). A resilient modulus correlates to a CBR of about 11 using correlations by AASHTO (AASHTO 1993) and WSDOT (WSDOT 2015).

3.17.2 Traffic Loading Information

We anticipate that the drive and parking areas will consist primarily of light passenger cars and trucks making several passes throughout the day, seven days per week. Heavier maintenance vehicles, busses, and delivery trucks my occasionally pass over the paved areas depending on Park usage. Based on preliminary project drawings, we understand that the east parking area will have 54 stalls, the west parking area will have 43 stalls, and the northwest parking area will have 24 stalls.

3.17.3 Pavement Sections

Utilizing WSDOT and AASHTO design methodology (AASHTO 1993) for low volume pavement design, the following pavement section recommendations were developed.

In parking areas expected to receive less than 1,000 vehicles per day (light duty), we recommend the following construction sequence and surfacing for the proposed parking lot.

- Grade the parking area to final subgrade, scarify the subgrade to a depth of 1 ft if cut into existing landfill soil cover, and compact the subgrade soil to at least 95 percent maximum dry density in accordance with Section 2-03.3(14)D of the 2016 WSDOT Standard Specifications
- 2. Place a minimum of 4 inches of CSBC and compact to at least 95 percent maximum dry density in accordance with Section 2-03.3(14)D of the 2016 WSDOT Standard Specifications
- 3. Place a minimum of 3 inches of hot mix asphalt (HMA) in one lift. If a thicker HMA pavement is desired, the asphalt should be placed in multiple lifts not less than 1.5 inches in thickness and no thicker than 3 inches.

In parking areas expected to receive more than 1,000 vehicles per day and less than 5,000 vehicles per day (heavy duty) or fire/emergency vehicle access lanes and areas to receive bus or heavy truck traffic, we recommend the following construction sequence and surfacing for the proposed parking lot.

- Grade the parking area to final subgrade, scarify the subgrade to a depth of 1 ft if cut into existing landfill soil cover, and compact the subgrade soil to at least 95 percent maximum dry density in accordance with Section 2-03.3(14)D of the 2016 WSDOT Standard Specifications
- 2. Place a minimum of 6 inches of CSBC and compact to at least 95 percent maximum dry density in accordance with Section 2-03.3(14)D of the 2016 WSDOT Standard Specifications
- 3. Place a minimum of 4 inches of hot mix asphalt (HMA) in two lifts. The asphalt should be placed in multiple lifts not less than 1.5 inches in thickness and no thicker than 3 inches.

The HMA should consist of Class ½-inch PG 64-22 based on the WSDOT Pavement Policy, and meet the requirements in Section 5-04 of the 2016 WSDOT Standard Specifications. The CSBC should meet the gradation requirements in Section 9-03.9(3) of the 2016 WSDOT Standard Specifications. The CSBC should be placed and compacted in accordance with Section 4-04 of the 2016 WSDOT Standard Specifications. If used, the gravel base should meet the gradation requirements in Section 9-03.10 of the 2016 WSDOT Standard Specifications. The gravel base should be placed and compacted in accordance with Section 4-04.3 of the 2016 WSDOT Standard Specifications.

3.17.4 Pavement Subgrade Preparation

Prior to placement of the crushed surfacing base, the prepared subgrade for new surfacing or pavement sections should be compacted to at least 95 percent of its maximum dry density and proof-rolled in the presence of a qualified geotechnical engineer to check for the presence of soft, loose, and/or disturbed areas. If any soft, loose, and/or disturbed areas are revealed during proof-rolling, these areas should be moisture conditioned and recompacted to the required density. Alternatively,
areas of soft, loose, and/or disturbed soil could be completely removed and replaced with Gravel Borrow meeting the requirements in Section 9-03.14(1) of the 2016 WSDOT Standard Specifications, and compacted to the required density. Crushed surfacing material should meet the requirements in Section 9-03.9(3) of the 2016 WSDOT Standard Specifications. Gravel base and crushed surfacing should be compacted in accordance with Section 4-04.3(5) of the 2016 WSDOT Standard Specifications. The maximum dry density and optimum moisture content may also be determined by the ASTM D 1557 test procedure (Modified Proctor).

3.18 Infiltration

Infiltration of stormwater will likely be feasible in portions of the site underlain by recessional outwash and possibly fill as these soils will provide more favorable infiltration characteristics. These areas are generally located on the northern area of the site. Areas underlain by glacial till and advance outwash deposits will likely not be favorable for infiltration of stormwater due to their relatively low infiltration characteristics. If the design team opts to include infiltration to manage stormwater, an additional boring will likely be required at the location of each infiltration facility to determine the depth to groundwater and impermeable surface (i.e. glacial till). Additionally, a pilot infiltration test (PIT) or single ring percolation test at the proposed bottom elevation of the infiltration facility will be required at each proposed infiltration facility to determine long term infiltration rates in accordance with the 2016 King County Surface Water Design Manual.

3.19 Cover System

The former Eastgate Landfill located below a portion of the proposed Park development will require a cover system which meets the requirements of the Ecology Minimum Functional Standards for Solid Waste Handling (MFS; Chapter 173-304 WAC). These regulations are the applicable or relevant and appropriate requirements (ARARs) for the site and contain typical closure requirements that are relevant based on the landfill closure dates and waste disposal history of the former Eastgate Landfill. The current refuse regulations, Criteria for Municipal Solid Waste Landfills (Chapter 173-351 WAC), are not applicable for the site because the current solid waste regulations are specifically applicable regulations for landfills that stopped accepting waste after October 9, 1991 (WAC 173-351-010[2][b]).

Per WAC 173-304-460 (3)(e) closure requirements, the landfill cover system shall consist of:

- 1. At least two feet of 1 x 10⁻⁶ cm/sec or lower permeability soil or equivalent shall be placed upon the final lifts. Artificial liners may replace soil covers provided that a minimum of fifty mils thickness is used;
- 2. The grade of surface slopes shall not be less than two percent, nor the grade of side slopes more than 33 percent; and
- 3. Final cover of at least 6 inches of topsoil be placed over the soil cover and seeded with grass, other shallow rooted vegetation or other native vegetation.

In addition to these MFS, the landfill cover system will be required to accommodate ballfields and buildings that are to be used by the general public. These end-use considerations will require additional design cover system elements to protect the public health and safety, including a landfill gas collection and control layer and a geogrid layer to help mitigate potential differential settlement. From the bottom up, the landfill cover system is therefore expected to consist of:

- Cut or fill of the existing soil cover material to the desired subgrade elevation
- Geogrid layer (embedded between subgrade and sand and gravel layer above)
- Sand and gravel layer six-inch thick to anchor geogrid
- Landfill gas collection and removal geocomposite layer (typically 200-mil thickness)
- Geosynthetic clay liner (GCL) (typically 100 to 150 mil thickness)
- Geomembrane liner (typically 40-mil thickness)
- Drainage layer geocomposite (typically 200-mil thickness)
- Minimum 2-foot thickness of landscape fill and/or synthetic ballfield surface layers. This depth of cover soil should be adequate to allow for evapotranspiration in natural landscape areas, thickness for synthetic ballfield layers and drainage pipes, and be thick enough to prevent penetration by incidental public activity or burrowing animals.

Combined together, the geosynthetic (geogrid, geocomposites, GCL, and geomembrane) portions of the landfill cover systems will be less than 1 inch thick. The sand and gravel layer and landscaping layer, however, will comprise the majority of the minimum 2-1/2-foot thick landfill cover system on the prepared subgrade. The above landfill cover section should be considered for the schematic design considerations. Specific design of the landfill cover system will be provided in the EEDR. Detailed construction drawings and specifications will be prepared to outline how the landfill cover system will be constructed. General construction considerations are provided in this section.

Per Section 3.9, the entire landfill footprint area will be preloaded/surcharges with soil to a design thickness in order to consolidate the underlying refuse. The settlement will be monitored until the settlement reaches 95 percent of primary settlement which is anticipated to require 9 to 20 months of loading. Once the majority of primary settlement is complete, the preload soil will be removed as necessary for site grading to the design subgrade of the final landfill cover system. The preload fill will need to be placed so that access will be allowed to the landfill gas system and monitoring wells, extending wells with risers, as necessary.

The landfill cover system will then be constructed in layers under the direction and observations of a geotechnical construction quality assurance (CQA) firm working on behalf of the City in order to verify that the cover system layers are constructed and tested according to the construction drawings and specifications. Each layer should be approved before the layer above it is constructed.

4.0 REVIEW OF DOCUMENTS AND CONSTRUCTION OBSERVATIONS

Landau Associates recommends that a geotechnical engineer familiar with the project design review the earthwork portions of the design drawings and specifications. The purpose of the review is to verify that the recommendations presented in this report have been properly interpreted and implemented in the design and specifications.

We recommend that geotechnical and environmental construction observation, testing, and consultation services be provided during trench excavation, fill placement and compaction, subgrade preparation, and other geotechnical related activities. We also recommend that periodic field density testing be performed to verify that an appropriate degree of compaction is obtained. The purpose of these services would be to observe compliance with the design concepts, specifications, and recommendations of this report, and, in the event subsurface conditions differ from those anticipated before the start of construction, provide revised recommendations appropriate to the conditions revealed during construction. Landau Associates would be pleased to provide these services.

5.0 USE OF THIS REPORT

This geotechnical engineering report has been prepared for the exclusive use of Walker Macy and the City of Bellevue for specific application to the proposed Bellevue Airfield Park development at the site of the former Eastgate Landfill in Bellevue, Washington. No other party is entitled to rely on the information included in this document without the express written consent of Landau Associates. Further, the reuse of information provided herein for extensions of the project or for any other project, without review and authorization by Landau Associates, shall be at the user's sole risk. Landau Associates warrants that within the limitations of scope, schedule, and budget, our services have been provided in a manner consistent with that level of care and skill ordinarily exercised by members of the profession currently practicing in the same locality under similar conditions as this project. We make no other warranty, either express or implied.

CE/KWW/DAP/rgm

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4/14/2016 NAD 1983 StatePlane Washington North FIPS 4601 Feet G:\Projects\1548\001\010\002\Geotech Report\F01 VicinityMap.mxd





















APPENDIX A

Boring Logs and Test Pit Photographs

		Soil	Classifi	ication Sys	stem		
	MAJOR DIVISIONS		GRAPHI SYMBO	C LETTER L SYMBOL ⁽¹⁾	DE	TYPICAL SCRIPTIONS ⁽²⁾⁽³⁾	
COARSE-GRAINED SOIL (More than 50% of material is larger than No. 200 sieve size)	GRAVEL AND GRAVELLY SOIL	CLEAN GRAVEL		GW	Well-graded gra	vel; gravel/sand mixture(s); little or no	fines
		(Little or no fines)		GP	Poorly graded g	ravel; gravel/sand mixture(s); little or	no fines
	(More than 50% of coarse fraction retained on No. 4 sieve)	GRAVEL WITH FINES (Appreciable amount of fines)	PBPBP	GM	Silty gravel; grav	vel/sand/silt mixture(s)	
			11/	GC	Clayey gravel; g	ravel/sand/clay mixture(s)	
	SAND AND	CLEAN SAND		SW	Well-graded sar	Well-graded sand; gravelly sand; little or no fines	
	SANDY SOIL	(Little or no fines)		SP	Poorly graded s	and; gravelly sand; little or no fines	
	(More than 50% of coarse fraction passed through No. 4 sieve)	SAND WITH FINES (Appreciable amount of fines)	SM		Silty sand; sand/silt mixture(s)		
			11/1	sc	Clayey sand; sa	nd/clay mixture(s)	
			MITT	ML	Inorganic silt an	d very fine sand; rock flour; silty or cla	ayey fine
TINE-GRAINED SOII (More than 50% of material is smaller than No. 200 sieve size)	SILT AND CLAY			CL	Inorganic clay of low to medium plasticity; gravelly clay; s		ay; sandy
	(Liquid limit less than 50)			OL	Organic silt; organic, silty clay of low plasticity		
				MH	Inorganic silt: micaceous or diatomaceous fine sand		
	SILT AND CLAY (Liquid limit greater than 50)			СН	Inorganic clay of high plasticity; fat clay		
				OH	Organic clay of medium to high plasticity: organic silt		
				PT	Peat: humus: swamp soil with high provide ontent		
	THORETO		<u></u>				
OTHER MATERIALS			GRAPHI SYMBO	C LETTER	TYPICAL DESCRIPTIONS		
PAVEMENT			×///×//	AC or PC	Asphalt concrete pavement or Portland cement pavement		
ROCK				RK	Rock (See Rock Classification)		
WOOD				WD	Wood, lumber, wood chips		
DEBRIS					Construction debris, garbage		
 Soil (Vis the Soil def 4. Soil 	descriptions are based of sual-Manual Procedure), Standard Test Method fo description terminology i ined as follows: Primary (Secondary C Additional C	on the general approach pre- butlined in ASTM D 2488. W or Classification of Soils for E is based on visual estimates Constituent: > 50 onstituents: > 30% and ≤ 50 > 15% and ≤ 30 onstituents: > 5% and ≤ 110 ≤ 50 escriptions are based on juc	sented in the /here labora Engineering l (in the abse)% - "GRAVI 0% - "very gr 0% - "very gr 1% - "very gr 5% - "with gr 5% - "with tra doement usir	 Standard Practic tory index testing Purposes, as outlight once of laboratory "SAND," "SIL avelly," "very sandy," "silty," avel," "with sandy," to gravel," "with sandy," 	e for Description a has been conduct ined in ASTM D 24 test data) of the p .T," "CLAY," etc. dy," "very silty," etc ' etc. ' with silt," etc. trace sand," "with	and Identification of Soils ed, soil classifications are based on 187. ercentages of each soil type and is c. trace silt," etc., or not noted. ation blow counts. drilling or	
exc	avating conditions, field t	ests, and laboratory tests, a	s appropriate	e.		, G	
	Drilling a	ey (Field and Lab Test Data			
Codo	SAMPLER TYPE	NUMBER &	INTERVAL		Description		
Code Description a 3.25-inch O.D., 2.42-inch I.D. Split Spoon b 2.00-inch O.D., 1.50-inch I.D. Split Spoon c Shelby Tube d Grab Sample e Single-Tube Core Barrel f Double-Tube Core Barrel g 2.50-inch O.D., 2.00-inch I.D. WSDOT h 3.00-inch O.D., 2.375-inch I.D. Mod. California i Other - See text if applicable 1 300-lb Hammer, 30-inch Drop 2 140.lb Hammer, 30-inch Drop				ample Identification Number — Recovery Depth Interval] ← Sample Depth Interval -Portion of Sample Retained for Archive or Analysis		Description Pocket Penetrometer, tsf Torvane, tsf Photoionization Detector VOC screening, ppr Moisture Content, % Dry Density, pcf Material smaller than No. 200 sieve, % Grain Size - See separate figure for data Atterberg Limits - See separate figure for data Other Geotechnical Testing Chemical Analysis	
3 Pushed United Stop Groundwater level at time of drilling (ATD)							
4 Vibr 5 Oth	ocore (Rotosonic/Geopro er - See text if applicable	be) <u> </u>	proximate w	ater level at time	other than ATD		
LANI ASS	DAU OCIATES	Bellevue Airfield Pa Bellevue, WA	ark	Soil Classification System and Key			
















































































Test Pit Photographs



Contact Cover Soil/Landfill Debris and Native Glacial Till Soils



Contact Cover Soil/Landfill Debris and Native Glacial Till Soils



Test Pit – TP-1-16



Contact of Cover Soil and Native Glacial Till Soils



Contact of Cover Soil and Native Glacial Till Soils



Test Pit – TP 2-16



Landfill Debris and Contact with Native Outwash Soils



Landfill Debris and Contact with Native Outwash Gravel Soils



Test Pit – TP-5-16



Seepage at Contact with Landfill Debris and Native Glacial Till Soils



Contact with Outwash Gravel Soils



Test Pit – TP-6-16



Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Landfill Debris and Cover Soils



Test Pit – TP-7-16



Contact Cover Soil/Landfill Debris with Native Glacial Till Soils



Contact Cover Soil/Landfill Debris with Native Glacial Till Soils



Test Pit – TP-8-16



Contact Cover Soil/Landfill Debris with Native Glacial Till Soils



Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Test Pit – TP-9-16



Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Test Pit – TP-10-16



Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Test Pit – TP-11-16



No Waste - Contact of Fill/Outwash and Native Glacial Till Soils



No Waste – Contact of Fill/Outwash and Native Glacial Till Soils



Test Pit – TP-12-16



No Waste - Contact Native Glacial Till Soils



No Waste – Contact Native Glacial Till Soils



Test Pit – TP-13A-16



Contact Cover Soil/Landfill Debris with Native Glacial Till Soils



Contact Cover Soil/Landfill Debris with Native Glacial Till Soils



Test Pit – TP 13B-16


Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Contact of Cover Soil/Landfill Debris with Native Glacial Till Soils



Bellevue Airfield Park Bellevue, Washington

Test Pit – TP-14-16



Contact Cover Soil/Landfill Debris with Native Glacial Till Soils



Contact Cover Soil/Landfill Debris with Native Glacial Till Soils



Bellevue Airfield Park Bellevue, Washington

Test Pit – TP-15-16

APPENDIX B

Laboratory Test Results

APPENDIX B LABORATORY SOIL TESTING

The laboratory testing program, which was performed in general accordance with the ASTM International (ASTM) standard test procedures described below, was limited to visual inspection to confirm our field soil descriptions and determination of the natural moisture content and grain size distribution of selected samples. The natural moisture contents of selected soil samples obtained from our exploratory borings were determined in general accordance with ASTM D 2216 test procedures. The results from the natural moisture content determinations are indicated adjacent to the corresponding samples obtained from our exploratory logs presented in Appendix A. The grain size distributions of selected soil samples obtained from our exploratory borings and test pits were determined in general accordance with ASTM D 422 test procedures. The results are presented in the form of a grain size distribution curves on Figures B-1 through B-2.





1548001.01 5/26/16 N:\PROJECTS\1548001.010.GPJ GRAIN SIZE FIGURE

APPENDIX C

Boring Logs by Others





07-03-2008 G-f04206007.00/Bering LegelE1-106R.ber







07-03-2008 G:04206007.00/Boring LogsWW-4R2.bor



07-03-2008 G:104206007.00/Boring LogsWW-6R.bor









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APPEHDIX

GENERALIZED SOIL LOCS

The generalized soil logs for the extraction wells, monitor wells and condensate traps are based on drill cuttings and other observations during construction activities. The soils have been classified visually in general accordance with ASTM D-2487-83.

GENERALIZED EXTRACTION WELL SOIL LOGS

EN-1	0 - 25 FEET	BROWN SILT AND SANDY SILT WITH PIECES OF CONCRETE
	25 - 38 FEET	BROWNISH-GRAY FINE TO COARSE SAND WITH GRAVEL AND OCCASIONAL COBBLES
EW-2	0 - 9 FEET	BROWN SILT WITH PIECES OF CONCRETE
	9 - 33 FEET	LAYERS OF SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES AND LANDFILL DEBRIS (DOMESTIC)
	33 - 35 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES
EV-3	0 - 13 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH Occasional Gravel, Cobbles, Red Brick And Concrete
	13 - 33 FEET	DARK GRAY SILT WITH LANDFILL DEBRIS (WOOD AND DOMESTIC WASTE)
	33 - 41 FEET	BROWN GRADING TO GRAY SILTY FINE TO Medium Sand with a trace of gravel
EW-4	0 - 15 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES AND WOOD WASTE
	15 - 18 FEET	LOG OR TREE STUMP
	18 - 40 FEET	GRAY SILTY FINE TO HEDIUH SAND WITH Gravel and occasional cobbles
EW-5	0 - 6 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES
	6 - 7 FEET	LANDFILL DEBRIS (PRIMARILY DOMESTIC WASTE)
	7 - 42 FEET	GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES
EW-6	0 - 40 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL AND COBBLES GRADES TO GRAY AT 5 FEFT

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EN-7	0 - 42 FEET	BROWN FIRE TO HEDIUM SAND WITH SILT AND GRAVEL GRADES TO GRAY AT 5 FEET
ew-8	0 - 3 FEET	BROWN SILTY FIRE TO MEDIUM SAND WITH OCCASIONAL GRAVEL AND COBBLES
	3 - S FEET	LANDFILL DEBRIS (DOMESTIC WASTE) WITH SILTY SAND
	5 - 40 FEET	GRAY SILTY FINE TO NEDIUM SAND WITH OCCASIONAL GRAVEL AND COBBLES
EN-9	0 - 1 FEET	BROWN SILTY FIRE TO MEDIOM SAND WITH GRAVEL
	1 - 21 FEET	GRAY SILTY FINE TO MEDIUMS AND WITH LANDFILL DEBRIS
	21 - 37 FEET	GRAY SILTY FINE TO HEDIUM SAND WITH GRAVEL
EV-10	0 - 9 FEET	SILTY SAND WITH GRAVEL
	9 - 31 FEET	LANDFILL DEBRIS (DOMESTIC WASTE)
EW-11	0 - 19 FEET	SILTY SAND WITH GRAVEL
	19 - 32 PEET	LANDFLL DEBRIS (DOMESTIC WASTE)
EW-12	0 - 3 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL
	3 - 20 FEET	GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL CONCRETE AND RED BRICK
	20 - 30 FEET	GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL AND LANDFILL DEBRIS (DOMESTIC WASTE)
	30 - 35 FEET	GRAY SILTY FINE TO MEDIUM SAND WITH A TRACE OF GRAVEL
EW-13	0 - 15 FEET	BROWN SILTY FINE TO HEDIUM SAND WITH OCCASIONAL GRAVEL AND COBBLES
	15 - 20 FEET	DARK GRAY SILTY FINE TO MEDIUM SAND AND LANDFILL DEBRIS (WOOD WASTE)
	20 - 30 FEET	GRAY GRAVELLY FINE TO COARSE SAND WITH A
	30 - 38 FEET	BROWN MEDIUM TO COARSE SAND WITH A TRACE

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EV-14	0 - 8 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH OCCASIONAL GRAVEL AND COBBLES
	8 - 25 FEET	LANDFILL DEBRIS (DOMESTIC WASTE)
	25 - 30 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH OCCASIONAL GRAVEL
	30 - 35 FEET	GRAY CRAVELLY HEDIUN TO COARSE SAND
	35 - 39 FEET	GRAY SILTY GRAVEL WITH SAND
E¥15	0 - 3 FEET	PIT RUN FILL
	3 - 13 FEET	DARK GRAY SILTY SAND WITH LANDFILL DEBRIS
	13 - 30 FEET	GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL AND SOME LANDFILL DEBRIS
	30 - 38 FEET	GRAY FINE TO COARSE SAND WITH GRAVEL SLOW GROUND WATER SEEPAGE AT 3 FEET
EW-16	0 - 5 FEET	GRAY GRAVELLY FINE TO COARSE SAND WITH SILT
	5 - 13 FEET	DARK BROWN TO BLACK SILT AND LANDFILL DEBRIS (DOMESTIC WASTE)
	13 - 28 FEET	GRAY SILTY GRAVELLY FINE TO MEDIUM SAND
	28 - 35 FEET	GRAY FINE TO COARSE SAND WITH GRAVEL AND A TRACE OF SILT
	35 - 37 FEET	BROWN FINE TO MEDIUM SAND WITH A TRACE OF GRAVEL
EW-17	0 - 8 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL AND TREE ROOTS
	8 - 19 FEET	BROWNISH-GRAY FINE TO MEDIUM SAND WITH GRAVEL, OCCASIONAL COBBLES AND A TRACE OF SILT
	19 - 24 FEET	BROWNISH-GRAY SANDY GRAVEL WITH COBBLES
	24 - 37 FEET	BROWNISH-GRAY SILTY FINE TO HEDIUM SAND WITH GRAVEL AND COBBLES
	37 TO 39 FEET	GRAY FINE TO COARSE SAND WITH A TRACE OF SILT
EW-18	0 - 3 FEET	PIT RUN FILL
	3 - 24 FEET	BROWNISH-GRAY FINE TO HEDIUM SAND WITH Gravel and a trace of silt
	24 - 25 FEET	GRAVEL AND COBBLES
	25 - 38 FEET	BROWNISH-GRAY FINE TO MEDIUM SAND WITH GRAVEL AND A TRACE OF SILT

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EV-19	0 - 2 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL
	2 - 15 FEET	DARK GRAY SILTY FINE TO MEDIUM SAND WITH PIECES OF CONCRETE AND ASPHALT
	15 - 36 FEET	DARK CRAY SILTY FINE TO HEDIUM SAND WITH LAYERS OF LANDFILL DEBRIS (DOMESTIC WASTE)
E¥-20	0 - 7 FEET	BROWN GRAVELLY FINE TO MEDIUM SAND WITH SILT
	7 - 27 FEET	LAYERS OF GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL, OCCASIONAL COBBLES AND LANDFILL DEBRIS (DOMESTIC WASTE)
	27 - 33 FEET	GRAY SILTY FINE TO MEDIUM SAND GROUND WATER ENCOUNTERED AT 33 FEET
EW-21	0 - 2 FEET	BROWN FINE TO MEDIUM SAND WITH GRAVEL
	2 - 9 FEET	GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES
	9 - 19 FEET	DARK GRAY SILTY FINE TO MEDIUM SAND WITH LAYERS OF LANDFILL DEBRIS (DOMESTIC)
	19 - 40 FEET	BROWNISH-GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL

GENERALIZED NONITOR WELL SOIL LOGS

HW-1	0 - 34 FEET	BROWN FINE TO MEDIUM SAND WITH GRAVEL, A TRACE OF SILT AND OCCASIONAL COBBLES NO GROUND WATER OBSERVED ATD
HW-2	0 - 29 FEET	BROWN FINE TO MEDIUM SAND WITH GRAVEL AND COBBLES AND A TRACE OF SILT
	29 - 32 FEET	BROWN AND GRAY CLAYEY SILT
	32 - 35 FEET	GRAY FINE TO MEDIUM SAND WITH A TRACE OF GRAVEL
		GROUND WATER LEVEL AT 31 FEET ATD
MV-3	0 - 10 FEET	SILTY SAND AND PIECES OF CONCRETE
	10 - 27 FEET	SILTY SAND WITH CRAVEL
	27 - 30 FEET	LANDETLL DEBRIS (DOMESTIC)
	30 - 43.5 FEET	SILTY SAND WITH GRAVEL
		NO GROUND WATER OBSERVED ATD
MW-4	0 - 20 FEET	BROWN SILTY SAND WITH GRAVEL AND COBBLES,
		ABUNDENT ROOTS FROM 15 TO 20 FEET
	20 - 44.5 FEET	GRAY SILTY SAND WITH GRAVEL
		GROUND WATER LEVEL AT 35 FEET ATD

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]\$1-5	0 - 9 FEET 9 - 25 FEET 25 - 31 FEET	RECORD SILTY SAND WITH GRAVEL GRAY SILTY SAND WITH A TRACE OF GRAVEL GRAY SAND WITH SILT GROUND WATER LEVEL AT 25 FEET ATD
NY-6	0 - 2 FEET 2 - 38 FEET 38 - 45 FEET	SILTY SAND WITH GRAVEL GRAY SILTY SAND WITH GRAVEL AND COBBLES GRAY SAND WITH SILT GROUND WATER AT 28 FEET ATD
HX-7	0 - 32 FEET 32 - 41.5 FEET	SILTY SAND WITH GRAVEL GRAY SILTY SAND WITH GRAVEL AND SAND WITH SILT GROUND WATER LEVEL AT 34 FEET ATD
MM-8	0 - 48 FEET	GRAY FINE SAND WITH SILT AND A TRACE OF GRAVEL AND OCCASIONAL COBBLES GROUND WATER LEVEL AT 46 FEET ATD
HW-9	0 - 4 FEET 4 - 22 FEET	BROWN SILTY SAND WITH GRAVEL GRAY MEDIUM SAND WITH SILT AND A TRACE OF GRAVEL
	22 - 27 FEDI	AND COBBLES NO GROUND WATER OBSERVED ATD
MW-10	0 - 2 FEET 2 - 12.5 FEET	BROWN SILTY SAND WITH GRAVEL AND ROOTS GRAY AND BROWN MEDIUM TO COARSE SAND WITH GRAVEL AND OCCASIONAL COBBLES NO GROUND WATER OBSERVED ATD
MW-11	0 - 2 FEET 2 - 12 FEET	BROWN SILTY SAND WITH GRAVEL AND ROOTS GRAY AND BROWN MEDIUM TO COARSE SAND WITH GRAVEL AND OCCASIONAL COBBLES NO GROUND WATER OBSERVED ATD
MW-12	0 - 6 FEET 6 - 34 FEET	BROWN SILTY SAND WITH GRAVEL GRAY MEDIUM TO COARSE SAND WITH SILT AND GRAVEL AND OCCASIONAL COBBLES
	34 - 41 FEET	GRAY MEDIUM TO COARSE SAND WITH GRAVEL AND COBBLES GROUND WATER LEVEL AT 36 FEET ATD
MW-13	0 - 25 FEET 25 - 32 FEET 32 - 48 FEET	CRAY SILTY SAND WITH GRAVEL AND COBBLES BROWN SAND WITH SILT AND GRAVEL BROWN MEDIUM TO COARSE SAND WITH A TRACE OF GRAVEL AND OCCASIONAL COBBLES SLIGHT SEEPAGE ENCOUNTERED IN UPPER HALF OF BORING ATD

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157-14	0 - 20 FEET	CRAY NEDION SAND WITH SILT, GRAVEL AND COBBLES
	20 - 31 FEET	GRAY SILTY SAND WITH GRAVEL
	31 - 45 FEET	BROWN MEDIUM TO COARSE SAND WITH A TRACE OF GRAVEL
		SLIGHT SEEPAGE AT VARIOUS DEPTHS ATD
HV-15	0 - 20 FEET	GRAY MEDIUM SAND WITH SILT, GRAVEL AND COBBLES
	20 - 35 FEET	GRAY SILTY SAND WITH GRAVEL
	35 - 41 FEET	BROWN HEDIUM TO COARSE SAND
		GROUND WATER SEEPAGE OBSERVED FROM 4 TO 16 FEET AND 36 TO 41 FEET ATD
HW-16	0 - 3 FEET	BROWN MEDIUM SAND WITH GRAVEL
	3 - 24 FEET	BROWN AND GRAY SILTY SAND WITH GRAVEL
	24 - 46.5 FEET	BROWN MEDIUM SAND WITH GRAVEL AND COBBLES
		HODERATE SEEPACE OBSERVED AT 6 FEET ATD
HW-17	0 - 6 FEET	BROWN SILTY SAND WITH GRAVEL
	6 - 25 FEET	GRAY SILTY SAND WITH GRAVEL AND OCCASIONAL COBBLES
	25 - 44.5 FEET	BROWN FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES
		SEEPAGE OBSERVED AT 6 FEET ATD
HW-18	0 - 3 FEET	BROWN MEDIUM SAND
	3 - 25 FEET	BROWN SILTY SAND WITH GRAVEL AND OCCASIONAL COBBLES
		NO GROUND WATER OBSERVED ATD

GENERALIZED CONDENSATE TRAP SOIL LOGS

-1	0 - 5	SILTY SAND WITH GRAVEL
	5 - 10 FEET	SILTY SAND AND LANDFILL DEBRIS (DOMESTIC
1	10 - 18 FEET	SILTY SAND WITH GRAVEL
-2	0 - 9 FEET	SILTY SAND WITH GRAVEL
	9 - 15 FEET	LANDFILL DEBRIS (DOHESTIC WASTE)
3	0 - 8 FEET	SILTY SAND WITH GRAVEL
	8 - 16 FEET	LANDFILL DEBRIS (DOMESTIC WASTE)
1	16 - 20 FEET	SILTY SAND WITH GRAVEL
·2 ·3	0 - 9 FEET 9 - 15 FEET 0 - 8 FEET 8 - 16 FEET 16 - 20 FEET	SILTY SAND WITH GRAVEL LANDFILL DEBRIS (DOHESTIC WASTE) SILTY SAND WITH GRAVEL LANDFILL DEBRIS (DOHESTIC WASTE) SILTY SAND WITH GRAVEL

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-T7-4	0 - 10 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL CORRESS
	10 - 13.5 FEET	LANDFILL DEBRIS (WOOD WASTE)
	13.5 - 20 FEET	GRAY SILTY FIRE TO MEDIUM SAND WITH GRAVEL
CT-5	0 - 13 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES AND CONCRETE
	13 - 17 FEET	DARK GRAY SILTY FIRE TO MEDIUM SAND AND LAYERS OF LANDFILL DEBRIS (DEMOLITION AND DOMESTIC)
CT-6	0 - 6 FEET	BROWN SILTY FINE TO ENDIUM SAND VITH GRAVEL
	6 - 21 FEET	DARK GRAY SILTY FINE TO MEDIUM SAND WITH LAYERS OF LANDFILL DEBRIS (DOMESTIC WASTE)
- CT-7	0 - 5 FEET 5 - 15 FEET	SILTY SAND WITH GRAVEL SILTY SAND AND LANDFILL DEBRIS (DOMESTIC WASTE)
- CT-8	0 - 3 FEET 3 - 18 FEET	SILTY SAND WITH GRAVEL LANDFILL DEBRIS (DOMESTIC WASTE)
CT-9	0 - 11 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL
	11 - 16 FEET	DARK GRAY SILTY FINE TO MEDIUM SAND WITH LANDFILL DEBRIS
	16 - 17 FEET	GRAY SILTY FINE TO HEDIUM SAND WITH GRAVEL
- CT-10	0 - 15 FEET 15 - 17 FEET	SILTY SAND WITH GRAVEL Landfill Debris (Domestic Waste)
-CT-11	0 - 12 FEET 12 - 16 FEET	SILTY SAND WITH GRAVEL Landfill Debris (Dohestic Waste)
CT-12	0 - 5 FEET	BROWN SILTY FINE TO MEDIUM SAND WITH GRAVEL
	5 - 13 FEET	GRAY SILTY FINE TO MEDIUM SAND WITH LAYERS OF LANDFILL DEBRIS
	13 - 18 FEET	BROWNISH-GRAY SILTY FINE TO MEDIUM SAND WITH GRAVEL AND OCCASIONAL COBBLES
-CT-13	0 - 5 FEET	SILTY SAND WITH GRAVEL
	5 - 15 FEET	LANDFILL DEBRIS (DOMESTIC WASTE)
	15 - 17 FEET	SILTY SAND WITH GRAVEL

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PROPOSED 1-90/BELLEVUE BUSINESS PARK

FIGURE 2

BELLEVUE, WASHINGT	ON PROJECT 78059	FIGURE 2
	78-1-74	
	TEST PIT] (EL. 332+)	
DEPTH, FEET		
0.0 - 1.0	LOOSE BROWN SILTY SAND WITH SOM GRAVEL (MOIST) (FILL)	E TO TRACE
1.0 - 1.5	LOOSE GRAY SILTY SAND WITH SOME (WET) (FILL)	GRAVEL
1.5 - 13.0	HOUSEHOLD GARBAGE MIXED WITH SI SOME GRAVEL AND LIMBS (WET) (MO STRONG ODOR)	LTY SAND WITH DERATE TO
	NO GROUNDWATER OBSERVED	
	TP-2-78	
	TEST PIT 2 (EL. 312+)	
DEPTH, FEET		
0.0 - 3.5	LOOSE BROWN SILTY FINE SAND WITH (MOIST) (FILL) SMALL TREES ON	H TRACE GRAVEL CONTACT
3.5 - 8.0	MEDIUM DENSE TO DENSE GRAY SILTY SOME GRAVEL TO GRAVELLY SILTY SA	SAND WITH AND (WET) (FILL)
8.0 - 9.5	MEDIUM DENSE GRAY CLEAN GRAVELLY (FILL)	SAND (WET)
	STICKS AT CONTACT	
9.5 - 12.5	MEDIUM DENSE BROWN SILTY SAND WI SOME GRAVEL (WEI)	TH TRACE TO
12.5- 14.0	FIRM BROWN AND GRAY MOTTLED SILT (WET) (BADLY WEATHERED TILL?)	Y FINE <u>SAND</u>
•,	GROUNDWATER SEEFAGE AT 3.0 AND 1 LIGHT ODOR	4.0 FEET
	•	

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PROPOSED 1-90/BELLEVUE BUSINESS PARK

BELLEVUE, WASHINGT	ON	PROJECT 78059	FIGURE 3
	TP-3-78 TEST PIT	<u>3</u> (EL. 309 <u>+</u>)	
DEPTH, FEET			
0.0 - 1.5	LOOSE TO VERY L WITH ROOTS (MOI DUFF LAYER)	OOSE DARK BROWN SI ST) (TOPSOIL AND T	ILTY <u>SAND</u> THIN FOREST
1.5 - 4.0	MEDIUM DENSE TO SILTY <u>SAND</u> WITH WITH SOME WET Z	DENSE GRAY AND BE TRACE TO SOME GRA ONES) (WEATHERED 7	ROWN MOTTLED AVEL (MOIST ILL)
4.0 - 10.0	DENSE TO VERY D TRACE TO SOME G NEAR- REFUSAL O FEET	ENSE GRAY SILTY <u>SA</u> RAVEL (MOIST) (GLA F EXCAVATING EQUIE	AND WITH ACIAL TILL) PMENT AT 10.0
	NO GROUNDWATER	OBSERVED	
	78-24-78		
	TEST PIT	4 (EL. 329 <u>+</u>)	
DEPTH, FEET			-
0.0 - 4.0	VERY SOFT TO SO SILTY FINE <u>SAND</u>	FT BROWN FINE SAN	DY <u>SILT</u> TO (WET) (FILL)
4.0 - 5.5	LOOSE TO MEDIUM AND <u>SAND</u> MIXED (WET) (FILL)	DENSE DARK BROWN WITH CONCRETE AND	TO BLACK <u>SILT</u> ASPHALT RUBBLE
5.5 - 7.0	CONCRETE RUBBLE		
7.0 - 12.0	LOOSE BROWN SIL GRAVEL AND SCAT	TY SAND WITH TRAC TERED GARBAGE (WE	E TO SOME T) (FILL)
	NO GROUNDWATER Slight to moder	OBSERVED	

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PROPOSED 1-90/EELLEVUE BUSINESS PARK

BELLEVUE, WASHINGTON

PROJECT 78059

FIGURE 4

70	-5	-7	Ø
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TEST PIT 5 (EL. 322+)

DEPTH, FEET

- 0.0 1.0 LOOSE BROWN SILTY SAND WITH TRACE GRAVEL (WET) (FILL)
- 1.0 12.0 HOUSEHOLD GARBAGE MIXED WITH SILTY SAND LUMBER AND LIMBS (WET) (NEWSPAPER FROM 1963 STILL READABLE)

NO GROUNDWATER OBSERVED STRONG ODOR

70-6-78

TEST PIT 6 (EL. 333+)

DEPTH, FEET

- 0.0 0.5 LOOSE BROWN SILTY <u>SAND</u> WITH TRACE GRAVEL (WET) (FILL)
- 0.5 1.5 LOOSE GRAY SILTY SAND WITH TRACE GRAVEL (WET) (FILL)
- 1.5 13.0 HOUSEHOLD GARBAGE MIXED WITH SAND, SILT, LIMBS AND LUMBER (WET) (1964 NEWSPAPER AT 3.0 FEET STILL READABLE)

VERY HEAVY GROUNDWATER FLOW AT 4.0 FEET, WATER DOES NOT POND IN BOTTOM OF TEST PIT

VERY STRONG ODOR

<u>TEST PIT 7</u> (EL. 332+)

DEPTH, FEET

- 0.0 0.2 . PEA GRAVEL
- 0.2 5.5 LOOSE TO MEDIUM DENSE BROWN GRAVELLY SAND WITH SOME SILT (MOIST) (FILL)
- 5.5 12.0 HOUSEHOLD GARBAGE MIXED WITH SILTY SAND, LIMBS AND LUMBER (WET) (1962 NEWSPAPER STILL READABLE)

NO GROUNDWATER OBSERVED STRONG ODOR

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PROPOSED 1-90/BELLEVUE BUSINESS PARK

BELLEVUE, WASHINGTON

PROJECT 78059

FIGURE 5

70-6-78

TEST PIT 8 (EL. 329+)

DEPTH, FEET

- 0.0 7.5 LOOSE TO MEDIUM DENSE BROWN SILTY SAND WITH TRACE TO SOME GRAVEL (MOIST) (FILL)
- 7.5 12.5 <u>HOUSEHOLD GARBAGE</u> MIXED WITH SILTY SAND, CAR PARTS AND OTHER DEBRIS (WET) (1963 NEWSPAPER STILL READABLE)

MODERATE GROUNDWATER FLOW AT 8.0 FEET STRONG ODOR

71-9-78

TEST PIT 9 (EL. 341+)

DEPTH, FEET

- 0.0 0.2 <u>SOD</u>
- 0.2 2.0 LOOSE TO MEDIUM DENSE BROWN SILTY SAND OF SOME GRAVEL (MOIST) (WEATHERED TILL) -
- 2.0 6.5 DENSE TO VERY DENSE GRAY WITH MINOR BROWN MOTTLING SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (GLACIAL TILL)

NO GROUNDWATER OBSERVED

(1-16-78) TEST PIT 10 (EL. 336+)

DEPTH, FEET

- 0.0 0.5 FOREST DUFF
- 0.5 3.0 LOOSE TO MEDIUM DENSE BROWN SILTY SAND (MOIST)
- 3.0 8.0 LOOSE TO MEDIUM DENSE GRAY SAND WITH SOME LENSES OF HARD GRAY SANDY SILT (MOIST)
- 8.0 10.0 DENSE TO VERY DENSE GRAY SILTY <u>SAND</u> WITH SOME GRAVEL AND TRACE TO OCCASIONAL COBBLES (MOIST) (GLACIAL TILL)

NO GROUNDWATER OBSERVED

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PROPOSED 1-90/BELLEVUE BUSINESS PARK

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FIGURE 8

BELLEVUE, WASHING	PROJECT 78059
	-78-16-78
	TEST PIT 16 (EL. 300+)
DEPTH, FEET	
0.0 - 0.4	SOD
0.4 - 2.5	MEDIUM DENSE BROWN SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (WEATHERED TILL) SLIGHT GROUNDWATER SEEPAGE AT 2.5 FEET
2.5 - 5.0	MEDIUM DENSE GRAY SILTY SAND WITH SOME GRAVEL (MOIST) (WEATHERED TILL)
5.0 - 10.0	VERY DENSE GRAY SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (GLACIAL TILL)
	TP-17-76 <u>TEST PIT 17</u> (EL. 314 <u>+</u>)
DEPTH, FEET	
0.0 - 5.5	LOOSE BROWN SILTY SAND WITH SOME GRAVEL (WET) (FILL)
5.5 - 6.5	LOOSE GRAY GRAVELLY SILTY SAND TO GRAVELLY SAND WITH SOME SILT (MOIST) (FILL)
6.5 - 11.0	LOOSE TO MEDIUM DENSE BROWN SILTY <u>SAND</u> WITH Some gravel (moist)
11.0-14.0	MEDIUM DENSE TO DENSE LIGHT BROWN TO GRAY SILTY SAND WITH SOME GRAVEL (MOIST) (WEATHERED TILL)
	NO GROUNDWATER OBSERVED

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LEVUE, WASHI	NGTON	PROJECT 78059	FIGURE 9
		~191-78	
	TEST	<u>T PIT 18</u> (EL. 312+) -78	3
DEPTH, FEET			
0.0 - 0.2	SOD		
0.2 - 2.0	LOOSE GRAY Some grave	AND BROWN LAYERED SIL	TY <u>SAND</u> WITH
2.0 - 3.5	LOOSE BROW Household	AN SILTY <u>SAND</u> AND STICK GARBAGE (MOIST) (FILL)	S MIXED WITH
3.5 - 5.0	LOOSE TO M SOME GRAVE	MEDIUM DENSE BROWN SILT EL (MOIST) (WEATHERED T	Y <u>SAND</u> WITH ILL)
5.0 - 12.0	DENSE TO V GRAVEL (MO	VERY DENSE GRAY SILTY <u>SA</u> DIST) (GLACIAL TILL)	AND WITH SOME
	NO GROUNDW	ATER OBSERVED	
	TP - TEST	-19 - 766 <u>PIT 19</u> (EL. 330 <u>+</u>) - 7	3
EPTH, FEET			
0.0 - 1.5	LOOSE BROW Some grave	N AND GRAY LAYERED SILT L (MOIST) (FILL)	Y SAND WITH
1.5 - 12.0	HOUSEHOLD GRAVELLY <u>S</u> ODOR)	GARBAGE MIXED WITH BLUE AND, LUMBER AND ASH (WE	-GRAY SILTY T) (STRONG
	MODERATE G	ROUNDWATER FLOW AT 7.0	TO 8.0 FEET

PROPOSED I-90/BEL	LEVUE BUSINESS PARK	ELCURE 10
BELLEVUE, WASHING	GTON PROJECT 78059	FIGURE IU
	TP-20-78 TEST PIT 20 (EL. 341+)-78	
DEPTH, FEET		
0.0 - 0.2	SOD	
0.2 - 1.5	LOOSE TO MEDIUM DENSE GRAY SILTY SOME GRAVEL TO GRAVELLY SILTY SAM	SAND WITH D (MOIST) (FILL)
1.5 - 3.0	HOUSEHOLD GARBAGE AND ASH (WET) (MODERATE ODOR)
3.0 - 4.0	MEDIUM DENSE LIGHT BROWN SILTY SA GRAVEL (MOIST) (WEATHERED TILL)	ND WITH SOME
4.0 - 9.0	DENSE TO VERY DENSE GRAY SILTY <u>SA</u> GRAVEL (MOIST) (GLACIAL TILL)	ND WITH SOME
	NO GROUNDWATER OBSERVED	
	TP-21-76 TEST PIT 21 (EL, 343+)-78	
0.0 - 0.1	LOOSE BROWN SILTY <u>SAND</u> WITH SOME (WEATHERED TILL)	GRAVEL (WET)
0.1 - 3.0	VERY DENSE GRAY SILTY <u>SAND</u> WITH S (MOIST) (GLACIAL TILL)	OME GRAVEL
	NO GROUNDWATER OBSERVED	
	TH- 22-16 TEST PIT 22 (EL. 338+) -78	
DEPTH, FEET		
0.0 - 2.0	LOOSE TO MEDIUM DENSE BROWN TO GRAWITH SOME GRAVEL (WET) (FILL)	AY SILTY <u>SAND</u>
2.0 - 12.0	HOUSEHOLD GARBAGE (WET) (STRONG OF	DOR) -
	NO GROUNDWATER OBSERVED	

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LOGS OF TEST PITS

-78

PROPOSED I-90/BELLEVUE BUSINESS PARK

TP-23-70

TEST PIT 23 (EL. 340+)

PROJECT 78059

DE	P1	ΤΗ,	F	EE	Т
		the second se	and the second second		

BELLEVUE, WASHINGTON

- 0.0 0.3 SOD
- 0.3 2.5 LOOSE BROWN SILTY <u>SAND</u> WITH SOME GRAVEL AND "BEDROCK" CHUNKS TO 10 INCHES IN DIAMETER (WET) (FILL)
- 2.5 4.0 LOOSE GRAY SILTY SAND WITH SOME GRAVEL AND STICKS (MOIST) (FILL)
- 4.0 7.0 LOOSE TO MEDIUM DENSE TAN GRADING TO GRAY-BROWN SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (WEATHERED TILL)
- 7.0 9.0 VERY DENSE GRAY SILTY <u>SAND</u> WITH SOME GRAVEL (MDIST) (GLACIAL TILL) NEAR-REFUSAL AT 9.0 FEET

NO GROUNDWATER OBSERVED

70-24-78

TEST PIT 24 (EL. 348+)

DEPTH, FEET

- 0.0 2.5 LOOSE TO MEDIUM DENSE BROWN, SILTY SAND WITH SOME GRAVEL (WET TO MOIST) (WEATHERED TILL)
- 2.5 6.0 DENSE TO VERY DENSE GRAY SILTY SAND WITH SOME GRAVEL (MOIST) (GLACIAL TILL)

NO GROUNDWATER OBSERVED

bucknam associates

					LOG OF BORING NO. B-1-94		Sh	leet	1 of	2
D	ate drille	ed	_10	/19/94	Sampler / Driving Weight SPT, 140 lb 30"/drop	Eleva	tion ((ft)	339	0.6
Depth. ft	Elevation	Sample No.		Blows/6" Graphic Sumbol	This log is part of the report prepared by Converse Consultants NW for the named project and should be read together with that report for complete interpretation. This summary applies only at the location of this boring and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented are a simplification of actual conditions encountered.		lonitoring Well	'y density pcf	Moisture ontent, %	her Tests
					3 1/2 inch Asphalt Pavement		E	à	Ū	to
5	335 -	1		1	FILL GRAVEL; brown, trace silt, fine to coarse; moist SILTY SAND; brown to gray mottled rust, little fine gravel; very dense, moist gray mottled brown, fine to coarse, trace fine gravel; loose					
		3	5 5 6		SILTY SAND WITH GRAVEL AND DEBRIS; brown, fine to coarse; medium dense, moist; with wood chips and glass					
10-		4	4 5 6		layer of paper at depth 11 feet - 4 inches thick layer of wood chips and peat ATE					
-	325 -	5	424		black, pieces of metal, paper, pieces of wire; loose, wet	=				
15		6	7 14 14		GRAVEL WITH DEBRIS; black, fine, debris consists of of rubber, metal and paper; medium dense, wet					
-		7	4 5 7		wood fragments, tape and wood chips; medium dense, wet					
	320-									

Continued Next Page

Parking Lot Subsidence Investigation

Project No.

Bellevue, Washington

94-35156-01

Boeing Computer Services



Converse Consultants NW

Geotechnical Engineering and Applied Earth Sciences

					LOG OF BORING NO. B-1-94	Sh	eet	2 of	2
Dat	e drille	đ	_10/1	9/94	Sampler / Driving Weight SPT, 140 lb 30"/drop	Elevation (ft)	339	.6
Depth, ft	Elevation	Sample No.	Blows/6"	Graphic Symbol	This log is part of the report prepared by Converse Consultants NW for the named project and should be read together with that report for complete interpretation. This summary applies only at the location of this boring and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented are a simplification of actual conditions encountered. DESCRIPTION	10nitoring Well	ry density pcf	Moisture ontent, %	ther Tests
	315- 310- 305-	9 10 11	3 4 4 3 5 7 6 7 8 5 50 50		SILTY SAND WITH DEBRIS; brown, fine to coarse, trace fine gravel with debris, wood chips, plastic; medium dense, wet layer of newspaper from a depth of 21 to 21-1/4 feet SAND AND GRAVEL; brown motiled gray, little silt; medium dense, wet little to some silt NATIVE DEPOSITS SILTY SAND AND GRAVEL; mottled brown, fine to coarse; very dense, moist Bottom of boring at depth 29 feet Boring backfilled with bentonite chips and concrete cap installed at the ground surface ATD = at the time of drilling				

Parking Lot Subsidence Investigation

Project No.

Bellevue, Washington

94-35156-01

Boeing Computer Services



Converse Consultants NW

Geotechnical Engineering and Applied Earth Sciences

A-2

						LOG OF BORING NO. B-2-94		S	neet	1 of	2
Date	e drille	ed	1	0/19	9/94	Sampler / Driving Weight SPT, 140 lb 30"/drop	Eleva	ation	(ft)	339	2.0
Depth, ft	Elevation		מווהרת ואס.	Blows/6"	Graphic Symbol	This log is part of the report prepared by Converse Consultants NW for the named project and should be read together with that report for complete interpretation. This summary applies only at the location of this boring and at the time of drilling. Subsurface conditions may differ at other locations and may change at this location with the passage of time. The data presented are a simplification of actual conditions encountered.		nitoring Well	dens i ty pcf	disture htent, %	er Tests
		0				DESCRIPTION		Moi	Drg	ΞÖ	0th
	335 -	1		8 6 4		3 inch Asphalt Pavement FILL SAND AND GRAVEL; brown, fine to coarse; wet grades to sand SILTY SAND; brown mottled gray; fine to medium, trace fine gravel; dense, moist fine to coarse, scattered organics composed of wood chips, charcoal, peat; medium dense, very moist					
	330 -	3				AT: SAND; gray, fine to coarse, trace fine gravel, scattered organics; medium dense, wet	D Z				
-		5				GARBAGE; paper, wood chips, plastic; loose, wet small layer of silty gravel plastic, wood, paper, egg shells, scattered fine gravel;					
15-	325 -	6	3			metal cans, steel wool, paper, glass, scattered gravel;					
		7	5 7 7 7 14			SILTY SAND; gray mottled, fine to coarse, trace fine					
	320-		19			staver, scattered organics; medium dense, wet					

Continued Next Page

Parking Lot Subsidence Investigation

Project No.

Bellevue, Washington

94-35156-01

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	Parking Lot S	ubsidence Investigation	Project No.
	Belle	vue, Washington	94-35156-01
	Boeing	Computer Services	
2	Converse Congultanta NW	Geotechnical Engineering	Figure No.
	Converse Consultants NW	and Applied Earth Sciences	A-3

Suriu	ce	Con	ditions		
uepm in feet Moisture %	Sample	Symbol	ľ	DESCRIPTION	REMARKS
1-			SILTY GRAVELLY SAND	brown, fine to coarse; moist, loose.	severely weathered
2-					Glacial IIII.
3- 4-			SILT and CLAY	gray-brown, with little sand and scattered gravel; moist, medium stiff.	
5- 6-			SILTY SAND	gray-brown, fine to coarse with little gravel, trace clay, scattered cobbles;	unweathered Glacial Till,
7-				moist, medium dense to dense.	
8-					
9-			grades to	with trace silt	
10-			SAND		
11-				wet.	
12-			Bottom of tort att at	11 51	
13-			No groundwater end Completed July 22,	countered. 1980.	
14-					
15					•

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Approved for publication

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LOG OF TEST PIT NO. TP-30 -81

Location: See Drawing 1.

Elevation: Approx. 343

181

Surface Conditions: Brush and grass.

n	Moisture %	Sample	Symbol		DESCRIPTION	REMARKS
1-			ML/ CL	SILTY CLAY (Construction Fill)	gray, trace gravel; moist soft.	
2-					concrete rubble (up to 4') through- out layer.	
3-						
4-						Light seepage at 4'.
5-					wood debris	
5-				SANITARY LANDFILL	silty sand tin cans, bottles, distinct odor.	
8-			SM	SAND (Weathered Till)	brown, fine to medium, some silt, little gravel; moist, medium dense.	
9-			SM	SAND (Fresh Till)	gray, fine to medium, some silt, little gravel; moist, very dense.	
1		_				
2-				Bottom Comple	of test pit at depth 11.0'. ted March 16, 1981.	
13-						
5						

I-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington for Cabot, Cabot & Forbes Project No. 81-5135



Drawing No

LOG OF TEST PIT NO. TP-4 -61

-ocation: See Drawing 1. Elevation: Approx. 332

-81

Surface Conditions: Brush and grass.

hi Ini Moisture % Symbol	DESCRIPTION	REMARKS
ML/ CL	SILTY CLAY gray, trace gravel; moist, soft. (Construction Fill)	
	concrete rubble (up to 4') through- out layer.	
	wood debris	
	SANITARY tin cans, bottles, distinct odor. LANDFILL	
	•	
-	Bottom of test pit at depth 12.0'. Completed March 16, 1981.	

THE PROTECTION PROTECTION PROJECTION I-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington for Cabot, Cabot & Forbes

81-5135

ConverseWardDavisDixon Geotechnical Consultants

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te t	ture	ed	19	DESCRIPTION	
i Oe	Mois %	Nom	Sym	DESCRIPTION	REMARKS
1-			SM	SILTY SAND brown, fine to medium, roots (Forest Duff) moist, loose	5
2-			SM/ SW	SILTY SAND (Weathered Till) brown, medium to coarse, som gravel; moist, medium dense	2
3- 4-				SILTY SAND gray, medium to coarse, (Fresh Till) some gravel; moist, very dense	roots to 2½' de
5-				cobbles	
7- 8- 9-				Bottom of test pit at depth 6.0' No groundwater encountered Completed 10/29/81	-
10-					
12-					
15-					
15				•	
		-			
				BUILDING SITE. 1 - 1-90 BELLEVUE BUSINESS PARK Bellevue, Washington	Project No. 81-5194
	Со	n١	/ers	eWardDavisDixon Geotechnical Consultants	Drawing No.

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Lo	ocati Irfac	on	: Con	See Drawing 1. Elevent ditions: Brush and grass.	ion: Approx. 318
In feet	Molsture %	Sample	Symbol	DESCRIPTION	REMARKS
1- 2- 3- 4-			SM	SILTY SAND (Construction Fill)brown, fine to medium, little gravel; moist, loose. wood debrisgrades toSANDgray, little gravel, trace silt; moist, medium dense.	Slight seepage at 2.5'.
5- 6- 7- 8- 9-				SANITARY silty sand, tin cans, paper, and bottles.	
10- 11- 12- 13- 14-				Bottom of test pit at depth 10.0'. Completed April 21, 1981.	
15-1	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.			I-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington	Project No. 81-5135

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SL	irfac	1: Approx. 334			
Depth in feet	Moisture %	Sample	Symbol	DESCRIPTION	REMARKS
1- 2-			SM	SILTY SAND (Weathered Till) reddish brown, little gravel, trace roots; moist, loose.	
3- 4-			SM	SILTY SAND gray, fine to medium, little gravel; (Fresh Till) moist, very dense.	Difficult to excavate belo 2½'.
6- 7- 8-				Bottom of test pit at depth 5.0'. Completed April 21, 1981.	
9-					-
2-					
3-					
)					

1-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington for Cabot, Cabot & Forbes

Project No 81-5135

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Drawing No.



ConverseWardDavisDixon Geotechnical Consultants

• •	DATE D	NILLED:	11/2/81		SUMMARY: BORING NO.B-1(Cont.) ELEVATION: Approx. 336					
EPTH	cel	E NO.E ON	SIS MERTES	OF DAT NO	THIS BUBURAR	APPLUS ONLY AT THE LOCATION OF THIS DOWN CONDITIONS MAY DIFFEN AT OTHER LOCATIONS AND SAGE OF THE THE DATA PRESENTED IS A SIMPLIF		E TIME OF ORILL BE AT THIS LOCA ACTUAL CONDI	TIONS	
-	6A	12 18 18	O P	0	SAND (Till)	gray, mottled brown medium to coarse, trace silt, fine gravel	p	wet	dense	
45_	7A	14 35 66				to brownish gray			v.dense	
50-										
					Bottom of bo Groundwater Piezometer i Completed 11	pring at depth 50.5' encountered at depth 31 nstalled to 50.5' /2/81	.5'			
* A. B. D	2* aplit 3* 0.D. 3-1 2'	-spoon sa thin-wall O.D. spli1	ampler sampler barrel samp	C. 3-1/4" ller X. 88	O.D. x 2-1/2" liner **/	A - Atterberg, C - consolidation, DS - dire 5 - grain alze, T - triaxial, P - permeabilit	ct shear, y	ľ	water level Impervious seal piezometer tip	
					BOEING M Bellevue for The I	ETHANE STUDY , Washington Boeing Company			Project No. 81-5186 Drawing No	
) C	onv	erseV	Vard	DavisDixor	Geolechnical Consultants			2a	

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2.4.1 41 104

SATE DRILLED:	SUMMARY: BORING NO. B-2-8 ELEVATION: Approx. 34				
orthere work work owe to the to be of the to	THIS BUBBARY APPLIES OULY AT THE LOCATION OF THIS BORN DUBSUBFACE CONDITIONS DAY DIFFER AT OTHER LOCATIONS AN WITH THE PASSAGE OF THE, THE DATA PRESENTED IS A SIMPL BECOUNTERED DESCRIPTION	SYMBOL	THE THE OF PRILEM	CONSISTENCY	
	GRAVELLY SAND brown, medium to (Fill) coarse		moist	loose to m. dense	
	LANDFILL paper, tin cans, cloth		moist	loose	
- 1A 29	SAND brown, medium to (Till) coarse, trace of gravel		moist	v.dense	
	Bottom of boring at depth 11.0' No groundwater encountered Piezometer installed to 11.0' Completed 11/2/81				
A. 2" split-spoon sampler B. 3" O.D. thin-wall sampler C. 3-1/4 D 3-1 2" OD split barrel sampler X. si	O.D. x 2-1/2" liner "A -Atterberg, C'- consolidation, DS - di simple not recovered G - grain alze, T - triaxial, P - permeab BOEING METHANE STUDY Bellevue, Washington	rect shear, llity		water level Impervious seal piezometer tip Projec: Nc 81-5186	

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ConverseWardDavisDixon Geotechnical Consultants

Lunten0.	ERTES OF DRA DENSIT	SUMMARY: BORING NO.	B-4-81 ELEVATION: AP	prox.
	SAND (Fill)	brown, medium, t silt, some grave	SYMBOL MOISTURE CON trace moist m.	dense
	Bottom o No groun Piezomete Completed	f boring at depth 5.0' dwater encountered er installed to 5.0' d 11/2/81		
Split-spoon sampler D.D. thin-wall sampler C. 3-1/. 2' O.D. split barret sampler X. t	4° O.D. x 2-1/2° Hoer **A - A Sample not recovered G - g	tterberg. C - consolidation, DS - direct shear train size, T - triaxist, P - Dermashin	r. Water level	-
Conversity	BOEING METH/ Bellevue, Wa for The Boei	ANE STUDY ashington ing Company	Project No E1-5186 Draw 55 Mo	
Converseward	DavisDixon Ge	otechnical Consultants	5	

BATE DALLED:	11/2/81	SUN	MARY: BORING NO. B-	5-81	BLEVATION	Approx. 3	
FFEET SPLESONE ON	AS IS WERE TESTS WORDS WERE	THIS BUWEA	THIS SUBBLARY APPLIES ONLY AT THE LOCATION OF THIS BOOMS AND AT THE THE OF DRILLING BUDSURFACE CONDITIONS HAT DWFFER AT DTHEN LOCATIONS AND HAT CHANGE AT THIS LOCATION WITH THE PASSAGE OF THE. THE BATA PRESENTED IS A BINPLIFICATION OF ACTUAL CONDITIONS BECOMPTERED CONSISTENC				
		DESCRIPTION SAND (Fill)	brown, medium, trace silt, some gravel	SYMBOL	moist	m. dense	
-							
		Bottom of b No groundwa Piezometer Completed 1	oring at depth 5.0' ter encountered installed to 5.0' 1/2/81				
						r.	
					•		
A. 2" split-spoon si E. 3" O.D. thin-wall T. 3-1/2" O.D. split	ampler samplør C. 3-1/4 [°] (i barrel sampler X. sam	D.D. x 2-1/2" liner ""	A - Atterberg, C - consolidation, DS - di G - grain size, T - triaxial. P - permeabl	ect shear, lity	ţ	water level Impervious seal piezometer tip	
		BOEING M Sellevue for The	KETHANE STUDY , Washington Boeing Company			Project No. 81-5186 Drawing No	
Conve	erseWard	DavisDixo	Geotechnical Consultants			6	





S.	Conv	erse Co	Insultants Geotechnical Engineering and Applied Sciences 13.14	-	
			for Brown and Caldwell 02-5169		
			EASTGATE TRUNK SEWER Project No. Bellevue, Washington P2 E1CO		
B 3" 0.D. D. 3-1/2"	thin-wall samp O.D. split barre	ler C. 3-1/4" I sampler X. set	0.D. z 2-1/2" Hner "A -Atterberg, C - consolidation, DS - direct shear, Impervious seat mple not recovered G - grain size, T - triazial, P - permeability piezometer tip		
A. 2" split	-spoon sample:	,	(Continued)		
A8 L	25 50/5"	7.8	grades cleaner with less silt		
- 7A - 5	A ¤ 50∕6"	10.1	SAND brown, fine to coarse, SP moist very (Advance some silt, trace Outwash) clayey silt, occasional gravel	305	
0 - 6/	A 18 50/5''	9.8	SILT gray, some fine sand, ML slightly very (Lacustrine Deposit) occasional layer of coarse sand	-315	
25 - 5	A = 50/3"	4.2	boulder 20-21' depth (refusal on boulder at 25' depth; redrilled hole 6' north of original location)	-320	
20 - 4	A = 50/5"	5.5	SILTY SAND blue-gray, fine to SM moist very (Glacial coarse, some gravel, Till) occasional cobbles		
.5 - 3	BA 5 17 13	14.1	grades finer with Clayey silt, fabric ML fragments	- 325	
, , 10 - 1 10 - 1	2A - 4 5 8	25.9	SILTY SAND black, fine to medium, (Sanitary with paper, wood, Landfill) plastic, metal & wire, organic odor (from drill action, concrete pieces 5-16.5' depth)	- 335	
	- 6 1A 12 10	10.8	SILTY SAND brown, organic, little SM very medium gravel, trace roots moist dense	F 340	
1 DEPATE	Stante NO.	OTHER REST BOT	BUSSURFACE CONDITIONS WAT THE LOCATION OF THIS DONING AND AT THE THE OF DRILLING BUSSURFACE CONDITIONS WAT DIFFER AT OTHER LOCATION BAT CHANGE ANT THIS LOCATION WITH THE PASSAGE OF TIME THE BATA POESENTED IS A SIMPLIFICATION OF ACTUAL CONDITIONS BECOUNTERED DESCRIPTION BUSSURFACE ADDITIONS	TLEV	
C	ATE DRILLED.	10/2/82	SUMMARY: BORING NO. 8 - 82 ELEVATION 340.4		
OFOTH	DATE DRILLED.	10/2/82	SUMMARY: BORING NO. 8-67	Cont.) ELEVATION	
-------	--	---	---	------------------	----------------------------
0 - 0	9A 50/5'	4.8	SAND (Cont.) brown, fine to coarse, silt matrix, trace gravel	moist ver den	y Se
5 -			Bottom of boring at depth 43.5' No groundwater encountered Piezometer installed to depth 43.5' with 2' slotted interval at bottom.	**	
-					-
					-
					-
1					
	apill-spoon sam 0.D. thin-wall sa -1/2 [°] 0.D. spill b	pier impier C. 3-1/4 erret sampier X. s	* O.D. x 2-1/2* Mner ** A = Atterberg, C = consolidation, D8 = direct ample not recovered G = grain size, T = triaxist, P = permeability	t shear,	vol lus cosi tor tip
			EASTGATE TRUNK SEWER Bellevue, Washington for Brown and Caldwell	Projec 82-5	5169
R	Con	verse C	DNSUITANTS Geolechnical Engineering and Applied Sciences	- Trawi	Ays







	ÎT		SILTY SAND	brown, fine to medium, little gravel, trace	SM	very	loose	F
1A	4 4 5	19.0	(+111)	wood, organic				~ ~ ~ ~
2A	7	5.6	GRAVELLY SAND (Fill)	gray, fine to medium, trace silt	SW	moist	dense	
	45		(concrete pi based on cut	eces throughout fill tings)				
3Х	50/3'		(sample 3 dr	riven on concrete)				
4A	20 15	16.6	CLAYEY SILT (Sanitary Landfill)	gray, mottled brown, some sand, trace glass, wire & paper	MH	very moist	medium dense	- 1 1- L
			SILTY SAND	brown, fine to medium,	SM	very moist	medium	
5A	7 12 15	25.1	Landfill)	TILLE GLAVET, WOOD			UENSE	
6A	50/6"	4.7	SAND	gray, fine to coarse, trace gravel, trace silt	SP	moist	very dense	
7A	50/6"	8.3						
88	23 23 30	12.1		(Continued)		 very moist		
split-s D.D. 11 1/2* 0	ipoon sampler hin-wall samp).D. split barre	ler C. 3-1/4 I sampler X. si	"O.D. z 2-1/2" Uner **/	i =Atterberg, C = consolidation, DS = direct 3 = grain size, T = triaxial, P = permeability	shear,	ľ	water level Impervious seal plezometer tip	
			EASTGATE Bellevue	TRUNK SEWER , Washington			Project No. 82-5169	

DATE	DRILLED:]	2/7/82	SUMMARY: BORING NO. 11 -82 ELEVATION 306.	6
FEET	PLE NO. ON SI	WER TESTS OF OFT	THIS BUMBARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF BRILLING BUBBURFACE CONCITIONS WAY BIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SUBPLIFICATION OF ACTUAL CONDITIONS ENCOUNTERED.	
	5° 6°	<u>0' f' + 0'</u>	DESCRIPTIONSYMBOL MOISTURECONSISSILTY SANDdk. brn., f/m, little SM wetloos(Fill)gravel, trace rootsloos	E E
1A	- 3 7 1	18.6	SAND gray, fine to medium, (Fill) trace silt, SP wet loose occasional gravel	e -
2A	7 8	16.6	SILTY TO brown, fine to coarseSM wet dense CLAYEY SAND trace to occasional (Advance grave)	
	30		Outwash) II2/7/82 INV grades to rust-brown, fine to SAND coarse, trace silt, SP	ERTE
ЗА	6 28 32	9.2	occasional gravel moist dense	
			Bottom of boring at depth 14.5' Groundwater encountered during drilling at depth 9.5'	2
				-
				-
				F
				F
0.D. thin 1/3" O.D	-wall sampler). split barrel	r C. 3-1/4° C sampler X. sam	D.D. x 2-1/2" liner **A - Atterberg, C - consolidation, DS - direct shear, impervious a ple not recovered G - grain size, T - triaxial, P - permeability plezometer	tip
			EASTGATE TRUNK SEWER Project No Bellevue, Washington 82-516 for Brown and Caldwell	5. 59



0	A. Somple	LEACHATE SAMPLI I-90/Bellevue B for Cabot, Cabo	n elze, T - triazial, P - permeability NG Usiness Park t. & Forbes	iear,		Project No. 81-5216
-spoon sampler thin-wall sampler O.D. split barrel s	C. 3-1/4" O.D.	x 2-1/2" Iner ** A - Atte	rberg, C - consolidation, DS - direct al		1	water level Impervious seal
			~			
		Bottom of bor Piezometer in for details) Groundwater e 7.0' at time	ring at depth 14.0' stalled (see schemati ncountered at depth of drilling.	C		
3 18 50/6'		SILTY SAND (Landfill Debris)	gray, fine to medium, abundant organics & metal debris	S11	wet	dense
2 39 18		SILTY GRAVELLY SAND (Fill)	dark gray, fine to coarse, trace organic (landfill debris?)	SM	wet	dense
1 18 19		SILTY SAND (Fill) SAND (Fill)	dark greenish-gray, fine to coarse, litt gravel light gray, fine to medium, trace silt	lesm	very moist	V 4/27/89 √ 4/27/89 √ 7/8/83 dense
Set grant stant or	OTHER TE DO DAY	OESCRIPTION	CONDITIONS MAY BIFFER AT OTHER LOCATIONS BRAGE OF TIME. THE DATA PRESENTED IS A DIM D	AND MAY CH PLIPICATION	THE TIME OF	BRILLING LOCATION CONDITIONS 4/14/83

Date Drilled: 3/26/83

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Elevation: Approx. 349



C/2/05		
DATE DRILLED: 0/ 3/ 85	SUMMARY: BORING NO. B-301	ELEVATION Approx. 342
OEPTHEET SPEEDONE THE TESTS OF ON THE	THIS SUBBARY APPLIES ONLY AT THE LOCATION OF THIS DOAINS AND A SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONE AND MAY C WITH THE PABBAGE OF TIME. THE BATA PRESENTED IS A DIMPLIFICATION SUCOUNTERED.	T THE THE OF DALLING MARGE AT THIS LOCATION OR OF ACTUAL CONDITIONS
	DESCRIPTION SYM	OL MOISTURE CONSISTENCY
	gray, fine to medium, little gravel, trace wood, concrete	moist [#] medium - dense - -
	SILTY SAND (Sanitary Landfill); SM black, fine to medium, some sanitary refuse: glass, wood, etc., strong organic smell;	moist medium dense
10 - - - - - - - - - - - - - - - - - - -	grades to debris fill: glass, wood, paper, cans; no soil matrix; visible methane	moist
	Bottom of boring at depth 12.8' 3/4" diameter PVC observation well installed with slotted screen from 7.5' to 12.5', pea gravel backfill from 5.0' to 10.5', backfill with cuttings from 5.0' to 3.0', benton- ite seal from 3.0' to surface, and install cast iron monument cover.	
		-
* A. 2" split-spoon sampler B. 3" O.D. thin-wall sampler C. 3-1/4" O.D D. 3-1/2" O.D. split barrel sampler X. sample FASTG2	D. I 2-1/2" Mner **A - Atterberg, C - consolidation, DS - direct shear, a not recovered G - grain elze, T - triazial, P - permeability ATE I ANDETITI WATED CAMDITING	water level impervious seal plezometer tip
for	Bellevue, Washington Boeing Computer Services	85-5104-02
Converse Com	Geotechnical Engineering	Drawing No.
e conterse con	SUILCIILS and Applied Sciences	2

19-19

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	DESCRIPTION	SYMBO	DL MOISTURE	CONSISTENC
1CII 50/5"	SILIY SAND (Fill); brown, fine to medium, little gravel, trace wood (sampler driving on rock)	SM	moist	medium dense
- 5 - 2C	SAND (Fill); gray, fine to medium, trace gravel, wood, & metal debris	SP	moist	medium dense
- 	SANITARY LANDFILL; consists of wood, glass, plastic, rubber, paper and metal; no soil matrix;		moist	dense
- 4C	occasional lense of sand	6/2	very moist 1/85▽	
5C 33 17 21	(possible free water)		6/7/85 very moist	
	Bottom of boring at depth 24.0' 3/4" dia. PVC observation well insta slotted screen from 17.5' to 22.5', pea gravel backfill from 9.0' to 22.5', backfilled with cuttings from 3.0' to 9.0', bentonite seal from 3.0' to surface, and install cast iron monument cover.	lled	with	
split-spoon sampler O.D. thin-wall sampler C. 3-1/ 1/2" O.D. split barrel sampler X. FA	 4° O.D. x 2-1/2″ liner A - Atterberg, C - consolidation, DS - direct al ample not recovered G - grain size, T - triaxial, P - permeability STGATE LANDETLL HATER ON PARTY 	Hear,	t ^v wa ∳ im ⊡ pie	ter level pervious seal zometer tip

DATE DRILLED: 6/4/85	SUMMARY: BORING NO. B-303-	45 ELEVATIN	ADDROY
0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	THIS SUBBARY APPLIES ONLY AT THE LOCATION OF THIS DOBING AND	TTHE TIME OF BAIL	CONSISTENT
- 1C 14 12	SILTY SAND (Fill); gray-brown, fine SM to medium, little gravel, trace wood	moist	medium dense
2C 8 14	grades to black, trace wood, plastic, and metal debris		
$3C = \frac{8}{12}$	SILTY SAND (Sanitary Landfill); SM black, fine to medium, trace gravel, wood, plastic, metal, wire, and paper	very moist	medium dense
4C 10 12 12 20			
5C 29 11 8	grades to Sanitary London		
	little silty sand	moist =	
20 - 13 - 8C 19	SILTY SAND (Old Soil Horizon/Fill); SM brown, tr. to little gravel track	very	medium
<u> </u>	wood & glass	moist	dense _
	(Continued)	<u>I</u>	
r spill-spoon sampler " O.D. thin-wall sampler C. 3-1/4" (-1/2" O.D. spill barrel sampler X. sam	D.D. x 2-1/2" liner ** A - Atterberg, C - consolidation, DS - direct shear, opie not recovered G - grain size, T - triaxial. P - marmashility	· · · · · · · · · · · · · · · · · · ·	ter level pervious seal
EAST	GATE LANDFILL WATER SAMPLING Bellevue, Washington r Boeing Computer Services	ti pie	zometer tip Project No. 85–5104–02
			Prawing No.

	DESCRIPTION	SYMB	OL MOISTURE	CONSISTENCY
90 1 68	SILTY SAND (Cont.);	SM		dense
50/3"				
100 <u>57</u> 50/3"	SILTY SAND (Weath. Glacial Till) gray, f/m, trace to little grave	; SM	wet	very dense
	grades to Unweath. Till, with occ. lense of gravelly silty sand and sandy silt	d SM	moist	
11AT 60/6"				
12AT 60/6"	SAND (Advance Outwash); brown, f to medium, trace silt, thinly bed ded with sandy silt layers	ine SP 1-	moist	very dense
			wet	
13AT 27 50/6"			6/7/85 6/21/85 	
14AT 20 50/6"	SANDY SILT (Lacustrine Sediments) gray, fine sand, thinly laminated with clayey silt and silty fine s	; ML and	very moist	very dense
7 15A 13	SAND; dark gray, very fine, trace to little silt	SM	wet	very dense
160 55 50/3"	grades fine to medium, thinly bed to laminated with clayey silt and brown sandy silt	ded	very moist	
	(Continued)			
BRIII-spoon sempler			- 21	rater level
0.D. thin-wall sampler C. 3- 1/2" 0.D. spilt barret sampler 3	1/4° O.D. x 2-1/2° liner * A -Atterberg, C - consolidation, DS - d A sample not recovered G - grain size, T - triaxial, P - permest	weet shear,		mpervious eesi lezometer tip
E	ASTGATE LANDFILL WATER SAMPLING			Project No.

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DATE DRILLED: 6/4/85	SUMMARY: BORING NO. B	-303 -45	ELEVATIO	N:
A. J. (NO. 16 (55.05	UNE CON THIS BURNARY APPLIES OULY AT THE LOCATION OF THIS AUBSUNPACE CONDITIONS MAY BIPPER AT OTHER LOCATION	LONT .)	E TINE OF BRILLI	NG TION
FEE SHOPLE ONS STHER THE OF OF			ACTUAL CONDIT	1016
	- BESCHIFTION	SYMBOL	WOISTURE	CONSISTENC
	Bottom of boring at depth 78.2' Groundwater encountered at depth 64' during drilling 2" diameter PVC observation well installed with slotted screen fro 55' to 75'; sand backfill from 50 to 71'; grout backfill from 19' t 50'; dry cement backfill from 12'	n ' D to		
	19'; backfilled with cuttings fro 1' to 12', and cast iron monument cover installed at surface.	n		
t" spilt-spoon sampler 1" O.D. thin-wall sampler C. 3-1/ 1-1/2" O.D. spilt berrel sampler X.	4° O.D. x 2-1/2″ liner ^{••} A ⁻ Atterberg, C - consolidation, DS - di sample not recovered G - grain size, T - triaxial, P - permesb STCATE I ANDELLI MATER CAMPLANC	rect shear, lilty		water level Impervious seal plezometer tip Project No.
EA	Bellevue, Washington for Boeing Computer Services			85-5104
Converse C	Onsultants Geolechnical Engineering and Applied Sciences			4 (COM

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DATE DRILLED: 4/4/85		1 115	
	THIS BURNARY APPLIES ONLY AT THE LOCATION OF THIS PORING	L -W3 ELEVATH	on: Approx. 302
OFFICE AND TRACE ONSING THE	A O A C C COUNTERED OF TIME THE BATA PRESENTED IS A SIMPLIF	MAY CHANDE AT THIS LOC ICATION OF ACTUAL COND	LING Cation Itions
0	C & DESCRIPTION	SYNBOL MOISTURE	CONSISTENCY
6	to medium, trace silt & organics	slight	ymedium
	grades to little gravel	moist	aense
5 7	SILTY SAND; mottled grav & light	moist	-
	brown, fine to medium, trace clay	morst	dense
28	SILTY SAND: GROUP Fine to The		I F
	little gravel, trace clav	wet	very -
- 4X _ 50/4"			
	SILTY SAND (Unweathered Till):	slight]	
	light brown, fine to medium, little	moist	dense -
-6C 15 50/4"	State cray		
			-
20 7A 50/4"			
	SAND (Advance Outwach) + hours		
	fine to medium, trace silt	wet	very -
- 50/4"			-
	CAND / Los I I I I		
30 - 7 26	light brown, fine, trace medium	slightly	very -
ЧЧЦ 40 Ч 50/5"	trace silt with thinly laminated to	morse	dense -
	silt		
35 25			
			E I
	Bottom of boring at depth 36 5'		
1 11 1	Groundwater encountered at depth 9'		F
	Hole filled with cement/bentonite		
	to surface.		
A. 2" SpHt-speen specie			
8. 3" O.D. thin-wall sampler C. D. 3-1/2" O.D. spill barrel samplar	3-1/4" O.D. z 2-1/2" liner **A -Atterberg, C - consolidation, DS - direct sha	ar, 1 ²² wa	iter leval Pervious seal
	SLURRY TRENCH FFASTRILITY STUDY	i pie	zometer tip
	Boeing Computer Services		Project No. 85-5104
	berievue, wasnington	;	
Converse	Consultants Geotechnical Engineering and Applied Sciences		
			~

DATE DRILLED.4/4/85	SUMMARY: BORING NO. CC-	2-45 ADDEOX 302
SEPTYFET SPERFERSONS STREETES	THIS BUBMARY APPLIES ONLY AT THE LOCATION OF THIS BOBIN THIS BUBMERACE CONDITIONS MAY DIFFER AT OTHER LOCATION OF THIS BOBIN THE PASSASE OF THE THE BATA PRESENTED IS A SHOPL OF A OF C SHCOUTEBED	IS AND AT THE THE OF BRILLING IS MAT CHANGE AT THIS LOCATION IFICATION OF ACTUAL CONDITIONS
0	DESCRIPTION	SYMBOL MOISTURE CONSISTENCY
17	GRAVELLY SAND (Fill); light brown, fine to medium, trace silt	slightly moist
$\begin{array}{c} 1 \\ 1 \\ 1 \\ 5 \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ -$	GRAVELLY SILTY SAND; mottled brown & light brown, fine to medium	slightly medium moist dense
-2A 5 -2A 7 8	SANDY SILT/CLAYEY SILT (Alluvium); mottled gray-green & light brown, fine, thinly laminated	slightly medium moist dense
	CLAYEY SAND (Advance Outwash); gray, fine to medium, trace gravel	moist very dense
5 _4A = 50/6	SAND; gray, fine to medium, little silt, trace gravel	moist very - dense -
5A 48 50/5	grades to trace silt and gravel	4/17/85
-6A -26 -26 -29	with occ. thin laminations of silty sand	moist to wet
-7A 44 - 50/2' - 124	to mottled gray & light brown	wet
-8A 37 -37 34 -9A 35 -50/5"	with medium bedded brown silt and thin laminations to thinly bedded silty fine sand	slightly very moist dense
$ \begin{array}{c} 10 \\ -10 \\ -11 \\$	SILTY SAND (Lacustrine); dark gray, fine, with thin laminations to thinly bedded silt and fine cand	slightly dense moist
39 12A 21 12A 29	SAND; brown, fine to medium, trace silt, with medium bedded fine sandy silt	wet very dense
43 1B 13A 25 42	to gray, fine, med. bedded gray <u>silt. thin lam. of fine sandy silt</u> SILT; dark gray, w/thin laminations to medium bedded sandy silt	wet very
	(Continued)	
2° spHi-spoon sampler 3° O.D. thin-wall sampler C. 8-1/ 3-1/2° O.D. spilt barrel sampler X.	4° O.D. x 2-1/2° liner **A - Atterberg, C - consolidation, DS - direct sh sample net recovered G - grain size, T - triaxisi, P - permeability	sar, piezomater tip
	BLURRY IRENCH FEASIBILITY STUDY Boeing Computer Services Bellevue, Washington	Project No. 85-5104
Converse C	Onsultants Geotechnical Engineering and Applied Sciences	Drawing No.





FEE SERVER SORS OTHER REPORT	THIS SUBMARY APPLIES BELV AT THE LOCATION OF THIS BOILD AND A SUBSURFACE CONDITIONS MAY SHIPPER AT OTHER LOCATION OF THIS BOILD AND M WITH THE PASSAGE OF THE THE DATA PRESENTED IS A DIMPLIFIC SUCCUMTERS.	AT THE THE OF DELLER AT CHANGE AT THIS LOCAT ATION OF ACTUAL CONDITI YMBOL MOISTURE	CONSISTEN
10AT 21 50/3" 11AT 26 50/6"	SAND (Adv. Outwash) (Cont.); SAND (Lacustrine); gray, fine, trace silt, with med. bedded silt <u>& thin lam, of fine sandy silt</u> SILT; dark gray, trace fine sand, w/thin beds of mottled gray & light brown, fine to medium sand and	wet moist moist	very dense very very
25 12A 35 38 13A 27 13A 50/3	silty sand, & thin lam. fine sandy silt, occ. thin lamination of peat w/thin laminations of fine sand with medium bedded silty fine sand, and thin laminae of fine sand time	slightly moist	navd
14A 27 40 53/3' 15A 36 50/3'	with thinly bedded silty fine sand, and thin laminations of fine sandy silt mottled dark gray & light brown, trace fine sand, with med. bedded fine sand	moist	
	Bottom of boring at depth 68.5' Groundwater encountered at depth 20' Hole filled with cement/bentonite slurry from 68.5 to surface.		
belit-spoon sampler D.D. thin-well sampler C. 3-1/ /2" O.D. spilt barrel sampler X. SL BC	4" O.D. x 2-1/2" Hnor "A - Attorborg, C - concolidation, DS - direct she sample not recovered G - grain size, T - triaxist, P - permeability URRY TRENCH FEASIBILITY STUDY being Computer Services	ar,	ter level pervious seat someter tip Project No. 35-5104



LOG OF TEST PIT NO. 201 (Cont.) PROJECT: 27.2 Acre Site JOB NO : 85-5156 ____DATE: 6/20/85 Boeing Computer Services ELEVATION: Approx. 344 CLIENT FEATURE: _____ LOCATION: ____ See Drawing GROUNDWATER LEVEL: _____ LOGGED BY: _____. DEPTH SAMPLE SOIL DESCRIPTION NO. SYM. (ft) REMARKS SM SILTY SAND (Fill); brown, fine to medium, little gravel, trace roots; moist, medium dense 1. 2color changes to gray color changes to brown 3. SANITARY LANDFILL; black, household garbage, cans, strong trash glass, wire; very moist odor throughout SILTY SAND (Weath. Till); brown, fine to medium, SM little gravel, occasional cobbles; moist, dense 5-(Unweath. Till); gray-brown; moist, very dense SM 6. Bottom of test pit at depth 6.0' No groundwater endountered Completed 6/20/85 **GRAPHIC LOG** - West Face 0-SM (Fill, brown) 1-

SM (Fill, gray) 2-SM (Fill, brown) 3-4 SM (Weathered Till) 5-Sanitary 6-Landfill SM (Unweathered Till) -0+500+60 0+70 0 + 80PROPOSED 27.2 ACRE SITE Project No. Bellevue, Washington 85-5156 for Boeing Computer Services Drawing No. Converse Consultants Geotechnical Engineering and Applied Sciences 1 (CONT.)

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PROJ	ECT:_	27.2 Ac	re Site	JOB NO :	DATE: 6/20
CLIEN	T:	Boeing	Computer Services	ELEVATION:	Approx. 3
FEAT	JRE:		L	OCATION: See Drawing	
GROU	NDWA	TER LEV	/EL:	LOGGED BY:	DAY
DEPTH	SAMPLE NO.	SOIL SYM.	DESCR	RIPTION	REMARKS
		SM	SILTY SAND (Fill); bro gravel, trace wood; mo	own, fine to medium, little	
2-					
3-			grades to gray in coro		
4-					
5-					
6-		ML	CLAYEY SILT (Fill); gr	ay, little sand and gravel,	strong tra
7-			ANITRAY LANDFILL; hou cans, glass; moist	sehold garbage, paper, rags,	out
-8			Rottom of tost transh	at donth 7 51	
			lo groundwater encount	ered	
_		C	Completed 6/20/85		
_					
		Sanita	SM (Fill, brown) SM (Fill, gray) <u>ML (Fill)</u> ry Landfill		
0+30		· · · ·	0+40	0+50	0.60
			PROPOSED 27.2 ACRE S Bellevue, Washingto	SITE	UTOU Project No. 85-5156

LOG OF TEST PIT NO. 203-85



LOG OF TEST PIT NO. TP-204-85

Location: See Drawing

Elevation: Approx. 344

Surface Conditions: Flat; sage brush and grass

Depth in feet	Moisture Content-%	Sample	Symbol	DESCRIPTION	REMARKS
12			SM	SILTY SAND (Fill); brown, fine to coarse, little fine to medium gravel, trace subrounded cobbles, roots and organics; slightly moist, medium dense	
3- 4- 5-			SM	SILTY SAND; brown, fine to medium, trace gravel, trace subrounded cobbles; concrete rubble (to 4'), timbers and wood (to 8"), bicycle tires; moist, dense (Fill)	test pit walls standing vertical
6-			ML	CLAYEY SILT; gray, trace gravel, trace fine to medium sand, scattered small branches, roots, and organics; moist, firm (Fill)	
8- 9- 10-					
11-				Bottom of test pit at depth 12.0'	
-				Completed 6/21/85	
				PROPOSED 27.2 ACRE SITE	Project No
~				Bellevue, Washington for Boeing Computer Services	85-5156
3	Con	ve	rse	Consultants Geotechnical Engineering and Applied Sciences	Drawing No 4

LOG OF TEST PIT NO. TP-213-85

Location: See Drawing

Elevation: Approx. 338

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Surface Conditions: Flat; some small weeds

the second s			
ristine internet	.vmhol	DESCRIPTION	REMARKS
	SM	SILTY SAND (Fill); brown, fine, trace medium to coarse sand, little fine to coarse subrounded gravel; scattered roots, and sticks; moist, medium dense	
9- 4 4 4 4 4 9- 10	K.	CLAYEY SILT; gray, trace fine to medium sand, little gravel, scattered small to medium cobbles; concrete rubble to (18"), wood, logs (6"), paper, plastic, and metal scraps; with occasional medium beds of silty sand, brown, fine to medium; moist, firm (Fill)	distinct organic odor
33-		Bottom of test pit at depth 12.0' No groundwater encountered Completed 6/21/85	
		PROPOSED 27.2 ACRE SITE Bellevue, Washington	Froject No 85-5156
Conver	se	Consultants Geotechnical Engineering and Applied Sciences	Drawing No 13

(OW-1)

5/28/02

A4IN1.GDT

B3.G

4IN1



OW-1

PROJECT: Bellevue Airport / Eastgate Landfill

A4IN1.GDT 5/28/02

4IN1 B3.C

Location: Noth stde of Pont A Approximate ground surface elevation: 305 feet 30 40 40 40 40 40 40 40 40 40 4	. EQ	Soil Description	SGS	щ	щe	9~	PEN	TRATION RESIST	ANCE	-
-30 Approximate ground surface elevation: 305 feet 98 31 42 83 0 0 00	(fee	Location: North side of Pond A	D'SAU	WPI	MPL	NE	Standard	Blows over inches	A	Page 2
Very dense SAND (as above) S6 0 20 30 40	-30-	Approximate ground surface elevation: 305 feet	GR	SA	SA	R S	0 10	Blows per foot	ouler	of 2
35 S6 S7 Image: Solution of the same fine same fi		Voridence DAND (T		8	: 10	20 30	40 50	TESTING
35 Hard, wet, gray, SLT, some fine sand (Glacial-Jacustrine Deposit) 57 Image: Strate		very dense SAND (as above)			S6 _				laori-	
35- Hard, wei, gray, SLT, some fine sand (Glacial-lacustrine Deposit) 57 80 40- 40- Boring terminated at approximately 41.5 feet below ground surface. 58 10 50- 55- 56- 56- 56- 56- 56- 56- 56- 56- 56									·····	
35 Hord, veil, gray, SILT, some fine sand (Olecial-licoustrie Deposit) 57 Image: Constraints of the sand (Olecial-licoustrie Deposit) 40 58 S8 Image: Constraints of the sand (Olecial-licoustrie Deposit) 50 58 Image: Constraint (Licoustrie Deposit) 50 58 Image: Cons										
35 Hard, wet, gray, SLIT, some fire and S7 S7 Image: Constraints of the stand 40 58 S8 S8 S8 S8 40 58 S8 S8 S8 S8 50 58 S8 S9 S9 </td <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td>					-					
35- Herd, wet, gray, SiLT, some fine aand (Clacial-lacuatrine Deposit) 57 57 40- 58 58 50 50- 58 58 50 50- 50 50 50 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 50- 1 1 1 1 50- 1 1 1 1 1 60- LEGEND Observation well: 1 1 1 10- 1 1 1 1 1 1 1 1 20- 0 0 0 </td <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	-									
Hard, wet, gray, Sill, T, some fine sand ((Bladal-lacustrine Deposit)) 57 57 1000000000000000000000000000000000000	- 35-								••• ••••	-
Halt, Wei, Gray, S.L.I, Some the sand (Gladial-lacustime Deposit) Boring terminated at approximately 41.5 feet below ground surface. 5 5 5 50 51 52 55 55 55 56 57 58 59 50 50 50 51 52 55 55 56 57 58 59 50 50 50 50 50 50 50 50 50 50 50 50 50 50 <			-		67					
-40- Boring terminated at approximately 41.5 feet 5-		(Glacial-lacustrine Deposit)	11114			日			50/4	
40- 58 58 Boring terminated at approximately 41.5 feet 58 58 5- 58 58						目				1
40 58 0 10 Boring terminated at approximately 41.5 feet 0 0 10 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 0 50 0 0 0 0 0 0 50 0 0 0 0 0 0 0 50 0 0 0 0 0 0].	目				-
40 58 1 10 Boring terminated at approximately 41.5 feet 0 0 0 5 0 0 0 0 50 0 0 0 0 50 0 0 0 0 50 0 0 0 0 55 0 0 0 0 55 0 0 0 0 55 0 0 0 0 55 0 0 0 0 0 55 0 0 0 0 0 0 55 0 0 0 0 0 0 0 55 0			-		-	日		•••••		1
40- 58 100 Borting terminated at approximately 41.5 feet 100 5- 100			1111-		- SOA					
S0 S0 ID Boring terminated at approximately 41.5 feet ID ID 5- ID ID ID 5- ID ID ID ID 5- ID ID ID ID 5- ID ID ID ID ID 5- ID ID ID ID ID ID 5- ID ID<	- 40-				P					1
Boring terminated at approximately 41.5 feet Image: Construction will below ground surface. 5- Image: Construction will below ground surface.					R					-
Boring terminated at approximately 41.5 feet below ground surface. 5- 5- 5- 5- 5- 5- 5- 5- 5- 5-					30 R				70:	1
below ground surface. 5- 5- 5- 5- 5- 5- 5- 5- 5- 5-		Boring terminated at approximately 41.5 feet			-					
5- -50- -		below ground surface.								1
50- 50- 50- 55- 60- LEGEND 200-rb0 combuster level at Bith spon sampler 200-rb0 combuster level at 200-rb0 combuster level at			11		1			••••		+
5 50 55 60 200-rote target are at at a set of the	1		1 1		1					-
-50- -50- 55- 60- LEGEND 200-rokoter iswi at gift-spons sampler → ☆ Groundwater iswi at splf-spons sampler → ☆ Groundwater iswi at Sml Till with PUC Rps Sml Till with PUC Rps	5-				4					
50- 55- 60 LEGEND Observation well: 200-trich OD gdi-spons sampler → trice of dating 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0										1
-50- -50- -50- -50- -50- -55- -50- -55-			11		1					-
-50- -50- -50- -55- -55- -56- -56- -57- <			1 1		-					1
-50- -50- -55-					-					
-50- -50- -55-										1
00 0	- 50-				1					+
2.00-inch OD split-spoon sampler Image: Constraint of the of dating 2.00-inch OD split-spoon sampler Image: Constraint of the of dating 0 LEGEND 0 Description of the of dating 0 20 1 3335 N.E. 122nd Way Suite 100 Kirkland, Washington 98034-6913	00		-		+	-				4
55- 60 LEGEND 2.00-inch OD split-spoon sampler Monumer 2.00-inch OD split-spoon sampler Monumer Monumer Bantonite Fill with Sicited PVC Pipe Groundwater lavel at Sand Fill with Sicited PVC Pipe Sand Fill with Sicited PVC Pipe Sand Fill with Sicited PVC Pipe Pipe Cp Sand Fill with Sicited PVC Pipe			-		-					
55- 60 LEGEND 2.00-Inch OD spB-spoon sampler Monumer Monumer Bantonite Fill with PVC Pipe Groundwater lavel at time of dailing Monumer Groundwater lavel at time of dailing										1
255- 60 LEGEND 200-inch OD split-spoon sampler ATD Groundwater lavel at split-spoon sampler Observation well: 0 200-inch OD split-spoon sampler Observation well: 0 Observation well: 0 200-inch OD split-spoon sampler Observation well: 0 200-inch OD split-spoon sampler Observation well: 0 200-inch OD split-spoon sampler Observation well: 0 0 20 40 60 8 60 9 0 9 0 9 0 9 0 9 0 9 0 9 0 1335 N.E. 122nd Way Suite 100 Kirkland, Washington 98034-6913					1	-				-
55- 60 LEGEND 2200-inch OD split-spoon sampler ATD Groundwater level at split-spoon sampler Observation well: 0 20 40 0 200-inch OD split-spoon sampler To Groundwater level at time of dtilling Observation well: 0 20 40 60 8 Monument Weisture Content Liquid Limit Groundwater Level Sand Fill with Stotted PVC Pipe Pipe Cap 11335 N.E. 122nd Way Suite 100 Kirkland, Washington 98034-6913			+	1	-					-
55- 60 LEGEND 2.00-inch OD split-spoon sampler ATD time of dilling U LEGEND 1.200-inch OD split-spoon sampler ↓ U LEGEND ↓ U			-		1					
60 LEGEND 2.00-inch OD split-spoor sampler ∑ applit-spoor sampler ∑ Groundwater lavel at time of dilling Observation well: Bartonite Fill with PVC Pipe Groundwater Lavel Sand Fill with Slotted PVC Pipe Sand Fill with Slotted PVC Pipe Discrete Care 11335 N.E. 122nd Way Suite 100 Kirkland, Washington 98034-6913	- 55-									1
60 LEGEND 2.00-inch OD split-spoon sampler Coundwater level at time of dailing Monument 0 200-inch OD split-spoon sampler Coundwater level at time of dailing Monument 0 Bentonite Fill with PVC Pipe Groundwater Level Sand Fill with Stotted PVC Pipe Pipe Cap Pipe Cap With stotted PVC Pipe 11335 N.E. 122nd Way Suite 100 Kirkland, Washington 98034-6913					T					-
60 LEGEND 2.00-inch OD split-spoon sampler Groundwater level at time of drilling 2.00-inch OD split-spoon sampler Groundwater level at time of drilling 0 Image: Content of the split spl			1		1					
60 LEGEND 2.00-Inch OD split-spoon sampler → TD Groundwater level at time of dniling With Advine Groundwater level Sand Fill with Stoted PVC Pipe Groundwater Level Sand Fill with Stoted PVC Pipe Pipe Cap Sinch at Bartonite Fill with PVC Pipe Fipe Cap Sinch at Bartonite for Stoted PVC Pipe 11335 N.E. 122nd Way Suite 100 Kirkland, Washington 98034-6913	-		4		-					
60 LEGEND 2.00-inch OD split-spoon sampler ATD time of dnilling Observation well: 0 20 40 60 80 100 Plastic Limit Meisture Content Liquid Limit Bentonite Fill with PVC Pipe Groundwater Level Sand Fill with Stotted PVC Pipe Fipe Cap Fipe Ca			1							1
60 LEGEND Observation well: 2.00-inch OD split-spoon sampler ATD time of drilling Observation well: Destroater Level Sand Fill with PVC Pipe Of the State of					1					-
60 LEGEND Observation well: 0 20 40 60 80 100 2.00-Inch OD split-spoon sampler To Groundwater level at time of dailing Monument Plastic Limit Molecture Content Liquid Limit Bentonite Fill with PVC Pipe Groundwater Level Sand Fill with Stoted PVC Pipe I1335 N.E. 122nd Way Suite 100 Viii a datume Pipe Cap Singh # Bartom of Hole 11335 N.E. 122nd Way Suite 100			1		+					-
2.00-Inch OD split-spoon sampler Split-spoon sampler Split-spoon sampler Split-spoon sampler Split-spoon sampler Observation well: 0 20 40 60 80 100 Plastic Limit Monument Plastic Limit Moisture Content Liquid Limit Bentonite Fill with PVC Pipe Groundwater Level Sand Fill with Stotted PVC Pipe 11335 N.E. 122nd Way Suite 100 With a bit wine Pipe Cap Pipe Cap 11335 N.E. 122nd Way Suite 100	60	LECEND				_				
split-spoon sampler ATD Groundwater level at Liquid Limit split-spoon sampler ATD time of drilling Groundwater level Sand Fill with Stotted PVC Pipe Sand Fill with Stotted PVC Pipe Sand Fill with Stotted PVC Pipe Single Cap Single Cap Sin	7 Of look		Obs	B Monur	on well:	0	20	60 80	100	
Groundwater Level Sand Fill with Stotted PVC Pipe Pipe Cap Pipe Cap Sindh at Bottom of Hole Sand Fill with Stotted PVC Pipe Pipe Cap	split-spoon	sampler Groundwater level at time of drilling	uum	Bantos		Plastic	: Limit J	Acisture Content L	iquid Limit	
Groundwater Level Sand Fill with Stotted PVC Pipe Pipe Cap Pipe Cap Singh at Battion of Hole Kirkland, Washington 98034-6913				and the search	NAR FILL WILL	PVG Pipe		0		
Sand Fill with Slotted PVC Pipe Pipe Cap Pipe Cap Singh at Bottom of Hole Kirkland, Washington 98034-6913				Gmun	dwater I av	el	9	nec		
Pipe Cap Slough at Bottom of Hole 11335 N.E. 122nd Way Suite 100 Kirkland, Washington 98034-6913				Sand I	Fill with Slo	tted PVC Pi				
Sound Store				Pipe C	ap	-	1133 Kirkl	5 N.E. 122nd Way S and, Washington 980	Suite 100	
hilling Method: HSA Hammer type: Winch Date drilled: March 27, 2002 Logged Bur KSS	Drilling Meth	od: HSA Hammer type: Winch		Date	e drilled	: March	27. 2002	Longed By	Kee	_

0W-2

5/28/02

/A4IN1.GDT

4IN1 B3.



et) H	Soil Description	SGS	щ.,,	щœ	9«	PENE	TRATION RESIST	TANCE	T
E E	Location: South side of Pond A	APH	MP	MPI	ATE	Standard	Blows over inches		1
- 30-	Approximate ground surface elevation: 308 feet	SUS	S	NUN	RSX	0 10	Blows per foot	ettici	L
		1.11			S	: 1	20 30	40 50	TE
	Dense, wet to saturated, light brown, fine to	- 190		S6					
	medium SAND, with some silt (Advance	6414	_					•••••	
	Outwash)	[d]		-					
		6 AN		1	3				
		Potor							-
		P.Z.F		+					
- 35-		p 44		1					
		-9H		S7				(source)	
	Hard, moist, gray SILT with some fine sand						•••••		•
	(Glacio-lacustrine Deposit)	4		-3					
		11117		1					
		1111-		-	日一				
40-					目				
			Щ	T8 10	the			50/5*	
	Boring terminated at approximately 40.5 feet	1 -		-					-
-	below ground surface			1					
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	LEGEND	Ohe	anyatic	1 walls	0	20 4		100	
2.00-inch O			Monum	ent	Plastic	Limit	laisture Content		
split-spoon	sampler V level		Bentoni	e Fill with	PVC Pipe		NAME COMEN	Liquid Limit	
split-Spoon	sampler ATD time of drilling						9		
		X	Ground	water Lava	N]	nec		
		通	Sand F	I with Slot	ted PVC Plo	•			
			Dine			1133	5 N.E. 122nd Way	Suite 100	
			ripe ca	P		Ville	and Manhl-1.		

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1-91M-14173-0 BORING No. B-3 W.O.



FIGURE 2

BELLEVUE, WASHINGT	ON PROJECT 7805	9
	70-1-74	I
	TEST PIT 1 (EL. 332+)	
DEPTH, FEET		
0.0 - 1.0	LOOSE BROWN SILTY SAND WITH GRAVEL (MOIST) (FILL)	SOME TO TRACE
1.0 - 1.5	LOOSE GRAY SILTY SAND WITH SO (WET) (FILL)	DME GRAVEL
1.5 - 13.0	HOUSEHOLD GARBAGE MIXED WITH SOME GRAVEL AND LIMBS (WET) (STRONG ODOR)	SILTY SAND WITH (MODERATE TO
	NO GROUNDWATER OBSERVED	
	TP-2-78	
	TEST PIT 2 (EL. 312+)	
DEPTH, FEET		
0.0 - 3.5	LOOSE BROWN SILTY FINE SAND W (MOIST) (FILL) SMALL TREES	ITH TRACE GRAVEL
3.5 - 8.0	MEDIUM DENSE TO DENSE GRAY SI SOME GRAVEL TO GRAVELLY SILTY	LTY <u>SAND</u> WITH SAND (WET) (FILL)
8.0 - 9.5	MEDIUM DENSE GRAY CLEAN GRAVE (FILL)	LLY <u>SAND</u> (WET)
	STICKS AT CONTACT	
9.5 - 12.5	MEDIUM DENSE BRUWN SILTY SAND SOME GRAVEL (WE1)	WITH TRACE TO
12.5- 14.0	FIRM BROWN AND GRAY MOTTLED S (WET) (BADLY WEATHERED TILL?)	ILTY FINE SAND
••	GROUNDWATER SEEFAGE AT 3.0 AN LIGHT ODOR	D 14.0 FEET
-	,	

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BELLEVUE, WASHINGT	ON	PROJECT 78059	FIGURE 3
	TP-3-76 TEST PIT	<u>3</u> (EL. 309 <u>+</u>)	
DEPTH, FEET			
0.0 - 1.5	LOOSE TO VERY L WITH ROOTS (MOI DUFF LAYER)	OOSE DARK BROWN SI ST) (TOPSOIL AND T	ILTY <u>SAND</u> THIN FOREST
1.5 - 4.0	MEDIUM DENSE TO SILTY <u>SAND</u> WITH WITH SOME WET Z	DENSE GRAY AND BE TRACE TO SOME GRA ONES) (WEATHERED 7	ROWN MOTTLED AVEL (MOIST ILL)
4.0 - 10.0	DENSE TO VERY D TRACE TO SOME G NEAR- REFUSAL O FEET	ENSE GRAY SILTY <u>SA</u> RAVEL (MOIST) (GLA F EXCAVATING EQUIE	AND WITH ACIAL TILL) PMENT AT 10.0
	NO GROUNDWATER	OBSERVED	
	78-2-78		
	TEST PIT	4 (EL. 329 <u>+</u>)	
DEPTH, FEET			-
0.0 - 4.0	VERY SOFT TO SO SILTY FINE <u>SAND</u>	FT BROWN FINE SAN	DY <u>SILT</u> TO (WET) (FILL)
4.0 - 5.5	LOOSE TO MEDIUM AND <u>SAND</u> MIXED (WET) (FILL)	DENSE DARK BROWN WITH CONCRETE AND	TO BLACK <u>SILT</u> ASPHALT RUBBLE
5.5 - 7.0	CONCRETE RUBBLE		
7.0 - 12.0	LOOSE BROWN SIL GRAVEL AND SCAT	TY SAND WITH TRAC TERED GARBAGE (WE	E TO SOME T) (FILL)
	NO GROUNDWATER Slight to moder	OBSERVED	

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BELLEVUE, WASHINGTON

PROJECT 78059

FIGURE 4

70	-5	-7	Ø
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TEST PIT 5 (EL. 322+)

DEPTH, FEET

- 0.0 1.0 LOOSE BROWN SILTY SAND WITH TRACE GRAVEL (WET) (FILL)
- 1.0 12.0 HOUSEHOLD GARBAGE MIXED WITH SILTY SAND LUMBER AND LIMBS (WET) (NEWSPAPER FROM 1963 STILL READABLE)

NO GROUNDWATER OBSERVED STRONG ODOR

70-6-78

TEST PIT 6 (EL. 333+)

DEPTH, FEET

- 0.0 0.5 LOOSE BROWN SILTY <u>SAND</u> WITH TRACE GRAVEL (WET) (FILL)
- 0.5 1.5 LOOSE GRAY SILTY SAND WITH TRACE GRAVEL (WET) (FILL)
- 1.5 13.0 HOUSEHOLD GARBAGE MIXED WITH SAND, SILT, LIMBS AND LUMBER (WET) (1964 NEWSPAPER AT 3.0 FEET STILL READABLE)

VERY HEAVY GROUNDWATER FLOW AT 4.0 FEET, WATER DOES NOT POND IN BOTTOM OF TEST PIT

VERY STRONG ODOR

<u>TEST PIT 7</u> (EL. 332+)

DEPTH, FEET

- 0.0 0.2 . PEA GRAVEL
- 0.2 5.5 LOOSE TO MEDIUM DENSE BROWN GRAVELLY SAND WITH SOME SILT (MOIST) (FILL)
- 5.5 12.0 HOUSEHOLD GARBAGE MIXED WITH SILTY SAND, LIMBS AND LUMBER (WET) (1962 NEWSPAPER STILL READABLE)

NO GROUNDWATER OBSERVED STRONG ODOR

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BELLEVUE, WASHINGTON

PROJECT 78059

FIGURE 5

70-6-78

TEST PIT 8 (EL. 329+)

DEPTH, FEET

- 0.0 7.5 LOOSE TO MEDIUM DENSE BROWN SILTY SAND WITH TRACE TO SOME GRAVEL (MOIST) (FILL)
- 7.5 12.5 <u>HOUSEHOLD GARBAGE</u> MIXED WITH SILTY SAND, CAR PARTS AND OTHER DEBRIS (WET) (1963 NEWSPAPER STILL READABLE)

MODERATE GROUNDWATER FLOW AT 8.0 FEET STRONG ODOR

71-9-78

TEST PIT 9 (EL. 341+)

DEPTH, FEET

- 0.0 0.2 <u>SOD</u>
- 0.2 2.0 LOOSE TO MEDIUM DENSE BROWN SILTY SAND OF SOME GRAVEL (MOIST) (WEATHERED TILL) -
- 2.0 6.5 DENSE TO VERY DENSE GRAY WITH MINOR BROWN MOTTLING SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (GLACIAL TILL)

NO GROUNDWATER OBSERVED

(1-16-78) TEST PIT 10 (EL. 336+)

DEPTH, FEET

- 0.0 0.5 FOREST DUFF
- 0.5 3.0 LOOSE TO MEDIUM DENSE BROWN SILTY SAND (MOIST)
- 3.0 8.0 LOOSE TO MEDIUM DENSE GRAY SAND WITH SOME LENSES OF HARD GRAY SANDY SILT (MOIST)
- 8.0 10.0 DENSE TO VERY DENSE GRAY SILTY <u>SAND</u> WITH SOME GRAVEL AND TRACE TO OCCASIONAL COBBLES (MOIST) (GLACIAL TILL)

NO GROUNDWATER OBSERVED

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FIGURE 8

BELLEVUE, WASHING	PROJECT 78059
	-78-16-78
	TEST PIT 16 (EL. 300+)
DEPTH, FEET	
0.0 - 0.4	SOD
0.4 - 2.5	MEDIUM DENSE BROWN SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (WEATHERED TILL) SLIGHT GROUNDWATER SEEPAGE AT 2.5 FEET
2.5 - 5.0	MEDIUM DENSE GRAY SILTY SAND WITH SOME GRAVEL (MOIST) (WEATHERED TILL)
5.0 - 10.0	VERY DENSE GRAY SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (GLACIAL TILL)
	TP-17-76 <u>TEST PIT 17</u> (EL. 314 <u>+</u>)
DEPTH, FEET	
0.0 - 5.5	LOOSE BROWN SILTY SAND WITH SOME GRAVEL (WET) (FILL)
5.5 - 6.5	LOOSE GRAY GRAVELLY SILTY SAND TO GRAVELLY SAND WITH SOME SILT (MOIST) (FILL)
6.5 - 11.0	LOOSE TO MEDIUM DENSE BROWN SILTY <u>SAND</u> WITH Some gravel (moist)
11.0-14.0	MEDIUM DENSE TO DENSE LIGHT BROWN TO GRAY SILTY SAND WITH SOME GRAVEL (MOIST) (WEATHERED TILL)
	NO GROUNDWATER OBSERVED

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LEVUE, WASHI	NGTON	PROJECT 78059	FIGURE 9
		~191-78	
	TEST	<u>T PIT 18</u> (EL. 312+) -78	3
DEPTH, FEET			
0.0 - 0.2	SOD		
0.2 - 2.0	LOOSE GRAY Some grave	AND BROWN LAYERED SIL	TY <u>SAND</u> WITH
2.0 - 3.5	LOOSE BROW Household	AN SILTY <u>SAND</u> AND STICK GARBAGE (MOIST) (FILL)	S MIXED WITH
3.5 - 5.0	LOOSE TO M SOME GRAVE	MEDIUM DENSE BROWN SILT EL (MOIST) (WEATHERED T	Y <u>SAND</u> WITH ILL)
5.0 - 12.0	DENSE TO V GRAVEL (MO	VERY DENSE GRAY SILTY <u>SA</u> DIST) (GLACIAL TILL)	AND WITH SOME
	NO GROUNDW	ATER OBSERVED	
	TP - TEST	-19 - 766 <u>PIT 19</u> (EL. 330 <u>+</u>) - 7	3
EPTH, FEET			
0.0 - 1.5	LOOSE BROW Some grave	N AND GRAY LAYERED SILT L (MOIST) (FILL)	Y SAND WITH
1.5 - 12.0	HOUSEHOLD GRAVELLY <u>S</u> ODOR)	GARBAGE MIXED WITH BLUE AND, LUMBER AND ASH (WE	-GRAY SILTY T) (STRONG
	MODERATE G	ROUNDWATER FLOW AT 7.0	TO 8.0 FEET

PROPOSED I-90/BEL	LEVUE BUSINESS PARK	ELCURE 10
BELLEVUE, WASHING	GTON PROJECT 78059	FIGURE IU
	TP-20-78 TEST PIT 20 (EL. 341+)-78	
DEPTH, FEET		
0.0 - 0.2	SOD	
0.2 - 1.5	LOOSE TO MEDIUM DENSE GRAY SILTY SOME GRAVEL TO GRAVELLY SILTY SAM	SAND WITH D (MOIST) (FILL)
1.5 - 3.0	HOUSEHOLD GARBAGE AND ASH (WET) (MODERATE ODOR)
3.0 - 4.0	MEDIUM DENSE LIGHT BROWN SILTY SA GRAVEL (MOIST) (WEATHERED TILL)	ND WITH SOME
4.0 - 9.0	DENSE TO VERY DENSE GRAY SILTY <u>SA</u> GRAVEL (MOIST) (GLACIAL TILL)	ND WITH SOME
	NO GROUNDWATER OBSERVED	
	TP-21-76 TEST PIT 21 (EL, 343+)-78	
0.0 - 0.1	LOOSE BROWN SILTY <u>SAND</u> WITH SOME (WEATHERED TILL)	GRAVEL (WET)
0.1 - 3.0	VERY DENSE GRAY SILTY <u>SAND</u> WITH S (MOIST) (GLACIAL TILL)	OME GRAVEL
	NO GROUNDWATER OBSERVED	
	TH- 22-16 TEST PIT 22 (EL. 338+) -78	
DEPTH, FEET		
0.0 - 2.0	LOOSE TO MEDIUM DENSE BROWN TO GRAWITH SOME GRAVEL (WET) (FILL)	AY SILTY <u>SAND</u>
2.0 - 12.0	HOUSEHOLD GARBAGE (WET) (STRONG OF	DOR) -
	NO GROUNDWATER OBSERVED	

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LOGS OF TEST PITS

-78

PROPOSED I-90/BELLEVUE BUSINESS PARK

TP-23-70

TEST PIT 23 (EL. 340+)

PROJECT 78059

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BELLEVUE, WASHINGTON

- 0.0 0.3 SOD
- 0.3 2.5 LOOSE BROWN SILTY <u>SAND</u> WITH SOME GRAVEL AND "BEDROCK" CHUNKS TO 10 INCHES IN DIAMETER (WET) (FILL)
- 2.5 4.0 LOOSE GRAY SILTY SAND WITH SOME GRAVEL AND STICKS (MOIST) (FILL)
- 4.0 7.0 LOOSE TO MEDIUM DENSE TAN GRADING TO GRAY-BROWN SILTY <u>SAND</u> WITH SOME GRAVEL (MOIST) (WEATHERED TILL)
- 7.0 9.0 VERY DENSE GRAY SILTY <u>SAND</u> WITH SOME GRAVEL (MDIST) (GLACIAL TILL) NEAR-REFUSAL AT 9.0 FEET

NO GROUNDWATER OBSERVED

70-24-78

TEST PIT 24 (EL. 348+)

DEPTH, FEET

- 0.0 2.5 LOOSE TO MEDIUM DENSE BROWN, SILTY SAND WITH SOME GRAVEL (WET TO MOIST) (WEATHERED TILL)
- 2.5 6.0 DENSE TO VERY DENSE GRAY SILTY SAND WITH SOME GRAVEL (MOIST) (GLACIAL TILL)

NO GROUNDWATER OBSERVED

bucknam associates

LOGS OF TEST PITS

Suriu	ce	Con	ditions		
uepm in feet Moisture %	Sample	Symbol	ľ	DESCRIPTION	REMARKS
1-			SILTY GRAVELLY SAND	brown, fine to coarse; moist, loose.	severely weathered
2-					Glacial IIII.
3- 4-			SILT and CLAY	gray-brown, with little sand and scattered gravel; moist, medium stiff.	
5- 6-			SILTY SAND	gray-brown, fine to coarse with little gravel, trace clay, scattered cobbles;	unweathered Glacial Till,
7-				moist, medium dense to dense.	
8-					
9-			grades to	with trace silt	
10-			SAND		
11-				wet.	
12-			Bottom of tort att at	11 51	
13-			No groundwater end Completed July 22,	countered. 1980.	
14-					
15					•

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Approved for publication

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LOG OF TEST PIT NO. TP-30 -81

Location: See Drawing 1.

Elevation: Approx. 343

181

Surface Conditions: Brush and grass.

n	Moisture %	Sample	Symbol		DESCRIPTION	REMARKS
1-			ML/ CL	SILTY CLAY (Construction Fill)	gray, trace gravel; moist soft.	
2-					concrete rubble (up to 4') through- out layer.	
3-						
4-						Light seepage at 4'.
5-					wood debris	
5-				SANITARY LANDFILL	silty sand tin cans, bottles, distinct odor.	
8-			SM	SAND (Weathered Till)	brown, fine to medium, some silt, little gravel; moist, medium dense.	
9-			SM	SAND (Fresh Till)	gray, fine to medium, some silt, little gravel; moist, very dense.	
1		_				
2-				Bottom Comple		
13-						
5						

I-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington for Cabot, Cabot & Forbes Project No. 81-5135



Drawing No

LOG OF TEST PIT NO. TP-4 -61

-ocation: See Drawing 1. Elevation: Approx. 332

-81

Surface Conditions: Brush and grass.

hi Inv Moisture % Symbol	DESCRIPTION	REMARKS
ML/ CL	SILTY CLAY gray, trace gravel; moist, soft. (Construction Fill)	
	concrete rubble (up to 4') through- out layer.	
	wood debris	
	SANITARY tin cans, bottles, distinct odor. LANDFILL	
	•	
-	Bottom of test pit at depth 12.0'. Completed March 16, 1981.	

THE PROTECTION PROTECTION PROJECTION I-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington for Cabot, Cabot & Forbes

81-5135

ConverseWardDavisDixon Geotechnical Consultants

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te t	ture	DESCRIPTION			
i Oe	Mois %	Sam	Sym	DESCRIPTION	REMARKS
1-			SM	SILTY SAND brown, fine to medium, roots (Forest Duff) moist, loose	5
2-			SM/ SW	SILTY SAND brown, medium to coarse, son (Weathered Till) gravel; moist, medium dense	2
3- 4-				SILTY SAND gray, medium to coarse, (Fresh Till) some gravel; moist, very dense	roots to 2½' de
5-				cobbles	
7- 8- 9-				Bottom of test pit at depth 6.0' No groundwater encountered Completed 10/29/81	-
10-					
12-					
13-					
15					
		-			
				BUILDING SITE. 1 - 1-90 BELLEVUE BUSINESS PARK Bellevue, Washington	Project No. 81-5194
	Со	n\	/ers	eWardDavisDixon Bestechnical Consultanta	Drawing No.

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Location: See Drawing 1. Elevation: Approx. 318 Surface Conditions: Brush and grass.									
In feet	Moisture %	Sample	Symbol	DESCRIPTION	REMARKS				
1- 2- 3- 4-			SM	SILTY SAND (Construction Fill)brown, fine to medium, little gravel; moist, loose. wood debrisgrades toSANDgray, little gravel, trace silt; moist, medium dense.	Slight seepage at 2.5'.				
5- 6- 7- 8- 9-				SANITARY silty sand, tin cans, paper, and - LANDFILL bottles.	-				
LO- L1- L2- L3-									
15	920/02 #10			I-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington	Project No. 81-5135				

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Surface Cor				nditions: Brush and grass.	1 Approx. 334
Depth in feet	Moisture %	Sample	Symbol	DESCRIPTION	REMARKS
1- 2-			SM	SILTY SAND (Weathered Till) reddish brown, little gravel, trace roots; moist, loose.	
3-			SM	SILTY SAND gray, fine to medium, little gravel; (Fresh Till) moist, very dense.	Difficult to excavate belo 2½'.
6- 7- 8-				Bottom of test pit at depth 5.0'. Completed April 21, 1981.	
9- .0- 1-					
2-					
4-					
5					

1-90/BELLEVUE BUSINESS PARK, BUILDING 5 Bellevue, Washington for Cabot, Cabot & Forbes

Project No 81-5135

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Drawing No.



ConverseWardDavisDixon Geotechnical Consultants

	DATE D	NILLED:	11/2/81		SUMMARY: BORING NO.B-1(Cont.) ELEVATION: Approx. 336					
EPTH	cel	E NO. CON	SIG THER TES	B BORDET BE	THIS BUBURAR	Y APPLUES ONLY AT THE LOCATION OF THIS DOAING CONDITIONS MAY DIFFEN AT OTHER LOCATIONS AND ISAGE OF THME. THE DATA PRESENTED IS A SIMPLIF		E TIME OF BRILL BE AT THIS LOCA ACTUAL CONDI	TIONS	
	6A	12 18 18	O PL		SAND (Till)	gray, mottled brown medium to coarse, trace silt, fine gravel	p	wet	dense	
45_	7A	14 35 66				to brownish gray			v.dense	
50-										
					Bottom of bo Groundwater Piezometer i Completed 11	pring at depth 50.5' encountered at depth 31 installed to 50.5' 1/2/81	.5'			
* A. B. D	2* aplit 3* 0.D. 3-1 2'	-spoon sa thin-wall O.D spli1	ampler sampler barrel samp	C. 3-1/4" oler X. 88	O.D. x 2-1/2" liner **/	A - Atterberg, C - consolidation, DS - dire G - grain alze, T - triaxial, P - permeabilit	ct shear, y	ľ	water level Impervious seal piezometer tip	
					BOEING M Bellevue for The I	ETHA''E STUDY , Washington Boeing Company			Project No. 81-5186 Drawing No	
	ConverseWardDavisDixon Geolechnical Consultants								2a	

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2.4.1 41 104

SATE DRILLED:	SUMMARY: BORING NO. B-2-8 ELEVATION: Approx. 342				
orthere work work owe to the to be of the to	THIS BUBBARY APPLIES OULY AT THE LOCATION OF THIS BORN DUBSUBFACE CONDITIONS DAY DIFFER AT OTHER LOCATIONS AN WITH THE PASSAGE OF THE, THE DATA PRESENTED IS A SIMPL BECOUNTERED DESCRIPTION	SYMBOL	THE THE OF PRILEM	CONSISTENCY	
	GRAVELLY SAND brown, medium to (Fill) coarse		moist	loose to m. dense	
	LANDFILL paper, tin cans, cloth		moist	loose	
- 1A 29	SAND brown, medium to (Till) coarse, trace of gravel		moist	v.dense	
	Bottom of boring at depth 11.0' No groundwater encountered Piezometer installed to 11.0' Completed 11/2/81				
A. 2" split-spoon sampler B. 3" O.D. thin-wall sampler C. 3-1/4 D 3-1 2" OD split barrel sampler X. si	O.D. x 2-1/2" liner "A - Atterberg, C'- consolidation, DS - di G - grain alze, T - triaxial, P - permeab BOEING METHANE STUDY Bellevue, Washington	rect shear, llity		water level Impervious seal piezometer tip Projec: Nc 81-5186	

The local data

and the second second



ConverseWardDavisDixon Geotechnical Consultants

surt and a consider or the second or the	PEDOFORT PERSING	SUMMARY: BORING NO. E	3-4-81 ELEVATION: APPTOX.
	SAND (Fill)	brown, medium, tra silt, some gravel	SYMBOL MOISTURE CONSISTENCY ace moist m. dense
	Bottom o No ground Piezomete Completed	f boring at depth 5.0' dwater encountered er installed to 5.0' 1 11/2/81	
Split-spoon Sampler D.D. thin-wall sampler 2' O.D. split barret sampler: X, s	4° O.D. x 2-1/2° liner °°A - At sample not recovered G - gi	terberg. C - consolidation, DS - direct shear, rain size, T - triaxist, P - Demochai	water level Impervious seat
Conversion	BOEING METHA Bellevue, Wa for The Boei	ANE STUDY shington ng Company	Prezometer tip Frojec: No E1-5186 Draw po bio
Converseward	Davis Dixon Gen	otechnical Consultants	5

BATE DALLED:	11/2/81	SUN	MARY: BORING NO. B-	5-81	BLEVATION:	Approx. 3
FFEET SPLESPLE ON	AS IS WERE TESTS WOST WERE	THIS BUWEA	RY APPLIES DOLY AT THE LOCATION OF THIS DOM I COMDITIONS MAY DIFFER AT D'INER LOCATIONS A SESAGE OF THE. THE DATA PRESENTED IS A BIMP ID	NE AND AT TH ND MAY CHAN LIFICATION DI	E TIME OF DRILLING GE AT THIS LOCAT F ACTUAL CONDITIO	B NGN DARS
		DESCRIPTION SAND (Fill)	brown, medium, trace silt, some gravel	SYMBOL	moist	m. dense
-						
		Bottom of b No groundwa Piezometer Completed 1	oring at depth 5.0' ter encountered installed to 5.0' 1/2/81			
						r.
A. 2" split-spoon si E. 3" O.D. thin-wall T. 3-1/2" O.D. split	ampler samplør C. 3-1/4 [°] (i barrel sampler X. sam	D.D. x 2-1/2" liner ""	A - Atterberg, C - consolidation, DS - di G - grain size, T - triaxial. P - permeabl	ect shear, lity	ţ,	water level Impervious seal piezometer tip
		BOEING M Sellevue for The	KETHANE STUDY , Washington Boeing Company			Project No. 81-5186 Drawing No
Conve	erseWard	DavisDixo	Geotechnical Consultants			6





S	Conv	erse Co	Insultants Geotechnical Engineering and Applied Sciences	
			for Brown and Caldwell 02-5109	
			EASTGATE TRUNK SEWER Project No. Bellevue, Washington P2 E1CO	
B 3° 0.D. D. 3-1/2"	thin-wall samp O.D. split barre	ler C. 3-1/4" I sampler X. sa	0.D. z 2-1/2" Mner ""A -Atterberg, C - consolidation, DS - direct shear, Impervious seat mple not recovered G - grain size, T - triazial, P - permeability plazometer tip	
A. 2" split	-spoon sample:	- <u>I</u>	(Continued)	
AB	25 50/5"	7.8	grades cleaner with less silt	
-5 - -5 -	s ≤50/6"	10.1	SAND brown, fine to coarse, SP moist very (Advance some silt, trace Outwash) clayey silt, occasional gravel	305
0 _ 6/	A 2 18 50/5"	9.8	SILT gray, some fine sand, ML slightly very (Lacustrine Deposit) occasional layer of coarse sand	315
25 - 5/	A = 50/3"	4.2	boulder 20-21' depth (refusal on boulder at 25' depth; redrilled hole 6' north of original location)	-320
20 - 4	A = 50/5"	5.5	SILTY SAND blue-gray, fine to SM moist very (Glacial coarse, some gravel, Till) occasional cobbles	020
.5 - 3	5 3A 17 13	14.1	grades finer with Clayey silt, fabric ML fragments	- 325
, , 10 - 1 10 - 1	2A - 4 5 8	25.9	SILTY SAND black, fine to medium, (Sanitary with paper, wood, Landfill) plastic, metal & wire, organic odor (from drill action, concrete pieces 5-16.5' depth)	- 335
	1A 12 10	10.8	SILTY SAND brown, organic, little SM very medium gravel, trace roots moist dense	E-340
0 th	Staple NO.	SIG THE TELDOS	BUSSURFACE CONDITIONS WAT THE LOCATION OF THIS DONING AND AT THE THE OF DEVILUES BUSSURFACE CONDITIONS WAT DIFFER AT OTHER LOCATIONS AND WAT CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME THE BATA POESEWISED IS A SWPLIFICATION OF ACTUAL CONDITIONS BUCDUNTERED DESCRIPTION BUCDUNTERED	LEV
D	ATE DRILLED.	10/2/82	SUMMARY: BORING NO. 8 - 82 ELEVATION 340.4	

OFOTH	DATE DRILLED.	10/2/82	SUMMARY: BORING NO. 8-67	Cont.) ELEVATION	
0 - 0	9A 50/5'	4.8	SAND (Cont.) brown, fine to coarse, silt matrix, trace gravel	moist ver den	y Se
5 -			Bottom of boring at depth 43.5' No groundwater encountered Piezometer installed to depth 43.5' with 2' slotted interval at bottom.	**	
-					-
					-
					-
1					
	spill-spoon sam 0.D. thin-wall as -1/2 [°] 0.D. spill b	pier impier C. 3-1/4 errei sampier X. s	* O.D. x 2-1/2* Mner ** A = Atterberg, C = consolidation, D8 = direct ample not recovered G = grain size, T = triaxist, P = permeability	t shear,	vol lus cosi tor tip
			EASTGATE TRUNK SEWER Bellevue, Washington for Brown and Caldwell	Projec 82-5	5169
R	Con	verse C	DNSUITANTS Geolechnical Engineering and Applied Sciences	- Trawi	Ays







	ÎT		SILTY SAND	brown, fine to medium, little gravel, trace	SM	very	loose	F
1A	4 4 5	19.0	(+111)	wood, organic				~ ~ ~ ~
2A	7	5.6	GRAVELLY SAND (Fill)	gray, fine to medium, trace silt	SW	moist	dense	
	45		(concrete pi based on cut	eces throughout fill tings)				
3Х	50/3'		(sample 3 dr	riven on concrete)				
4A	20 15	16.6	CLAYEY SILT (Sanitary Landfill)	gray, mottled brown, some sand, trace glass, wire & paper	MH	very moist	medium dense	- 1 1- L
			SILTY SAND	brown, fine to medium,	SM	very moist	medium	
5A	7 12 15	25.1	Landfill)	TILLE GLAVET, WOOD			UENSE	
6A	50/6"	4.7	SAND	gray, fine to coarse, trace gravel, trace silt	SP	moist	very dense	
7A	50/6"	8.3						
88	23 23 30	12.1		(Continued)		 very moist		
split-s D.D. 11 1/2* 0	ipoon sampler hin-wall samp).D. split barre	ler C. 3-1/4 I sampler X. si	"O.D. z 2-1/2" Uner **/	i =Atterberg, C = consolidation, DS = direct 3 = grain size, T = triaxial, P = permeability	shear,	ľ	water level Impervious seal plezometer tip	
			EASTGATE Bellevue	TRUNK SEWER , Washington			Project No. 82-5169	

DATE	DRILLED:]	2/7/82	SUMMARY: BORING NO. 11 -82 ELEVATION 306.	6
FEET	PLE NO. ON SI	WER TESTS OF OFT	THIS BUMBARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF BRILLING BUBBURFACE CONCITIONS WAT BIFFER AT OTHER LOCATIONS AND MAT CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SUBPLIFICATION OF ACTUAL CONDITIONS ENCOUNTERED.	
	5° 6°	<u>0' f' + 0'</u>	DESCRIPTIONSYMBOL MOISTURECONSISSILTY SANDdk. brn., f/m, little SM wetloos(Fill)gravel, trace rootsloos	E E
1A	- 3 7 1	18.6	SAND gray, fine to medium, (Fill) trace silt, SP wet loose occasional gravel	e -
2A	7 8	16.6	SILTY TO brown, fine to coarseSM wet dense CLAYEY SAND trace to occasional (Advance grave)	
	30		Outwash) II2/7/82 INV grades to rust-brown, fine to SAND coarse, trace silt, SP	ERTE
ЗА	6 28 32	9.2	occasional gravel moist dense	
			Bottom of boring at depth 14.5' Groundwater encountered during drilling at depth 9.5'	2
				-
				-
				F
				F
0.D. thin 1/3" O.D	-wall sampler). split barrel	r C. 3-1/4° C sampler X. sam	D.D. x 2-1/2" liner **A - Atterberg, C - consolidation, DS - direct shear, impervious a ple not recovered G - grain size, T - triaxial, P - permeability plezometer	tip
			EASTGATE TRUNK SEWER Project No Bellevue, Washington 82-516 for Brown and Caldwell	5. 59



0	A. Somple	LEACHATE SAMPLI I-90/Bellevue B for Cabot, Cabo	n elze, T - triazial, P - permeability NG Usiness Park t. & Forbes	iear,		Project No. 81-5216
-spoon sampler thin-wall sampler O.D. split barrel s	C. 3-1/4" O.D.	x 2-1/2" Iner ** A - Atte	rberg, C - consolidation, DS - direct al		1	water level Impervious seal
			~			
		Bottom of bor Piezometer in for details) Groundwater e 7.0' at time	ring at depth 14.0' stalled (see schemati ncountered at depth of drilling.	C		
3 18 50/6'		SILTY SAND (Landfill Debris)	gray, fine to medium, abundant organics & metal debris	S11	wet	dense
2 39 18		SILTY GRAVELLY SAND (Fill)	dark gray, fine to coarse, trace organic (landfill debris?)	SM	wet	dense
1 18 19		SILTY SAND (Fill) SAND (Fill)	dark greenish-gray, fine to coarse, litt gravel light gray, fine to medium, trace silt	lesm	very moist	V 4/27/89 √ 4/27/89 √ 7/8/83 dense
Set grant stant or	OTHER TE DO DAY	OESCRIPTION	CONDITIONS MAY BIFFER AT OTHER LOCATIONS BRAGE OF TIME. THE DATA PRESENTED IS A DIM D	AND MAY CH PLIPICATION	THE TIME OF	BRILLING LOCATION CONDITIONS 4/14/83

Date Drilled: 3/26/83

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Elevation: Approx. 349



6/2/05						
DATE DRILLED: 0/ 3/ 85	SUMMARY: BORING NO. B-301	ELEVATION Approx. 342				
OEPTHEET PROLE DAS THE TESTS OF ON THE	THIS SUBBARY APPLIES ONLY AT THE LOCATION OF THIS DOAINS AND A SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONE AND MAY C WITH THE PABBAGE OF TIME. THE BATA PRESENTED IS A DIMPLIFICATION SUCOUNTERED.	T THE THE OF DALLING MARGE AT THIS LOCATION OR OF ACTUAL CONDITIONS				
	DESCRIPTION SYM	OL MOISTURE CONSISTENCY				
	gray, fine to medium, little gravel, trace wood, concrete	moist [‡] medium - dense - -				
	SILTY SAND (Sanitary Landfill); SM black, fine to medium, some sanitary refuse: glass, wood, etc., strong organic smell;	moist medium dense				
10 - - - - - - - - - - - - - - - - - - -	grades to debris fill: glass, wood, paper, cans; no soil matrix; visible methane	moist				
	Bottom of boring at depth 12.8' 3/4" diameter PVC observation well installed with slotted screen from 7.5' to 12.5', pea gravel backfill from 5.0' to 10.5', backfill with cuttings from 5.0' to 3.0', benton- ite seal from 3.0' to surface, and install cast iron monument cover.					
		-				
*A. 2° split-spoon sampler B. 3° O.D. thin-wall sampler C. 3-1/4° O.D. II 2-1/2° Mer *A - Atterberg, C - consolidation, DS - direct shear, D. 3-1/2° O.D. split barrel sampler X. sample not recovered G - grain eize, T - triaxial, P - permesbility piezometer tip EASTCATE LANDER L. MATER. CAMPLEND						
for	Bellevue, Washington Boeing Computer Services	85-5104-02				
Converse Com	Geotechnical Engineering	Drawing No.				
e conterse con	SUILCIILS and Applied Sciences	2				

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	DESCRIPTION	SYMBO	DL MOISTURE	CONSISTENC
1CII 50/5"	SILIY SAND (Fill); brown, fine to medium, little gravel, trace wood (sampler driving on rock)	SM	moist	medium dense
- 5 - 2C	SAND (Fill); gray, fine to medium, trace gravel, wood, & metal debris	SP	moist	medium dense
- 	SANITARY LANDFILL; consists of wood, glass, plastic, rubber, paper and metal; no soil matrix;		moist	dense
- 4C	occasional lense of sand	6/2	very moist 1/85▽	
5C 33 17 21	(possible free water)		6/7/85 very moist	
	Bottom of boring at depth 24.0' 3/4" dia. PVC observation well insta slotted screen from 17.5' to 22.5', pea gravel backfill from 9.0' to 22.5', backfilled with cuttings from 3.0' to 9.0', bentonite seal from 3.0' to surface, and install cast iron monument cover.	lled	with	
split-spoon sampler O.D. thin-wall sampler C. 3-1/ 1/2" O.D. split barrel sampler X. FA	 4° O.D. x 2-1/2″ liner A - Atterberg, C - consolidation, DS - direct al ample not recovered G - grain size, T - triaxial, P - permeability STGATE LANDETLL HATER ON HER 	Hear,	t ^v wa ∳ im ⊡ pie	ter level pervious seal zometer tip

DATE DRILLED: 6/4/85	SUMMARY: BORING NO. B-303-	45 ELEVATIN	ADDROY
0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	THIS SUBBARY APPLIES ONLY AT THE LOCATION OF THIS DOBING AND	TTHE TIME OF BAIL	CONSISTENT
- 1C 14 12	SILTY SAND (Fill); gray-brown, fine SM to medium, little gravel, trace wood	moist	medium dense
2C 8 14	grades to black, trace wood, plastic, and metal debris		
$3C = \frac{8}{12}$	SILTY SAND (Sanitary Landfill); SM black, fine to medium, trace gravel, wood, plastic, metal, wire, and paper	very moist	medium dense
4C 10 12 12 20			
5C 29 11 8	grades to Sanitary London		
	little silty sand	moist =	
20 - 13 - 8C 19	SILTY SAND (Old Soil Horizon/Fill); SM brown, tr. to little gravel track	very	medium
<u> </u>	wood & glass	moist	dense _
	(Continued)	<u>I</u>	
r spill-spoon sampler " O.D. thin-wall sampler C. 3-1/4" (-1/2" O.D. spill barrel sampler X. sam	D.D. x 2-1/2" liner ** A - Atterberg, C - consolidation, DS - direct shear, opie not recovered G - grain size, T - triaxial. P - marmashility	· · · · · · · · · · · · · · · · · · ·	ter level pervious seal
EAST	GATE LANDFILL WATER SAMPLING Bellevue, Washington r Boeing Computer Services	ti pie	zometer tip Project No. 85–5104–02
			Prawing No.

	DESCRIPTION	SYMB	OL MOISTURE	CONSISTENCY
90 1 68	SILTY SAND (Cont.);	SM		dense
50/3"				
100 <u>57</u> 50/3"	SILTY SAND (Weath. Glacial Till) gray, f/m, trace to little grave	; SM	wet	very dense
	grades to Unweath. Till, with occ. lense of gravelly silty sand and sandy silt	d SM	moist	
11AT 60/6"				
12AT 60/6"	SAND (Advance Outwash); brown, f to medium, trace silt, thinly bed ded with sandy silt layers	ine SP 1-	moist	very dense
			wet	
13AT 27 50/6"			6/7/85 6/21/85 	
14AT 20 50/6"	SANDY SILT (Lacustrine Sediments) gray, fine sand, thinly laminated with clayey silt and silty fine s	; ML and	very moist	very dense
7 15A 13	SAND; dark gray, very fine, trace to little silt	SM	wet	very dense
160 55 50/3"	grades fine to medium, thinly bed to laminated with clayey silt and brown sandy silt	ded	very moist	
	(Continued)			
BRIII-spoon sempler			- 21	rater level
0.D. thin-wall sampler C. 3- 1/2" 0.D. spilt barret sampler 3	1/4° O.D. x 2-1/2° liner * A -Atterberg, C - consolidation, DS - d A sample not recovered G - grain size, T - triaxial, P - permest	weet shear,		mpervious eesi lezometer tip
E	ASTGATE LANDFILL WATER SAMPLING			Project No.

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DATE DRILLED: 6/4/85	SUMMARY: BORING NO. B	-303 -45	ELEVATIO	N:
A. J. (NO. 16 (55.05	UNE CON THIS BURNARY APPLIES OULY AT THE LOCATION OF THIS AUBSUNPACE CONDITIONS MAY BIPPER AT OTHER LOCATION	LONT .)	E TINE OF BRILLI	NG TION
FEE SHOPLE ONS STHER THE OF OF			ACTUAL CONDIT	1016
	- BESCHIFTION	SYMBOL	WOISTURE	CONSISTENC
	Bottom of boring at depth 78.2' Groundwater encountered at depth 64' during drilling 2" diameter PVC observation well installed with slotted screen fro 55' to 75'; sand backfill from 50 to 71'; grout backfill from 19' t 50'; dry cement backfill from 12'	n ' D to		
	19'; backfilled with cuttings fro 1' to 12', and cast iron monument cover installed at surface.	n		
t" spilt-spoon sampler 1" 0.D. thin-wall sampler C. 3-1/ 1-1/2" O.D. spilt berrel sampler X. E A	4° O.D. x 2-1/2″ liner ^{••} A ⁻ Atterberg, C - consolidation, DS - di sample not recovered G - grain size, T - triaxial, P - permesb STCATE I ANDELLI MATER CAMPLANC	rect shear, lilty		water level Impervious seal plezometer tip Project No.
EA	Bellevue, Washington for Boeing Computer Services			85-5104
Converse C	Onsultants Geolechnical Engineering and Applied Sciences			4 (COM

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DATE DRILLED: 4/4/85		1 115	
	THIS BURNARY APPLIES ONLY AT THE LOCATION OF THIS PORING	L -W3 ELEVATH	on: Approx. 302
OFFICE AND TRACE ONSING THE	A O A C C COUNTERED OF TIME THE BATA PRESENTED IS A SIMPLIF	MAY CHANDE AT THIS LOC ICATION OF ACTUAL COND	LING Cation Itions
0	C & DESCRIPTION	SYNBOL MOISTURE	CONSISTENCY
6	to medium, trace silt & organics	slight	ymedium
	grades to little gravel	moist	aense
5 7	SILTY SAND; mottled grav & light	moist	-
	brown, fine to medium, trace clay	morst	dense
28	SILTY SAND: GROUP Fine to The		I F
	little gravel, trace clav	wet	very -
- 4X _ 50/4"			
	SILTY SAND (Unweathered Till):	slight]	
	light brown, fine to medium, little	moist	dense -
-6C 15 50/4"	State cray		
			-
20 7A 50/4"			
	SAND (Advance Outwach) + hours		
	fine to medium, trace silt	wet	very -
- 50/4"			-
	CAND / Los I I I I		
30 - 7 26	light brown, fine, trace medium	slightly	very -
ЧЧЦ 40 Ч 50/5"	trace silt with thinly laminated to	morse	dense -
	silt		E
35 25			
			E I
	Bottom of boring at depth 36 5'		
1 11 1	Groundwater encountered at depth 9'		F
	Hole filled with cement/bentonite		
	to surface.		
A. 2" SpHt-speen specie			
8. 3" O.D. thin-wall sampler C. D. 3-1/2" O.D. spill barrel samplar	3-1/4" O.D. z 2-1/2" liner **A - Atterberg, C - consolidation, DS - direct sha	ar, 1 ²² wa	iter leval Pervious seal
	SLURRY TRENCH FFASTRILITY STUDY	i pie	zometer tip
	Boeing Computer Services		Project No. 85-5104
	berievue, wasnington	;	
Converse	Consultants Geotechnical Engineering and Applied Sciences		
			~

DATE DRILLED.4/4/85	SUMMARY: BORING NO. CC-	2-45 ADDECK 302
SEPTIFET SPERAL POLLOWS STREETES	THIS BUBMARY APPLIES ONLY AT THE LOCATION OF THIS BOBIN THIS BUBMERACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND THE PASSAGE OF THES. THE BATA PRESENTED IS A SHOPL OF A OF C SUCOUTEBED	IS AND AT THE THE OF BRILLING IS MAT CHANGE AT THIS LOCATION IFICATION OF ACTUAL CONDITIONS
0	DESCRIPTION	SYMBOL MOISTURE CONSISTENCY
17	GRAVELLY SAND (Fill); light brown, fine to medium, trace silt	slightly moist
5 - 15 5 - 15	GRAVELLY SILTY SAND; mottled brown & light brown, fine to medium	slightly medium moist dense
-2A 5 -2A 7 8	SANDY SILT/CLAYEY SILT (Alluvium); mottled gray-green & light brown, fine, thinly laminated	slightly medium moist dense
	CLAYEY SAND (Advance Outwash); gray, fine to medium, trace gravel	moist very dense
5 _4A = 50/6	SAND; gray, fine to medium, little silt, trace gravel	moist very - dense -
5A 48 50/5	grades to trace silt and gravel	4/17/85
-6A -26 -26 -29	with occ. thin laminations of silty sand	moist to wet
-7A 44 - 50/2' - 124	to mottled gray & light brown	wet
-8A 37 	with medium bedded brown silt and thin laminations to thinly bedded silty fine sand	slightly very moist dense
-10A 18 -10A 25 21 -11A 25	SILTY SAND (Lacustrine); dark gray, fine, with thin laminations to thinly bedded silt and fine cand	slightly dense moist
39 12A 21	SAND; brown, fine to medium, trace silt, with medium bedded fine sandy silt	wet very dense
43 1B 13A 25 42	to gray, fine, med. bedded gray <u>silt. thin lam. of fine sandy silt</u> SILT; dark gray, w/thin laminations to medium bedded sandy silt	wet very
	(Continued)	
2° spHi-spoon sampler 3° O.D. thin-wall sampler C. 3-1/ 3-1/2° O.D. split barrel sampler X.	4° O.D. x 2-1/2° liner **A - Atterberg, C - consolidation, DS - direct sh sample net recovered G - grain size, T - triaxisi, P - permeability	sar, piezomater tip
Boeing Computer Services Bellevue, Washington		Project No. 85-5104
Converse Consultants Geotechnical Engineering and Applied Sciences		Drawing No.




	DESCRIPTION BI	MBOL MOISTURE	CONSISTEN
10AT 21 50/3" 11AT 26 50/6"	SAND (Adv. Outwash) (Cont.); SAND (Lacustrine); gray, fine, trace silt, with med. bedded silt <u>& thin lam, of fine sandy silt</u> SILT; dark gray, trace fine sand, w/thin beds of mottled gray & light brown, fine to medium sand and	wet moist moist	very dense very very
25 35 38 13A 13A 27 47 50/3	silty sand, & thin lam. fine sandy silt, occ. thin lamination of peat w/thin laminations of fine sand with medium bedded silty fine sand, and thin laminag of fine sand time	slightly moist	nard
14A 27 40 53/3' 15A 36 50/3'	with thinly bedded silty fine sand, and thin laminations of fine sandy silt mottled dark gray & light brown, trace fine sand, with med. bedded fine sand	moist	
	Bottom of boring at depth 68.5' Groundwater encountered at depth 20' Hole filled with cement/bentonite slurry from 68.5 to surface.		
spitt-spoon sampler D.D. thin-well sampler C. 3-1/ /2° O.D. spilt berret sampler X. SL BC Rc	4° O.D. x 2-1/2° Mmer ** A - Atterberg, C - concolidation, D2 - direct shear sample not recovered G - grain also, T - triaxial, P - permosability URRY TRENCH FEASIBILITY STUDY eing Computer Services		ter level pervious seat zometer tip Project No. 35-5104



LOG OF TEST PIT NO. 201 (Cont.) PROJECT: 27.2 Acre Site JOB NO : 85-5156 ____DATE: 6/20/85 Boeing Computer Services ELEVATION: Approx. 344 CLIENT FEATURE: _____ LOCATION: ____ See Drawing GROUNDWATER LEVEL: _____ LOGGED BY: _____. DEPTH SAMPLE SOIL DESCRIPTION NO. SYM. (ft) REMARKS SM SILTY SAND (Fill); brown, fine to medium, little gravel, trace roots; moist, medium dense 1. 2color changes to gray color changes to brown 3. SANITARY LANDFILL; black, household garbage, cans, strong trash glass, wire; very moist odor throughout SILTY SAND (Weath. Till); brown, fine to medium, SM little gravel, occasional cobbles; moist, dense 5-(Unweath. Till); gray-brown; moist, very dense SM 6. Bottom of test pit at depth 6.0' No groundwater endountered Completed 6/20/85 **GRAPHIC LOG** - West Face 0-SM (Fill, brown) 1-

SM (Fill, gray) 2-SM (Fill, brown) 3-4 SM (Weathered Till) 5-Sanitary 6-Landfill SM (Unweathered Till) -0+500+60 0+70 0 + 80PROPOSED 27.2 ACRE SITE Project No. Bellevue, Washington 85-5156 for Boeing Computer Services Drawing No. Converse Consultants Geotechnical Engineering and Applied Sciences 1 (CONT.)

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PROJ	ECT:_	27.2 Ac	re Site	JOB NO :	DATE: 6/20
CLIEN	T:	Boeing	Computer Services	ELEVATION:	Approx. 3
FEAT	JRE:		L	OCATION: See Drawing	
GROU	NDWA	TER LEV	/EL:	LOGGED BY:	DAY
DEPTH	SAMPLE NO.	SOIL SYM.	DESCF	RIPTION	REMARKS
		SM	SILTY SAND (Fill); bro gravel, trace wood; mo	own, fine to medium, little	
2-					
3-			grades to gray in coro)T	
4-					
5-					
6-		ML	CLAYEY SILT (Fill); gr	ay, little sand and gravel,	strong tra
7-			ANITRAY LANDFILL; hou ans, glass; moist	sehold garbage, paper, rags,	out out
-8			Rottom of tost transh	at donth 7 51	
			lo groundwater encount	ered	
_		C	completed 6/20/85		
_					
		Sanita	SM (Fill, brown) SM (Fill, gray) ML (Fill) ry Landfill		
0+30	1		0+40	0+50	0+60
			PROPOSED 27.2 ACRE S Bellevue, Washingto	SITE	0+00 Project No. 85-5156

LOG OF TEST PIT NO. 203-85



LOG OF TEST PIT NO. TP-204-85

Location: See Drawing

Elevation: Approx. 344

Surface Conditions: Flat; sage brush and grass

Depth in feet	Moisture Content-%	Sample	Symbol	DESCRIPTION	REMARKS
12			SM	SILTY SAND (Fill); brown, fine to coarse, little fine to medium gravel, trace subrounded cobbles, roots and organics; slightly moist, medium dense	
3- 4- 5-			SM	SILTY SAND; brown, fine to medium, trace gravel, trace subrounded cobbles; concrete rubble (to 4'), timbers and wood (to 8"), bicycle tires; moist, dense (Fill)	test pit walls standing vertical
6-7-			ML	CLAYEY SILT; gray, trace gravel, trace fine to medium sand, scattered small branches, roots, and organics; moist, firm (Fill)	
8- 9- 10-					
11-				Bottom of test pit at depth 12.0'	
-				Completed 6/21/85	
.lll					
1				PROPOSED 27.2 ACRE SITE	Project No
				Bellevue, Washington for Boeing Computer Services	85-5156
٢ ک	Con	ve	rse	Consultants Geotechnical Engineering and Applied Sciences	Drawing No

LOG OF TEST PIT NO. TP-213-85

Location: See Drawing

Elevation: Approx. 338

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Surface Conditions: Flat; some small weeds

the second s			
ristine internet	.vmhol	DESCRIPTION	REMARKS
	SM	SILTY SAND (Fill); brown, fine, trace medium to coarse sand, little fine to coarse subrounded gravel; scattered roots, and sticks; moist, medium dense	
9- 4 4 4 4 4 9- 10	K.	CLAYEY SILT; gray, trace fine to medium sand, little gravel, scattered small to medium cobbles; concrete rubble to (18"), wood, logs (6"), paper, plastic, and metal scraps; with occasional medium beds of silty sand, brown, fine to medium; moist, firm (Fill)	distinct organic odor
33-		Bottom of test pit at depth 12.0' No groundwater encountered Completed 6/21/85	
		PROPOSED 27.2 ACRE SITE Bellevue, Washington	Froject No 85-5156
Conver	se	Consultants Geotechnical Engineering and Applied Sciences	Drawing No 13

(OW-1)

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PROJECT: Bellevue Airport / Eastgate Landfill

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B Location: Noth side of Pont A Page 5 Standard Buow Registration One of the stand o	. Eg	Soil Description	SGS	щ	щe	9~	PEN	TRATION RESIST	NCE	-
-30 Approximate ground surface elevation: 305 feet 98 51 52 93 0 00	(fee	Location: North side of Pond A	D'SAU	WPI	MPL	NE	Standard	Blows over inches	∆ Other	Page 2
Very dense SAND (as above) S6 0 20 30 40 so [TESTING -35-	-30-	Approximate ground surface elevation: 305 feet	GR	SA	SA	R S	0 10	Blows per foot	ouler	of 2
35- Hard, wei, gray, SiLT, some fine sand (Glacial-lacustrine Deposit) 57 Image: Control of the sand sector o	00	Vorsidence DAND (T			: 10	20 30	40 50	TESTING
35- Hard, weit, gray, SiLT, some fine sand (Glacial-lacustrine Deposit) 40- 57 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 40- 58 50- 58 50- 1<		very dense SAND (as above)			S6 _				laori-	
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35 Hard, wat, gray, SiLT, some fine sand (Gladal Accustine Deposit) 57 S7 40- 58 S8 S8 50 58 S8 S8 S8 50 58 S8 S8 S8 S8 <										
35 Hard, yet, gray, SiLT, some fine sand 57 Image: Srad and State and					-					
35 Hard, wet, gray, SiLT, some fine sand (Clicical-lacustrine Deposit) 57 Image: Clicical-lacustrine Deposit) 40 58 Image: Clicical-lacustrine Deposit) 58 50 58 Image: Clicical-lacustrine Deposit) 50 58 Image: Clicical-lacustrine Deposit) 50 58 Image: Clicical-lacustrine Deposit) 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 1 50 1 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td></td<>										-
Hard, wei, gray, SiLT, some fine sand (Glacial-lacustrine Deposit) 40- 58 Boring terminated at approximately 41.5 feet below ground surface. 5- 5- 5- 5- 5- 5- 5- 5- 5- 5-	- 35-								••• ••••	-
Image: Party set in some time sand (Glackal-lacustrine Deposit) Education Boring terminated at approximately 41.5 feet below ground surface. 5- <			-		67					
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1-91M-14173-0 BORING No. B-3 W.O.



APPENDIX D

Report on the Geophysical Surveys at the Eastgate Landfill, Bellevue, Washington by Global Geophysics **Global Geophysics**



March 1, 2016

Our Ref.: 105-0904.000

Landau Associates, Inc. 130 2nd Avenue S Edmonds, WA 98020

Attention: Mr. Kent Wiken

RE: REPORT ON THE GEOPHYSICAL SURVEYS AT THE EASTGATE LANDFILL, BELLEVUE, WA

Dear Mr. Wiken:

Global Geophysics conducted electrical resistivity tomography (ERT), induced polarization tomography (IPT), EM61 and ground penetration radar (GPR) surveys across the Eastgate landfill in Bellevue, WA. The proposed objective of the geophysical investigation is to assist in delineating the vertical and lateral extents of the landfill materials.

METHODOLOGY AND INSTRUMENTATION

Electrical resistivity tomography and induced polarization tomography (IPT) were used for this study. The following paragraphs describe the methods and field procedures.

Electrical Resistivity Tomography (ERT)

The electrical resistivity tomography technique maps differences in the electrical properties of geologic materials. These differences can result from variations in lithology, water content, and pore-water chemistry. The method involves transmitting an electric current into the ground between two electrodes and measuring the voltage between two other electrodes. The direct measurement is an apparent resistivity of the area beneath the electrodes that includes deeper layers as the electrode spacing is increased. Recent advances in technology permit rapid collection of multiple soundings, using up to 56 electrodes for each spread. The data are modeled to create a 2-D geo-electric cross-section that is useful for mapping both vertical and horizontal variations of the subsurface strata.

The data were acquired with an AGI SuperSting R8 using up to 112 electrodes spaced at a 5-7 feet interval. Once the electrode array was installed in the ground, multiple soundings were automatically carried out by the control unit. Downloading and routine modeling of the data was done on-site to provide preliminary analysis and QA/QC of the data. These results were

displayed on a color monitor as cross-section that highlight changes in resistivity with depths along the transects.

Induced Polarization Tomography (IPT)

The IPI method studies the decaying potential difference as a function of time. In this method the geophysicist looks for portions of the earth where current flow is maintained for a short time after the applied current is terminated.

When a metal electrode is immersed in a solution of ions of a certain concentration and valence, a potential difference is established between the metal and the solution sides of the interface. This difference in potential is an explicit function of the ion concentration, valence, etc. When an external voltage is applied across the interface, a current is caused to flow and the potential drop across the interface changes from its initial value. The change in interface voltage is called the "over voltage" or "polarization" potential of the electrode. Over voltages are due to an accumulation of ions on the electrolyte side of the interface. The time constant of buildup and decay is typically several tenths of a second.

The IP data were collected at the same time as the resistivity data.

Time Domain Electromagnetic (EM61)

The time-domain electromagnetic system is capable of detecting buried metal objects. It transmits a pulsed electromagnetic field into the ground, which induces eddy currents in buried metallic objects. These eddy currents generate secondary electromagnetic fields that are detected by the system. The time duration or decay rate, of the secondary EM field is related to the electrical conductivity characteristics of the buried object.

A four-channel (gate) high sensitivity metal detector, Geonics EM61 Mk2, was used to collect the data along the traverses at a 20 ft interval. The low channel number (1) represents anomalies produced by shallow objects and the high channel number (4) represents anomalies produced by deeper objects. The subsurface depth range is from approximately 1 to 15 feet. The data was stored digitally and downloaded after the survey for analysis and mapping

Ground Penetrating Radar

The GPR method uses electromagnetic pulses, emitted at regular intervals by an antenna to map subsurface features. The electromagnetic pulses are reflected where changes in electrical properties of materials occur such as changes in lithology or where underground utilities are present. The reflected electromagnetic energy is received by an antenna, converted into an electrical signal, and recorded on the GPR unit. The data is recorded and viewed in real time on a graphical display that depicts a continuous profile or cross-section image of the subsurface directly beneath the path of the antenna.

The depth of penetration of the GPR signal varies according to antenna frequency and the conductivity of the subsurface material. The depth of subsurface penetration with GPR decreases with an increase in the frequency of the antenna and an increase in soil conductivity. Low frequency antennas (50 to 500 MHz) provide the best compromise between obtaining good subsurface penetration and resolution.

The data were collected along the same EM transects at a 20 foot interval using Geophysical Survey Systems, Inc. (GSSI) SIR 2000 GPR system with antennas having a center frequency of 80, 100 and 200 MHz. The data was digitally recorded for post processing.

RESULTS

The ERT and IPT data were collected along 11 transects. The locations of these lines are shown in Figure 1. The interpreted resistivity and IP profiles are shown in Figures 2-3. The borehole logs and test pit logs were used to calibrate the interpretation.

The landfill materials are inhomogeneous comparing to native soil. The interpreted bottom of the landfill material is based on the borehole logs and IP responses of the landfill materials.

- The bottom of the interpreted cover layer is represented by the dashed pink line. And the bottom of the interpreted landfill is presented by the dashed blue line. The thickness of this landfill varies between 0 and 60 ft.
- The zones with resistivity less than 28 ohm-m are interpreted as leachate saturated soil.
- The EM61 data contour plan with interpreted boundary (in dashed res line) is presented in Figure 4.

LIMITATIONS OF THE GEOPHYSICAL METHOD

Global geophysics services are conducted in a manner consistent with the level of care and skill ordinarily exercised by other members of the geophysical community currently practicing under similar conditions subject to the time limits and financial and physical constraints applicable to the services. ERT, IPT, EM61 and GPR are remote sensing geophysical methods that may not detect all subsurface conditions due to the limitations of the methods and soil conditions. In general, the errors in the interpreted depths, dependent on the resolution of the technique, are estimated to be approximately ± 10 % of the true depths.

Sincerely,

Global Geophysics

John Liu, Ph.D., R.G. Principal Geophysicist







