West Vancouver Freight Access Project

Project 03 Terminal 5

SPL Landfill Cap Construction Certification Report

August 2010



Prepared for: **Port of Vancouver** 3103 NW Lower River Road Vancouver, Washington 98660-1027



Prepared by: HDR Engineering, Inc. 1001 SW Fifth Ave, Suite 1800 Portland, Oregon 97204



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1.0 Introduction

As part of the West Vancouver Freight Access Project, the Port of Vancouver (Port) constructed a two-mile rail loop at Terminal 5 in 2010. This project extends west from Gateway Avenue to the edge of the contiguous Evergreen property and consists of a storage track, a car preparation track, and loop lead track (Figure 1). Construction of the loop lead track required disturbance of two areas protected under a restrictive covenant administered by the Washington Department of Ecology (Ecology): Spent Pot Liner (SPL) Landfill Storage Area and Vanexco Cap (Figure 1).

Prior to construction the Port coordinated with Ecology to design a replacement cap for each site. In October 2009, Ecology approved the final design of the replacement caps (Appendix A). This report documents the construction of the SPL landfill at Terminal 5 at the Port of Vancouver as required by the Ecology, and certifies that construction was in accordance with the plans, specifications, and Construction Quality Assurance (CQA) plan. Documentation of asbuilt drawings, test results, daily reports, and acceptance forms for the base grades and liner are included in Appendix B and C.

2.0 Background

The SPL landfill consists of an approximately 3.8 acre area that was initially covered with 1 to 2 feet of clean soil, a high-density polyethylene (HDPE) liner, and contaminated soil and crushed spent potliner below the liner. The HDPE liner, the crushed spent potliner, and all soil beneath the HDPE liner are Resource Conversation and Recovery Act (RCRA) and Chapter 173-303 of the Washington Administrative Code (WAC) hazardous waste that is designated as K088.

The Port performed sampling and analysis of the soils in May 2009 to ensure appropriate management of these soils during the construction of the rail and associated laydown area (HDR 2009a). The results of this sampling effort confirmed that soils remain K088 waste. No "contained in" determination was presented to Ecology. While the design originally planned for off-site disposal of soils, in the final design, it was determined that no soils would leave the site. The Port has prepared a Contaminated Media Management Plan to ensure safe and compliant management of these soils during construction (HDR 2009b).

The 1992 Consent Decree (Ecology 1992) required that the cap for the SPL Landfill be either a synthetic liner (40 mil PVC or 50 mil HDPE) covered with two feet of clean sand and topsoil including vegetation, or two feet of recompacted clay or other material with a permeability of no more than 1 x 10^{-6} cm/sec.

To mitigate the removal of the SPL cover, the Port proposed to replace the soil cover with an asphalt cap system. The cap system would consist of a minimum of two lifts of asphaltic concrete with an asphaltic cement-impregnated geotextile between lifts. Asphalt sections would include a 2.5 inch asphalt base below the geotextile, and a 5.5-inch thick asphalt above the geotextile. This represents a 2.5 inch cap layer plus a 3 inch wearing course. The final hydraulic conductivity of the asphalt would have a maximum permeability of 10⁻⁷ cm/sec, which provides equivalent or better protection than the requirements under the 1992 Consent Decree (no more than 10⁻⁶ cm/sec).

In addition to the design, a bench scale analysis of the proposed cap system was completed. The bench scale test measured hydraulic conductivity results for samples compacted to 91%, 94%, and 98% of theoretical density. Results of the testing indicated that the target hydraulic conductivity of 1×10^{-7} cm/sec can be achieved at all three of the target densities, and that there

is a trend of decreasing hydraulic conductivity as asphalt density is increased. These results supported the final design (HDR 2009d).

This final construction design was submitted to Ecology in October 2009 (HDR 2009c) and subsequently approved by Ecology (Appendix A) prior to construction.

3.0 Construction Narrative

The proposed construction of the cap was reviewed in the Pre-Construction meeting held on February 16, 2010 with the General Contractor, Rotschy Inc., Port, City of Vancouver (COV), and HDR staff. Construction of the replacement cap began in March 2010 and was completed in April 2010. The entire 3.38 acre soil cover was replaced with asphalt. Approved submittals related to the materials of construction and construction methods are included in Appendix B as part if the Test Pad Construction Report and summarized in Table 1.

Submittal Number	Description	
18	Substitute TerraTex OL Asphalt Fabric for Propex Petromat 4599	
30	34" Hot Mix Asphaltic Concrete Mix Design	
73	SPL Test Pad Area Work Plan for Test Pad Construction	
83.2	TRI Environmental Testing Laboratory	
108	Specification and Material Certification for PG-64-22 oil for paving fabric	
118	Hot Oil Application Data Sheet	

Table 1: Approved Submittals for SPL Landfill Cap Construction

Minor modifications to plans and specifications to accommodate conditions in the field were proposed and approved by the COV, POV, and HDR. These modifications are provided in the as-builts in Appendix C and include:

- Request for Information (RFI) 22 which requested a change in the application of oil (tack coat) to both sides of the paving fabric was approved and subsequently the test pad passed/exceeded the specified hydraulic conductivity.
- Submittal 73 which requested the use of a vibratory roller to achieve Hot Mix Asphalt (HMA) compaction versus the pneumatic roller specified by the Washington State Department of Transportation (WSDOT) specifications for paving during the months of October through April.

Construction was observed by the HDR Construction Quality Assurance Monitor (CQAM). Construction consisted of the following elements and met the construction specifications:

- Subgrade material placement and compaction to meet the construction specification of 94% compaction. This specification was verified by the COV.
- Tensar Triaxial Geogrid was placed and consisted of rolling the material out over the compacted subgrade and covering with the surfacing base course. The Triaxial Geogrid was overlapped approximately 12 inches with the roll widths extending over the cap area. Three inches of surfacing base course was placed and compacted over the Triaxial Geogrid.

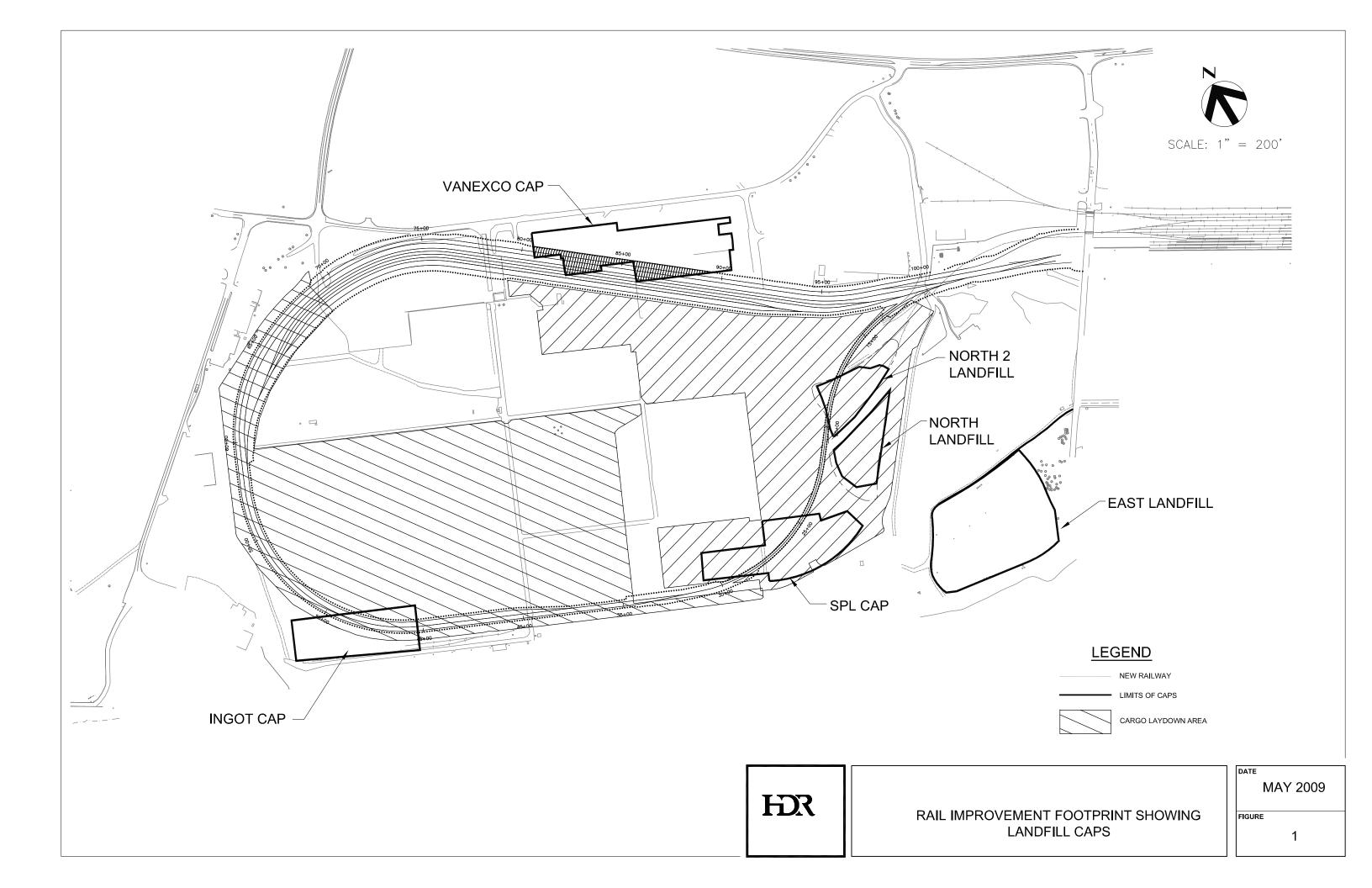
- ³⁄₄-inch PG-64-22 Level 3 hot mix asphalt (HMA) was placed over the subgrade. 2 ½inch HMA was applied with a Blaw Knox PF 4410 with a Carlson Easy Screed. The HMA was then compacted with a HYPAC tandem-drum vibratory roller and a Volvo DD90 HF roller. Static rolling was applied in the forward rolling direction with vibratory rolling applied in the reverse rolling direction. HMA compaction was verified by roller pattern observation by the COV.
- A tack coat of PG-64-22 oil was then mechanically applied over the HMA base course. The tack coat was applied by a mechanical sprayer at a rate of 0.203 gallons per square yard. The application rate was verified by Vancouver Paving.
- TerraTex OL asphalt overlay fabric was placed over the tack coat using a roller system developed by Rotschy. Overlay fabric creases were either straightened out or cut to provide a smooth surface and panels were overlapped 2 feet.
- The ¾-inch Level 3 HMA was then placed over the fabric overlay. The 2 ½-inch HMA overlay was applied with a Blaw Knox PF 4410 with a Carlson Easy Screed. The HMA was then compacted with a HYPAC tandem-drum vibratory roller and a Volvo DD90 HF roller. Static rolling was applied in the forward rolling direct with vibratory rolling applied in the reverse rolling direction. HMA compaction was verified by the COV using ASTM D2950.

4.0 Conclusions

Construction of the SPL Landfill Cap was observed by HDR CQAM. The equipment used in construction met the specified requirements, and materials delivered to the site were in good condition. Based on the CQAM construction observations and the results of the hydraulic conductivity and density testing during Test Pad installation, the final SPL Landfill Cap was constructed in accordance with the design criteria, plans, and specifications, with the exception of the two modifications noted in Section 3. The constructed SPL Landfill Cap meets the 1×10^{-7} or greater hydraulic conductivity and meets the design requirements as approved by Ecology.



Kurt Reichelt, P.E. HDR Project Manager



5.0 References

(Ecology) Washington State Department of Ecology

1992 Consent Decree No. 92-2-00783-9. Washington State Department of Ecology, Olympia, Washington.

HDR Engineering, Inc.

- 2009a Environmental Investigation of the SPL Landfill, Port of Vancouver, Washington. July 13, 2009. Portland, Oregon.
- 2009b. Contaminated Media Management Plan, Terminal 5, Port of Vancouver, Washington. July 31, 2009. Portland, Oregon.
- 2009c. Final Request for Review and Approval of Disturbance of Landfills on Former Alcoa/Evergreen Properties. October 15, 2009. Portland, Oregon.
- 2009d. Memo to Patty Boyden and Jessi Belston, Port of Vancouver: Re SPL Cap Bench Scale Asphalt Testing Results. August 31, 2009.

APPENDIX A

Ecology Approval of Final Request for Review and Approval of Disturbance of Landfills on Former Alcoa/Evergreen Properties



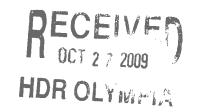
STATE OF WASHINGTON

DEPARTMENT OF ECOLOGY

PO Box 47600 • Olympia, WA 98504-7600 • 360-407-6000 711 for Washington Relay Service • Persons with a speech disability can call 877-833-6341

October 21, 2009

Ms. Patty Boyden Director of Environmental Services Port of Vancouver 3103 NW Lower River Rd. Vancouver, WA 98660



Re: Review of Terminal 5 Rail Improvement Engineering.

Dear Ms. Boyden:

Ecology has reviewed the October 15, 2009 Terminal 5 Improvements - Final Request for Review and Approval of Disturbance of Landfills on Former Alcoa/Evergreen Properties work plan for the former Alcoa/Evergreen smelter facility. The site is located on the former Alcoa/Evergreen aluminum smelter west of Vancouver, WA. The Terminal 5 rail improvements consist of a two-mile rail loop that will traverse four of five covered areas on the site. These affected areas are known as: Vanexco Cap, Ingot Cap, North and North2 landfills, and Spent Potliner NPL site cap. Ecology received and commented on the draft work plan on July 15, 2009 by e-mail. The final work plan is the result of the July review.

The October 15, 2009 Final Request for Review and Approval of Disturbance of Landfills on Former Alcoa/Evergreen Properties is approved as submitted in the October 15 document. The revised document fulfills the requirements of the MTCA consent decrees that regulate the four areas. The Port of Vancouver is approved to begin work at the site once local permits are final.

We look forward to visiting the site once construction has begun. If you have any questions regarding the approval of the work plan, please contact me in Lacey (360) 407-6949 or psky461@ecy.wa.gov.

Sincerely,

Paul Skyllingstad Industrial Section

Cc: B. Morson - HDR M. Stiffler - Alcoa

APPENDIX B

Test Pad Construction Report

West Vancouver Freight Access Project

Project 03 Terminal 5 Spent Pot Liner Test Pad Construction Report

May 6, 2010



Prepared for: **Port of Vancouver** 3103 NW Lower River Road Vancouver, Washington 98660-1027



Prepared by: HDR Engineering, Inc. 1001 SW Fifth Ave, Suite 1800 Portland, Oregon 97204



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Attachment D	City of Vancouver Subgrade Density Test
Attachment E	City of Vancouver HMA Compaction Testing
Attachment F	Photographic Documentation
Attachment G	TRI Environmental SPL Hydraulic Conductivity Test
Attachment H	City of Vancouver SPL HMA Density Testing

1.0 Introduction

This report documents the construction of the Spent Pot Liner (SPL) Asphalt Cap Test Pad as presented in the SPL Asphalt Cap Test Pad Protocol, HDR Engineering (HDR) dated July 30, 2009 (Attachment A). The SPL Asphalt Cap Test Pad Protocol proposes the construction of an asphalt cap over the SPL Cap (3.8 acres) that contains contaminated soils. The cap consists of a layer of asphalt overlain by an asphalt-impregnated geotextile (a combination of non-woven polypropylene fabric and asphalt cement tack coat) overlain by a second layer of asphalt. The fabric and tack coat combination form an asphalt membrane interlayer within the pavement section. The purpose of the test pad is to verify the results, under field conditions, of the bench scale testing of the asphalt section (Attachment B).

2.0 Test Pad Objectives

The test pad objectives for the SPL Asphalt Cap are:

- To verify that the materials and methods of construction will produce an asphalt liner that meets the target hydraulic conductivity for the project. The target hydraulic conductivity for the test pad section is 1x10⁻⁷ cm/sec, or less.
- To establish a correlation between the bench scale testing and full-scale testing. If the test pad meets the performance objectives for the cap (as verified by hydraulic conductivity and density tests) and the full-scale liner is constructed to density standards that equal or exceed those used in building the test pad, then assurance is provided that the full-scale liner will also meet hydraulic conductivity performance objectives.

3.0 Construction Narrative

The test pad was constructed on March 4, 2010 by Vancouver Paving a subcontractor of Rotschy Inc., the General Contractor for this project. As required by the SPL Test Pad Protocol, Rotschy Inc. prepared the SPL Test Pad Construction Plan which detailed the methods and techniques for constructing the SPL Test Pad. The Plan was reviewed and approved by the City of Vancouver (COV), Port of Vancouver (POV), and HDR. The Plan was also reviewed in the Pre-Construction meeting held on February 16, 2010. Approved submittals related to the materials of construction and construction methods are listed in Table 1 and are included in Attachment C.

Submittal Number	Description
18	Substitute TerraTex OL Asphalt Fabric for Propex Petromat 4599
30	34" Hot Mix Asphaltic Concrete Mix Design
73	SPL Test Pad Area Work Plan for Test Pad Construction
83.2	TRI Environmental Testing Laboratory
108	Specification and Material Certification for PG-64-22 oil for paving fabric
118	Hot Oil Application Data Sheet

Table 1: Approved Submittals for SPL Test Pad Construction

Construction was observed by the HDR Construction Quality Assurance Monitor (CQAM). Construction consisted of the following elements:

- Subgrade material placement and compaction to meet the construction specification of 94% compaction. This specification was verified by the COV (Attachment D). The subgrade was tested in 19 separate locations and all test locations met or exceeded the 94% compaction specification. The overall dimension of the test pad is 28 feet wide and 200 feet long for a total area of 6,000 square feet.
- Tensar Triaxial Geogrid was placed on February 23, 2010. Placement of the Triaxial Geogrid consisted of rolling the material out over the compacted subgrade and covering with the surfacing base course. The Triaxial Geogrid was overlapped approximately 12 inches with the roll widths extending over the test pad area. Three inches of surfacing basecourse was placed and compacted over the Triaxial Geogrid.
- On March 4, 2010 the ³/₄-inch PG-64-22 Level 3 hot mix asphalt (HMA) was placed over the subgrade. The 2 ¹/₂-inch HMA was applied with a Blaw Knox PF 4410 with a Carlson Easy Screed with a panel width of 14 feet. The HMA was then compacted with a HYPAC tandem-drum vibratory roller and a Volvo DD90 HF roller. Static rolling was applied in the forward rolling direction with vibratory rolling applied in the reverse rolling direction. HMA compaction was verified by roller pattern observation by the COV.
- A tack coat of PG-64-22 oil was then mechanically applied over the HMA base course. The tack coat was applied by a mechanical sprayer at a rate of 0.203 gallons per square yard. The application rate was verified by Vancouver Paving based on the test shot and gallons of PG-64-22 applied to the HMA base course.
- TerraTex OL asphalt overlay fabric was placed over the tack coat using a roller system develop by Rotschy. Overlay fabric creases were either straightened out or cut to provide a smooth surface. The overlap fabric rolls were 12.5 feet wide and overlapped 2 feet.
- The ¾-inch Level 3 HMA was then placed over the fabric overlay. The 2 ½-inch HMA overlay was applied with a Blaw Knox PF 4410 with a Carlson Easy Screed with a panel width 14 feet. The HMA was then compacted with a HYPAC tandem-drum vibratory roller and a Volvo DD90 HF roller. Static rolling was applied in the forward rolling direct with vibratory rolling applied in the reverse rolling direction. HMA compaction was verified by the COV using ASTM D2950 (Attachment E). Six density tests were performed at different locations on the paved panels with percent compactions ranging from 92.8% to 95%. The average compaction density was 93.7% meeting the Washington State Department of Transportation (WSDOT) specification of 92%.

Construction of the SPL Test Pad is documented in the photographs presented in Attachment F.

4.0 Materials Testing

HDR obtained core samples for hydraulic conductivity testing on March 5, 2010. Three 12 inch by 12 inch core samples were cut from the west end of the SPL test pad using a cut-off saw. Sample ID 1 is from the first overlay fabric, base HMA and HMA overlay. Sample ID 2 is from the second overlay fabric, base HMA and HMA overlay. Sample ID 3 is form the overlay fabric overlap, base HMA and HMA overlay. The samples were sent for hydraulic conductivity analysis by ASTM D5084 to TRI Environmental Laboratory in Austin, TX (Attachment G). HDR specified that the testing must be performed with 70 kPa confining pressure with the sides of the core samples treated with silicone vacuum grease or bentonite paste to reduce sidewall leakage. Three inch diameter cores were taken from the 12 inch by 12 inch samples for testing. Hydraulic conductivity test results are provided in Table 2.

Submittal Number	Analysis Result	Analysis Result
Test Pad required	1x10 ⁻⁷	.000001
hydraulic conductivity		
Sample ID 1	1.5E-08	.00000015
Sample ID 2	1.1E-08	.00000011
Sample ID 3	1.1E-08	.00000011

Table 2: Hydraulic Conductivity Test Results

Six 3 inch core samples were taken on March 17, 2010 and sent for density testing to the COV using method ASTM 2950 (Attachment F). Core samples were collected from each side of the 12 inch by 12 inch cores samples taken for hydraulic conductivity testing. The samples were split to test each lift of HMA. Density testing results are presented Table 3.

Core Sample Identification	Core Density	Percent Compaction
North 1 Top	149.98	96.4
North 1 Bottom	146.47	94.2
North 2 Top	146.49	94.2
North 2 Bottom	143.43	92.2
Middle 1 Top	149.21	96.0
Middle 1 Bottom	145.43	93.5
Middle 2 Top	149.23	96.0
Middle 2 Bottom	148.72	95.6
South 1 Top	146.35	94.1
South 1 Bottom	147.14	94.6
South 2 Top	145.97	93.9
South 2 Bottom	147.35	94.8

Table 3: Density Testing Results

The densities achieved in the Bench Scale Testing were 91%, 94% and 98%. Hydraulic conductivity of 1×10^{-7} was achieved at all of these densities. Comparison of the Bench Scale Testing results to the core densities from the SPL Test Pad indicates that all SPL Test Pad densities are comparable to the Bench Scale Testing.

5.0 SPL Test Pad Construction Analysis

Construction of the SPL Test Pad was observed by HDR CQAM. The CQAM noted that the construction was performed in general compliance with design criteria, plans and specifications. The equipment used in construction met the test requirements and materials delivered to the site were in good condition. The samples taken from the SPL Test Pad were in general accordance with the ASTM methodology and procedures. The CQAM verified that the SPL Test Pad was constructed in accordance with plans and specifications with no noted deviations.

Based on the CQAM construction observations and the results of the hydraulic conductivity and density testing, the SPL Test Pad was constructed in accordance with the design criteria, plans

and specifications. SPL Test Pad core sample results indicate that 1×10^{-7} hydraulic conductivity was achieved in two test panels and the panel overlap. Density test results were within those achieved in the Bench Scale Study. These testing results strongly correlation with the Bench Scale Study Results and SPL Test Pad results and this construction technique applied over the existing SPL Cap should provide 1×10^{-7} or greater hydraulic conductivity. No deviations from the project documents were noted other than the following which were approved by the POV, COV, and HDR: 1) RFI 22 which requested a change in the application of oil (tack coat) to both sides of the paving fabric which was approved and subsequently the test pad passed/exceeded the specified hydraulic conductivity; and, 2) Submittal 73 which requested the use of a vibratory roller to achieve HMA compaction versus the pneumatic roller specified by the WSDOT specifications for paving during the months of October through April.

Kurt Reichelt, P.E.

HDR Construction Quality Assurance Engineer



ATTACHMENT A

SPL Asphalt Cap Test Pad Protocol

PORT OF VANCOUVER SPL ASPHALT CAP TEST PAD PROTOCOL VANCOUVER, WASHINGTON

PREPARED FOR:

Port of Vancouver

PREPARED BY:

HDR ENGINEERING, INC. Omaha, Nebraska

July 30, 2009

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1. Introduction

The Port of Vancouver, Washington proposes to place an asphalt cap over the SPL Cap (3.8 acres) that contains contaminated soils. The cap will consist of a layer of asphalt overlain by an asphalt-impregnated geotextile (a combination of non-woven polypropylene fabric and asphalt cement tack coat) overlain by a second layer of asphalt. The fabric and tack coat combination will form an asphalt membrane interlayer within the pavement section. Additional asphalt layers will be required for structural design purposes, but are not included in this protocol. The purpose of the test pad is to verify the results, under field conditions, of bench scale testing of the asphalt section.

2. Test Pad Objectives

- 1. To verify that the materials and methods of construction will produce an asphalt liner that meets the target hydraulic conductivity for the project. The target hydraulic conductivity for the test pad section is 1×10^{-7} cm/sec, or less.
- 2. To establish a correlation between the bench scale testing and full-scale testing. If the test pad meets the performance objectives for the cap (as verified by hydraulic conductivity and density tests) and the full-scale liner is constructed to density standards that equal or exceed those used in building the test pad, then assurance is provided that the full-scale liner will also meet hydraulic conductivity performance objectives.

3. Test Pad Protocol

3.1 Definitions

Construction Quality Assurance (CQA) Engineer: The owner's representative responsible for verification of the construction methods and materials to project plans, specifications, and protocols.

Construction Quality Assurance Monitor: The individual responsible for observation and documentation of construction under the supervision of the CQA Engineer.

3.2 Test Pad Dimensions

The test pad shall be constructed to the minimum compaction as determined by the Bench Scale Protocol, References 2 and 3. Details of construction shall be proposed by the Contractor and approved by the CQA Engineer. The configuration of the test pad shall conform to the following criteria:

1. The lane width must be sufficient to allow the specified compaction equipment to operate without overlapping the drum into the ballast and introducing ballast material into the asphalt.

- 2. The lane length must be sufficient to allow the compaction equipment to reach its design operating speed.
- 3. Lanes must be adequately separated to ensure that each lift can be compacted to the desired relative compaction.
- 4. The test pad shall be constructed in two lifts with a minimum compacted thickness of 2.5 inches per lift. An asphalt-impregnated geotextile shall be placed between the asphalt lifts.

3.3 Materials and Construction

All materials and methods used in the construction of the test pad shall conform to the project specifications, the Bench Scale Testing Protocol (HDR, 2009b), and the Bench Scale Test Final Report (HDR, 2009c). The methods, materials and equipment used in successful completion of the test pad shall be used in construction of the Cap. Each lift of each lane shall be compacted using the same equipment, operating speed and number of passes. The lower lift of the test pad shall provide a smooth surface, with consistent texture and free of irregularities. The lift must be constructed and finished to provide continuous intimate contact with the overlying geotextile. Adequate geotextile shall be left exposed along the ends and sides of the pad to allow incorporation of the pad into the final cap, if the cap section meets the hydraulic conductivity specification.

3.4 Test Pad Construction Observation

Full time observation of subgrade preparation is not required. The CQA Monitor shall document and observe proof-rolling and density testing of the subgrade. The CQA monitor shall observe the completed placement of the recycled concrete. Observations shall be documented in daily reports. Full-time observation and documentation of the placement of the asphalt and asphalt impregnated geotextile is required. The number of passes of the compactor over each lane shall be documented. Daily field reports will note observations and any deviations from the plans, specifications, and this protocol.

3.5 Required Tests

The tests listed in Table 1 are required to evaluate the hydraulic conductivity of the test section and its ability to control infiltration. At the owner's request, additional testing may be performed per WSDOT test pad requirements to verify the structural suitability of the section.

Material Tested	Parameter	Frequency	Test method
Subgrade Placement and compaction		Full coverage	Visual observation
Subgrade density testing	Placement and compaction	2 per lane	ASTM D2922
Crushed Concrete Base	Placement and compaction	2 per lane	ASTM D2922
Hot Mix Asphalt	Mix Design	1 per mix	Submittal review
Geotextile Interlayer	Strength and retention properties	Bracketed by manufacturer's quality control testing	Verification of manufacturer's QC
Geotextile Interlayer	Retention properties	Full coverage	Observation
Asphalt	Compaction	3 per lane per lift	ASTM D2950
Asphalt and Geotextile Interlay	Hydraulic conductivity	2 representing the range of compaction	Modified ASTM D-5084 ¹

Table 1: Required Tests

¹70kPa confining pressure, sides of core treated with silicone vacuum grease or bentonite paste to reduce sidewall leakage.

3.6 Deviations from this Protocol

The CQA Engineer may propose deviations from the protocol, if warranted by the results of the bench scale testing. Deviations proposed by the Contractor to more efficiently utilize available machinery may also be considered, if the machinery will be used in full-scale construction as well. Proposed deviations must be provided to and approved by the Port of Vancouver prior to submittal to the Washington Department of Ecology (WDOE). Once submitted to the WDOE, an approval in writing from the WDOE must be obtained and provided to the Port of Vancouver 5 days before construction of the test pad begins.

4. Documentation and Recommendations

Test pad construction shall be documented in a written report, sealed by the CQA Engineer. The report shall include at a minimum:

- Construction narrative detailing methods, materials and equipment used
- Construction daily reports documenting activities and noting deviations from the project plans,
- Specifications and this protocol
- Test results and a statement that the test pad was constructed in substantial accordance with the project documents.
- Deviations from the project documents shall also be noted in the report.

The report shall be submitted to the Port of Vancouver 5 days prior to construction of the SPL replacement cap.

5. References

HDR, 2009a. Contract Provisions and Plans for Construction of West Vancouver Freight Access Project Terminal 5 Unit Train Improvements. August 2009.

HDR, 2009b. Port of Vancouver SPL Landfill Asphalt Cap Bench Scale Testing Protocol. July 2009.

HDR, 2009c. Final Report for Port of Vancouver SPL Landfill Asphalt Cap Bench Scale Testing Protocol. August 2009.

ATTACHMENT B

SPL Landfill, Asphalt Cap Bench Scale Testing Protocol

HR ONE COMPANY Many Solutions ⁸⁴	Memo
To: Patty Boyden, Port of Vancouver Jessi Belston, Port of Vancouver	
From: Ted Alexander, HDR	Project: WVFA Project Port of Vancouver, Washington
CC: Scott Hale, HDR Greg Shafer, HDR Bruce Larsen, HDR	
Date: August 31, 2009	Job No: 98539

RE: SPL Cap Bench-Scale Asphalt Testing Results

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The bench scale testing results (see attached) includes measured hydraulic conductivity results for samples compacted to 91%, 94% and 98% of theoretical density. Results of the testing indicate that the target hydraulic conductivity of 1×10^{-7} cm/sec can be achieved at all three of the target densities, and that there is a trend of decreasing hydraulic conductivity as asphalt density is increased. In the bench scale tests, the asphalt pills were "glued together by the asphalt cement with only hand pressure to distribute the asphalt cement and press the textile into contact with the asphalt samples. It is possible that the measured hydraulic conductivities in the test pad will be substantially lower than the laboratory measurements. In the field, the upper layer of asphalt will be compacted over the lower layer and the textile, which may result in a more intimate contact between the textile and the asphalt, as well as a more uniform distribution of the asphalt cement within the textile.

The protocol allows deviation from established test pad construction procedures if warranted by the results of the bench scale testing. Given the results of the bench-scale tests, construction of the asphalt test pad can proceed as outlined in the Asphalt Full Scale Test Pad Protocol (July 2009).



Cal-Tech Testing, Inc. • Engineering

Geotechnical

Environmental

LABORATORIES

P Ol Box 1625 + Lake City FL 32056 4784 Rosselle Street + Jacksonvide FL 32254 Tel 386) 755-3633 · Fax (386) 752-5456

Tel 904) 381-8901 · Fax (904) 381-8902

August 26, 2009

HDR Engineering, Inc.

200 West Forsyth Street, Suite 800 Jacksonville, Florida 32202

.

Attention: Mr. Ted Alexander, P.E.

Reference: SPL landfill, Asphalt Cap Bench Scale Testing Protocol Port of Vancouver Cal-Tech Project No. 09-00233-01

Dear Mr. Alexander:

On June 1, 2009 Cal-Tech Testing (CTI) received a request via e-mail to provide bench scale testing per a written Protocol (the Protocol) prepared by HDR Engineering, revised and finalized July of 2009 and received by CTI on July 20, 2009. We understand that our scope of services consists of preparing eighteen (18) asphalt specimens in general accordance with the Materials and Density Testing of Samples sections of the attached Protocol. These pills were prepared and blended in accordance with the approved mix design (attached). Each of these gyratory compacted samples were cored through the approximate center to extract a 2³/₄-inch diameter specimen. The specimens were then saw-cut (using a wet saw) on both ends to produce 2¹/₂-inch high pills for use in the permeameters.

For each permeability test sample, two of the $2\frac{3}{4}$ "-diameter by $2\frac{1}{2}$ "-high pills were bonded together by means of two layers of tack-coat separated by a layer of Petromat® PV-4599 geotextile fabric manufactured by PROPEX. The geotextile was placed smooth-face down. With each face coated with tack, a rate of about ± 0.20 gal/yd² was applied. The coated geotextile was placed between the two cored samples to create a bonded 2-layer $2\frac{3}{4}$ "-diameter 5"-high specimen to be tested for hydraulic conductivity. Human pressure was applied to align and join the two specimens. The side face of the hydraulic conductivity specimens were treated with silicon vacuum grease (the top and bottom were not treated).

The nine (9) hydraulic conductivity specimens were then placed in the permeameters and tested in general accordance with ASTM D-5084. The following table summarizes our laboratory test results:

Sample ID	% Theoretical Max. SpecificUnit WeightSample IDGravity, Gmm(AASHTO T 312)(AASHTO T 209)(pcf)		Hydraulic Conductivity (ASTM D 5084) (cm/sec)	
91-1-Top	91.1	144.9	6.213x10 ⁻⁸	
91-1-Bottom	91.0	144.8	6.213x10	
91-2 Top	91.1	144.9	0,510,10 ⁻⁸	
91-2 Bottom	91.0	144.8	6.518x10 ⁻⁸	
91-3-Top	91.1	144.9	2 202 40 ⁻⁸	
91-3-Bottom	91.5	145.6	3.393x10 ⁻⁸	
94-1-Top	94.1	149.7	0.044.408	
94-1-Bottom	94.2	149.9	2.844x10 ⁻⁸	
94-2-Top	94.2	149.9	0.070.108	
94-2-Bottom	94.2	149.9	3.270x10 ⁻⁸	
94-3-Top	93.7	149.1	a 100 10 ⁸	
94-3-Bottom	94.1	149.7	3.426x10 ⁻⁸	
98-1-Top	97.8	155.6	1.746x10 ⁻⁸	
98-1-Bottom	97.7	155.5	1.746X10 ⁻	
98-2-Top	98.0	155.9	1 010 40 ⁸	
98-2-Bottom	97.9	155.8	1.613x10 ⁻⁸	
98-3-Top	97.6	155.3	4 700 40-8	
98-3-Bottom	97.8	155.6	1.708x10 ⁻⁸	

We appreciate the opportunity to be of service on this project and look forward to a continued association. Should you have questions concerning this report or if we may be further service, please contact this office.

Respectfully submitted, Cal-Tech Testing, Inc.

6/09 Nabil O. Hmeidi, P.E.

Senior Geotechnical Engineer Licensed, Florida No. 57842

David B. Brown Executive Vice President

STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION STATEMENT OF SOURCE OF MATERIALS AND JOB MIX FORMULA FOR BITUMINOUS CONCRETE

SUBMIT TO T	THE STATE M	ATERIALS EN	GINEER, CEN	TRAL BITUMING	DUS LABORAT	ORY, 5007 N	ORTHEAST 39T	'H AVENU	E, GAINES	VILLE, FL 32609
Project No.					СТОР С	Qualified Mix	Designer		Richard	Godbold
Contractor					Address					
Phone No.	<u></u>		Fax No.			E-mail				
Submitted By	Cal-	al-Tech Testing, Inc. Type Mix				Intendeo	d Use of N	Vix		
							Submitter Mix ID. 09-233;12			09-233;12398
TYP	E MATERIA	L	F.D.O.T. CODE		PRODUCER		PIT NO.		DATE S	AMPLED
1. #67 Stone			42	Junction City	Mining, L.L.	С.	GA-553		07 / 30	/ 2007
2. #78 Stone			44	Martin Marie	NS-315		07 / 30	/ 2007		
3. #89 Stone			54	Martin Marietta Aggregates NS-315			07/30	/ 2007		
4. W-10 Screen	ings		21	Martin Marietta Aggregates		GA-383 07 / 30 / 2007			/ 2007	
5. M-10 Screen	ings		22	Martin Marie	Martin Marietta Aggregates			GA-383 07 / 30 / 2007		
6. Sand				Duval Aspha	It Products		Gunner 07 / 30 / 2007			/ 2007
7. PG 76-22							07 / 30 / 2007			/ 2007
		PER	CENTAGE E	Y WEIGHT T	OTAL AGGR	EGATE PA	SSING SIEVE	ES		
Blend	18%	15%	12%	20%	20%	15%	JOB MIX	CON	TROL	
Number	1	2	3	4	5	6	FORMULA		NTS	
3/4" 19.0mm	100	100	100	100	100	100	100	90 -	- 100	
ш <u>1/2" 12.5mm</u>	59 27	<u>83</u> 59	100 94	100	100 100	100 100	90	•	- 90	
N 3/8" 9.5mm	21	- 59 - 7	<u>94</u> 40			100	80			
ー No.4 4.75mm の No.8 2.36mm	<u> </u>			100	100		61	00	40	
		2	12	59	71	100	43	23 -	- 49	
No. 16 1.18mm	1	1	5	44	47	95	33			
Ш No. 30 600µm	1	1		25	35	87	26			
> No. 50 300µm	1	1 1	3	16 7	27	50	17			
ш No. 100 150µm — No. 200 75µm	1.0	1.0	2	5.0	20 14.0	17 3.0	9 4,7	2 •	7	
и G _{sв}	2.808	2.627	2.625	2.725	2.735	2.626	2.699		- 1	

Optimum Asphalt	=	4.8
Viscosity of M.M.	=	
AC in M.M.	=	

SHEET
SN DATA
IX DESIGI
HOT M

09-233;12398

P _{0.075} /P _{be} %G _{tim} @ N _{ia} %G _{tim} @ N _{trax}	87.7 95.7	89.0 97.0	90.2 98.2	91.5 99.5		4.8 5.3 5.8 6.3 % Asphait % Asphait % 6.3 %
P.005 / P.	1.3	1.1	1.0	0.9		⁹⁰ ⁹⁰ ⁸⁴ ⁸⁵ ⁸⁵ ⁸⁶ ⁸⁶ ⁸⁶ ⁸⁶ ⁸⁶ ⁸⁸ ⁸⁹
<u>2</u>	3.6	4.1	4.6	5.1		emperature
VMA	13.8 61	13.7 71	13.7 80	13.7 89		
N ^a	5.4	4.0	2.8	1.5		A 45 %
Grim	2.570	2.550	2.530	2.510		14.0 14.0 13.6 13.6 13.6 53.6 13.6 13.6 13.7 13.5 13.8 13.6 13.8 13.6 13.8 13.6 13.8 13.6 13.8 13.7 13.8 13.6 13.8 13.7 13.8 13.8 <
Gnb @ Ndes	2.432	2.448	2.460	2.473		Asphalt 2448 Kg/m ³ (+To
ഹ്	4.3	4.8	5.3	5.8		98.6 97.0 97.0 96.1 96.1 96.3 94.5 94.5 94.5 3.8 4.3 4.3 7.8 Asphalt Total Binder Content <u>4.80</u> % MA <u>13.7</u> %

ATTACHMENT C

Submittals

Submittal 18

irt of Va	Port of Vancouver USA	FROM: Rotschy, Inc 9210 NE 62nd Ave Varnouver, Washington 93665	e nglon 98665		DATE	12/04/2009	Thiss becon by CO	This section to be completed by COV:
CONSTRUCTION MANAGER 3103 NW Lower River Road Vancouver, Washington 93656	CONSTRUCTION MANAGER 3103 NW Lower River Road Vandouver, Washington 93660	PROJECT: Terminal 5 Unit Train improvements CP0144 This section to be completed by contractor:	ain improvements Mactor.		Resubmat Previous a	Resubmittat Revious Submittai No.	Suban	Submittal No.
Bid Item Drawing Number(s) Sheet No.	Ving t.No.	Description - Manufacturer's Specific Product	Affic Product*	Type"		Manufacturer / Brand futerior of #	Review	
	1	TerraTex OL Asphalt Overlay Fabric meets the requirements listed on F-71 as is an exact	isled on F-71 as is an exact	YP Y	Hanes Geotextile;	Hanes Geo; Satem NC	0	Man ta Jer
	equal to Propex (same	equat to Propex (same mill, same material, different tabel). See attached certification letter	e attached certification letter				<u> </u>	
65-63		TerraTex NOS for seperation under access roads; meets Washdot 9-33.2(1) no other spec	hdot 9-33.2(1) no other spec	¥ ₽	Hartes Geotextile; Puvailup Wa	Hanes Geo: Safem NC	60	man tarter man
	found			-				
			and the second					
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			a provide a supervision de la constante de la c					
				1990.0000		4		
ior shall sub	Contractor shall submit 6 copies of each	* one component per line	** Type Codes:	approval or		mpliance Raceived:	(ed:	
ent, and sha (s)) on each	attachment, and shall write bid item number(s)) on each attached page.		B - Catalog Cut/Data Sheet C - Mrx Design	CuttData S Sim		nigs	12-1-09	60
			D-OPL		H - Other	ŀ		
the le	By: By:		tegend: Keview Action 1 No exceptions taken		Distribution	Target Date	initial	Date
COV Review Comments-	41		2 Note markings		Reviewed by: 17Dia	ľ.	DKN	PO-F-C1
			3 Comments attached.		Reviewed by Mark Lab			
			Resubrat 4 Rejected		Reviewed by:			
			5 Submit WSDOT Pitt		COV, Construction			
					Relumed to contractor			

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TerraTex OL ASPHALT OVERLAY FABRIC

TerraTex OL is a nonwoven geotextile made up of polypropylene fibers. These fibers are needled to form a stable and durable network such that the fibers retain their relative position. It is non-biodegradable and resistant to most soil chemicals, acids and alkali with a pH range of 3 to 12. **TerraTex OL** is manufactured to meet or exceed the following minimum average roll values:

Property	Test Method	Ro	um Average II Value Inglish	Ro	um Average III Value <u>Wetric</u>
Unit Weight	ASTM D-5261	3.8	oz/yd²	128	g/m²
Tensile Strength	ASTM D-4632	90	lbs	.400	kN
Tensile Elongation	ASTM D-4632	50	%	50	%
Trapezoidal Tear	ASTM D 4533	35	lbs	.16	kN
Puncture Resistance	ASTM D 4833	55	lbs	.25	kN
Mullen Burst	ASTM D-3786	180	psi	1240	kPa
UV Resistance	ASTM D-4355	70	% @ 150 hr	70	% @ 150 hr
Asphait Retention	TX DOT 3099	0.2	gal/yd²	0.9	l/m²
Melting Point	ASTM D 276	300°	F	149°	С

9/08

815 Buxton Street · Winston Salem, NC 27101 888-239-4539 · Fax: 336-747-1652 www.hanesgeo.com · info@hanesgeo.com



Greg Osendorf greg.osendorf@hanesindustries.com 5927 Balfour Ct., Suite 108 Carlsbad, CA 92008 Tel. 760-431-2452 Fax 760-431-2453

Tuesday, December 01, 2009

Hanss Schmeusser Rotschy, Inc. 9210 NE 62nd Ave. Vancouver, WA 98665

Re: Petromat vs Terratex OL

Dear Hanss:

This letter is to address the equivalency between Petromat 4599 and Terratex OL. Below, please find a property by property comparison between the two products showing the Terratex OL meets or exceeds the properties of the Petromat 4599:

		Propex Petromat 4599	Terratex OL
Property	<u>Test Method</u>	MARV Value	MARV Value
Weight (Typical)	ASTM D-5261 ASTM D-4632	3.6 oz/sy	3.8 oz/sy 90 lbs
Tensile Strength Tensile Elongation	ASTM D-4632	90 lbs 50%	50%
Trapezoidal Tear Mullen Burst	ASTM D-4533 ASTM D-3786	N/A 180 psi	35 lb 180 psi
Asphalt Retention Puncture Strength	TX DOT 3099 ASTM D-4833	0.20 gal/yd² N/A	0.20 gal/yd² 50 lb
UV Stability	ASTM D-4355	70% @ 150 hr	70% @ 500 hr

If you have any questions or need any additional information, please do not hesitate to contact me. Thank you.

Regards,

Greg Osendorf



TerraTex N06

Nonwoven Geotextile

TerraTex N06 is a nonwoven geotextile made up of polypropylene fibers. These fibers are needled to form a stable and durable network such that the fibers retain their relative position. It is non-biodegradable and resistant to most soil chemicals, acids and alkali with a pH range of 3 to 12. TerraTex N06 is manufactured to meet or exceed the following minimum average roll values:

Property	<u>Test Method</u>	Minimum Average Roll Value <u>English</u>	Minimum Average Roll Value <u>Metric</u>
Tensile Strength	ASTM D-4632	160 lb	0.711 kN
Tensile Elongation	ASTM D-4632	>50%	>50%
Seam Strength	ASTM D-4632	140 lb	0.623 kN
Mullen Burst	ASTM D-3786	315 psi	2170 kPa
Puncture Strength	ASTM D-4833	90 lb	0.400 kN
CBR Puncture	ASTM D-6241	450 lb	1.998 kN
Trapezoid Tear	ASTM D-4533	65 lb x 65 lb	0.289 kN
UV Resistance	ASTM D-4355	70% @ 500 hr	70% @ 500 hr
AOS	ASTM D-4751	70 US Sieve	0.212 mm
Permittivity	ASTM D-4491	1.6 sec ⁻¹	1.6 sec ⁻¹
Water Flow Rate	ASTM D-4491	110 gal/min/ft ²	4480 l/min/m²

9/2009

815 Buxton Street Winston Salem, NC 27101 888 - 239 - 4539 • Fax: 336 - 747 - 1652 www.hanesgeo.com www.webtecgeos.com

Rose, Gretchen

From:Hans Schmeusser [hanss@rotschyinc.com]Sent:Tuesday, December 01, 2009 1:34 PMTo:Rose, GretchenSubject:Emailing: T5 geotextile submittal.pdf

Attachments:

T5 geotextile submittal.pdf



T5 geotextile submittal.pdf (2...

The message is ready to be sent with the following file or link attachments:

T5 geotextile submittal.pdf

Note: To protect against computer viruses, e-mail programs may prevent sending or receiving certain types of file attachments. Check your e-mail security settings to determine how attachments are handled.

Submittal 30

SUBMITTAL TRANSMITTAL / SOURCE APPROVAL	
FROM: Rotschy, Inc	DATE:
9210 NE 62nd Ave	1
Vancouver, Washington 98865	

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			FROM: Rolschy, Inc			DATE:	12/08/2009	This 5	This section to
Port of	f Vanco	Port of Vancouver 1150	9210 NE 62nd Ave					pe coi	be completed
			Vancouver, Washington 98865	glon 38865				by COV:	ÿ
TO: CONSTI	CONSTRUCTION MANAGER	ANAGER	PROJECT: Terminal 5 Unit Train Improvements	n improvements		Resubmi	Resubmittal Previous Submittal No.	Submi	Submittal No.
3103 NI	3103 NW Lower River Road	er Road						Ŕ	
Vancou	Vancouver, Washington 98660	ton 98660	This section to be completed by contractor.	actor.				Q	
Bid Item Wombordet	Drawing Short No.			1	Type		Manufacturer /	<u> </u>	
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23, 24, 75, 90		3/4" Levei 3 HMAC Mix Design	Design		0	Porter Yett	Porter Yett & Santosh	P	<u>م</u>
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Contractor she	all submit 6	Contractor shall submit 6 copies of each	* one component per line	** Type Codes: A- Source approval only	proval or	nly E - Cert. of Compliance	ompliance Received:	fved:	
attachment, and shall write bid item	nd shall wri	ite bid item		B - Catalog Cut/Data Sheet	ut/Data S			1 Jal	2
number(s)) on each attached page.	each attac	ched page.		C - Mix Design D - QPL	c.	G - Shop Drawings H - Other	wings	11-1	_
Contractor Set file	s forformoe	plance with Contract Documents.		Legend: Reviow Action			Review		
By William	K			1 No exceptions taken	Z B	1 water button	Date	Initial	Date
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The second		Town King the way led had in the for	n.	Resubmit 4 Reitsded		Reviewed by:	Ţ	ل م	1/1 110
-	-		}	5 Submit WSDOT Pit#		ğ			
						Returned to contractor			
Contractor	Ē	Project File	Project Inspector Ma	Malerials Lab Port of Vancouver	wer	HDR hc			

Updated Jan 2009

BEAVERTON, OREGON 97075 KE & ASSOCIATES, LLC PO BOX 1062

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SUPERPAVE MIX DESIGN

		H胎丸 344" L evel 3	Quanty
		WSDOT	Santosh Quarry
(TUENT: Porter Yeth	PROJECT: Vortous	MTX DESIGNATION: WSDOT HIEA 344" Level 3	SAMPLE SOURCE:

COMPOSITE GRADATION

1.4B NO: DBL - 0911

		CLISIN %		0.3520 %
MATERIAL LD.	Ö	WITHOUT ADMIX	MIX	WITH ADIAX
88 - 0.0	Sand	8		0.77
dr:		1 7		
	iller V	77		0.12
107 - 14	Agg	50		20.0
3/1-1/2	Are.	11		17.0
RAP	488 1	20		20.0
ADMEN		0.0		0.0
TOIM		100		100
	WID ADMIX	XINDAIW	SPEC	
SIEVE / mm	% PASSING	SK PASSING	LIMITS	••••
1.5	100	100		-
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BULK OD SP CR	SP GR		2.659	r -
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11/17/2008	NIA	OR-27	Client
DATE	PROJECT NO.	SOURCE NO.:	SAMPLED BY:

.

% MINERAL ADADX:

3

DESIGN DATA

			DESIGN			
SPECIMEN ID	+	ы		m	4	Project
BITUMEN GRADESP GR	PG 64 - 22	1 0371				Specification
% of Bitumen		5.0		5.5	6.0	
Bulk Donsin: (Deell3)		152.0		153.2	154.1	
96 Air Virith		4.1		2.6	ъ.,	4,0%
\$\$ VNLA		12.9		12.8	12.7	13.0 min.
% Air Voids Filled		68.5		795	6,98	65 - 75
°ú Effective Amhalt Total Mfk	327	3.78	3.7B	4.28	4.73	
N initial 8 Gyration		26.0		88.0	90.0	8 8 V
N design 80 Gynations		95.9		97.4	98.7	
P.075/Pbc		134		1,18	1.08	.8 -1.6
P.075/Pb		£.0;		0.92	0.84	

TENSILE STRENGTH RATIO

SET LD.	DRY	WET	TENSILE RATRO	PERCENT ASPIIALT	PERCENT
NO.1 PSI Specification :	189.41 WSDOT T ₆₈	189.41 168.15 88.8 VSDOT Text Method I 762/I 718	88.8 12/T 718	5.0	0.0

3.0 RECOMMENDED BITUMEN CONTENT (%) =

MEXing Tempature: 307 - 316 F VVSDOT RIMAC 3/4" LEVEL 3

ADDITIONAL DATA

Compaction Tempature: 288 - 295 F NDES 100 Gypafous SIGNED

÷ ŝ 2.540 @ 1.287 MANDAUM THEORDITCAL DENSELY * ASPHALT ABSORPTION ON DRY AGG (%) * ASPHALT TYPE PG 64-22 ASPHALT SOURCE MECAE OF

COMBINED	2.659	2704	273	1.720	
ļ	- 				 4
MATERIAL	BULK OD SP CR	SST) SP GR	APPARENI SP GR	ABSORPTION	

Rose, Gretchen

From: Hans Schmeusser [hanss@rotschyinc.com]

Sent: Wednesday, December 09, 2009 12:02 PM

To: Rose, Gretchen

Subject: FW:

Attachments: WSDOT 19mm VP~Port of V I.JPG; ac mix design submittal cover.pdf

HMAC mix design submittal attached.

Hans Schmeusser

Project Manager



O: 360.334.3128 F: 360. 334.3101 C: 360.608.5056

From: Gregg Walker [mailto:gwalker@vancouverpavingco.com] Sent: Wednesday, December 09, 2009 9:06 AM To: Hans Schmeusser Subject:

Hans, Here is the mix design for the 3/4" HMAC.

Gregg

Submittal 73

SUBMITTAL TRANSMITTAL / SOURCE APPROVAL FROM ROMM IN FOURCE APPROVAL FROM ROMM IN FOURCH CONCOUVER USA ROMM ROMM IN CONSTRUCTION MANGER FOURCH CONVENTION ROMM IN CONSTRUCTION MANGER POLICET: Terminal 5 unit Train improvements Vacuum End Vacuum Vacuum End Vacuum End Vacuum End Vacuum End Vacuum Vacuum End Vacuum Vacuu

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Updated Jan 2009

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9210 NE 62nd Ave Vancouver, WA 98665



P 360.334.3100 F 360.334.3101

SPL (Spent Pot Liner) Area Work Plan

(specific to test pad construction)

Introduction: Rotschy Inc. under contract with the Port of Vancouver (for the Terminal 5 Unit Train Improvement Project) intends to conduct drainage installation, excavation, grading and paving work in the area known as the "SPL Cap". The paving design incorporates a "oil soaked" impermeable geotextile inner -layer. This geotextile and paving form an impermeable "cap". To provide assurance of the quality and impermeability of the said cap; the project specs require a test section be constructed and proven (IE: tested) prior to construction. This submittal addresses just work associated with this test section.

Location of work: The SPL Area exists at 45* 38' 51" Lat and 122* 43' 49" Lon. See attached site map (nearest address is 5701 NW Lower River Rd, Vancouver Wa.) on the former "Alcoa" Site outskirts.

<u>Site Description:</u> 3.8 acre site is flat (or very little gradient) ranging from elevation 29.0 to 32.0 feet above sea level.

Important notes: See attached Health and Safety Plans (HASP), Contaminated Media Plans, Hazardous Materials Management plan, Exposure Monitoring Plan and Quality Assurance plan for all requirements regarding personnel health, safety, decontamination, etc regarding work in contaminated media. This work plan is solely intended to describe the test plot work sequence.

Description and order of work:

Step 1 (general excavation and embankment): Existing sub-soils will be excavated, graded and compacted to design subgrade. "Fill areas" will receive embankment per plan lines and grades. In areas of minimal cover (over existing liner) we would propose the initial soil lift will be 12" thick to insure less ground pressure affect to the liner below.

Step 2 (base rock and geogrid): work shall commence after subgrade is graded, compacted & approved; IE step 1) Work shall be placing Tensar Tri-axial geogrid (in accordance with manufactures recommendations) and crushed surfacing base rock in accordance with specs / standard practice. Occasional Construction Quality Assurance (CQA) engineer oversight (by owner) will be required per the Test Pad Protocol (attached). Compaction testing will be approved in writing prior to step 3 work.

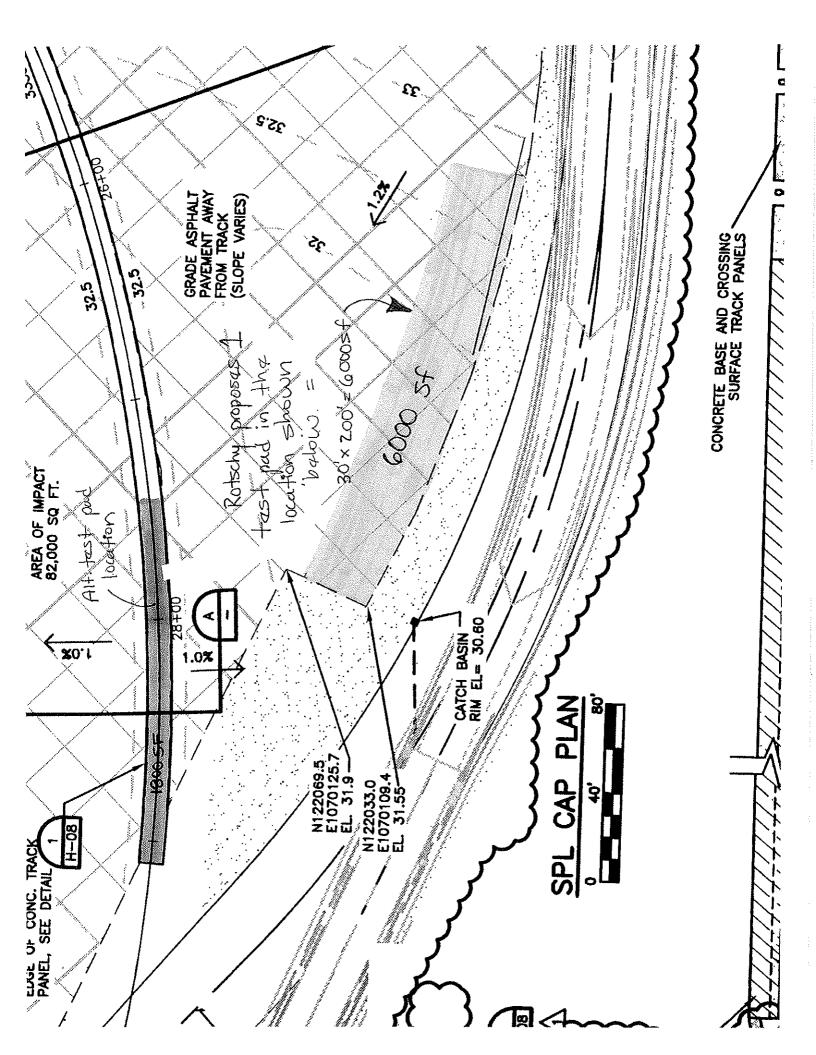
Step 3 (paving test section): Rotschy Inc and subcontractor Vancouver Paving will construct an asphalt cap test section per the requirements of the attached SPL Asphalt Test Pad Protocol. Asphalt mix design has been approved and is attached. <u>Test Pad Size and location will be as shown on exhibit A attached.</u> Conduct preconstruction meeting with engineer, owner, contractors, CQA person and others to review construction means and methods. Place base lift paving with continuous CQA engineer oversight as required per the Test Pad Protocol. After approval of the base lift asphalt, hot oil will be surface applied by subcontractor utilizing a "spray truck" (per spec and at the rate recommended by the fabric manufacture; materials submittal forthcoming later this week) and then subsequently overlain by approved 6oz paving fabric. This fabric will be applied via a "mechanical applicator". We can provide a website for an online demonstration of this process should you be interested. Oil will not be applied over the fabric as approved in RFI #22 response. Top lift paving timing to follow in accordance with the fabric manufactures recommendations.

Step 4 (testing of cap cores): Per the requirements of the SPL Asphalt Cap Test Pad Protocol the CQA engineer will core and test the asphalt cap for impermeability requirements. Failure of the test pad to meet impermeability requirements will result in removal of such and the need to construct a new test pad / retest. Passing tests will allow the test section to remain and be part of the permanent cap.

Step 5 (permanent asphalt cap construction): Only after approval of the impermeability test results, agreement on the proper work sequence plans (to insure a cap like the test pad) including timing, means & methods, etc. will work commence in strict accordance with such agreed plans. At minimum the initial phase will include paving under the tub crossing. At most it would be the entire SPL cap area base lift. Continuous CQA engineer oversight required per Test Pad Protocol will be required. Top lift paving may wait till spring / better weather.

Step 6 (tub crossing placement): Subcontractor Coast Rail or Rotschy Inc will place a 1.5" thick layer of fine aggregate leveling course over the new asphalt cap. Coast Rail will then place the tub crossing directly on the leveling course.

Step 7 (top lift paving): With ambient temperatures in accordance with Washdot spec; Top lift paving will occur in strict accordance with Test Pad Protocol. This will include paving against the new tub crossing. Continuous CQA engineer oversight shall be required per the Test Pad Protocol.





406 N. E 139th STREET Vancouver, WA 98685 (360) 573-7973 (360) 574-1609 Fax

COMPACTION CONTROL PLAN

December 16, 2009

PROJECT: Terminal 5 Unit Train Improvements PROJECT #: CP0144

Equipment used:

2 10 ton steel wheeled vibratory rollers.

5-04.3 (10)a requires a pneumatic roller between October 1 and April 1. We would request release from this requirement as pneumatic rollers tend to pick up on the tires at cooler temperatures. Wind even mild winds aggravate this problem. We feel the vibratory rollers will give compaction without the problems of pneumatic rollers.

Process:

1. A rolling pattern will be established to best achieve compaction during the construction of the SPL cap test strip. Breakdown will be with the 10 ton vibratory roller, and finished with the 10 ton vibratory. The Foreman will work with the roller operators and the Density Technician to determine the method and number of passes required toachieve compaction. Once the compaction pattern is established, the rollers will continue running that pattern unless there is a need for additional compactive effort. Throughout the day, the Foreman and Density Technician will monitor compaction to ensure that the required density is being achieved. Coordinate paving speed to insure that the lay-down rate does not exceed the capabilities of the rolling train. Paving operations will be stopped if the required compaction results are not being achieved.

Detailed daily procedure:

- 1. Project Mgr or Superintendent will lay out the schedule for the day with the Foreman and the Density Technician.
- 2. Foreman, Density Technician and Roller operators will establish rolling patterns and determine the number of passes required at a given temperature to achieve compaction for the specific depth before the mat begins to break over. This would be the maximum compactive effort for the work at that depth. This sequence will be repeated through the entirc rolling train.
- 3. Foreman will be responsible for monitoring compaction throughout the day to insure that compaction is continuing to be achieved. He/she will also monitor temperature and direct the Density Technician monitor the rolling train to insure that the established pattern is followed.
- 4. Both the Foreman and the Density Technician may recommend rolling pattern changes as required by changes in conditions

1. Introduction

The Port of Vancouver, Washington proposes to place an asphalt cap over the SPL Cap (3.8 acres) that contains contaminated soils. The cap will consist of a layer of asphalt overlain by an asphalt-impregnated geotextile (a combination of non-woven polypropylene fabric and asphalt cement tack coat) overlain by a second layer of asphalt. The fabric and tack coat combination will form an asphalt membrane interlayer within the pavement section. Additional asphalt layers will be required for structural design purposes, but are not included in this protocol. The purpose of the test pad is to verify the results, under field conditions, of bench scale testing of the asphalt section.

2. Test Pad Objectives

- 1. To verify that the materials and methods of construction will produce an asphalt liner that meets the target hydraulic conductivity for the project. The target hydraulic conductivity for the test pad section is 1×10^{-7} cm/sec, or less.
- 2. To establish a correlation between the bench scale testing and full-scale testing. If the test pad meets the performance objectives for the cap (as verified by hydraulic conductivity and density tests) and the full-scale liner is constructed to density standards that equal or exceed those used in building the test pad, then assurance is provided that the full-scale liner will also meet hydraulic conductivity performance objectives.

3. Test Pad Protocol

3.1 Definitions

Construction Quality Assurance (CQA) Engineer: The owner's representative responsible for verification of the construction methods and materials to project plans, specifications, and protocols.

Construction Quality Assurance Monitor: The individual responsible for observation and documentation of construction under the supervision of the CQA Engineer.

3.2 Test Pad Dimensions

The test pad shall be constructed to the minimum compaction as determined by the Bench Scale Protocol, References 2 and 3. Details of construction shall be proposed by the Contractor and approved by the CQA Engineer. The configuration of the test pad shall conform to the following criteria:

1. The lane width must be sufficient to allow the specified compaction equipment to operate without overlapping the drum into the ballast and introducing ballast material into the asphalt.

- 2. The lane length must be sufficient to allow the compaction equipment to reach its design operating speed.
- 3. Lanes must be adequately separated to ensure that each lift can be compacted to the desired relative compaction.
- 4. The test pad shall be constructed in two lifts with a minimum compacted thickness of 2.5 inches per lift. An asphalt-impregnated geotextile shall be placed between the asphalt lifts.

3.3 Materials and Construction

All materials and methods used in the construction of the test pad shall conform to the project specifications, the Bench Scale Testing Protocol (HDR, 2009b), and the Bench Scale Test Final Report (HDR, 2009c). The methods, materials and equipment used in successful completion of the test pad shall be used in construction of the Cap. Each lift of each lane shall be compacted using the same equipment, operating speed and number of passes. The lower lift of the test pad shall provide a smooth surface, with consistent texture and free of irregularities. The lift must be constructed and finished to provide continuous intimate contact with the overlying geotextile. Adequate geotextile shall be left exposed along the ends and sides of the pad to allow incorporation of the pad into the final cap, if the cap section meets the hydraulic conductivity specification.

3.4 Test Pad Construction Observation

Full time observation of subgrade preparation is not required. The CQA Monitor shall document and observe proof-rolling and density testing of the subgrade. The CQA monitor shall observe the completed placement of the recycled concrete. Observations shall be documented in daily reports. Full-time observation and documentation of the placement of the asphalt and asphalt impregnated geotextile is required. The number of passes of the compactor over each lane shall be documented. Daily field reports will note observations and any deviations from the plans, specifications, and this protocol.

3.5 Required Tests

The tests listed in Table 1 are required to evaluate the hydraulic conductivity of the test section and its ability to control infiltration. At the owner's request, additional testing may be performed per WSDOT test pad requirements to verify the structural suitability of the section.

Material Tested	Parameter	Frequency	Test method
Subgrade	Placement and compaction	Full coverage	Vísual observation
Subgrade density testing	Placement and compaction	2 per lane	ASTM D2922
Crushed Concrete Base	Placement and compaction	2 per lane	ASTM D2922
Hot Mix Asphalt	Mix Design	1 per mix	Submittal review
Geotextile Interlayer	Strength and retention properties	Bracketed by manufacturer's quality control testing	Verification of manufacturer's QC
Geotextile Interlayer	Retention properties	Full coverage	Observation
Asphalt	Compaction	3 per lane per lift	ASTM D2950
Asphalt and Geotextile Interlay	Hydraulic conductivity	2 representing the range of compaction	Modified ASTM D-5084

Table 1: Required Tests

¹70kPa confining pressure, sides of core treated with silicone vacuum grease or bentonite paste to reduce sidewall leakage.

3.6 Deviations from this Protocol

The CQA Engineer may propose deviations from the protocol, if warranted by the results of the bench scale testing. Deviations proposed by the Contractor to more efficiently utilize available machinery may also be considered, if the machinery will be used in full-scale construction as well. Proposed deviations must be provided to and approved by the Port of Vancouver prior to submittal to the Washington Department of Ecology (WDOE). Once submitted to the WDOE, an approval in writing from the WDOE must be obtained and provided to the Port of Vancouver 5 days before construction of the test pad begins.

4. Documentation and Recommendations

Test pad construction shall be documented in a written report, sealed by the CQA Engineer. The report shall include at a minimum:

- Construction narrative detailing methods, materials and equipment used
- Construction daily reports documenting activities and noting deviations from the project plans,
- Specifications and this protocol
- Test results and a statement that the test pad was constructed in substantial accordance with the project documents.
- Deviations from the project documents shall also be noted in the report.

The report shall be submitted to the Port of Vancouver 5 days prior to construction of the SPL replacement cap.

Submittal 83.2

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Submittal 108

SUBMITTAL TRANSMITTAL / SOURCE APPROVAL

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Updated Jan 2009

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McCall

Oil & Chemical Corporation

PG64-22

Feb 18, 2010

		Specification
Original Properties		
Specific Gravity @ 15.6 C (60 F)	1.0294	
Flashpoint, C	316	230+
Dynamic Shear, G*/sin δ, 64 C, kPa	1.20	1.0+
Rotational Viscosity, 135 C, Pas	0.435	3.00-
RTFO Residue Properties		
Loss on Heat, %	0.020	1.00-
Dynamic Shear, G*/sin δ, 64 C, kPa	3.12	2.20+
PAV Residue Properties		
Dynamic Shear, G*sin δ, 25 C, kPa	4630	5000-
Creep Stiffness, -12 C, Mpa	238	300-
m-value, -12 C	0.312	0.300+

I certify that the asphaltic material identified above complies with current AASHTO M320-05, ASTM D6373, Washington State Department of Transportation specifications, and Oregon Department of Transportation Standard Specifications for Asphalt Materials.

Terri Zahler Lab Manager McCall Oil & Chemical Co.

Rose, Gretchen

From:	Hans Schmeusser [hanss@rotschyinc.com]
Sent:	Tuesday, February 23, 2010 8:44 AM
То:	Rose, Gretchen
Subject:	FW:
Attachments	: 2010 Header PG 64-22.doc; Submittal form 2009.xls

Urgent oil submittal / cert attached. Thanks!

Hans Schmeusser Project Manager



O: 360.334.3128 F: 360. 334.3101 C: 360.608.5056

From: Troy Tindall [mailto:Troy@bluelinetrans.com] Sent: Monday, February 22, 2010 2:09 PM To: hanss@rotschyinc.com Subject: FW:

From: Troy Tindall Sent: Thursday, February 18, 2010 2:00 PM To: 'hanss@rotsbhyinc.com' Subject:

Above it the product sheet and the MSDS is at this website. http://www.mccalloil.com/asphalt.html

Troy Tindall 503-702-1236

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Updated Jan 2009

McCall

Oil & Chemical Corporation

PG64-22

Feb 18, 2010

		Specification
Original Properties		-
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Flashpoint, C	316	230+
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RTFO Residue Properties		
Loss on Heat, %	0.020	1.00-
Dynamic Shear, G*/sin δ, 64 C, kPa	3.12	2.20+
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Dynamic Shear, G*sin δ, 25 C, kPa	4630	5000-
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m-value, -12 C	0.312	0.300+

I certify that the asphaltic material identified above complies with current AASHTO M320-05, ASTM D6373, Washington State Department of Transportation specifications, and Oregon Department of Transportation Standard Specifications for Asphalt Materials.

Terri Zahler Lab Manager McCall Oil & Chemical Co.

5480 NW Front Ave. Portland, Oregon 97210 503-221-6400 Fax: 503-221-6405

Rose, Gretchen

From: Hans Schmeusser [hanss@rotschyinc.com]

Sent: Tuesday, February 23, 2010 8:44 AM

To: Rose, Gretchen

Subject: FW:

Attachments: 2010 Header PG 64-22.doc; Submittal form 2009.xls

Urgent oil submittal / cert attached. Thanks!

Hans Schmeusser

Project Manager



O: 360.334.3128 F: 360. 334.3101 C: 360.608.5056

From: Troy Tindall [mailto:Troy@bluelinetrans.com] Sent: Monday, February 22, 2010 2:09 PM To: hanss@rotschyinc.com Subject: FW:

From: Troy Tindall Sent: Thursday, February 18, 2010 2:00 PM To: 'hanss@rotsbhyinc.com' Subject:

Above it the product sheet and the MSDS is at this website. http://www.mccalloil.com/asphalt.html

Troy Tindall 503-702-1236 Submittal 118

Port of Vancouver Lower River Road 3103 NW Lower River Road Vancouver, Washington 98660 Bid Item Drawing SPL Dwugs SPL Specification 0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,		SUBMITTAL TRANSMITTAL / SOURCE APPROVAL	Port of Vancouver USA 22010 Noteshy inc Vancouver, Washington 98665	PROJECT: Terminal 5 Unit Train Improvements CP0144 Submittal No.	I rus section to be completed by contractor.	Type** Manufacturer / Review Sheet No. Specification Description - Manufacturer's Specific Product* Code Local Supplier Brand / WSDOT Pit # Action Notes		SPL Dwgs SPL Specs Hot oil application data sheet He Blueline McCall												Contractor shall submit 6 copies of each * one component per line ** Type Codes: A - Source approval only E - Cert of Compliance Received:	B - Catalog Cut/Data Sheet F - Sample	each auacheu page. C - Mix Design G - Shop Drawings 3/9/2010 D - QPL H - Other		By: Hans Schmeusser & Eric w / Blueline 7arget 1 No exceptions taken Distribution Date Initial Date	Iments: 2 Note markings Reviewed by: HTXC	Iched- Reviewed by: }	Reviewed by:	5 Submit WSDOT Pit # COV, Construction	
---	--	---	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	---------------------------------------	---	--	---	---	-----------------------	--------------	--	--

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Updated Jan 2009

Rotschy Inc. DATE <u>3/4/10</u> DESTINATION <u>Vancouver</u>, Wa, <u>7</u> SNIVEY <u>2</u> PRODUCT <u>AC764-22</u> JOB DISC. <u>Defro</u> Mat <u>611</u> GAL SHOT <u>125</u> AVG SHOT <u>205</u> TONS/HR CUSTOMER PRESSURE YDS SHOT FLOAT GALLONS GALS WIDTH LENGTH SQ. YDS. DES STREET OR ROAD ACT 2,400 USED SHOT SHOT 2275 125 13 423 611 .205.20 Test Short Upon Redurn Torage shot come Dut to .41. In this situation the "Float gallons" ¿ Challons Used," is the most accurate number. 20 gallons residuk asphalt would make tonage Innacurate & is probable. I shot .49 tows. .49 tons @ 253 gallons per ton @ 340°F = 12397 gallons 124-611 = 203 gallons for sq/yd

Rose, Gretchen

From:	Hans Schmeusser [hanss@rotschyinc.com]
Sent:	Tuesday, March 09, 2010 12:53 PM
To:	Rose, Gretchen
Cc:	Lee, Steve; samuel.albino@hdrinc.com; Kelsey, Mike; Burggraff, Joe
Subject:	FW: Shot Sheet
Attachments	: Shot Sheet.PDF; Submittal form 2009.xls

Gretchen,

Blueline oil amounts used on the test strip attached for your records. Looks like the quantity / application rate was per spec. Thanks!

Hans Schmeusser

Project Manager



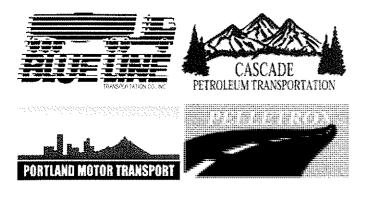
O: 360.334.3128 F: 360. 334.3101 C: 360.608.5056

From: Ross Imes [mailto:ROSS@bluelinetrans.com] Sent: Tuesday, March 09, 2010 12:18 PM To: hanss@rotschyinc.com Subject: Shot Sheet

Hi Hans,

Here is the shot sheet from Eric.

Ross B. Imes 503-279-2627

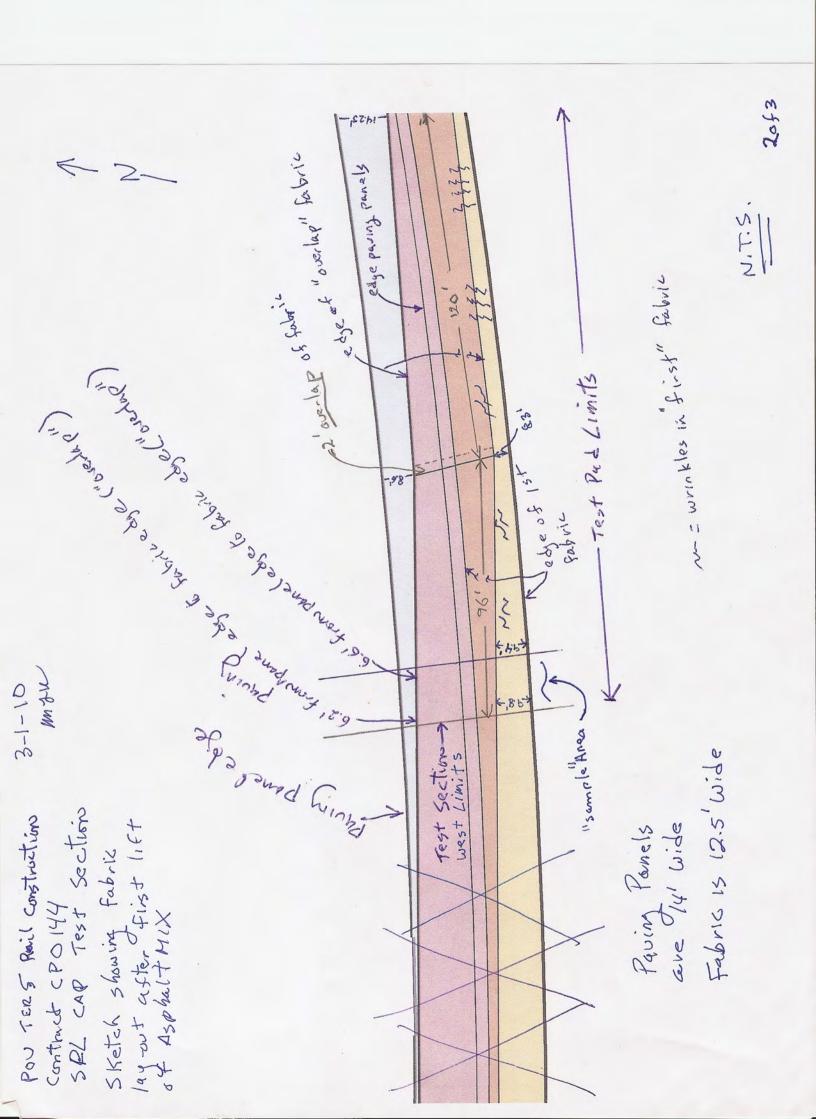


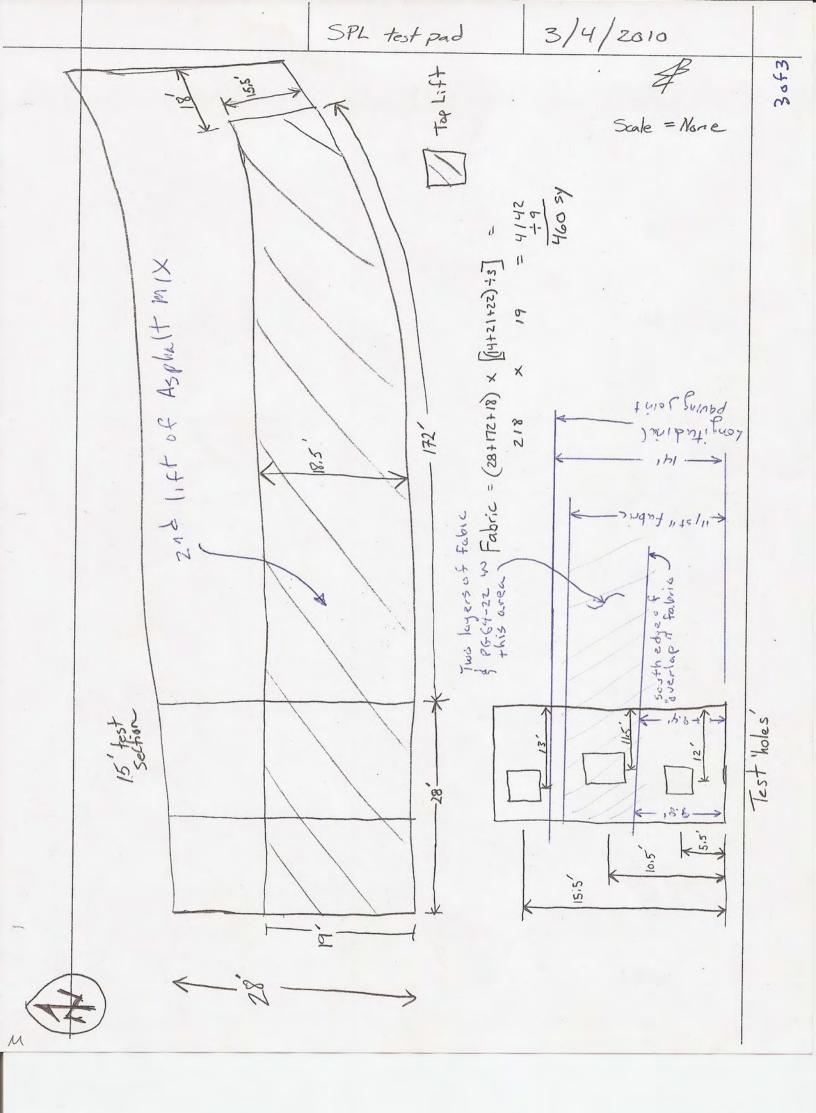
ATTACHMENT D

City of Vancouver Subgrade Density Test



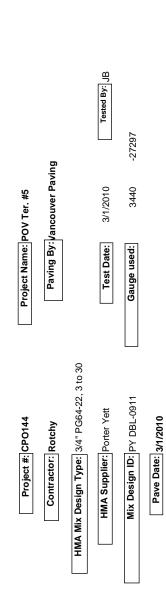
No.	Standard	Density	Pooding					Date 3/1	/2010			uge OV 3440):	
	Standard Read		Reading	Correcte	ed	Proje				ant a	-	Cont. N		
1.	145.6	inge	145.6			POV Pad	Ter 5 R	ail Cons	truction:	SPL Cap	Test	SR No		
2.	144.7		144.7			Project	ct Engine	or						
3.	144.7		144.7			Steve	-	er						
	435.4					Weat				Air Temp				
Cum			02.20	(1)		HMA	/ Cloudy		Other	From:	3 -1	/- To Thicknes		5+/-
Avg.	145.1		93.3%	° U			PG64-2	2	PY 11-1	7-09		2.5"	55	
Remark						Wear	ing		Leveling first lift			Class 3.0 to 3	60	
	tatic pass; "v d & back acr					Left		Right Nort	h Panel		3 [SB [EB	
of mat;	;					Other SPL	Test Pad							
("s/v"	' = forward w	/static &	back w/ v	vibe)	-			, Type, a	Ind Mass					
						-	HyVac C							
Rice 15	55.5**	_Std. Den	. % of Ric	e <u>92</u>		-	Pneumati	and the second						
Stand. I	Density - Initia I <u>K / JB</u> ("Test So Sta.	I Pt. **A	Actual Ric	e for the c	lay	-	Volvo DI							_
2	roller pattern	patte Non t	rn esi Re sou	tablish ,th Pa	ed ow inel al	the	Norted 91	h pa. 1.8%	w/ on	An in e less	time	l nol Icdown	ler NVie	be f
		1-s/v	1-s/v	1-s/v	2	2	2	3-s	3-s	15' +	15'	-	T	
Roller	e Reading		140.1	142.3				144.6	145.6	144.7	145	.1		
Roller									1					
Gaug	(min. After		23	20				55	63					
Gaug Time Pavt	(min. After Laydown		23	29	202			55	63					
Gaug Time Pavt Temp	(min. After Laydown).	1	224	209	203	5	6	55 170 7	166		10	1	1	12
Gaug Time Pavt Temp	(min. After Laydown	1			203 4	5	6			9	10	11	1	12
Gaug Time Pavt Temp	(min. After Laydown).	1	224	209		5	6	170 7	166	9	10	11	1	12
Gaug Time Pavt Temp	(min. After Laydown).		224	209		5	6	170 7	166	9	10		1	12
Gaug Time Pavt Temp Roller	(min. After Laydown).		224	209		5	6	170 7	166	9	10	11	1	12
Gaug Time Pavt Temp Roller	(min. After Laydown).		224	209		5	6	170 7	166	9	10	11	1	
Gaug Time Pavt Temp Roller	(min. After Laydown).		224	209		5	6	170 7	166	9	10		1	
Gaug Time Pavt Temp Roller	(min. After Laydown).		224	209		5	6	170 7	166	9	10		1	
Gaug Time Pavt Temp Roller	(min. After Laydown).		224	209		5	6	170 7	166	9	10		1	
Gaug Time Pavt Temp Roller	(min. After Laydown).		224	209		5	6	170 7	166	9	10		1	





ATTACHMENT E

City of Vancouver HMA Compaction Testing



	Location & Comments		26+98, -152'	27+10, -136'	27+57, -112'	27+78, -90'	27+97, -77'		
-	Percent	Comp.	92.8	93.2	93.3	94.7	95.0	93.3	
	Rice	Density	155.5	155.5	155.5	155.5	155.5	155.5	
Test	Depth	(feet)	BS	BS	BS	BS	BS	BS	
Ave	Density	Reading	144.3	144.9	145.1	147.2	147.8	145.1	
Density	Reading	#3							
Density	Reading	#2							
Density	Reading	#1	144.3	144.9	145.1	147.2	147.8	145.1	
	Test	Number	-	2	e	4	5	9	

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AVE= 93.7

Comments SPL Cap Test Section second lift Test results. First lift tested by roller pattern establishment approx. pavement surface temp = 238. Trucks on site for second lift at 3:30pm, finish rolling at 4:40pm

ATTACHMENT F

Photographic Documentation

SPL Test Pad Construction Photograph Log



Photo 1 SPL Test Pad Triaxial Geogrid Installation 2/23/201



Photo 2 SPL Test Pad Triaxial Geogrid and Subgrade Installation 2/23/2010



Photo 3 SPL Test Pad Subgrade Placement and Compaction 3/05/2010



Photo 4 SPL Test Pad Subgrade Preparation 3/05/2010



Photo 5 SPL Test Pad HMA Base Layer 2 1/2" Placement and Compaction 3/05/2010



Photo 6 SPL Test Pad HMA Base Layer 2 1/2" Placement and Compaction 3/05/2010



Photo 7 SPL Test Pad Geotextile Roll Placement Equipment 3/05/2010



Photo 8 SPL Test Pad Tack Coat Application 3/05/2010



Photo 9 SPL Test Pad Tack Coat Application 3/05/2010



Photo 10 SPL Test Pad Geotextile Inerlayer Application 3/05/2010



Photo 11 SPL Test Pad Geotextile Inerlayer Application 3/05/2010



Photo 12 SPL Test Pad Geotextile Inerlayer Application 3/05/2010



Photo 13 SPL Test Pad Geotextile Inerlayer Application 3/05/2010



Photo 14 SPL Test Pad Geotextile Interlayer Application 3/05/2010



Photo 15 SPL Test Pad Geotextile Interlayer between HMA Base Layer and Top Layer 3/05/2010



Photo 16 SPL Test Pad HMA Top Layer Application



Photo 17 SPL Test Pad HMA Top Layer Application



Photo 18 SPL Test Pad Hydraulic Conductivity Sample Locations 3/17/2010



Photo 19 SPL Test Pad Density Test Boring Locations 3/17/2010

ATTACHMENT G

TRI Environmental SPL Hydraulic Conductivity Test

March 11, 2010

Mail To:

Bill To:

<= Same

Dave Wineman HDR 184 Creekside Park, Suite 100 Spring Branch, Texas 78070

email: david.wineman@hdrinc.com

Dear Mr. Wineman:

Thank you for consulting TRI/Environmental, Inc. (TRI) for your geosynthetics testing needs. TRI is pleased to submit this final report for laboratory testing.

Project:	Port of Vancouver, Test Pad
TRI Job Reference Number:	E2337-22-03
Material(s) Tested:	3 Aggragate and Asphalt Blocks
Test(s) Requested:	Hydraulic Conductivity (ASTM D 5084)

If you have any questions or require any additional information, please call us at 1-800-880-8378.

Sincerely,

h Malla

John M. Allen, P.E. Division Director Geosynthetic Services Division www.GeosyntheticTesting.com



GCL TEST RESULTS

TRI Client: HDR

Project: Port of Vancouver, Test Pad

Material: Aggragate and Asphalt Block Sample Identification: 1 TRI Log #: E2337-22-03

PARAMETER	-	TEST RE	PLICAT	E NUMB	ER							MEAN
Hydraulic Conductivity (ASTM D 50	1 184, 70 kF	2 Pa)	3	4	5	6	7	8	9	10	
Hydraulic Conductivity (cm.	/sec)	1.5E-08										1.5E-08
MD Machine Direction	TD Trar	nsverse Dir	ection		NA	Not Availa	able					1

The testing is based upon accepted industry practice as well as the test method listed. Test results reported herein do not apply to samples other than those tested. TRI neither accepts responsibility for nor makes claim as to the final use and purpose of the material. TRI observes and maintains client confidentiality. TRI limits reproduction of this report, except in full, without prior approval of TRI.



GCL TEST RESULTS

TRI Client: HDR

Project: Port of Vancouver, Test Pad

Material: Aggragate and Asphalt Block Sample Identification: 2 TRI Log #: E2337-22-03

PARAMETER		TEST RE	PLICAT	E NUMB	ER							MEAN
Hydraulic Conductivity (A	STM D 50	1)84, 70 kF	2 Pa)	3	4	5	6	7	8	9	10	
Hydraulic Conductivity (cm/s	sec)	1.1E-08										1.1E-08
MD Machine Direction	TD Tra	nsverse Dir	ection		NA	Not Availa	ible					I

The testing is based upon accepted industry practice as well as the test method listed. Test results reported herein do not apply to samples other than those tested. TRI neither accepts responsibility for nor makes claim as to the final use and purpose of the material. TRI observes and maintains client confidentiality. TRI limits reproduction of this report, except in full, without prior approval of TRI.



GCL TEST RESULTS

TRI Client: HDR

Project: Port of Vancouver, Test Pad

Material: Aggragate and Asphalt Block Sample Identification: 3 TRI Log #: E2337-22-03

PARAMETER		TEST REI	LICAT	E NUME	ER							MEAN
Hydraulic Conductivity (ASI	MD:	1 5084)	2	3	4	5	6	7	8	9	10	
Hydraulic Conductivity (cm/sec	c)	1.1E-08										1.1E-08
MD Machine Direction	TD T	ransverse Dire	oction			Not Availa	ble			······		

The testing is based upon accepted industry practice as well as the test method listed. Test results reported herein do not apply to samples other than those tested. TRI neither accepts responsibility for nor makes claim as to the final use and purpose of the material. TRI observes and maintains client confidentiality. TRI limits reproduction of this report, except in full, without prior approval of TRI.

ATTACHMENT H

City of Vancouver SPL HMA Density Testing

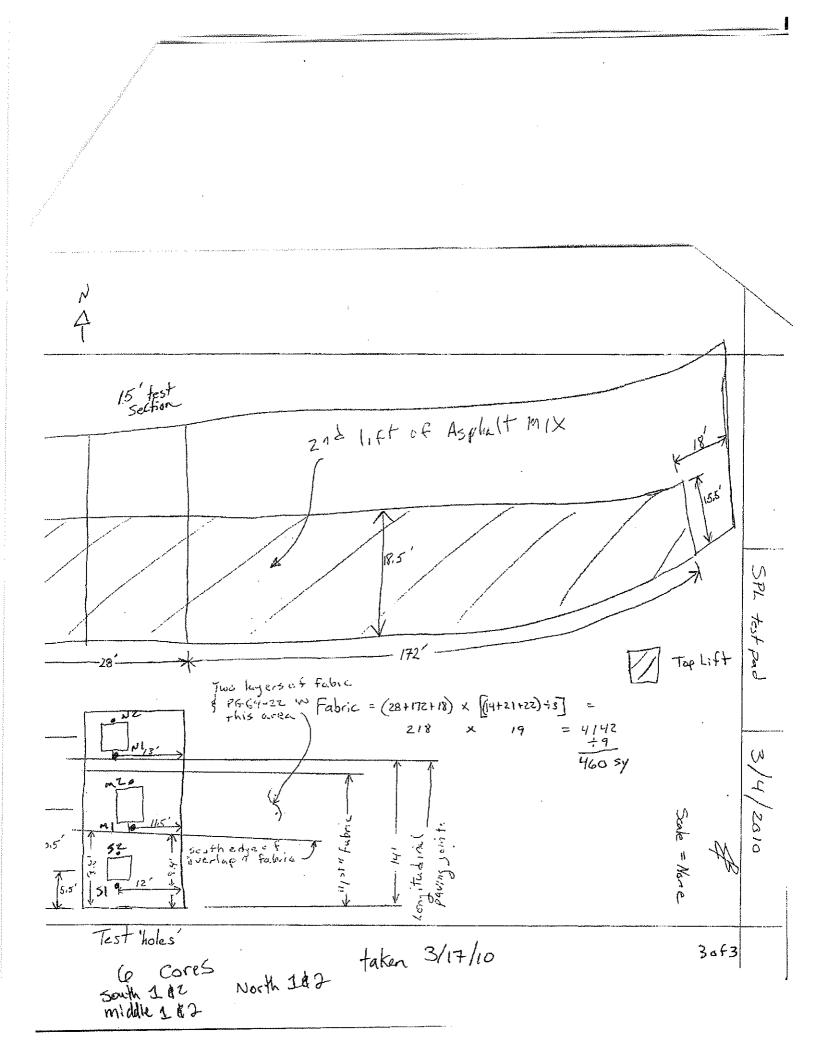
THE CITY OF VANCOUVER CONSTRUCTION DIVISION: MATERIALS LABORATORY REPORT

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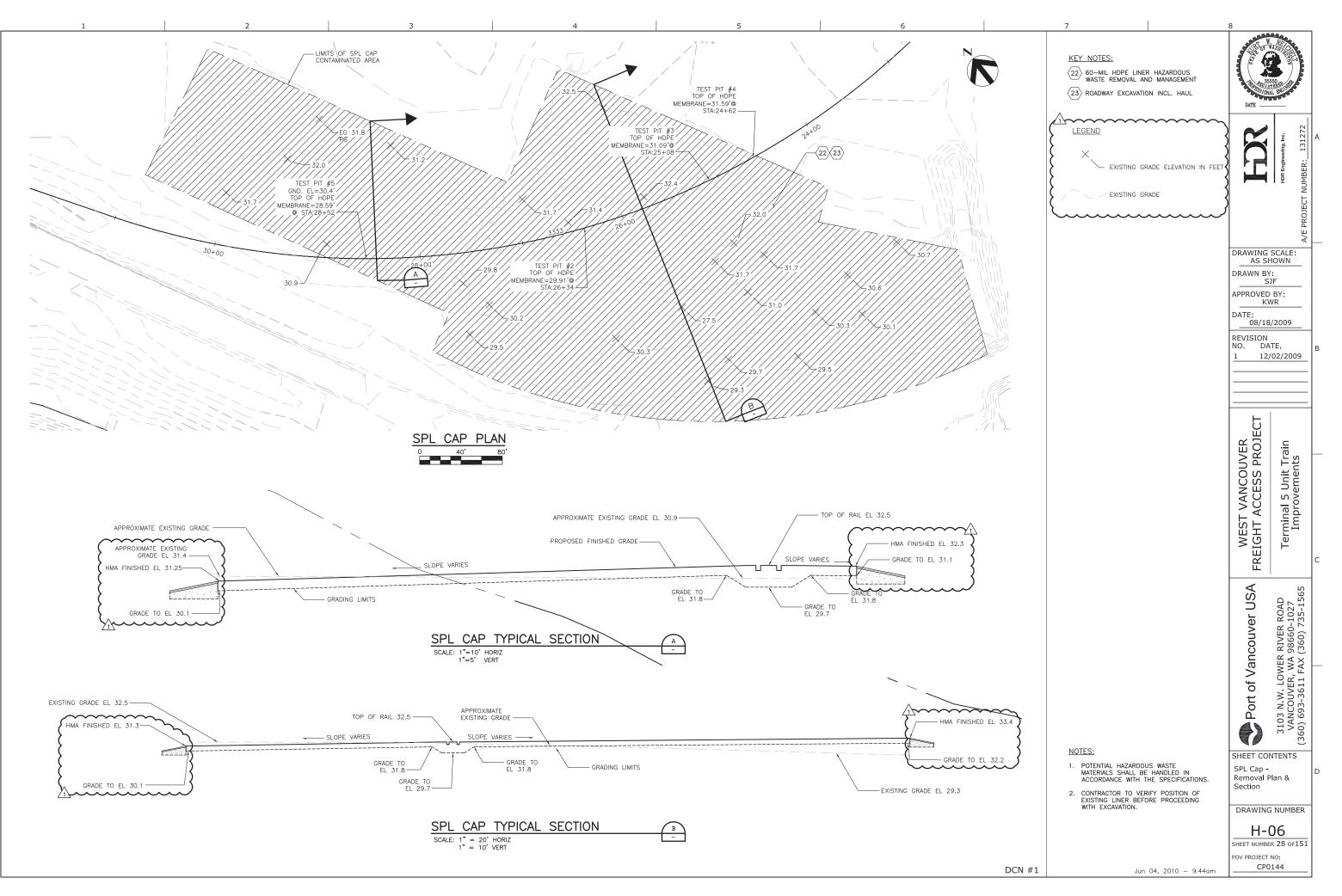
	PROJECT #: CONTRACTOR: F	CP0144 Rotschy	DESCRIP	TION:	DESCRIPTION: POV T-5				MIX CLASS	MIX CLASS 3 to 30 PG64-22
	Arrest (3/17/2010 Vancouver Paving	S	RED BY:	CORED BY: Mayes Testing		TESTING DATE(S):	TE(S):	3/25/2010	3/25/2010 3/26/2010
		Porter Yett DBL-0911	DRYING 1	EMP:	DRYING TEMP: 125F - over night plus	er night	sniq			
CORE ID STREET	STATION	OFFSET	THKNESS WT. IN	WT.IN	S.S.D.	TARE	GROSS	NET	CORE	Percent
				H20	WT	۲۲ ۲	DRY WT	DRY WT	DENSITY Comp.	Comp.
N1T SPL Cap Test Pad	Location Sketch	i attached	0.175	530.1	905.5	0.0	904.6	904.6	149.98	96.4
~			0.215	608.1	1056.4	0.0	1055.0	1055.0	146.47	
			0.195	571.6	992.3	0.0	990.2	990.2	146.49	94.2
~			0.185	499.2	877.8	0.0	872.5	872.5	143.43	
			0.180	526.5	902.3	0.0	900.9	900.9	149.21	-
m ı			0.230	642.6	1121.6	0.0	1119.2	1119.2	145.43	-
			0.190	567.0	971.9	0.0	970.8	970.8	149.23	
n			0.230	681.3	1170.2	0.0	1168.2	1168.2	148.72	
			0.210	614.6	1065.2	0.0	1059.5	1059.5	146.35	•
			0.230	694.4	1202.2	0.0	1200.5	1200.5	147.14	•
			0.200	571.7	992.8	0.0	987.6	987.6	145.97	
~~			0.220	669.8	1158.8	00	1157 7	1157 7	147 35	-

ASPHALT CORES

3/26/2010



APPENDIX C As-Built Drawings



aggone C:\pwworking\sea\d0254446\P3-98532_H-06.dw

