

## **TECHNICAL MEMORANDUM**

DATE May 24, 2018

Project No. 152030401.001

TO Travis Bennett Holcim (US) Inc.

FROM Joseph Xi, Gary Zimmerman (Golder)

EMAIL jxi@golder.com

## **RE: INTERCEPTOR TRENCH INVESTIGATION SUMMARY AND RECOMMENDATIONS**

## 1.0 BACKGROUND

The location of the Ravensdale site is shown in Figure 1. In 2016 and 2017, subsurface investigations were conducted to determine the geologic materials and groundwater conditions along the proposed alignment of the interceptor trench extension. In portions of the Ravensdale site, perched groundwater flows within overburden soils along the top of bedrock. Investigations were completed in October 2016 and in December 2017, which consisted of drilling 16 boreholes between 10 to 30 feet in depth to determine the depth to bedrock and detect the presence of perched groundwater. Piezometers were installed in five of the boreholes in December 2017 to allow water level measurements and thereby determine the perched groundwater gradient and flow direction in the general area of the proposed alignment of the interceptor trench extension. Information collected from the October 2016 and December 2017 borehole drilling, piezometer installation, and subsequent water level measurements were used to evaluate a potential extension to the interceptor trench.

## 2.0 SUMMARY OF INVESTIGATIONS

## 2.1 October 2016 Investigation

Prior to conducting the 2016 investigation, the proposed alignment for the interceptor trench extension was to the north along the access road that borders the east side of the Lower Disposal Area (LDA). A limited test pit program in 2010 (Golder 2013<sup>1</sup>) had indicated bedrock or fill near the ground surface along this alignment. A work plan (Golder 2016<sup>2</sup>) was prepared describing the scope of the interceptor trench extension predesign investigation.

Drilling was performed by Cascade Drilling, L.P. (Cascade) using a model 100C track-mounted sonic drill rig. A total of 9 boreholes were drilled on October 25 and 26, 2016. The locations of the boreholes are shown on Figure 2.

Drilling began with borehole B-12 and proceeded north along the access road to boreholes B-13 through B-17 in numerical sequence. Because cement kiln dust (CKD) was unexpectedly encountered in several of these boreholes, additional boreholes B-19, B-19A, and B-20 were drilled in an attempt to delineate the eastern lateral

<sup>&</sup>lt;sup>1</sup> Golder Associates Inc. (Golder). 2013. Lower Disposal Area Hydrogeological Investigations Report, Ravensdale Site, Ravensdale, Washington. June 11.

<sup>&</sup>lt;sup>2</sup> Golder Associates Inc. (Golder). 2016. Interceptor Trench Extension Predesign Investigation Field Work Plan, Ravensdale Site, Ravensdale, Washington. October 12.

extent of the CKD. B-16 and B-17 were drilled to depths of 30 feet below ground surface (bgs) in an attempt to reach bedrock.

Fill overlying CKD was encountered in all boreholes except B-17, where no CKD was present, and B-16, where zones of CKD were interspersed with fill. Fill was encountered from the ground surface to depths of between 2 and 23 feet bgs, increasing in thickness to the north. The fill consisted predominantly of silty sand mine spoils, with clayey material and coal fragments, but also included debris. Underlying the fill, CKD was encountered to the depths explored, except in B-17, where material that was interpreted to be highly weathered siltstone/sandstone bedrock was encountered from 25 feet to the end of the hole at 30 feet bgs, and in B-16, where fill material was encountered beneath the CKD from a depth of 25 feet to the bottom of the borehole at 30 feet.

Boreholes B-19, B-19A, and B-20 were drilled as close as practicable to the toe of the slope east of the access road, which forms the hill upon which the Bonneville Power Administration (BPA) transmission line towers are founded. B-19A and B-20 were drilled at angles of 30 degrees and 10 degrees, respectively, to extend under the slope to determine if the CKD was present below the hill. In each of these borings, CKD was encountered below fill to the total depths of the boreholes.

Groundwater was encountered in all of the boreholes except B-13 and B-17. The depth to groundwater ranged from 8 to 18 feet bgs, but the water levels measured within short time periods after drilling do not necessarily represent the static water levels. Boreholes B-15, B-16, and B-19 were backfilled with sand and the upper 5 feet was plugged with bentonite chips, so that they could be easily re-drilled for piezometer installation in the future. All other 2016 boreholes were backfilled completely with bentonite chips in accordance with Washington State requirements. Groundwater was not encountered in boreholes installed north of borehole B-16, namely borehole B-17 and two previously installed boreholes B-9 and B-2 (Golder 2013). This indicates that any interceptor trench extension will not be required further north than B-16, as there is insufficient water to be intercepted.

The borehole information for both the 2016 and 2017 investigations are summarized in Table 1. Borehole logs are presented in Attachment A. A cross-section schematic of the 2016 investigation is shown in Figure 3A.

Results of this 2016 phase of the interceptor trench borehole investigation were summarized in the work plan (Golder 2017<sup>3</sup>) that presented the next phase of the investigation. A copy of this work plan is included with this letter as Attachment B.

## 2.2 December 2017 Investigation

Following the results from the 2016 investigation the proposed 2017 extension of the interceptor trench was moved further to the east, further uphill along the existing access road. Additional borings were located along this new proposed alignment to evaluate the extent of the CKD intercepted during the October 2016 borehole drilling, and to determine the geologic materials and presence of perched groundwater.

Drilling was performed by Cascade using a Terrasonic model 150 track-mounted sonic drill rig. A total of seven boreholes were drilled on December 11 and 12, 2017. The locations of the boreholes are shown on Figure 2. Three of these boreholes (B-21, B-24, and B-27) were converted to permanent piezometers on December 12 and 13, 2017. Two of the nine previously drilled boreholes from 2016 (B-12 and B-15) were also converted to

<sup>&</sup>lt;sup>3</sup> Golder Associates Inc. (Golder). 2017. Lower Disposal Area Interceptor Trench Borehole Investigation Work Plan, Ravensdale Site, Ravensdale, Washington. September 18.



## Travis Bennett Holcim (US) Inc.

piezometers on December 13, 2017. All boreholes drilled in 2017 that were not converted to piezometers were backfilled with hydrated bentonite chips on December 13, 2017 in accordance with Washington State requirements.

Drilling for the 2017 investigation began with borehole B-21 and proceeded north along the access road to borehole B-26 in numerical sequence. Boring B-27 was subsequently drilled to fill a data gap between B-22 and B-23. Fill material was encountered from the ground surface to depths of between 7.5 and 17 feet bgs during the drilling. The fill consisted predominantly of silty sand mine spoils, with clayey material and coal fragments. No CKD was encountered in any of the seven boreholes.

Groundwater was encountered in all of the boreholes except B-22, and only minimally in boreholes B-25 and B-26. Wet soil cuttings in borehole B-22 were observed at around 11 feet bgs. Moist to wet soil was observed at around 7 feet bgs in B-25, and 3 feet bgs in B-26. Soil cores collected below these depths in B-25 and B-26 were dry, and did not indicate that perched groundwater was present at the top of the bedrock surface. Water was measured at approximately 24 feet bgs (1 foot of water in borehole) in B-25 at time of drilling, and at approximately 22 feet bgs (3 feet of water in borehole) in B-26 at time of drilling. The water measured in these boreholes was deeper than the top of the bedrock, and is interpreted to be water that entered from shallower depths. The water detected in these boreholes was likely caused by near-surface flow entering the boreholes during drilling rather than inflow of perched water on top of the bedrock. These observations indicate that perched groundwater may not be present in significant volumes north of borehole B-24, and extending the interceptor trench beyond this location may not be useful.

The depth to groundwater encountered during drilling ranged from 10 to 24 feet bgs, and five piezometers were installed at boreholes B-12, B-15, B-21, B-24, and B-27 in order to provide information on groundwater elevations. Boreholes B-12 and B-15 were previously drilled in October 2016 and converted to piezometers in December 2017. Piezometers were constructed of 2-inch Schedule 40 PVC pipe with at least 5 feet of 0.010-inch slotted screen. Each piezometer annulus was backfilled with 10/20 silica sand to approximately 2 feet above the slotted screen, and sealed from there to the ground surface with a hydrated bentonite seal. Finally, the piezometers were completed with flush-mounted steel monuments. The locations and elevations of the piezometers were surveyed by Encompass Engineering & Surveying on February 7, 2018, so that groundwater elevations could be accurately determined.

The 2017 borehole information is summarized in Table 1. Borehole logs are presented in Attachment A. A cross-section of the borehole profile for the December 2017 investigation is provided in Figure 3B.

## 3.0 GROUNDWATER GRADIENTS

Groundwater elevations were measured beginning in December 2017 from the piezometers installed during the December 2017 investigation and from a number of previously installed piezometers across the site. Groundwater elevations are presented in Table 2. This information was used to develop groundwater potentiometric maps, as shown in Figures 4A to 4F representing measurements taken at monthly intervals. Groundwater flow in a perched aquifer is dependent on numerous conditions, including the topography of the underlying bedrock, volumes of recent precipitation, and infiltration within various areas of the site. Groundwater gradients shown are based on groundwater elevation measurements at a given point in time, and do not necessarily represent the predominant groundwater flow across the entire site.

The information indicates that during the period of December 2017 to April 2018, static water level depths ranged from approximately 4 to 18 feet bos (corresponding to elevations of approximately 780 to 800 feet above mean sea level) in the area of the proposed interceptor trench extension. The potentiometric maps show that the groundwater gradient is steep with a generally east northeast to west southwest direction in the immediate area of the proposed interceptor trench. This investigation indicates that an interceptor trench installed along the proposed alignment (as shown in Figure 2) would likely intercept and divert additional perched groundwater away from the LDA.

### 4.0 CONCLUSIONS

Based on the results of the investigations completed to date, extending the groundwater interceptor trench will potentially allow further interception and diversion of shallow groundwater before it enters the LDA, thereby reducing seepage from the LDA. The December 2017 investigation confirmed that CKD is not present along the revised alignment.

Groundwater elevations obtained from December 2017 to April 2018 indicate groundwater levels range from approximately 4 to 18 feet bgs in the areas of investigation, and locally the gradient is towards the west indicating potential flow into the LDA. Top of bedrock is intercepted at depths of approximately 10 to 25 feet bgs in this area. This information supports potentially extending the interceptor trench along the proposed alignment as shown on Figure 2.

However, before a final proposal can be made on installation of the interceptor trench extension, some additional data and evaluation are needed. Although the pH measured in the piezometers located along the proposed alignment is near neutral, water samples should be collected and analyzed from the piezometers to verify that water is this area is not impacted. Water level measurements and evaluation of gradients should continue into the drier seasons to evaluate seasonal changes. Following additional studies, if the conclusion is made that installation of an interceptor trench extension will effectively reduce the volume of water entering into the LDA, an engineering design report describing the proposed interceptor trench construction will be prepared and submitted for approval.

Joseph Xi, PE Project Engineer

List of Attachments:

Tables	
Table 1	Borehole Summary
Table 2	Groundwater Elevations

Figures	
Figure 1	Vicinity Map
Figure 2	Investigation Site Plan (October 2016 and December 2017)
Figure 3A	Borehole Profile (October 2016)
Figure 3B	Borehole Profile (December 2017)
Figure 4A	Groundwater Potentiometric Map (December 19, 2017)

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Principal

Figure 4B	Groundwater Potentiometric Map (January 25, 2018)
Figure 4C	Groundwater Potentiometric Map (February 6, 2018)
Figure 4D	Groundwater Potentiometric Map (March 6, 2018)
Figure 4E	Groundwater Potentiometric Map (March 27, 2018)
Figure 4F	Groundwater Potentiometric Map (April 4, 2018)

## Attachments

Attachment A	Boring Logs
Attachment B	2017 Work Plan

## JX/GLZ/sb

1520304-tm-rev0-final\_interceptor trench field investigation-052418.docx

Tables

## Table 1: Borehole Summary

Date of Borehole Installation	Borehole ID	Borehole Depth (ft)	Fill Depth (ft bgs)	CKD Depth (ft bgs)	Bedrock (?) Depth (ft bgs)	Depth to Water at Time of Drilling (ft bgs)	Converted to Piezometer?
10/25/2016	B-12	20	0-4.5	4.5-20	-	18	Yes
10/25/2016	B-13	20	0-3	3-20	-	-	No
10/25/2016	B-14	20	0-5, 8.5-11	5-8.5, 11-20	-	15	No
10/25/2016	B-15	15	0-14.5	14.5-15	-	8	Yes
10/26/2016	B-16	30	0-19, 20-22, 25-30	19-20, 22-25	-	Wet soil below 16	No
10/26/2016	B-17	30	0-25	-	25-30	-	No
10/26/2016	B-19	20	0-2	2-20	-	17	No
10/26/2016	B-19A (borehole angled 30 degrees from vertical toward the East)	10	0-2	2-10	-	Cannot determine (water from ditch water flowing into hole)	No
10/26/2016	B-20 (borehole angled 10 degrees from vertical toward the East)	20	0-12	12-20	-	Water present, but unable to measure depth due to angle of hole	No
12/11/2017	B-21	20	0-8	-	13-20	11	Yes
12/12/2017	B-22	20	0-11	-	11-20	Wet soil below 11	No
12/11/2017	B-23	25	0-11.5	-	-	19	No
12/11/2017	B-24	20	0-10	-	15	10	Yes
12/11/2017	B-25	25	0-7.5	-	18	24	No
12/12/2017	B-26	25	0-5	-	8	22	No
12/12/2017	B-27	25	0-17	-	22	14	Yes

Note: " - " Not Encountered



## Table 2: Groundwater Elevations

Well ID	TOC ELEV <sup>1</sup>	Date Measured	Depth to Water (feet below TOC)	Groundwater Elevation
		12/19/2017	23.44	730.46
<b>D</b> 4	750.00	1/25/2018	22.39	731.51
P1	753.90	2/6/2018	22.11	731.79
		4/4/2018	21.72	732.18
		12/19/2017	40.82	740.05
		1/25/2018	36.71	744.16
P3	780.87			
		2/6/2018	35.35	745.52
		4/4/2018	40.06	740.81
		12/19/2017	6.81	728.00
P4B	734.81	1/25/2018	17.07	717.74
		2/6/2018	16.96	717.85
		4/4/2018	17.38	717.43
		12/19/2017	29.88	739.82
P5	769.70	1/25/2018	27.02	742.68
10	100110	2/6/2018	25.91	743.79
		4/4/2018	28.61	741.09
		12/19/2017	7.00	735.18
P9	742.18	1/25/2018	5.57	736.61
		2/6/2018	5.09	737.09
		4/4/2018	5.61	736.57
		12/19/2017	14.21	720.88
P11	735.09	1/25/2018	13.22	721.87
		2/6/2018	12.69	722.40
		4/4/2018 12/19/2017	13.18 5.80	721.91 751.27
		1/25/2017		753.03
P12	757.07	2/6/2018	4.04 3.70	753.37
		4/4/2018	5.11	751.96
		12/19/2017	6.16	798.47
		1/25/2018	2.13	802.50
P13	804.63	2/6/2018	2.85	801.78
		4/4/2018	6.19	798.44
		12/19/2017	7.89	750.82
		12/20/2017	7.40	751.31
		1/25/2018	4.46	754.25
B12	758.71	2/6/2018	3.99	754.72
		3/6/2018	4.91	753.80
		3/27/2018	8.13	750.58
		4/4/2018	7.60	751.11
		12/19/2017	8.13	767.28
		12/20/2017	5.99	769.42
		1/25/2018	3.41	772.00
B15	775.41	2/6/2018	3.11	772.30
		3/6/2018	5.26	770.15
		3/27/2018	7.01	768.40
		4/4/2018	6.76	768.65



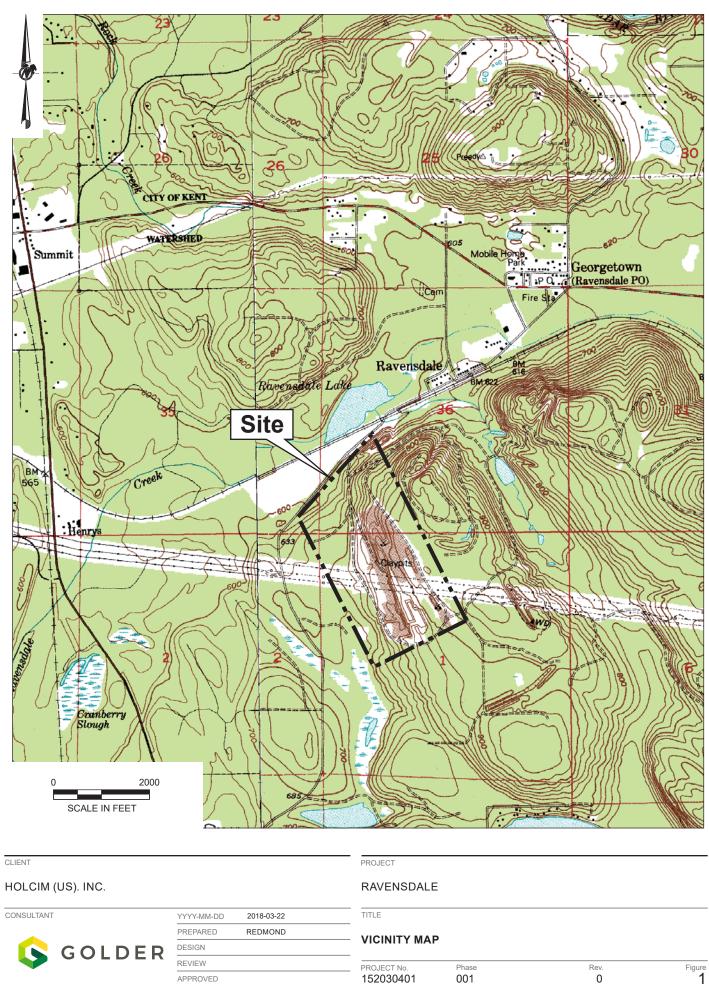
## Table 2: Groundwater Elevations

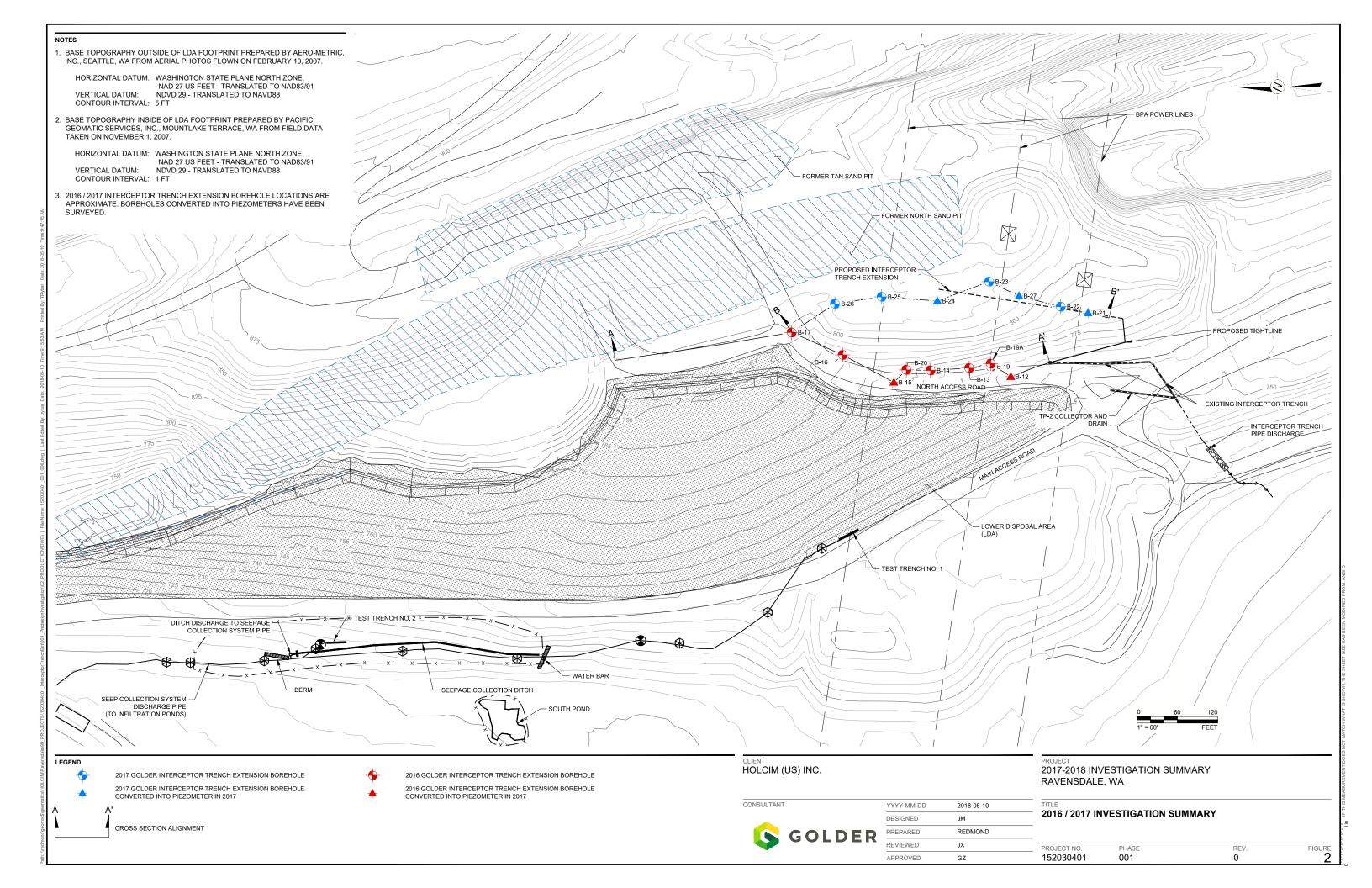
Well ID	TOC ELEV <sup>1</sup>	Date Measured	Depth to Water (feet below TOC)	Groundwater Elevation
		12/19/2017	6.49	776.51
		12/20/2017	5.08	777.92
		1/25/2018	4.39	778.61
B21	783.00	2/6/2018	4.90	778.10
		3/6/2018	6.23	776.77
		3/27/2018	8.25	774.75
		4/4/2018	7.71	775.29
		12/19/2017	16.77	792.99
		12/20/2017	16.77	792.99
		1/25/2018	13.45	796.31
B24	809.76	2/6/2018	5.85	803.91
		3/6/2018	16.77	792.99
		3/27/2018	DRY	
		4/4/2018	DRY	
		12/19/2017	18.37	785.03
		12/20/2017	18.08	785.32
		1/25/2018	17.41	785.99
B27	803.40	2/6/2018	17.09	786.31
		3/6/2018	17.42	785.98
		3/27/2018	17.73	785.67
		4/4/2018	18.00	785.40

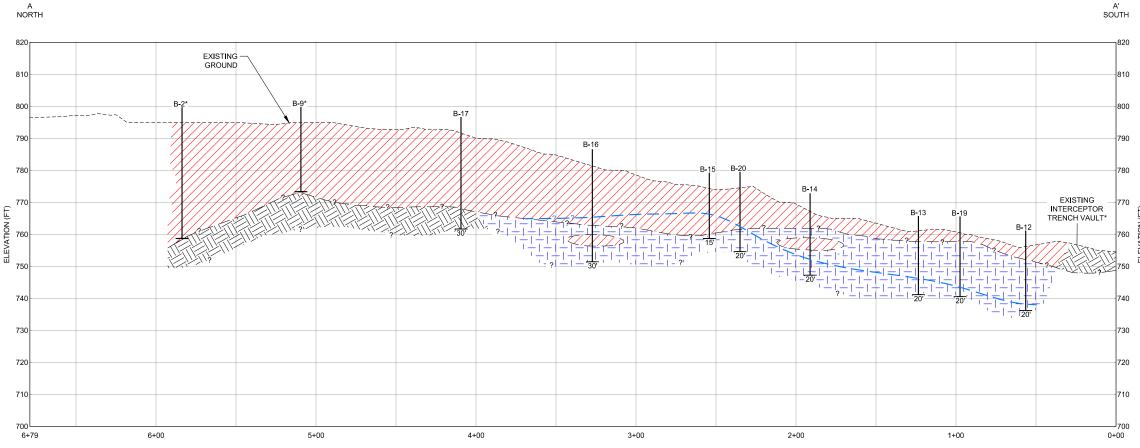
<sup>1</sup> Top of Casing Elevation surveyed 2016-2018



Figures







BOREHOLE PROFILE (OCTOBER 2016) HORIZ. SCALE 1" = 30' VERT. SCALE 1" = 15'

CLIENT HOLCIM (US) INC. LEGEND FILL (NON-CKD)  $\frac{1}{1} \frac{1}{1} \frac{1}$ BEDROCK CONSULTANT YYYY-MM-DD 2018-05-10 DESIGNED BORING (DEPTH) JM \* FROM 2013 INVESTIGATION - NOT SHOWN ON FIGURE 2 **GOLDER** PREPARED REDMOND REVIEWED JX ------ APPROXIMATE WATER LEVEL AT TIME OF DRILLING APPROVED GZ

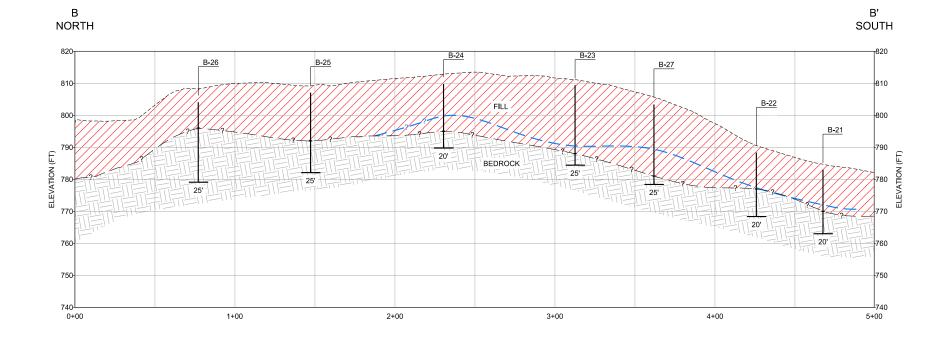


## PROJECT 2017-2018 INVESTIGATION SUMMARY RAVENSDALE, WA

## (OCTOBER 2016)

TITLE				
BOF	REHOL	E PR.	OFILI	E (0

PROJECT NO.	PHASE	REV.	FIGURE
152030401	001	0	
102000101	001	•	0/1



BOREHOLE PROFILE (DECEMBER 2017) HORIZ. SCALE 1" = 30' VERT. SCALE 1" = 15'

20'

- NOTE(S)
  1. SURFICIAL PROFILE CREATED FROM BASE TOPOGRAPHY MAP 02/10/2007. BORING LOCATIONS SURVEYED ON 02/05/2018. ON SITE ACTIVITIES MAY HAVE ALTERED GROUND SURFACE BETWEEN SURVEYS.
- MINIMAL WATER WAS ENCOUNTERED IN BOREHOLES B-25 AND B-26 DURING DRILLING.
   WATER LEVELS IN B-25 AND B-26 ARE NOT USED TO DETERMINE APPROXIMATE WATER LEVEL AT TIME OF DRILLING.



FILL (NON-CKD) ////// BEDROCK

- APPROXIMATE WATER LEVEL AT TIME OF DRILLING \_ \_

# CLIENT HOLCIM (US) INC.

	CONSULTANT		YYYY-MM-DD	2018-05-10	
	<u> </u>		DESIGNED	JM	
BORING (DEPTH)		GOLDER	PREPARED	REDMOND	
		OOLDER	REVIEWED	JX	
			APPROVED	GZ	



2017-2018 INVESTIGATION SUMMARY RAVENSDALE, WA

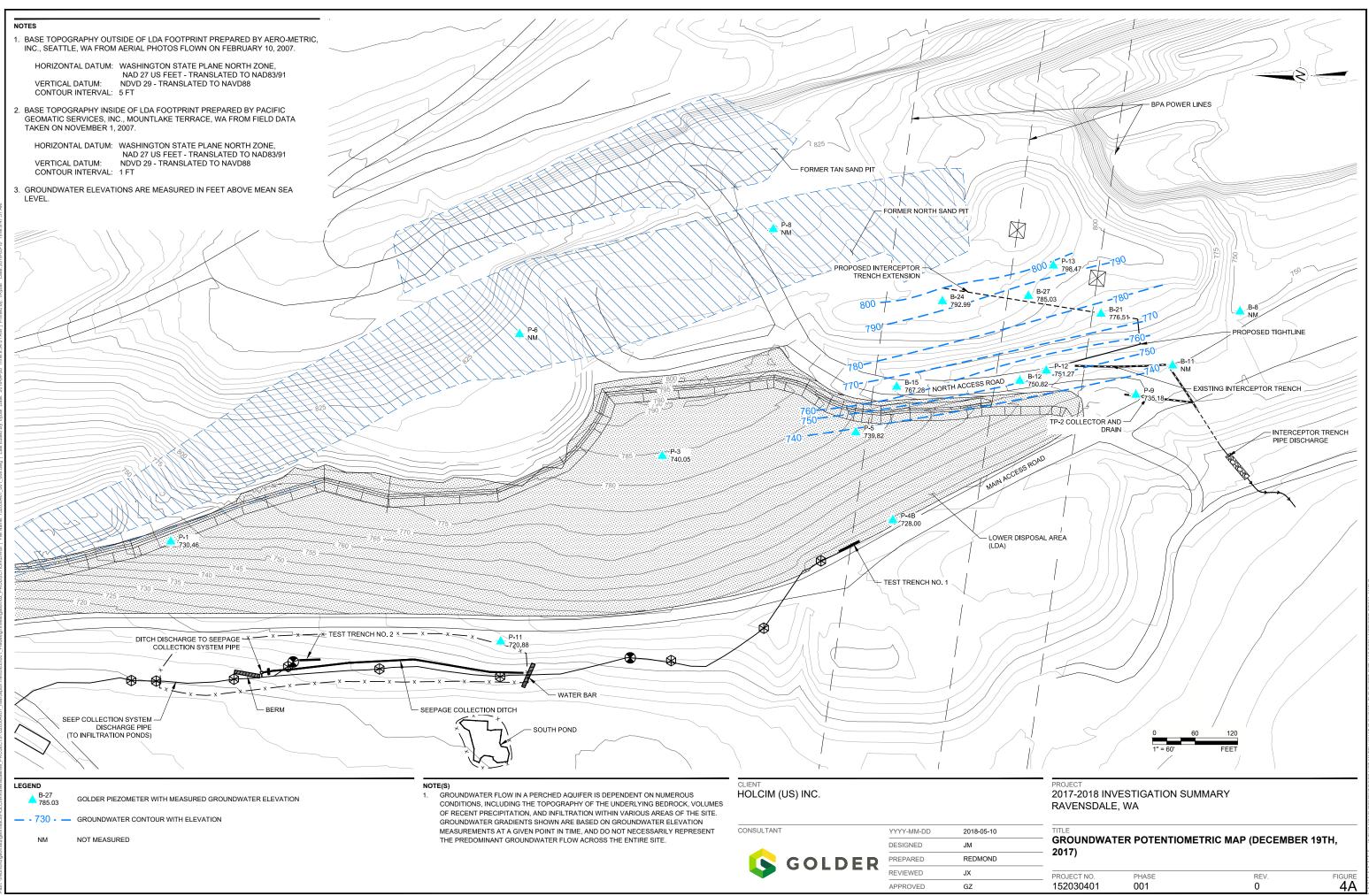
# BOREHOLE PROFILE (DECEMBER 2017)

PROJECT NO. 152030401

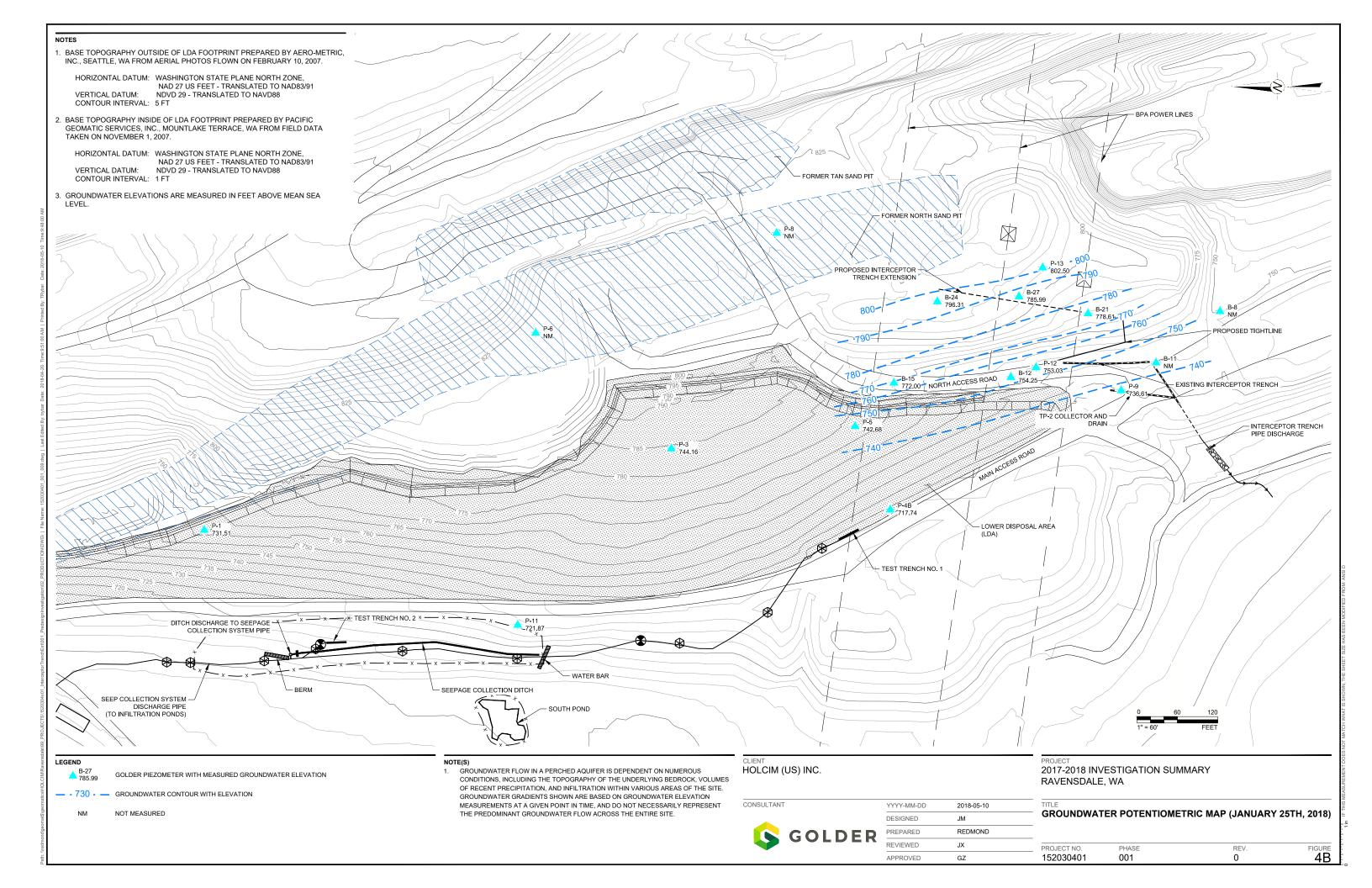
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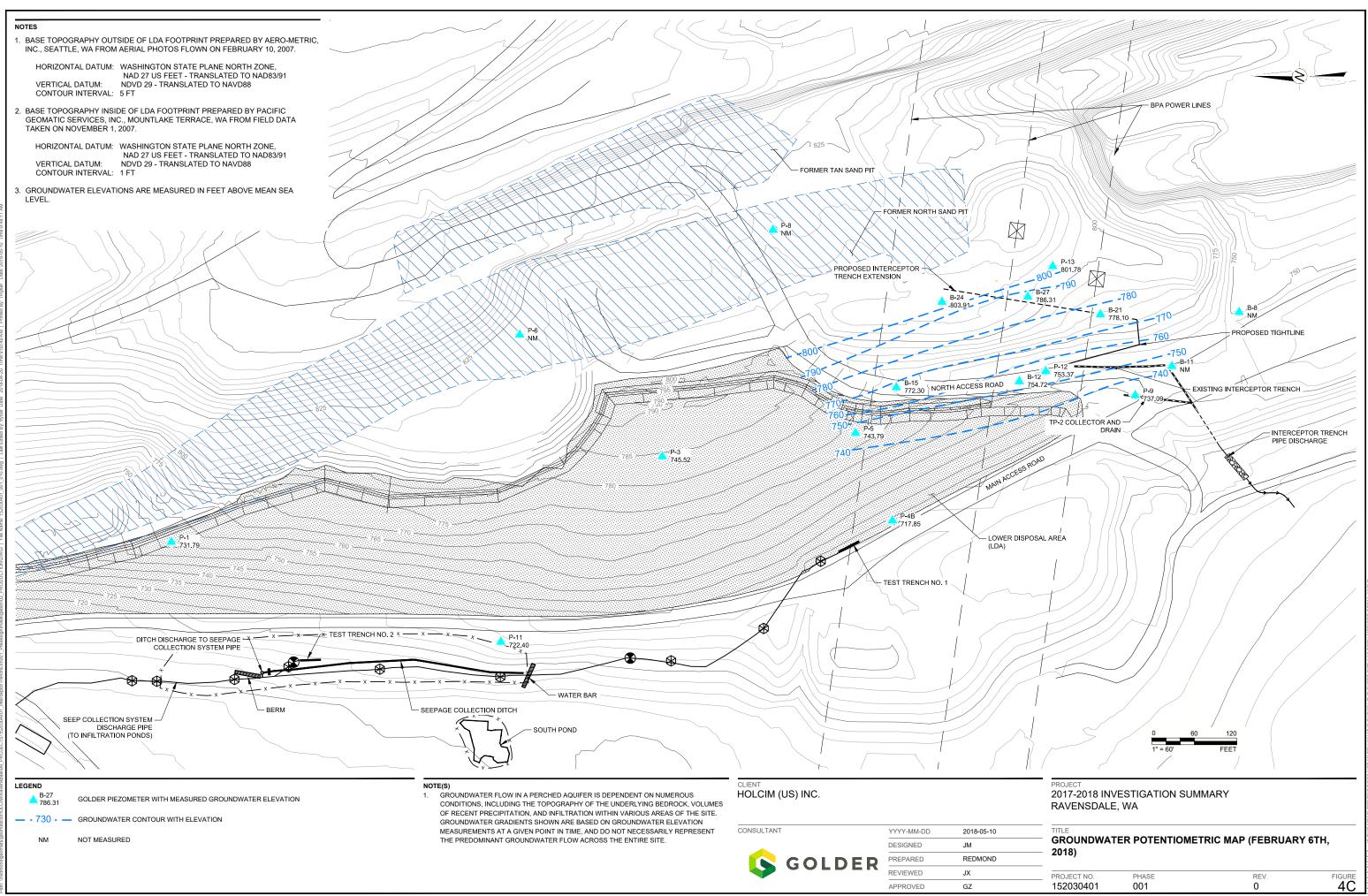
REV. 0

FIGURE

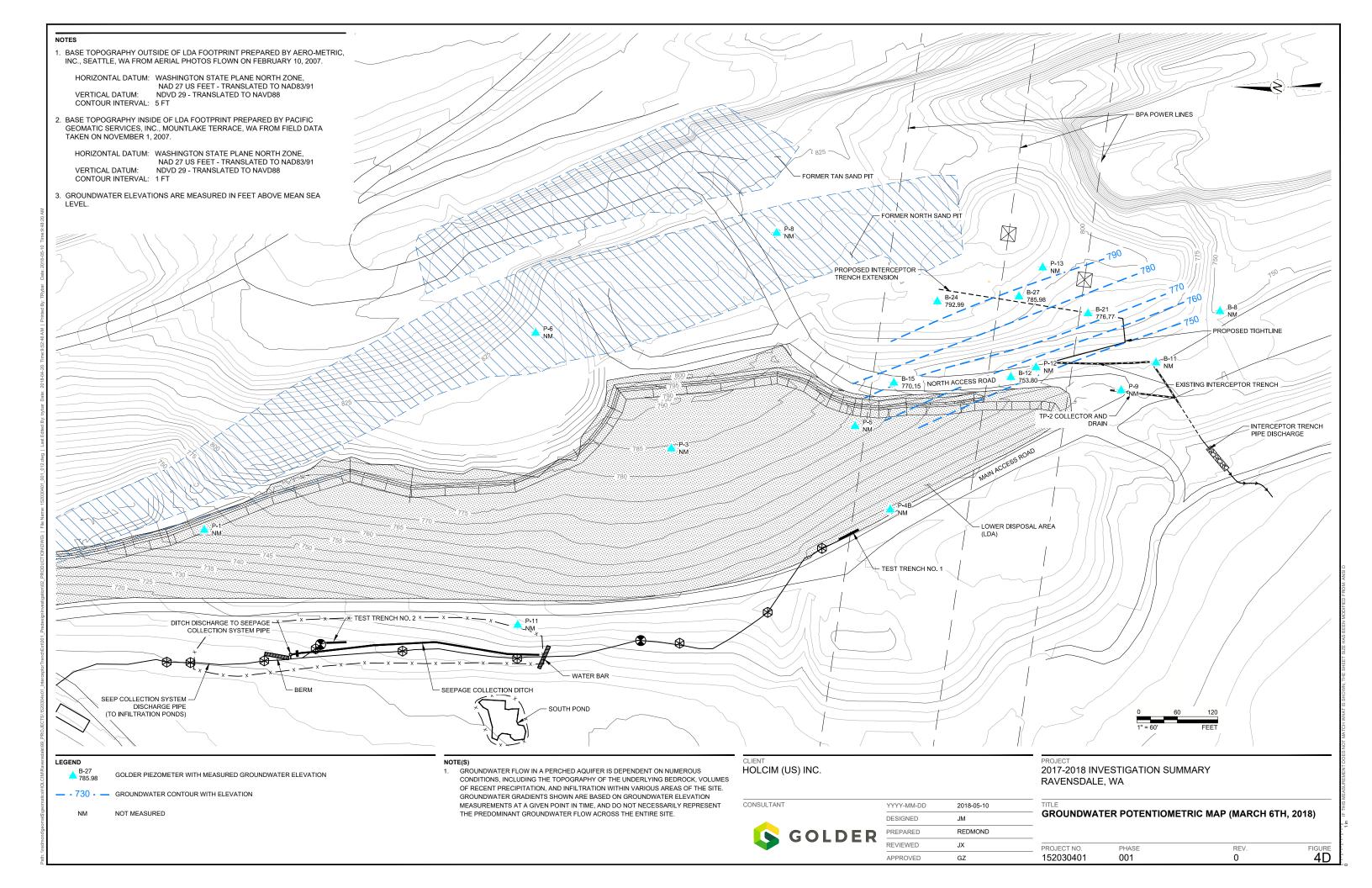


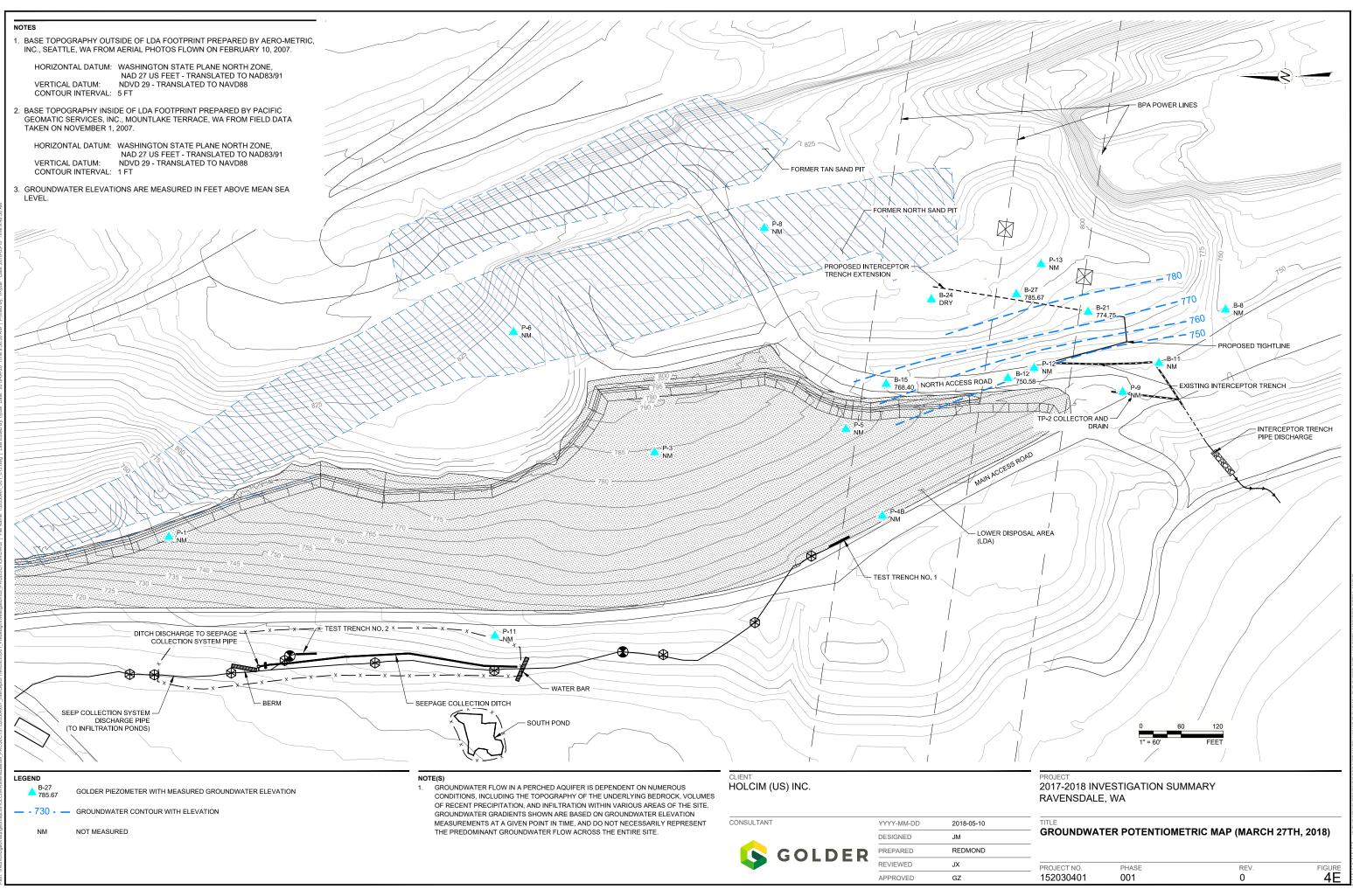
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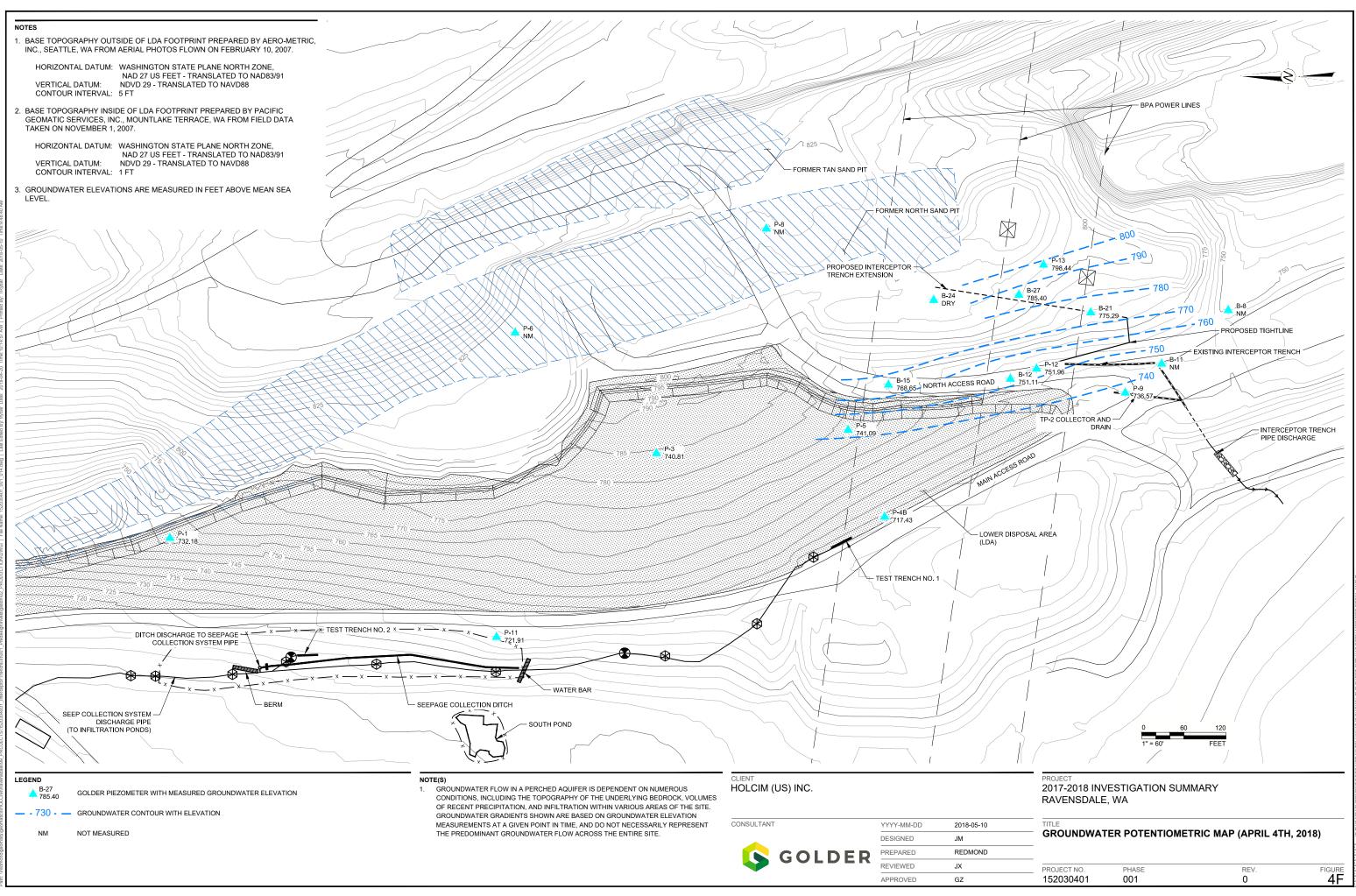


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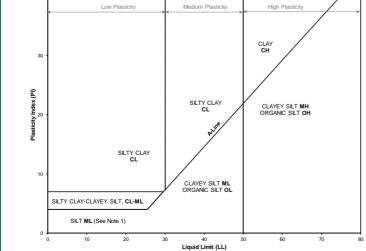
ATTACHMENT A

**Boring Logs** 



## **METHOD OF SOIL CLASSIFICATION**

The Gol	der Asso	ciates In	c. Soil Cla	ssification S	System is b	ased on t	he Unifi	ed Soil Clas	ssification S	ystem (US	SCS)													
Organic or Inorganic	Soil Group	Туре	of Soil	Gradation or Plasticity	Cu	$=\frac{D_{60}}{D_{10}}$		$Cc = \frac{(D)}{D_{10}}$	$\frac{(30)^2}{xD_{60}}$	Organic Content	USCS Group Symbol	Group Name												
		nm) is of	Gravels with <12% *	Poorly Graded		<4		≤1 or ≧	≥3		GP	GRAVEL												
(ss	5 mm)	GRAVELS 3% by mass trse fraction r than 4.75 r	fines (by mass)	Well Graded		≥4		1 to 3	3		GW	GRAVEL												
by ma	SOILS	GRAVELS (>50% by mass of coarse fraction is larger than 4.75 mm)	Gravels with	Below A Line			n/a				GM	SILTY GRAVEL												
INORGANIC (Organic Content ≺30% by mass)	VINED ger tha	large C) S	>12% fines (by mass)	Above A Line			n/a			1	GC	CLAYEY GRAVEL												
NORG	E-GR/ s is lar	of mm)	Sands with	Poorly Graded		<6		≤1 or ≩	≥3	<30%	SP	SAND												
Janic C	OARS by mas	DS mass e action i	<12% * fines (by mass)	Well Graded		≥6		1 to 3	3		SW	SAND												
(Org	COARSE-GRAINED SOILS (>50% by mass is larger than 0.075 mm)	SANDS (>50% by mass of coarse fraction is smaller than 4.75 mm)	Sands with	Below A Line			n/a			-	SM	SILTY SAND												
		(>5 co small	>12% fines (by mass)	Above A Line			n/a			-	SC	CLAYEY SAND												
Organic			(6) (1000)			I	Field Indica	itors																
or Inorganic	Soil Group	Туре	of Soil	Laboratory Tests	Dilatancy	Dry Strength	Shine Test	Thread Diameter	Toughness (of 3 mm thread)	Organic Content	USCS Group Symbol	Primary Name												
		SILTS SILTS (Non-Plastic or Pl and LL plot below A-Line on Plasticity Chart below)		- plot city	Linuted Linute	Rapid	None	None	>6 mm	N/A (can't roll 3 mm thread)	<5%	ML	SILT											
(ss	<sup>5</sup> mm)		and Ll Plasti ow)		Liquid Limit <50	Slow	None to Low	Dull	3 mm to 6 mm	None to low	<5%	ML	CLAYEY SILT											
by ma	01LS an 0.07		SILTS	SILTS	SILTS	SILTS	SILTS	SILTS	SILTS	SILTS	SILTS	SILTS	SILTS	SILTS	corPl Lineon artbel		Slow to very slow	Low to medium	Dull to slight	3 mm to 6 mm	Low	5% to 30%	OL	ORGANIC SILT
ANIC <30%	IED SC aller the		-Plasti Iow A-I Ch	n-Plast slow A- Ch	Liguid Limit	Slow to very slow	Low to medium	Slight	3 mm to 6 mm	Low to medium	<5%	МН	CLAYEY SILT											
INORGANIC content <30%	FINE-GRAINED SOILS mass is smaller than 0.	į	be be	≥50	None	Medium to high	Dull to slight	1 mm to 3 mm	Medium to high	5% to 30%	ОН	ORGANIC SILT												
INORGANIC (Organic Content <30% by mass)	FINE- y mass	lot	art	Liquid Limit <30	None	Low to medium	Slight to shiny	~ 3 mm	Low to medium	0% to	CL	SILTY CLAY												
(Org	FINE-GRAINED SOILS (≥50% by mass is smaller than 0.075 mm)	:50% b	±50% b	=50% b	±50% b	≥50% b	≥50% b	≥50% b	≥50% b	CLAYS and LL p	A-Line city Ch elow)	Liquid Limit 30 to <50	None	Medium to high	Slight to shiny	1 mm to 3 mm	Medium	30%	CL	SILTY CLAY				
	(1)	(Pl ar	above A-Line on Plasticity Chart below)	Liquid Limit ≥50	None	High	Shiny	<1 mm	High	(see Note 2, below)	СН	CLAY												
-S NIC	ass)	Peat and mineral soil mixtures					30% to 75%		SILTY PEAT, SANDY PEAT															
HIGHLY ORGANIC SOILS	(Organic Content >30% by mass)	Predominantly peat, may contain some o mineral soil, fibrous, or amorphous peat				75% to 100%	PT	PEAT																
40		Low Plasticity	N	Nedium Plasticity	High Plasticit	y /		* Dual Syr	mbol — A du	ual symbol	is two symbo	ols separated												
				· • •				, ,,	,	• •	GM, SW-SC,	,												
						/				-	al symbols m													
30 -					CLAY CH						6 and 12% i	•												
											tween "clean' oils, the dual	,												
					/			sanu ur yi	aven. FULC	OURSING 20	ula, the utal	Symbol mus												



Note 1 – Fine-grained materials with PI and LL that plot in this area are named (ML) SILT with slight plasticity. Fine-grained materials which are Non-plastic (i.e. a PL cannot be measured) are named SILT.

Note 2 – For soils with <5% organic content, include the descriptor "trace organics." For soils with between 5% and 30% organic content include the prefix "organic" before the Primary name.

and or gravel). For cohesive soils, the dual symbol must be used when the liquid limit and plasticity index values plot in the CL-ML area of the plasticity chart (see plasticity chart at left).

Borderline Symbol — A borderline symbol is two symbols separated by a slash, for example, GM/SM, CL/ML. A borderline symbol should be used to indicate that the soil has been identified as having properties that are on the transition between similar materials. In addition, a borderline symbol may be used to indicate a range of similar soil types within a stratum.



## METHOD OF SOIL CLASSIFICATION

### PARTICLE SIZES OF CONSTITUENTS

Soil	Particle Size	Millimeters	Inches
Constituent	Description		(US Std. Sieve Size)
BOULDERS	Not Applicable	> 300	> 12
COBBLES	Not Applicable	75 to 300	3 to 12
GRAVEL	Coarse	19 to 75	0.75 to 3
	Fine	4.75 to 19	(4) to 0.75
SAND	Coarse	2.00 to 4.75	(10) to (4)
	Medium	0.425 to 2.00	(40) to (10)
	Fine	0.075 to 0.425	(200) to (40)
SILT/CLAY	Classified by plasticity	< 0.075	< (200)

### MODIFIERS FOR SECONDARY AND MINOR CONSTITUENTS

Percentage by Mass	Modifier
≤ 5	trace
> 5 to 12	some
> 12 to 35	Primary soil name prefixed with "gravelly, sandy, SILTY, CLAYEY" as applicable
> 35	Use 'and' to combine major constituents ( <i>i.e.</i> , SAND and GRAVEL, SAND and CLAY)

### PENETRATION RESISTANCE

### Standard Penetration Resistance (SPT), N:

N = the number of blows required to drive a 2 inch (50 mm) split-spoon sampler one foot (300 mm) using a 140 lb (63.5 kg) hammer falling 30 inches (760 mm) after an initial 6 inch (150 mm) seating (ASTM D1586).

### Cone Penetration Test (CPT):

An electronic cone penetrometer with a 60° conical tip and a typical projected end area of 10 or 15 cm<sup>2</sup> pushed through ground at a penetration rate of 2 cm/s. Measurements of tip resistance (q<sub>i</sub>), porewater pressure (u) and sleeve friction (f<sub>s</sub>) are recorded electronically in real time during penetration. The seismic CPT (SCPT) adds measurement of shear wave velocity (V<sub>s</sub>) to the standard CPT.

### Dynamic Cone Penetration Test (DCP), Nd:

The penetration rate by an 8 kg (17.6 lb) hammer dropped 575 mm (22.6 in.) to drive uncased a 20 mm (0.79 in.) diameter,  $60^{\circ}$  cone attached to 16 mm (5/8 in.) drive rods (ASTM D6951). Other test methods exist for DCPs with different configurations and different correlations.

- PH: Sampler advanced by hydraulic pressure
- PM: Sampler advanced by manual pressure
- WH: Sampler advanced by static weight of hammer
- WR: Sampler advanced by weight of sampler and rod

|--|

Compactness <sup>1</sup>										
SPT 'N' (blows/foot) <sup>2</sup>										
0 - 4										
4 to 10										
10 to 30										
30 to 50										
>50										

1. Definition of compactness descriptions based on SPT 'N' ranges from Terzaghi and Peck (1967) and correspond to typical average  $N_{\rm 60}$  values.

 SPT 'N' in accordance with ASTM D1586, uncorrected for overburden pressure effects. 'N'-values should be considered ONLY an approximate guide to consistency; for sensitive clays the 'N'-value approximation for consistency terms does not apply.

Field Moisture Con	dition
--------------------	--------

Term	Description
Dry	Soil flows freely through fingers.
Moist	Soils are darker than in the dry condition and may feel cool.
Wet	As moist, but with free water forming on hands when handled.

### SAMPLE TYPES

SAMPLE TYPE	3
AS	Auger sample
CS	Chunk sample
DO or DP	Drive open (SPT) or direct pushed tube sampler
DS	Denison type sample
FS	Foil sample
PS	Pitcher type sample
RC	Rock core
SC	Soil core
ST	Slotted tube
то	Thin-walled, open
TP	Thin-walled, piston
WS	Wash sample

### SOIL TESTS

М	
	water content
А	Atterberg limits (plastic and liquid limits)
G, H	grain size, hydrometer
UW	unit weight
Com	compaction
С	consolidation (oedometer) test
U	unconfined compression test
UU	unconsolidated undrained triaxial test
CD	consolidated isotropically drained triaxial test1
CU	consolidated isotropically undrained triaxial test with porewater pressure measurement <sup>1</sup>
D	direct shear test
V (FV)	field vane (LV-laboratory vane test)
SG	specific gravity
Р	permeability
PD	pinhole dispersion
0	organic content test
PH	рН
CHEM	chemical analysis (refer to text)

 Tests which are anisotropically consolidated prior to shear are shown as CAD, CAU.

### COHESIVE SOILS

	Consistency											
Term	Undrained Shear Strength (kPa)	Undrained Shear Strength (tsf)	SPT 'N' <sup>1</sup> (blows/foot)									
Very Soft	<12	<0.12	0 to 2									
Soft	12 to 25	0.12 to 0.25	2 to 4									
Firm	25 to 50	0.25 to 0.5	4 to 8									
Stiff	50 to 100	0.5 to 1	8 to 15									
Very Stiff	100 to 200	1 to 2	15 to 30									
Hard	>200	>2	>30									

 SPT 'N' in accordance with ASTM D1586, uncorrected for overburden pressure effects; approximate only.

	water Content
Term	Description
w < PL	Material is estimated to be drier than the Plastic Limit.
w ~ PL	Material is estimated to be close to the Plastic Limit.
w > PL	Material is estimated to be wetter than the Plastic Limit.



PRC	DJECT	Ravensdale Trench Extension DRILLING NUMBER: 1520304-01 DRILLING I: Access Rd East of LDA DRILL RI	G METI G DATE	HOD: F E: 10/2	Rotosonic		OR	EHOLE DATUM: COORDIN	NAD	88	126,354 E: 1,353,2	SHEET ?	1 of 1 ELEVATION: INCLINATION WELL TAG: E	1: -90
DEPTH (Ft)		SOIL PROFILE	s s s s s s s s s s s s s s s s s s s	GRAPHIC LOG	ELEV.	NUMBER	ТҮРЕ	SAMPLES BLOWS per 6 in	N	REC	PENETRATION RE BLOWS / 1 10 20 3	t 🕈	NOTE WATER LI	:S EVELS
-0 -	BORIN		SU	GRAI	DEPTH (Ft)	NUM	Τ	140 lb hammer 30 inch drop	IN	ATT	PL MC 20 40 6		GRAPI	liC
-		0.0 - 2.0 FILL - MINE SPOILS, (GP-GM) GRAVEL, fine to coarse, some silt; brown; non-cohesive, moist, loose.		×	757.0	-							Flush Mount Monument	
		FILL - MINE SPOILS, (SM) SILTY SAND, some gravel, fine; dark brown to brown, thin laminations; non-cohesive, moist, compact.		×	754.5								Medium (3/8")	-
- 5		4.5 - 20.0 FILL - CEMENT KILN DUST, trace wood ash, trace coal fragments; light gray; non-cohesive, dry to moist, dense.			4.5								Bentonite Seal, 2" Schedule 40 PVC Riser	-
		4.5 ft: Odor in core barrel, tested pH ~12 (mixture of DI water and soil)												
- 10	Rotosonic												10/20 Silica Sand	
													0.010-inch Slot	
- 15		15 ft: Hole staying open, sample sticking to											Schedule 40 PVC Screen	
		core barrel												
- 20					739.0	-								
		Boring completed at 20.0 ft.			20.0									-
														-
- 25														-
														-
· 30														-
														-
0.5														-
- 35														-
														_
	to 5 ft				GED: 、									
		CONTRACTOR: Cascade Drilling D. Rider			CKED: E: 11/2			n				G	<b>B</b> Assoc	ler Liates

	CATION	NUMBER: 1520304-01 DRILLIN d: Access Rd East of LDA DRILL R SOIL PROFILE		E: 10/25 360				SAMPLES			PENETRATION F		INCLINATION: -90 WELL TAG:
e verin (Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	10 20 PL MC	30 40 LL 60 80	NOTES WATER LEVELS GRAPHIC
0 -		0.0 - 1.5 FILL - MINE SPOILS, (GP) GRAVEL, fine to coarse, some sand; brown, non-cohesive, moist, loose.	GP	R	759.5								
5	<u>c</u>	1.5 - 3.0       FILL - MINE SPOILS, (CL) CLAY, some sint, trace gravel, trace coal fragments; brown; cohesive, moist, stiff.         1.5 ft to 3 ft: Trace shale, coal tailings/fill       1         3.0 - 10.0       FILL - CEMENT KILN DUST, some coal fragments; brown, mottled; non-cohesive, moist, dense.         3 ft: Trace sandstone (fine grained), brown tailings/fill       5 ft: pH ~12 (mixture of DI water and soil)	CL		758.0								
10	Rotosonic	10.0 - 20.0			751.0								Backfilled with Medium (3/8") Bentonite Chips
15													
20		Boring completed at 20.0 ft.			20.0								
25													
30													
35													
40 1. in	to 5 ft				GED: 、								

		N: Access Rd East of LDA DRILL RIC SOIL PROFILE	3. 00					SAMPLES			PENETRATION F		WELL TAG: NOTES
(Ft) (Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	TYPE	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	PL MC	30 40 LL 60 80	GRAPHIC
J _		0.0 - 1.5 FILL - MINE SPOILS, (SP) SAND, some gravel, fine to coarse; brown to gray; non-cohesive, moist, loose.	SP	R	765.5	-							
		1.5 - 4.0 FILL - MINE SPOILS, (SM) SILTY SAND, fine, some gravel, trace coal fragments; brown to gray; non-cohesive, moist, dense.	SM	Æ	763.0								
5		4.0 - 5.0 FILL - MINE SPOILS, (ML) Sandy SILT, some clay, brown mottled gray; cohesive, m <-PL, stiff			4.0 762.0 5.0								
10	Rotosonic	8.5 - 11.0 FILL - MINE SPOILS, (SM) SILTY SAND, fine, trace coal fragments; orange-brown mottled gray, fine laminations; non-cohesive, moist, dense.			758.5 8.5 756.0	-							Backfilled with Medium (3/8") – Bentonite Chips
		11.0 - 20.0 FILL - CEMENT KILN DUST; gray, fine laminations; non-cohesive, moist, dense.			11.0								Chips .
15		15 ft to 20 ft: Trace coal fragments, last material in core barrel wet.											¥
20		Boring completed at 20.0 ft.			747.0 20.0	-							
25													
30													
35													
40													

(Ft)		I: Access Rd East of LDA DRILL RI SOIL PROFILE			ELEV.	R		SAMPLES				RESISTANCE S / ft ◆ 30 40	WELL TAG: BI	5
0 -	BORING	DESCRIPTION	nscs	GRAPHIC LOG	DEPTH (Ft)	NUMBER	ТҮРЕ	per 6 in 140 lb hammer 30 inch drop	N	REC ATT	PL N 20 40		GRAPHI	с
		0.0 - 2.0 FILL - MINE SPOILS, (GP) GRAVEL, fine to coarse, some sand; brownish-gray; non-cohesive, dry, loose.	GP	×	773.8 2.0	-							Flush Mount Monument Medium (3/8") Bentonite Seal,	× × -
5		FILL - MINE SPOILS, (SP) SAND, fine to medium, some gravel, fine; gray to brown; non-cohesive, moist, compact. 4.0 - 5.0 FILL - MINE SPOILS, (ML) Sandy SILT,	SP  ML		771.8 4.0 770.8								2" Schedule 40 PVC Riser	
5	onic	trace gravel, trace coal fragments; brown, mottled; cohesive, m < PL, very stiff. 5.0 - 7.0 FILL - MINE SPOILS, (SP) SAND, fine to coarse, trace silt, trace gravel;	SP	×	5.0 768.8 7.0	-								
	Rotosonic	Inn-cohesive, moist, loose/ 7.0 - 10.0 FILL - MINE SPOILS, (SM) SILTY SAND, fine to medium, trace coal fragments, trace wood fragments; non-cohesive, moist, compart	SM		765.8								10/20 Silica Sand	
10			 ML	Ř	10.0 763.8								0.010-inch Slot Schedule 40 PVC Screen	
		12.0 - 13.0 FILL - MINE SPOILS, (ML) SILT, some sand, trace gravel; gray; cohesive, w < PL, firm. 13.0 - 14.5	ML ML		12.0 762.8 13.0 761.3									
15		FILL - MINE SPOILS, (ML) Sandy SILT,         trace gravel; orange-brown; cohesive, w <			760.8 15.0									-
		Boring completed at 15.0 ft.												-
20														-
														-
25														-
														-
30														-
														-
35														-
														-
40														

LOC		N: Access Rd East of LDA DRILL R SOIL PROFILE	IG: DB	360				SAMPLES			PENET	RATION I BLOWS	RESISTANC	WELL TAG:
(Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	10 PL 20	20 MC 40	30 40	NOTES WATER LEVEL
0 -		0.0 - 2.0 FILL - MINE SPOILS, (GP) GRAVEL, fine to coarse, some silt, trace cobble; brown; non-cohesive, moist, loose.	GP	X	779.0									
		2.0 - 5.0 FILL - MINE SPOILS, (SM) SILTY SAND, fine, some gravel, trace coal fragments, trace wood; gray to brown; non-cohesive, moist, compact.	SM		2.0									
5		5.0 - 10.0 FILL - MINE SPOILS, (SM) SILTY SAND, some coal fragments, trace gravel; dark brown mottled black; non-cohesive, moist, compact.	SM		5.0	-								
10		10.0 - 12.0 FILL - MINE SPOILS, (ML) Sandy SILT; dark brown mottled brown, fine laminations;	— — - мl		771.0									
		cohesive, m < PL, soft 12.0 - 13.0 FILL - MINE SPOILS, (ML) SILTY, trace ↑ fine sand; gray; cohesive, moist, very stiff/ 13.0 - 15.0	— — –  ,	×	769.0 12.0 768.0 13.0									
15	Rotosonic	FILL - MINE SPOILS, (SM) SILTY SAND, trace gravel, trace coal fragments; dark gray mottled brown; non-cohesive, moist, compact.	SM	×	766.0	-								Backfilled with Medium (3/8") Bentonite
	-	13 ft: pH 7 (mixture of DI water and soil) 15.0 - 17.0 FILL - MINE SPOILS, (ML) Sandy SILT, some coal fragments, trace gravel; dark	ML		764.0 17.0									Chips
20		brownish-gray; cohesive, firm	 		762.0 19.0 761.0	-								
		Inon-cohesive, moist	SM		20.0 759.0									
		FILL - MINE SPOILS, (SP-SM) SAND, some silt; brownish gray, musty odor; non-cohesive, wet, loose.												
25		FILL - CEMENT KILN DUST, some silt, some sand, trace gravel; gray, finely laminated; non-cohesive, moist. 25.0 - 30.0 FILL - MINE SPOILS, (SM) SILTY SAND,	+		756.0 25.0									
		trace gravel; fill debris (brick, asbestos); non-cohesive, moist, compact.	SM											
30		Boring completed at 30.0 ft.	+	    }	751.0 30.0									
35														
40														

		J: Access Rd East of LDA DRILL RI SOIL PROFILE	IG: DB	360				SAMPLES				RATION F	RESISTANC	
(Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	10 PL  20	MC	30 40 LL 60 80	NOTES WATER LEVELS GRAPHIC
5		0.0 - 5.0 FILL - MINE SPOILS, (GP) GRAVEL, fine to coarse, some sand, some silt, trace cobbles; brown to gray; non-cohesive, loose.	GP		787.0									
,		5.0 - 7.0 FILL - MINE SPOILS, (SM) SILTY SAND, fine, trace gravel; brown; non-cohesive, moist, loose.	SM	X	5.0 785.0 7.0									
		FILL - MINE SPOILS, (ML) Sandy SILT, trace gravel; dark brown mottled black; cohesive, firm.	ML	×	783.0									
0		FILL - MINE SPOILS, (ML) SILT, trace Sand; light gray; cohesive, m ≤ PL, firm/ 10.0 - 13.0 FILL - MINE SPOILS, (SP-SM) SAND, some silt, trace gravel; brown mottled gray; non-cohesive, compact	SP-SM	Ø	- 782.0 - 10.0									
5	Rotosonic	13.0 - 15.0 FILL - MINE SPOILS, (ML) SILT, some clay, trace sand, trace gravel; black to dark brown, finely laminated; cohesive, m < PL, v stiff.	 ML		779.0 13.0 777.0									Backfilled with Medium (3/8")
-		15.0 - 21.0 FILL - MINE SPOILS, (SM) SILTY SAND, trace gravel; dark brown; non-cohesive, moist, compact.			15.0									Bentonite Chips
20		15 ft to 20 ft: Water in core barrel above sample	SM		771.0									
		21.0 - 23.0 FILL - MINE SPOILS, (ML) Sandy SILT, some woody debris; brown mottled gray; non-cohesive, moist 23.0 - 24.0	ML		21.0 769.0 23.0									
25		FILL - MINE SPOILS, (ML) SILT; gray;         _ cohesive, firm.         _ 24.0 - 25.0         ] FILL - MINE SPOILS, (ML) SILT; black;         _ cohesive, dry, soft.	ML ML		768.0 24.0 767.0 25.0									
		25.0 - 29.0 (ML) Sandy SILT, trace gravel; reddish-brown, [BEDROCK?]; cohesive, w < PL, soft.	ML											
80		29.0 - 30.0 (ML) Sandy SILT; gray with black specks, [BEDROCK?]; cohesive, w < PL, soft.	 ML 		763.0 29.0 762.0 30.0									
		29 ft: pH 7 (mixture of DI water and soil) Boring completed at 30.0 ft.												
85														
0														

PRO	OJECT	: Ravensdale Trench Extension DRILLIN NUMBER: 1520304-01 DRILLIN 4: Access Rd East of LDA DRILL R	IG MET IG DATI	HOD: F E: 10/20	Rotosonic		OR	EHOLE DATUM: 1 COORDIN	NAD 8	8		l of 1 ELEVATION: 760 INCLINATION: -90 WELL TAG:
DEPTH (Ft)	BORING METHOD	DESCRIPTION	SUCS N	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	SAMPLES BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	ANCE 40	NOTES WATER LEVELS GRAPHIC
- 0 - - - - - - - - - - - - - - - - - -	Rotosonic	0.0 - 2.0 FILL - MINE SPOILS, (ML) Sandy SILT, trace gravel; cohesive, moist, soft. 2.0 - 20.0 FILL - CEMENT KILN DUST, trace coal fragments; gray; non-cohesive, moist, dense. 10 ft to 15 ft: Putrid odor	ML		758.0							Backfilled with Medium (3/8") Bentonite Chips
		Boring completed at 20.0 ft.			740.0 20.0							
DRI		CONTRACTOR: Cascade Drilling D. Rider		CHE	GED: 、 CKED: E: 11/2	S. №	lorga	n			Ĝ	Golder

P	ROJEC	T: Ravensdale Trench Extension DRILLIN T NUMBER: 1520304-01 DRILLIN	IG METI IG DATE	HOD: F E: 10/26	Rotosonic		DRE	HOLE DATUM: 1 COORDIN	NAD 8	8	SHEET	ELEVATION: 760 INCLINATION: -60
		DN: Access Rd East of LDA DRILL F SOIL PROFILE	<u>RIG: DB</u>	360				SAMPLES			PENETRATION RESISTANCE	WELL TAG:
DEPTH 0 (Ft)	BORING METHOD	DESCRIPTION	NSCS	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	BLOWS / ft ◆ 10 20 30 40 PL MC LL 20 40 60 80	NOTES WATER LEVELS GRAPHIC
- - - 5 - -	Rotosonic	0.0 - 1.0 FILL - MINE SPOILS, (ML) Sandy SILT; <u>wet.</u> 1.0 - 10.0 FILL - CEMENT KILN DUST, trace coal fragments, trace scay; gray; non-cohesive, moist, dense.	J		759.1							- Backfilled with Medium (3/8") Bentonite Chips - -
		Boring completed at 10.0 ft.			10.0							
LOGS.GPJ SPARKLE_1.0_DATA_TEMPLATE.GDT 4/10/18												
RECORD OF BOREHOLE 15-20304 HOLCIM RAVENSDALE BOREHOLE LOGS.GPJ SPARKLE_1.0           JU         0         1         0         1 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
												-
0 1 i DF DF		ft G CONTRACTOR: Cascade Drilling R: D. Rider		CHE	GED: 、 CKED: E: 11/2	S. N	lorga	n			G	Golder

PF	ROJECT	: Ravensdale Trench Extension DRILLINO NUMBER: 1520304-01 DRILLINO N: Access Rd East of LDA DRILL RI	G METI G DATE	HOD: R E: 10/26	otosonic		OR	EHOLE DATUM: N COORDIN	NAD 8	8	SHEET	1 of 1 ELEVATION: 775 INCLINATION: -80 WELL TAG:
DEPTH (Ft)	BORING METHOD	SOIL PROFILE DESCRIPTION	nscs	GRAPHIC LOG	ELEV.	NUMBER	ТҮРЕ	SAMPLES BLOWS per 6 in 140 lb hammer	N	REC ATT	PENETRATION RESISTANCE BLOWS / ft ◆ 10 20 30 40 PL MC LL	
- 0 - - - - 5 - - - -		0.0 - 10.0 FILL - MINE SPOILS, (CL) CLAY, some silt, trace sand; brown to dark brown; cohesive, moist. 1" cobble caught in bit	CL		(Ft) 765.2			30 inch drop				Backfilled with
- 10 	Rotosonic	10.0 - 12.0         FILL - MINE SPOILS, (ML) CLAYEY SILT, trace sand, trace gravel; cohesive, moist, stiff.         12.0 - 20.0         FILL - CEMENT KILN DUST; gray; non-cohesive, moist, dense.	ML		763.2 10.0 763.2 12.0							Medium (3/8") Bentonite - Chips - - - - - - - - - - - - - - - - - -
30REHOLE LOGS.GPJ SPARKLE 1.0_DATA_TEMPLATE.GDT 4/10/18 0		Boring completed at 20.0 ft.			20.0							
	n to 5 ft	CONTRACTOR: Cascade Drilling			GED: C							Golder

							OR	EHOLE	B-2	21		SHEET 1	of 1	
PRO	OJECT	Ravensdale Trench Extension DRILLING NUMBER: 1520304-01 DRILLING	G DATE	: 12/1	1/2017	;		DATUM: N COORDIN			126,239 E: 1,3	53,336	ELEVATION: INCLINATION	N: -90
		I: Access Rd East of LDA DRILL RI SOIL PROFILE	G: Ter	rasonic	150			SAMPLES					WELL TAG: B	
DEPTH (Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer	N	REC ATT	10 20 PL N	S / ft ◆ <u>30 40</u> IC LL	NOTE WATER LE GRAPH	EVELS
- 0 -	Ш	0.0 - 1.0 Silty SAND (SM), Fine to Medium Sand, <u>Few 6° Cobbles, Brown, Loose, Moist</u> / 1.0 - 8.0 Silty SAND (SM), Fine to Medium Sand, Trace Fine to Coarse Gravel, Brown, Compact, Moist	SM		782.3			30 inch drop			20 40	60 80	Flush Mount Monument	
- 5			SM										Medium (3/8") Bentonite Seal, 2" Schedule 40 PVC Riser	
- - 10 -	Rotosonic	8.0 - 13.0 Clayey SAND (SC), Fine to Medium Sand, Some Silt, Trace Fine Gravel, Brown, Compact, Moist -Becomes Wet	sc		775.3								10/20 Silica Sand 0.010-inch Slot Schedule 40	
- - - 15 - -		13.0 - 20.0 SANDSTONE, Fine-grained with Silt, Weathered, Weak, Orange/Gray Mottled, Dry to Moist, Driller Note: Tough drilling at 13'	Sandstone		13.0								PVC Screen	
		Boring completed at 20.0 ft.			763.3									-
														-
														-
														-
 														-
2 25 - 25 - 30 - 30 - 40 - 1 in DRI DRI DRI														-
1 in DRI DRI		CONTRACTOR: Cascade Drilling D. Rider		CHE	GED: CKED: E: 4/5/2	G. Z		erman				Ć	Gold	ler ciates

	CATION	NUMBER: 1520304-01 DRILLING <u>Carrier Constant</u> Constant Solic Profile						SAMPLES		5. IN. I	26,280 E: 1,3	RESISTANCE	INCLINATION: -90 WELL TAG:
(Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	BLOWS	30 40	NOTES WATER LEVELS GRAPHIC
5		0.0 - 2.0 Silty SAND (SM), Fine to Coarse Sand, Trace Fine Gravel, Dark Brown, Loose, Moist 2.0 - 11.0 Silty SAND (SM), Fine Sand, Some Fine to Coarse Gravel, Rounded, Trace Cobbles, Trace Charcoal, Brown, Loose, Moist	SM 		786.4								
10	Rotosonic	- becomes wet 11.0 - 20.0 Fine Grained SANDSTONE, Some Silt, Weathered, Weak, Yellowish Brown, Moist			777.4								Backfilled with Medium (3/8") Bentonite Chips
15		- reddish-yellow, yellowish-brown, light gray mottled	Sandstone										
20 -		Boring completed at 20.0 ft.			768.4 20.0								
25													
30													
35													
40 1 in 1 DRIL	to 5 ft			LOG	GED: 、	J. Mil	ler						

LOC		I: Access Rd East of LDA DRILL RI SOIL PROFILE	<u>G: Te</u>	rasonic	150			SAMPLES				N RESISTANCE	WELL TAG:
(Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	10 20 PL	VS / ft ◆ <u>30</u> 40 MC LL <u>60</u> 80	NOTES WATER LEVELS GRAPHIC
,		0.0 - 5.0 Silty SAND (SM), Fine to Coarse Sand, Some Fine Gravel, Compact, Dark Brown, Moist	SM		804.4								
5		5.0 - 10.0 —			5.0								
0		8.5 - 9.5 - wood fragments			799.4								
	Rotosonic	10.0 - 11.5 Sitty SAND (SM), Fine to Medium Sand, Trace Fine Gravel, Roots, Compact, Brown, Gray, Wet/ 11.5 - 16.0 CLAY (CL), Blocky, Yellowish-Brown/Gray Mottled, Stiff, Dry	SM		10.0 797.9 11.5	-							Backfilled with Medium (3/8") Bentonite
15		15.0 - 16.0 increase Sand	CL		793.4 16.0	_							Chips - -
		COAL, Weak, Black, Dry	COAL		10.0								
20		19.0 - 21.0 CLAY (CL), Some Coal, Laminated, Yellowish-Brown, Stiff, Dry	 CL		790.4	_							
		21.0 - 25.0	COAL		788.4 21.0								
25		Boring completed at 25.0 ft.			784.4 25.0	-							
30													
35													
10													

PRO	OJECT	Ravensdale Trench Extension DRILLINO NUMBER: 1520304-01 DRILLINO I: Access Rd East of LDA DRILL Ri	G METI G DATE	HOD: F E: 12/1	Rotosonic 1/2017		OR	EHOLE DATUM: I COORDIN	NAD	88	126,464 E: 1,353,353	SHEET ?	l of 1 ELEVATION: INCLINATION WELL TAG: E	N: -90
DEPTH (Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	SAMPLES BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	PENETRATION RESI BLOWS / ft ● 10 20 30 PL MC 20 40 60		NOTE WATER LE GRAPH	S EVELS
0 - - - - - - 5		0.0 - 10.0 Sitty SAND (SM), Fine to Medium Sand, Some Fine Gravel, Trace Clay, Brown to Dark Brown, Compact, Moist	SM										Flush Mount Monument Bentonite Seal, 2" Schedule 40 PVC Riser	
- - 10 - - -	Rotosonic	-Trace Coal Clasts 10.0 - 12.0 Silty SAND (SM), Fine to Medium Sand, Trace Fine Gravel, Dark Gray, Loose, Moist to Wet 12.0 - 15.0 Poorty Graded SAND (SP), Some Silt, Yellowish Brown/Light Gray Mottled, Wet	 SM 		800.0 10.0 798.0 12.0 795.0	-							10/20 Silica Sand 0.010-inch Slot Schedule 40 PVC Screen	
- 15 - - - - 20 - - -		15.0 - 20.0 Fine grained SANDSTONE, Weathered, Yellowish Brown/Light Gray Mottled, Weak, Moist Boring completed at 20.0 ft.			15.0 790.0 20.0	-								
25   														-
- 35 - - - - - 40														
1 in DRI		CONTRACTOR: Cascade Drilling D. Rider	1	CHE	GED: CKED: E: 4/5/2	G. Z		erman	1	<u> </u>		Ĝ	Gold	ler Liates

		I: Access Rd East of LDA DRILL RI SOIL PROFILE	G: Ter		150			SAMPLES			LOWS / f	t 🔶	WELL TAG: E NOTES
(Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	Ν	REC ATT	20 30 MC 40 60		WATER LEVELS
,		0.0 - 3.0 Silty SAND (SM), Fine to Coarse Sand, some Fine Gravel, Dark Gray, Compact, Dry 	SM		804.1 3.0								
0		Gravel, 7" Cobbles, Dense, Moist	ML		799.6 7.5								
15	Rotosonic	- Drilling tough	COAL										Backfilled with Medium (3/8") Bentonite Chips
20		18.0 - 23.0	Shale		789.1 18.0 784.1								
25		23.0 - 25.0 SHALE, some Coal, some Silt, Friable, Laminated, Weak, Black, Dark Gray, Dry Boring completed at 25.0 ft.			23.0 782.1 25.0								
80													
5													
10													

		Ravensdale Trench Extension DRILLIN NUMBER: 1520304-01 DRILLIN	G METH	HOD: F	Rotosonia		ORI	EHOLE DATUM: 1 COORDIN		88	Sł 126,616 E: 1,353,348	HEET 1 of 1 ELEVATION: 804.0 INCLINATION: -90	8
	CATION	Access Rd East of LDA DRILL R SOIL PROFILE						SAMPLES			PENETRATION RESIST	WELL TAG:	_
DEPTH (Ft)	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV. DEPTH (Ft)	NUMBER	ТҮРЕ	BLOWS per 6 in 140 lb hammer 30 inch drop	N	REC ATT	BLOWS / ft ◆ 10 20 30 PL MC L	40 NOTES WATER LEVELS L GRAPHIC	
- 0 -		0.0 - 2.0 Silty SAND (SM), Fine to Coarse Sand, Trace Gravel, Brown/Black/Gray Mottled, Loose, Moist	SM		802.1								
_		2.0 - 5.0 Poorly Graded SAND with Silt (SP-SM), Fine Sand, Gray to Light Gray, Loose, Moist-Wet	SP-SM		2.0								-
— 5 —		5.0 - 8.0 SILT (ML), Fine Laminations, Light Gray, Dry 7.0 - 8.0			5.0								-
_ 10		pH 7-8 8.0 - 25.0 SILTSTONE, Trace Fine Sand, Laminated, <2mm Coal Beds, Gray, Dark Gray, Very Stiff, Dry			796.1 8.0	_							-
_ _ _ _ 15 _ _	Rotosonic	-Increase Shale, Trace Coal, Tight Drilling	SILTSTONE									Backfilled with Medium (3/8") Bentonite Chips	I I I I I I I I I I I I I I I I I I I
— 20 —		-becomes Hard											22.00 DTW after drilling on
-		-Increase thickness of silt beds		× × × × × × × × × × × × × × × × × × ×	779.1								-
25      30  		Boring completed at 25.0 ft.			25.0								
- 35  -													-
DRI		CONTRACTOR: Cascade Drilling D. Rider		CHE	GED: CKED: E: 4/5/	G. Z	Zimme	erman				Golder	25

PR	OJECT	: Ravensdale Trench Extension DRILLIN NUMBER: 1520304-01 DRILLIN V: Access Rd East of LDA DRILL RI	G METI G DATE	HOD: F E: 12/12	Rotosonio 2/2017		OR	EHOLE DATUM: 1 COORDIN	NAD	88	126,342 E: 1,353,	SHEET 1 360	l of 1 ELEVATION INCLINATIC WELL TAG: 1	N: -90		
DEPTH (Ft)	BORING METHOD	SOIL PROFILE		SOIL PROFILE       DESCRIPTION         SOIL PROFILE         EL         DESCRIPTION		SOIL PROFILE     SAMPLES       DESCRIPTION     Sold Profile     ELEV.     Max H     BLOWS per 6 in N				N	REC ATT	PENETRATION RESISTANCE BLOWS / ft ◆ 10 20 30 40 PL MC LL				
- 0 - - -	<u>a</u>	0.0 - 17.0 Silty SAND (SM), Fine to Coarse Sand, Trace Fine Gravel, Trace Wood Fragments, Trace Shale, Dark Brown/Yellow Brown Mottled, Loose, Moist (Fill)			(Ft)			30 inch drop			20 40 61	0 80	Flush Mount Monument			
- - 5 - - - - 10 - - -	Rotosonic	-Trace Coal	SM										Medium (3/8") Bentonite Seal 2" Schedule 40 PVC Riser		14.03' DTW After well installation 12/13/17	
		17.0 - 22.0			786.6 17.0 781.6	-							10/20 Silica Sand 0.010-inch Slot Schedule 40 PVC Screen			
2		22.0 - 25.0 Fine Grained SANDSTONE, Weak, Yellowish Brown, Dry	Sandstone		22.0 778.6											
		Boring completed at 25.0 ft.			25.0											
1 in DRI DRI DRI		G CONTRACTOR: Cascade Drilling	1	CHE	GED: . CKED: E: 4/5/	G. Z	Zimme	erman	I			Ć	Gol	der ciates		

ATTACHMENT B

2017 Work Plan



# LOWER DISPOSAL AREA INTERCEPTOR TRENCH BOREHOLE INVESTIGATION WORK PLAN

## **RAVENSDALE SITE, WASHINGTON**

REPORT

Submitted To: Holcim (US) Inc. 8677 Hwy 45 S Alt. Artesia, MS 39736

Submitted By: Golder Associates Inc. 18300 NE Union Hill Road, Suite 200 Redmond, WA 98052 USA

Distribution: Seattle King County Public Health Washington State Department of Ecology Reserve Silica Corp. Holcim (US) Inc. Golder Associates Inc.

September 18, 2017

Project No. 152030401.001





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Easement Figure Exhibit A



#### **1.0 INTRODUCTION**

#### 1.1 Background

The Ravensdale site (site) is located at 28131 Ravensdale-Black Diamond Road in Ravensdale, Washington (Figure 1). Historically, sand and coal mining operations occurred on the site until 2007. The site is currently owned by the Reserve Silica Corporation (Reserve Silica). Reserve Silica is backfiling the remaining historical excavation areas under an inert waste landfill permit (Permit #PR0082027). Holcim (US) Inc. (Holcim) has entered into agreements with Reserve Silica for addressing environmental conditions associated with historic disposal of cement kiln dust (CKD) at the site by predecessor companies.

The Lower Disposal Area (LDA) is a former open pit sand mine that was backfilled by placing cement kiln dust CKD and other materials into the mine excavation from June 1979 to October 1982. The approximate location of the LDA is shown in Figure 2. Historically, high-pH seepage has surfaced along the down-slope area west of the LDA. The seeps are primarily located along the northern half of the western boundary of the LDA. The seepage historically drained through low-lying, marshy areas and commingled with stormwater before flowing to the infiltration ponds. Currently, the seepage is collected in a ditch and catch basin system and piped to the infiltration ponds at the northern end of the site.

Holcim is addressing the high-pH seepage from the LDA through two primary methods:

- 1. Reducing, to the extent practical, the amount of meteoric and groundwater entering the LDA and contacting the CKD, thereby reducing the volume of high pH seepage.
- 2. Capturing and directing the high pH seepage to a treatment system (scheduled for construction in the fall of 2017) for neutralization and removal of dissolved arsenic prior to discharge to the existing infiltration ponds.

#### **1.2 Previous Remediation Activities**

In September and October 2007, the soil cover on the LDA was upgraded to meet industry standards and to reduce infiltration that could contribute to high-pH seepage observed in this area. Specific activities included regrading the cover to provide positive surface water runoff at all locations, increasing the thickness of the low-permeability cover soil layer to a minimum of two feet at all locations, and constructing a surface water diversion ditch around the upslope boundary of the cover.

Qualitative observations after construction of the improved cover, however, did not indicate a significant reduction in seepage volume. On this basis, it was considered most likely that the primary cause of seepage is up-gradient shallow groundwater inflow into the LDA, rather than surface water or infiltration through the cover.





Under this interpretation, the most practical approach for reducing seepage would be to reduce the influx of groundwater to the LDA. Therefore, a comprehensive program of test pit excavations, borehole drilling, piezometer measurements, tracer tests, and geophysical investigations was performed during 2010 to 2012. The results of these investigations were summarized in the *Lower Disposal Area Hydrogeologic Investigation* report (Golder 2013), and strongly suggested that groundwater was entering the LDA from the southern end and flowing to the north, producing the observed high-pH seeps and shallow groundwater impacts.

A groundwater interceptor trench was constructed at the south end of the LDA during August through October of 2013 as a first phase of reducing groundwater inflow to the LDA. The trench is approximately 220 feet long and up to 20 feet deep. Only about 50 feet of the trench length extends up the east side of the LDA from the southern end. Figure 2 shows the location of the existing interceptor trench. The trench is filled with gravel with a perforated drainage pipe in the bottom that discharges diverted shallow groundwater via gravity drainage to a point on the hillside to the south of the LDA. Flows from this trench are clean (non-impacted) groundwater and generally range between about 0.5 and 2.5 gallons per minute (gpm), although flows of 5 gpm have been measured following periods of heavy rainfall. The attached Table 1 presents monthly measurements of clean water discharging from the existing interceptor trench during the period of August 2016 to August 2017. Since construction of this trench, seepage along the western side of the LDA has continued, although any volume changes have not been measured.

In September 2008 in order to evaluate remedial options for the seepage water along the western side of the LDA, two test trenches were installed to collect high-pH seepage from the LDA. One trench was located on the bench immediately to the west of the LDA, where several seeps (and resulting carbonate deposits) had been observed over the course of several years. The second trench was located at the toe of the cover slope near the south end of the LDA. The trenches themselves were backfilled with gravel and each included a perforated drain pipe and a standpipe system to measure flow rate. Collected seepage was discharged through a 4-inch tightline pipe installed from the trenches to the infiltration ponds. The purpose of this test program was to determine the effectiveness of gravel-filled trenches in collecting seepage, evaluate the construction methods used for the trenches and to provide data for estimating the quantity and chemical characteristics of the seepage. The last objective would, in turn, help to identify the most appropriate method for managing the seepage.

In February 2013, a collection ditch was excavated along the bench below the western seepage zone to collect seepage, and a drop inlet structure was installed to direct seepage into the tightline and convey it directly to the infiltration ponds, thereby reducing the volume that commingles with surface water. In 2015, the 4-inch tightline downstream of the drop inlet was replaced with a 10-inch pipe to reduce the required frequency of cleaning resulting from carbonate precipitation in the pipe. Table 2 presents monthly flow measurements of the collected seepage water discharging from the 10-inch pipe to the infiltration ponds





during the period of August 2016 to August 2017. The collection ditch proved effective in capturing and conveying seepage, and the discharge pipe will be re-routed to convey the collected seepage to a seepage water treatment system. The design, construction, and operation of the seepage collection treatment system are being submitted to the Washington State Department of Ecology (Ecology) and to the Public Health Seattle and King County department under separate cover.

Chain-link fencing with 3-strand barbed wire at the top has been placed around site areas where high pH surface water is present. The fenced areas include: the seepage area and seepage collection ditch located west of the LDA; the South Pond located west of the LDA; and the infiltration ponds that receive the collection trench water discharge via the tightline. In addition, minor seepage water exposures observed along the southwest toe of the LDA were covered with coarse rock to allow flow of the water into the collection ditch system, while preventing direct contact by humans or animals at the ground surface.

#### 1.3 Purpose and Scope

The existing interceptor trench demonstrates that shallow groundwater flowing along the top of the bedrock at the south end LDA can be diverted around the LDA. The existing 220-foot-long interceptor trench, however, only extends approximately 50 feet along the southeast upgradient side of the LDA. The purpose of the proposed borehole investigation program is to determine if constructing an additional branch of the interceptor trench upgradient of the southeast side of the LDA could effectively divert additional shallow groundwater around the LDA, thus potentially reducing the volume of high pH seepage discharging from the downgradient side of the LDA.

The scope of the current investigation is to determine the depth to bedrock and to identify shallow groundwater flow zones on top of the bedrock in the area along the southeast, hydrologically upgradient, side of the LDA. If the initial borehole investigation indicates that constructing an additional branch of the interceptor trench is feasible, installation of additional groundwater piezometers/wells may be necessary to evaluate the effectiveness of the interceptor trench extension. An additional work plan would be prepared for if additional piezometers/wells they are considered necessary.



#### 2.0 BOREHOLE INVESTIGATION ACTIVITIES

#### 2.1 Preliminary Investigation

In October 2016, Golder performed a preliminary investigation along the southeast side of the LDA. A total of 9 boreholes were drilled to depths of between 10 and 30 feet below ground surface. As shown in Figure 3, the boreholes were located on a line that started near the end of the existing interceptor trench and extended along the southeast side of the LDA. In summary, fill material comprised of mine spoils and CKD was encountered in most of the boreholes, and the competent bedrock needed for effective installation of the interceptor trench was not detected along this line. Shallow groundwater was encountered in most of the boreholes.

Results of the preliminary investigation indicate that the interceptor trench extension alignment would need to be moved further to the east and constructed as a separate branch, connected to the existing interceptor trench, so as to be hydraulically upgradient of the fill and CKD material, and located in an area where competent bedrock and shallow groundwater are potentially present.

#### 2.2 Proposed Field investigations

A targeted field investigation program will be performed to determine the depth to bedrock and to identify shallow groundwater flow zones in the area east of the preliminary borehole alignment. This activity will primarily involve drilling approximately 8 boreholes along or near the proposed interceptor trench extension alignment as shown on Figure 3. Figure 3 only shows the proposed location for 4 of the potential 8 boreholes included in this investigation. Following drilling of the first 4 boreholes, the additional boreholes will be located in the field in an adaptive and iterative approach. Data collected from each borehole(s) will be used to locate additional boreholes as necessary to collect data on the depth to bedrock and presence of shallow groundwater along the alignment of the proposed interceptor trench branch. Drilling will be conducted using a track-mounted sonic drill rig to provide better core recovery and less disturbance than other methods. Drilling will extend until bedrock is encountered or until 30 feet, whichever is less. Stratigraphic and groundwater data will be obtained, and if shallow groundwater is encountered, several of the holes may be completed as 2-inch diameter wells for measurement of water levels and potential additional hydraulic testing if necessary.

An investigation report will be prepared presenting the results of the field investigation and an assessment of the efficacy of adding a new branch to the existing interceptor trench. The report will be submitted to Ecology and Public Health.





#### 3.0 SCHEDULE

In January 2011, an Easement Agreement involving Site Environmental Activities (Easement) was filed on record between Reserve Silica and Holcim (Reserve 2010). The areas covered by the Easement include both the DSP and LDA, access roads, monitoring wells, and the LDA leachate seepage areas and infiltrations ponds as shown in Exhibit A. The proposed borehole investigation area is just outside of the existing easement, and Holcim and Reserve Silica are working on an agreement to include the proposed drilling in this area. Additionally, the Bonneville Power Administration (BPA) requires permitting for drilling under their power lines and the presence of a qualified "safety watcher". The BPA permit has been obtained, but the availability of the safety watcher could also affect the schedule.

We would like to obtain regulatory approval to proceed, so the field investigation could occur upon finalization of the access agreement and scheduling of the BPA safety watcher.





#### 4.0 CLOSING

The information presented in this work plan is intended solely for the purpose described herein and should not be used for any other purposes without written authorization from Golder Associates Inc.

GOLDER ASSOCIATES INC.

Frank S. Shuri

Frank S. Shuri, PE, LG, LEG Principal

FS/GLZ/sb

Gary L. Zimmerman Principal





#### 5.0 **REFERENCES**

- Golder Associates Inc. (Golder) 2013. Lower Disposal Area Hydrogeological Investigations, Ravensdale Site. Prepared for Holcim (US) Inc. June 11.
- Golder 2014. Technical Memorandum: *Ravensdale Site Groundwater and Surface Water Statistical Characterization: Arsenic Background Level Evaluation.* Prepared for Holcim (US) Inc. January 3.



TABLES

Location	Date	Time	Flow (ml/min)	Flow gpm	рΗ	Notes
Interceptor Trench	8/22/2016	11:00	312	0.08	7.8	measured with pH meter
Interceptor Trench	9/14/2016	9:15	262	0.07	8.0	measured with pH strip
Interceptor Trench	10/18/2016	12:13	7,966	2.07	7.0	measured with pH strip
Interceptor Trench	11/1/2016	14:40	8,900	2.31	8.2	measured with pH meter
Interceptor Trench	12/8/2016	11:55	8,200	2.13	7.0	measured with pH strip
Interceptor Trench	1/6/2017	9:05	5,817	1.51	7.0	measured with pH strip
Interceptor Trench	2/2/2017	9:25	7,933	2.06	7.6	measured with pH meter
Interceptor Trench	3/8/2017	12:15	10,033	2.61	7.2	measured with pH meter
Interceptor Trench	4/11/2017	8:40	5,167	1.34	7.7	measured with pH meter
Interceptor Trench	5/30/2017	15:45	4,000	1.04	7.3	measured with pH meter
						>1" rain previous day
Interceptor Trench	6/16/2017	7:38	19,333	5.03	6.9	pH measured with YSI multimeter
Interceptor Trench	7/21/2017	8:15	706	0.18	7.2	measured with pH meter
Interceptor Trench	8/18/2017	8:50	460	0.12	7.6	measured with pH meter

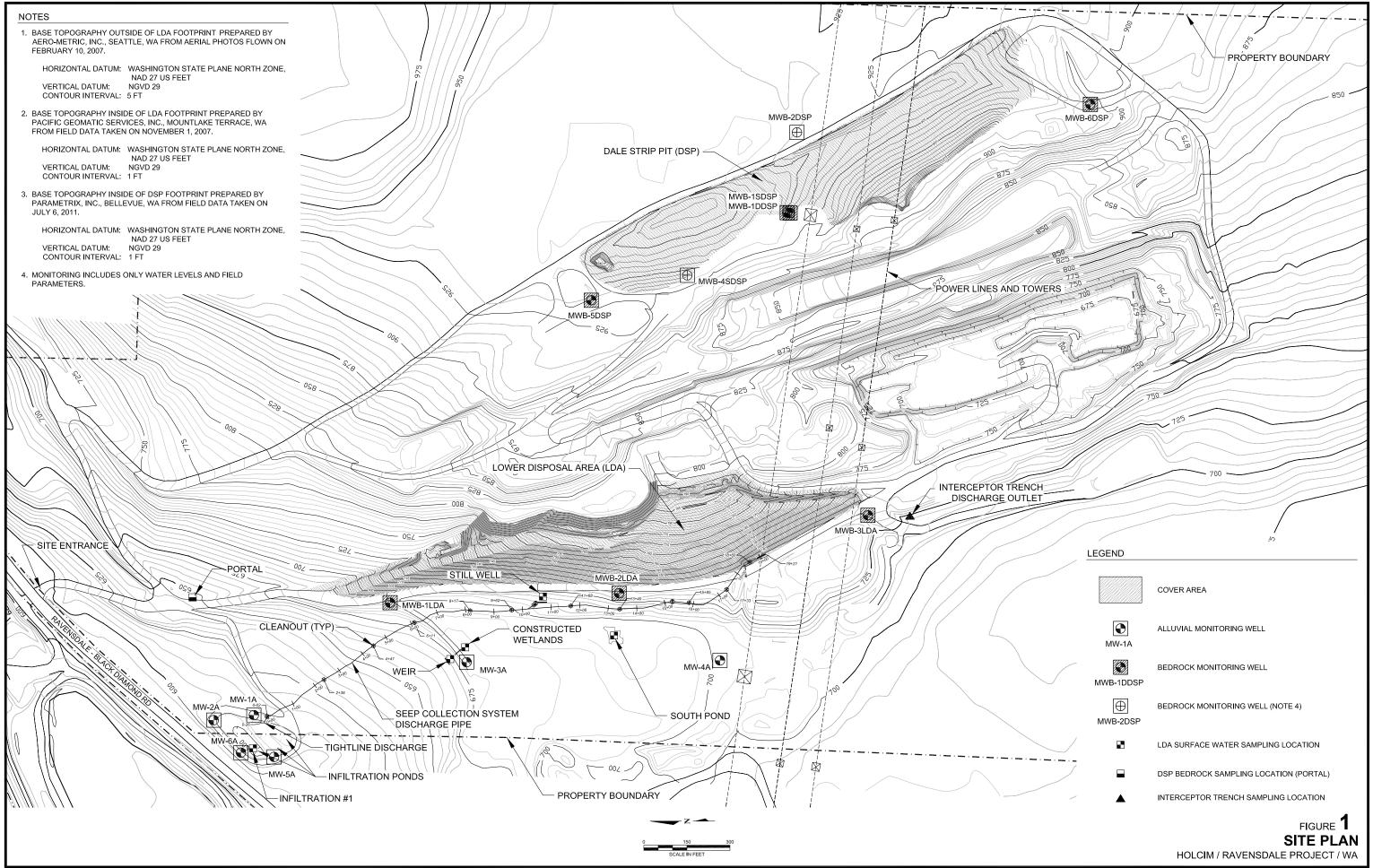
Table 1: Monthly Flow Volumes of Clean Water Diverted Around the Lower Disposal Area by the Interceptor Trench

#### Table 2: Monthly Flow Volumes of Collected Seepage Water Discharged to the Infiltration Ponds

Location	Date	Time	Flow (ml/min)	Flow gpm	рΗ	Notes
Infiltration Discharge	8/23/2016	8:50	4,400	1.1	11.8	pH from sampling location
Infiltration Discharge	9/14/2016	8:25	4,467	1.2	12.0	measured with pH strip
Infiltration Discharge	10/18/2016	12:42	8,283	2.2	11-12	measured with pH strip
Infiltration Discharge	11/1/2016	11:00	24,800	6.4	13.0	measured with pH meter
Infiltration Discharge	12/8/2016	12:10	29,000	7.5	12.0	measured with pH strip
Infiltration Discharge	1/6/2017	8:18	27,333	7.1	13.0	measured with pH strip
Infiltration Discharge	2/1/2017	8:55	17,600	4.6	13.3	measured with pH meter
Infiltration Discharge	3/8/2017	12:35	32,667	8.5	13.2	measured with pH meter
Infiltration Discharge	4/11/2017	9:05	26,000	6.8	13.2	measured with pH meter
Infiltration Discharge	5/30/2017	10:22	21,000	5.5	13.0	measured with pH meter
						>1" rain previous day
Infiltration Discharge	6/16/2017	8:00	21,133	5.5	12.7	pH measured with YSI multimeter
Infiltration Discharge	7/21/2017	8:40	5,533	1.4	12.8	measured with pH meter
Infiltration Discharge	8/17/2017	9:20	2,540	0.7	11.9	measured with pH meter

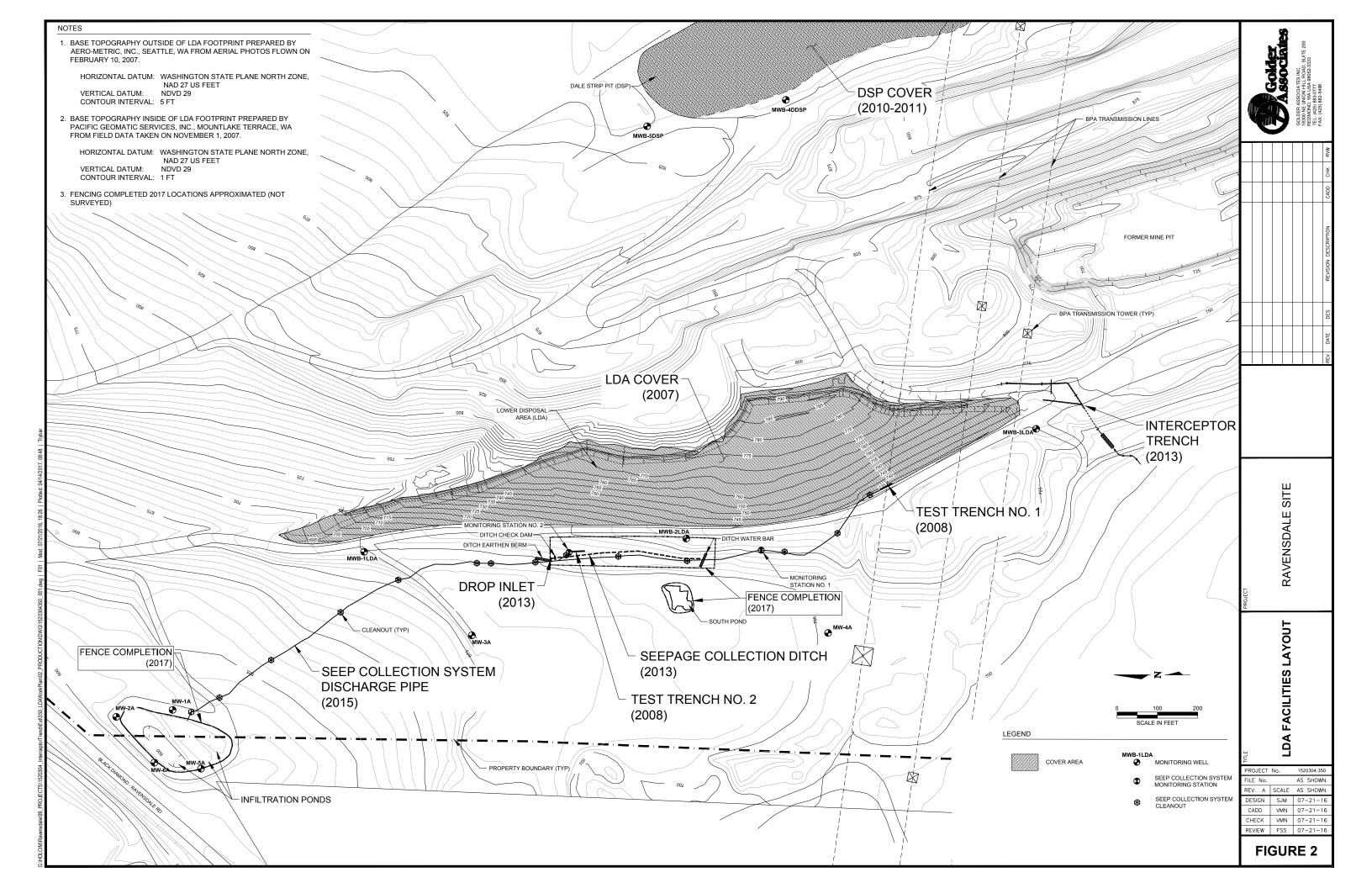


FIGURES



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**Golder Associates** 



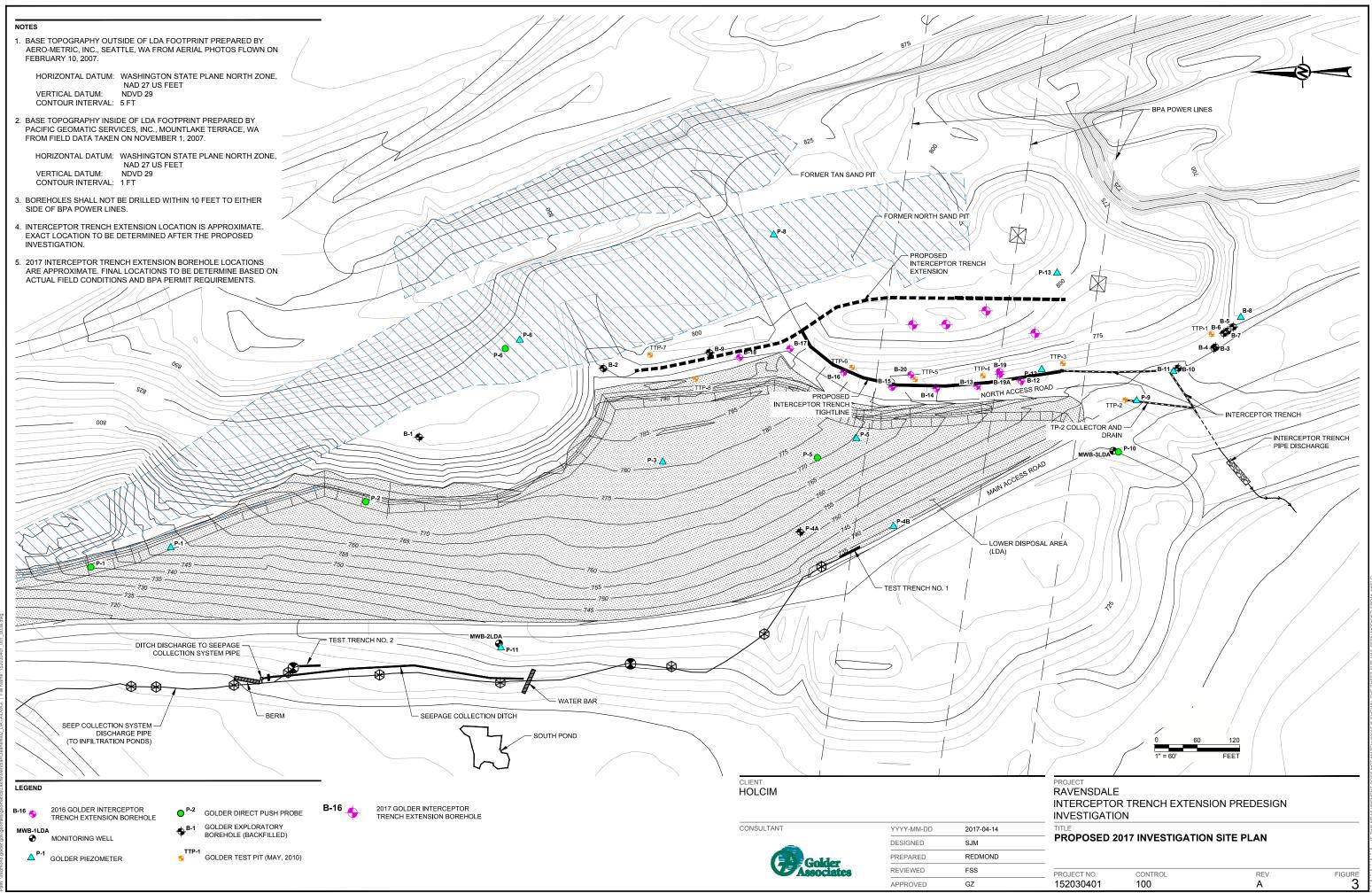
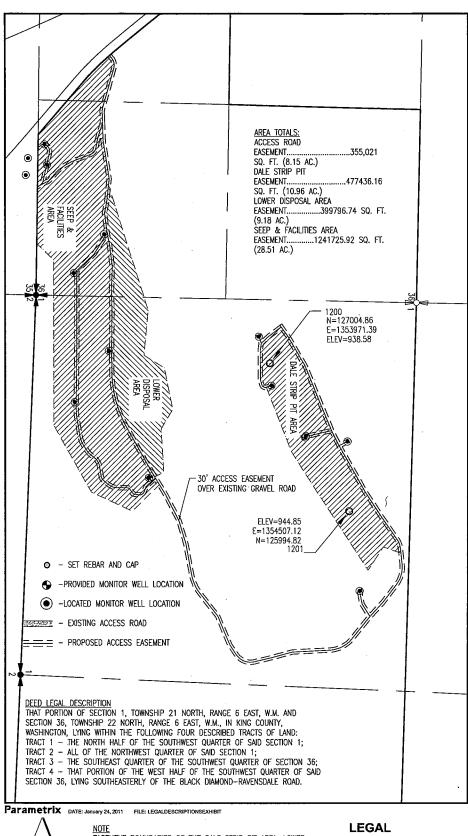


EXHIBIT A





Ν 500 1"=500

DEASEMENT BOUNDARIES OF THE DALE STRIP PIT AREA, LOWER DISPOSAL AREA, AND SEEP & FACILITIES AREA RUN ALONG THE ROAD CENTERLINE WHEN THEY ARE COINCIDENT WITH THE ACCESS ROAD EASEMENT. LEGAL DESCRIPTION EXHIBIT

EXHIBIT A: LDA LEACHATE SEEPAGE AREAS AND INFILTRATIONS PONDS Established in 1960, Golder Associates is a global, employee-owned organization that helps clients find sustainable solutions to the challenges of finite resources, energy and water supply and management, waste management, urbanization, and climate change. We provide a wide range of independent consulting, design, and construction services in our specialist areas of earth, environment, and energy. By building strong relationships and meeting the needs of clients, our people have created one of the most trusted professional services organizations in the world.

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- + 27 11 254 4800
  - + 852 2562 3658
  - + 61 3 8862 3500
  - + 356 21 42 30 20

solutions@golder.com www.golder.com

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**Golder Associates Inc.** 18300 NE Union Hill Road, Suite 200 Redmond, WA 98052 USA Tel: (425) 883-0777 Fax: (425) 882-5498

