Appendix H

Investigation-Derived Waste Management

A	NON-HAZARDOUS WASTE MANIFEST	1. Generator ID Number		2. Page 1 of	3, Ernerg	ency Response	Phone	4. Wasto Tr	acidng Nu	mber 4 Koa	1 11	· is
		ng Address The BK 5	E Partin		Generator	r's Site Address	(if different	than mailing addre	88)	1 - 102	-63,-	/
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		605 Pu Tadoma 53-571-25	(204.	JI		20	ISAV	werf Araba in	À.			
Ш							- '	U.S. EPA ID I				
	b. Iransporer i Company Nan	wivonmental	Com.	respect	7 10 d					00 300	111	
	7. Transporter 2 Company Nam	18	Jeve 18	<u></u>	<u>LFC.</u>	<u>'</u>		U.S. EPA ID I	Yumber	00 200	7 V	
		<i>.</i>										
	8. Designated Facility Name an	d Site Address Wasco 2550 - 296-4685	Countr	1 Lan	SE	W/		U.S. EPA ID I				
		2550	Street	Road				N	A.			
Ш	Facility's Phone: 540	- 296 - The	alles OR	970	18,50							
	9. Waste Shipping Name		·			10. Conta	iners	1 f. Total	12. Unit		*	
			- A -			No.	Туре	Quantity	Wt./Vol.	965-765-754-757-757-757-757-757-757-757-757-75	BARANTER VI	ivestores
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	4.										Waxa A	
	13. Special Handling Instruction	ns and Additional Information							<u>. </u>	Control of the second		
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	Tala at	a distribution	is the	. 1	<i>i</i> #							
	ALL	Project # 10 rection	, 2 3 4/5/0 1/2	oval		<i>20</i> 45	-16 -	223				
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	marked and labeled/placard	n'S CERTIFICATION: I hereby declare il led, and are in all respects in proper con								e, and are classifie	и, раскаде	30,
	Generator's/Offeror's Printed/T	yped Name	Bur	Sig	nature	.	1 0	il of	/ `	Month	Day	Year
¥	15. International Shipments	Stayton Cor Deposit to U.S.	ISNSF	er	fl.	my &		Lay f	631 1	02	5/	//
E	Transporter Signature (for expx	L. I finish to U.S.	<u>L</u>	Export from U	J.S.	Port of en	try/exit: ing U.S.:	X		*		
E.	16. Transporter Acknowledgme	ent of Receipt of Materials				2310 1941	~7a					
TRANSPORTER	Transagater 1 Printed/Typed No	121		Sig	nature 12		11	٠		Month	Day	Year
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À	17. Discrepancy					· · ·						
T	17a. Discrepancy Indication Sp	ace Quantity	Птуре			Residue		Partial Rej	ection		Full Rejecti	en 🌡
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 -	17b. Alternate Facility (or Gene	erator)			Manif	est Reference i	Number:	U,S. EPA ID I	Number `			
片	()	•				*				•		
¥.	Facility's Phone:			.,							ь.	
ATE!	17c. Signature of Alternate Far	cility (of Generator)		i						Month 	Day 	Year
ESIGNATED FACILITY	1		**************************************	<u>l</u> Nakalas	i waaa sa		8 (8 (7 Z (1)		(E)(E)(E)			
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					ordinklik Sajakasa			是自然的意				
	18. Designated Facility Owner Pipped Name	or Operator: Certification of receipt of m	aterials covered by the r		ot es fibled majore	In Item 17a	71			Month	fluo	Year
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16	9-BLC-0 5 11977 (Rev	, 9/09)		1 /	Her	7) Designate	D FAC	ILITY TO G	ENER	TOR
		, V				•		v.				-,

A	NON-HAZARDOUS Waste Manifest	1. Generator ID Number	2. Page 1 of	3. Emergency Response	Phone	4. Waste Tr ファノ	acking Nu 7 70	wher y Lord "3
	5. Generator's Name and Mallin	ng Address The Bi	NSP Rallway,	Generator's Sile Address	s_(ii different ti	han mailing addro	ess)	
		605 1	NSFRATIWELLEN AVE.	F 1		rade t		
	Generator's Phone: 2	53 5 91 - 3	2567	١ کافئا.	SOLVA	M WA	č.	
	6. Transporter 1 Company Nam	e .	tal Services			U.S. EPA ID I		N 5 7 5 (1) 2
	7. Transporter 2 Company Nam	<u>10 lyon menl</u>	VER DENVICES	ind,		U.S. EPAID	es () () . Number	0030114
	8. Designated Facility Name and	d Sile Address Was	co County Land Strule Room Dalles, OR 970	S Fill		U.S. EPA (D)	ر	
		2550	Stude Rom	de a		NCF	*	
	Facility's Phone: 54	11-296-40	787	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~				
	9. Waste Shipping Name	and Description		10. Conta	liners Type	11. Total Quantity	12. Unit Wt./Vol.	
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	NASI 4	c connect	ORS APPRIVAL	2042	-16-	3 43		
								
			clare that the contents of this consignment a er condition for transport according to applic					e, and are classified, packaged,
	Generator's/Offeror's Printed/Ty	yped Name	BUSFAR	nature Licensel L	No.	gi. my		Month Day Year
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 - -	17b. Alternate Facility (or Gene	erator)		Manifest Reference	Number:	U.S. EPA ID I	Vumber	
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O FA	Facility's Phone:	Elist Int Cappyolo			,	1		Mostly D. V.
SIGNATED FACILITY	17c. Signature of Alternate Fac	any (or designator)	1					Monih Day Year
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Satisfanting Control	18. Designated Facility Owner	or Operator: Certification of receip	of materials covered by the manifest excer	n as noted in Henri Ta	<u> </u>		300 P. S.	
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A	NON-HAZARDOUS WASTE MANIFEST	1. Generator ID Number		2. Page 1 of 3	Emergency Response		4. Waste T			118	
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		605	Puyallus.	Koe	1 Ra	uro	ed ko	e i			
	Generator's Phone: 2.5	Car Salcas	Phyallup."	1	W E	averi	y WA.				
							U.S. EPA ID				
	7. Transporter 2 Company Nam	vivorment	el Bervic	es, Li	ic.		U.S. EPA ID	SUO Number	0030	114_	
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	8. Designated Facility Name ar	nd Site Address Was	co County	Land	Eill	* * * * * * * * * * * * * * * * * * * *	U.S. EPA ID			ì.".	
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	Facility's Phone: 54/-	296-403	co County of Steels	2 9 10	/3 &		<u> </u>		1000		
	9. Waste Shipping Nam				10. Conta	Type	11. Total Quantity	12. Unit .WI./Vol.	Ser Ser		
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	13. Special Handling Instructio	ns and Additional Information		· ·			<u></u>	<u>.</u>		- Sandara and Assessable	
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A	NON-HAZARDOUS WASTE MANIFEST	1. Generator ID Number	/	3. Emergency Response 800 - 879	9-46	4. Wasle Tr	970	nber 4 Koan	l #	1
	5. Generator's Name and Mallin Generator's Phone:	ng Addioss The BNSF 605 Pmy aller 52-591-556	Railway S Ave.		ilvoo	ian majling addre	enu	e.		
	C Transporter 1 Caranany blass	Emironmenta	l Larvices	1 Fred		U.S. EPAIDI		030	112	
	7. Transporter 2 Company Nam		Odlassa	3		U.S. EPA ID I			<u>,, </u>	
	8. Designated Facility Name on	nd Site Address Wasco	Couply hang	lfill		U.S. EPA ID N				
	Facility's Phone: 54	2550 S The Bull 11-276-4085	Sounty hang teele troad les, or 970:	58		1				
	9. Waste Shipping Name	e and Description		10. Contai No.	Туре	11. Total Quantity	12. Unit Wt./Vol.			
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	13. Special Handling Instruction	ns and Additional Information	ور پر وجہ			· · · · · ·		· · · · · · · · · · · · · · · · · · ·		
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	NAC	Truck #1	291.			*	•	•		
	marked and labeled/placare	R'S CERTIFICATION: I hereby declare that ded, and are in all respects in proper conditi	on for transport according to applica	able international and natio	onal governm	ental regulations				
V		Typed Names tay ton Ear	BKSFRA	nature Early	ζ,	Slay	Lon	Month OQ	27	Year 187
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V	18. Designated Facility Owne Print Apped Name	er or Operator: Contification of receipt of mate		ot as noted in Hem 17a		9		Month	Day).	Xear



WASTE MATERIAL PROFILE SHEET Profile No. 405184

A. GENERAL INFORMA GENERATOR EPA ID #/ GENERATOR CODE (As ADDRESS 510 W Bri CUSTOMER CODE (Ass ADDRESS 2454 Oc	REGISTRATION # ssigned by Clean Harbo dgeway Rd sligned by Clean Harbon ccidental Av South i	BN06309	CITY	MATOR NAI Wishra MER NAM Seattle	m STATE E: BNS F	PROVINCE PHONE: (56 Sea Jennifer PROVINCE	WA ZIP/POST 09) 748-3203 Wiener WA ZIP/POST		98673 98134	
B. WASTE DESCRIPTION: WASTE DESCRIPTION:	Olly waste water				•					
PROCESS GENERATING	WASTE: Was	te water impacted with pe	troleum	hydroca	rbons					
IS THIS WASTE CONTAIN	IED IN SMALL PACKA	GING CONTAINED WITHIN A L	ARGER	SHIPPING	CONTAINER? N	0				
C. PHYSICAL PROPERT	IES (at 25C or 77F)									
PHYSICAL STATE SOLID WITHOUT FR POWDER MONOLITHIC SOLID LIQUID WITH NO SO) DLIDS	NUMBER OF PHASES/LA	TQI MID	DLE	0.00 0.00 0.00	101 - 500	lif liquid present) e.g. Water) D (e.g. Motor Oil) 000 (e.g. Molasses)		OLOR deer- rown	-
LIQUID/SOLID MIXTO % FREE LIQUID % SETTLED SOLID % TOTAL SUSPENDE SLUDGE GAS/AEROSOL		ODOR INONE MILD STRONG Describe:		BOILING	S POINT °F (°C) <= 95 (<=35) 95 - 100 (35-38) 101 - 129 (38-54) >= 130 (>54)	1,40-	·	1	GANIC = 1% -9% = 10%	
FLASH POINT °F (°C) pH SPECIFIC GRAVITY ASH < 73 (<23) <=2 < 0.8 (e.g. Gasoline) < 0.1 > 20 < 2,000 (<4.6) 73 - 100 (23-38) 2.1 - 6.9 0.8-1.0 (e.g. Ethanol) 0.1 - 1.0 Unknown 101 - 140 (38-60) 7 (Neutral) 1.0 (e.g. Water) 1.1 - 5.0 141 - 200 (60-93) 7.1 - 12.4 1.0-1.2 (e.g. Antifreeze) 5.1 - 20.0 > 200 (>93) >= 12.5 > 1.2 (e.g. Methylene Chloride) Ash BTU/LB (MJ/kg)									e)	
D. COMPOSITION (List to	he complete composition	on of the waste, include any iner	t compor	ents and/o	r debris. Renges for	individuai comp	onents are acceptabl	e. If a trade	name is used	,
CHEMICAL OIL WATER							MIN - 0.0000000 - 100.0000000 -	1.0000		• •
DOES THIS WASTE CON >12" LONG, METAL REINI PIECES OF CONCRETE >	FORCED HOSE >12° L	IGE METAL DEBRIS OR OTHE ONG, METAL WIRE >12" LONG	R LARG 3, META	E OBJECT L VALVES,	S (EX., METAL PLA PIPE FITTINGS, CO	TE OR PIPING: DNCRETE REIN	>1/4° THICK OR IFORCING BAR OR	YES	NO	
if yes, describe, inclu	•	,								
DOES THIS WASTE COM	NTAIN ANY METALS IN	POWDERED OR OTHER FIN	ELY DIV	DED FOR	M ?			YES	☑ NO	
DOES THIS WASTE COI FLUIDS, MICROBIOLOG POTENTIALLY INFECTION	IICAL WASTE, PATHOI	ITACTED ANY OF THE FOLLO LOGICAL WASTE, HUMAN OR	WING; A ANIMAL	NIMAL WA DERIVED	ASTES, HUMAN BLC SERUMS OR PROT	OOD, BLOOD PI EINS OR ANY	RODUCTS, BODY OTHER	YES	₩ NO	
		ther infectious nor does it conta lect the answer below that appli		ganism kno	own to be a threat to I	numan health. 1	This certification is			
	r exposed to potentially							YES	NO	
Chemical disinfection	or some other form of	sterilization has been applied to	the was	te.				YES	NO	
I ACKNOWLEDGE THAT	THIS PROFILE MEETS	THE CLEAN HARBORS BATT	TERY PA	CKAGING	REQUIREMENTS.			YES	NO	
LACKNOWLEDGE THAT	MY FRIABLE ASBEST	OS WASTE IS DOUBLE BAGG	ED AND	WETTED.				YES	NO	
SPECIFY THE SOURCE (WASTE.	CODE ASSOCIATED W	/ITH THE G15		SPEC	DIFY THE FORM CO	DE ASSOCIATE	ED WITH THE WAST	TE. W219		



Profile No. 405184

Testing

The Responsible Solution

Are these values based on testing or knowledge?

•	CON	100	-	-	-

Please indicate which constituents below apply. Concentrations must be entered whon applicable to assist in accurate review and expedited approval of your waste profile. Please note that the total regulated metals and other constituents sections require answers. RCRA REGULATED METALS REGULATORY TCLP TOTAL UOM NOT APPLICABLE	if based of (MSDS) v	n knowledge, please describe in deta then applicable. Include the chemical	il, the rationale applied to or trade-name represen	ldentify and chi led by the MSD	aracterize the waste material. If S, and or detailed process or op	Please include n eraling procedu	eference to Material Safe res which generate the w	ty Data Sheels aste.
## PROPRIATE OF YOUR WESSE profile. Please note that the total regulated metals and other constituents sections require answers. ### PROFILE OR ### PROFIL	بالأحسان والمستنيخ							
DOM	Please in approva	ndicate which constituents belo i of your waste profile. Please r	ow apply. Concentration that the total rep	itions must b gulated metal	e entered when applicable s and other constituents s	to assist in a sections requ	accurate review and ire answers.	expedited
Decision	RCRA	REGULATED METALS			TOTAL	UOM I		
CADBUM 10	D004	ARSENIC	5.0					
LOCATION CONTROL CO	D005	BARIUM	100.0				V	
LEAC LEAC LEAC CO CO CO CO CO CO CO	D006	CADMIUM	1.0	,				
MERCHY	D007	CHROMIUM	5,0					
SILVER 5.0 OTHER CONSTITUENTS MAX	D008	LEAD	5.0					
VOLATILE COMPOUNDS	D009	MERCURY	0.2				Ø	
VOLATILE COMPOUNDS	D010	SELENIUM	1.0				V	
D019	D011	SILVER	5.0				<u> </u>	
DB19 CARSON TETRACH-LORIDE 0.5 BROMINE		VOLATILE COMPOUNDS			OTHER CONSTITUENTS		MAX UOM	NOT
D021 CHLOROSENZÈNE 100.0	D018	BENZENE	0.5		·			
DO22	D019	CARBON TETRACHLORIDE	0.5		BROMINE			
1,2-DicHLOROETHYLENE 0.5 SULPR	D021	CHLOROBENZENE	100.0		CHLORINE			
1,1-DicHLOROETHYLENE 0.7 SULFUR	D022	CHLOROFORM	6.0					<u> </u>
D035 METHYLETHYL KETONE 200.0 POTASSIUM	D028	1,2-DICHLOROETHANE	0.5		~~~~~~~~~~~~~~			<u>\</u>
D039 TETRACHLOROETHYLENE 0.7 SODIUM	D029	1,1-DICHLOROETHYLENE	0.7		********	** * * * * * * * * * *		
DD40	D035	METHYL ETHYL KETONE	200.0					
D033	D039	TETRACHLOROETHYLENE	0.7			-, .		
SEMI-VOLATILE COMPOUNDS	D040	TRICHLOROETHYLENE	0.5		AMMONIA			
D023 O-CRESOL 200.0 CYANDE TOTAL	D043	VINYL CHLORIDE	0.2					
D024 m-CRESOL 200.0 SULFIDE REACTIVE		SEMI-VOLATILE COMPOUND	S					
D025	D023	o-CRESOL	200.0					
D026 CRESOL (TOTAL)	D024	m-CRESOL	200.0	•••••	SULFIDE REACTIVE			<u></u>
DO27	D025	p-CRESOL	200.0		HOCs		PCBs	
D027	D026	CRESOL (TOTAL)	200.0		MONE		NONE	
D030 2,4-DINITROTOLUENE 0.13 >= 1000 PPM >=50 PPM FCBS ARE PRESENT, IS THE WASTE REGULATED BY TSCA 40 CFR 7817 YES	D027	1,4-DICHLOROBENZENE	7.5		ļ 		1—	
D033	D030	2,4-DINITROTOLUENE	0.13					
D034 HEXACHLOROBUTADIENE 0.5 WASTER REGULATED BY TSCA 40 CFR 7617 D034 HEXACHLOROBUTANE 3.0 YES ✓ NO D036 NITROBENZENE 2.0 YES ✓ NO D037 PENTACHLOROPHENOL 100.0 D038 PYRIDINE 5.0 D041 2,4,5-TRICHLOROPHENOL 400.0 D042 2,4,6-TRICHLOROPHENOL 2.0 PESTICIDES AND HERBICIDES D012 ENDRIN 0.02 D013 LINDANE 0.4 D014 METHOXYCHLOR 10.0 D015 TOXAPHENE 0.5 D016 2,4-D 10.0 D017 2,4-5-TP (SILVEX) 1.0 D020 CHLORDANE 0.03 D031 HEPTACHLOR (AND ITS EPOXIDE) 0.008 ADDITIONAL HAZARDS D055 THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES ✓ NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING CSHA REGULATED CARCINOGENS	D032	HEXACHLOROBENZENE	0.13				IF PCBS ARE PRESE	NT. IS THE
D036 HEXACHORGE HAVE 3.0 YES	D033	HEXACHLOROBUTADIENE	0.5	****			WASTE REGULATED	BY TSCA 40
D037 PENTACHLOROPHENOL 100.0	D034	HEXACHLOROETHANE	3.0				1 _	_
D038 PYRIDINE 5.0 D041 2,4,5-TRICHLOROPHENOL 400.0 D042 2,4,6-TRICHLOROPHENOL 2.0 PESTICIDES AND HERBICIDES D012 ENDRIN 0.02 D013 LINDANE 0.4 D014 METHOXYCHLOR 10.0 D015 TOXAPHENE 0.5 D016 2,4-D 10.0 D017 2,4,5-TP (SILVEX) 1.0 D020 CHLORDANE 0.03 D031 HEPTACHLOR (AND ITS EPOXIDE) 0.008 ADDITIONAL HAZARDS D0ES THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	D036	NITROBENZENE	2.0		t		YES	NO
D041 2,4,5-TRICHLOROPHENOL 400.0	D037	PENTACHLOROPHENOL	100.0	********				
D042 2.4,6-TRICHLOROPHENOL 2.0	D038	PYRIDINE						
PESTICIDES AND HERBICIDES D012 ENDRIN 0.02 D013 LINDANE 0.4 D014 METHOXYCHLOR 10.0 D015 TOXAPHENE 0.5 D016 2,4-D 10.0 D017 2,4,5-TP (SILVEX) 1.0 D020 CHLORDANE 0.03 D031 HEPTACHLOR (AND ITS EPOXIDE) 0.008 ABDITIONAL HAZARDS D0ES THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES ☑ NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	D041							
D012 ENDRIN 0.02 D013 LINDANE 0.4 D014 METHOXYCHLOR 10.0 D015 TOXAPHENE 0.5 D016 2,4-D 10.0 D017 2,4,5-TP (SILVEX) 1.0 D020 CHLORDANE 0.03 D031 HEPTACHLOR (AND ITS EPOXIDE) 0.008 ADDITIONAL HAZARDS D0ES THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES ✓ NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	D042	2,4,6-TRICHLOROPHENOL	2.0					
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D017 2.4.5-TP (SILVEX) 1.0 D020 CHLORDANE 0.03 D031 HEPTACHLOR (AND ITS EPOXIDE) 0.008 ADDITIONAL HAZARDS D0ES THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	D015	TOXAPHENE						
D020 CHLORDANE 0.03 D031 HEPTACHLOR (AND ITS EPOXIDE) 0.008 ADDITIONAL HAZARDS D055 THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	D016	2,4·D		*****				
D031 HEPTACHLOR (AND ITS EPOXIDE) 0.008 ADDITIONAL HAZARDS DOES THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES V NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	D017	2,4,5-TP (SILVEX)						
ADDITIONAL HAZARDS DOES THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES V NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS		*****************						
DOES THIS WASTE HAVE ANY UNDISCLOSED HAZARDS OR PRIOR INCIDENTS ASSOCIATED WITH IT, WHICH COULD AFFECT THE WAY IT SHOULD BE HANDLED? YES V NO (If yes, explain) CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	D031	HEPTACHLOR (AND ITS EPOXIDE	0.008					
CHOOSE ALL THAT APPLY DEA REGULATED SUBSTANCES EXPLOSIVE FUMING OSHA REGULATED CARCINOGENS	ADDIT	IONAL HAZARDS HIS WASTE HAVE ANY UNDISCLOSE	ED HAZARDS OR PRIO	R INCIDENTS A	SSOCIATED WITH IT, WHICH	COULD AFFEC	T THE WAY IT SHOULD	8E HANDLED?
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	CHOO	SE ALL THAT APPLY						
POLYMERIZABLE RADIOACTIVE REACTIVE MATERIAL V NONE OF THE ABOVE	DEA	REGULATED SUBSTANCES	EXPLOSIVE		FUMING		OSHA REGULAT	ED CARCINOGENS
	POL	YMERIZABLE	RADIOACTIVE		REACTIVE MATERI	AL	MONE OF THE A	BOVE



Profil	a N	lo.	40	51	84

F. RE	GULAT	ORY	STATE	us	ratus .	
	YES	V	NQ	USEPA HAZARDOUS WASTE?	VO USEPA HAZARDOUS WASTE?	
	YES	V	NO	DO ANY STATE WASTE CODES APPLY?	DO ANY STATE WASTE CODES APPLY?	 -
				Texas Wasle Code OUTS6091	Texas Waste Code OUTS6091	\dashv
	YES	V	NO	DO ANY CANADIAN PROVINCIAL WASTE CODES APPLY?		
	YES		NO	IS THIS WASTE PROHIBITED FROM LAND DISPOSAL WITHOUT FURTHER TREATMENT PER 40 CFR PART 268?	IO IS THIS WASTE PROHIBITED FROM LAND DISPOSAL WITHOUT FURTHER TREATMENT PER 40 CFR PART 268?	<u> </u>
				LDR CATEGORY: VARIANCE INFO: Not subject to LDR		_
	YES	4	NO	IS THIS A UNIVERSAL WASTE?	10 IS THIS A UNIVERSAL WASTE?	
V	YES		NO	IS THE GENERATOR OF THE WASTE CLASSIFIED AS CONDITIONALLY EXEMPT SMALL QUANTITY GENERATOR (CESQG)?	IO IS THE GENERATOR OF THE WASTE CLASSIFIED AS CONDITIONALLY EXEMPT SMALL QUANTITY GENERATOR (CESQG)?	
	YES		NO	IS THIS MATERIAL GOING TO BE MANAGED AS A RCRA EXEMPT COMMERCIAL PRODUCT, WHICH IS FUEL (40 CFR 261.2 (C)(2)(II))?	IO IS THIS MATERIAL GOING TO BE MANAGED AS A RCRA EXEMPT COMMERCIAL PRODUCT, WHICH IS FUEL (40 CFR 261.2 (C)(2)(II))?	
	YES		NO	DOES TREATMENT OF THIS WASTE GENERATE A F006 OR F019 SLUDGE?	40 DOES TREATMENT OF THIS WASTE GENERATE A FO06 OR F019 SLUDGE?	
	YES	_	NO	IS THIS WASTE STREAM SUBJECT TO THE INORGANIC METAL BEARING WASTE PROHIBITION FOUND AT 40 CFR 268.3(C)?	IO IS THIS WASTE STREAM SUBJECT TO THE INORGANIC METAL BEARING WASTE PROHIBITION FOUND AT 40 CFR 268.3(C)?	
	YES	V	NO	DOES THIS WASTE CONTAIN VOC'S IN CONCENTRATIONS >=500 PPM?	IO DOES THIS WASTE CONTAIN VOC'S IN CONCENTRATIONS >=500 PPM?	
	YE\$		NO	DOES THE WASTE CONTAIN GREATER THAN 20% OF ORGANIC CONSTITUENTS WITH A VAPOR PRESSURE >= .3KPA (.044 PSIA)?	IO DOES THE WASTE CONTAIN GREATER THAN 20% OF ORGANIC CONSTITUENTS WITH A VAPOR PRESSURE >= .3KPA (.044 PSIA)?	
	YES	V	NO	DOES THIS WASTE CONTAIN AN ORGANIC CONSTITUENT WHICH IN ITS PURE FORM HAS A VAPOR PRESSURE > 77 KPA (11.2 PSIA)?	IO DOES THIS WASTE CONTAIN AN ORGANIC CONSTITUENT WHICH IN ITS PURE FORM HAS A VAPOR PRESSURE > 77 KPA (11.2 PSIA)?	
	YES	V	NO	IS THIS CERCLA REGULATED (SUPERFUND) WASTE?	IO IS THIS CERCLA REGULATED (SUPERFUND) WASTE?	
	YES		NO	IS THE WASTE SUBJECT TO ONE OF THE FOLLOWING NESHAP RULES?	IO IS THE WASTE SUBJECT TO ONE OF THE FOLLOWING NESHAP RULES?	
				Hazardous Organic NESHAP (HON) rule (subpart G) Pharmaceuticals production (subpart GGG)	Hazardous Organic NESHAP (HON) rule (subpart G) Pharmaceuticals production (subpart GGG)	
	YES		NO	IF THIS IS A US EPA HAZARDOUS WASTE, DOES THIS WASTE STREAM CONTAIN BENZENE?	IO IF THIS IS A US EPA HAZARDOUS WASTE, DOES THIS WASTE STREAM CONTAIN BENZENE?	
		YES		NO Does the waste stream come from a facility with one of the SIC codes listed under benzene NESHAP or is this waste regulated under the benzene NESHAP rules because the original source of the waste is from a chemical manufacturing, coke by-product recovery, or petroleum refinery process?	NO Does the waste stream come from a facility with one of the SIC codes listed under benzene NESHAP or is this waste regulated under the benzene NESHAP or is this waste regulated under the benzene NESHAP or is the waste be original source of the waste is from a chemical manufacturing, coke by product recovery, or petroleum refinery pro-	ne ess?
		YES		NO Is the generating source of this waste stream a facility with Total Annual Benzene (TAB) >10 Mg/year?		
		Wha	t is the	TAB quantity for your facility? Megagram/year (1 Mg = 2,200 lbs)	s the TAB quantity for your facility? Megagram/year (1 Mg = 2,200 lbs)	
		The	basis f	or this determination is: Knowledge of the Waste Or Test Data Knowledge Testing	asis for this determination is: Knowledge of the Waste Or Test Data Knowledge Testing	
		Desc	cribe Ih	le knowledge :	be the knowledge:	
e	. DOT/T	DG II	IFORN	MATION	ORMATION	
DOT	T/TDG P	ROPE	R SH	PPING NAME:	SHIPPING NAME:	
	NON	DO	REG	GULATED MATERIAL, (OILY WASTE WATER)	REGULATED MATERIAL, (OILY WASTE WATER)	
					ION REQUIREMENTS ENT FREQUENCY 🗹 ONE TIME WEEKLY MONTHLY QUARTERLY YEARLY OTHER	
		¥	CO	NTAINERIZED BULK SOLID BULK SOLID	CONTAINERIZED BULK SOLID BULK SOLID	
				GALLONS/SHIPMENT: O'MIN -O MAX GAL. SHIPMENT COM: TON TARD	O'TE O'TE IN THE O	RD
	RAGE C ITAINER	TYP	Ξ:	TONS/YARDS/SHIPMENT: <u>O Min - O Max</u>	TONS/YARDS/SHIPMENT: <u>O Min - O Max</u>	
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	OTHE	C YARO ER.	POX	DRUM SIZE: 55		
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GEN	ERATOR	S CE	RTIFICA	TION	IFICATION	
sem	ples subm	sitted a	re repre	to execute this document as an authorized agent. I hereby certify that all information submitted in this and attached documents is correct to the best of my knowledge. I also certify that an sentiative of the actual waste. If Clean Herbors discovers a discrepancy during the approval process, Generator grants Clean Harbors the authority to amend the profite, as Clean Harbors the discrepancy.	rized to execute this document as an authorized agent. I hereby certify that all information submitted in this and attached documents is correct to the best of my knowledge. I also certify it representative of the actual waste. If Clean Herbors discovers a discrepancy during the approval process, Generator grants Clean Harbors the authority to amend the profite, as Clean Harbors. The authority to amend the profite, as Clean Harbors.	at any rbors
	AUT	HOR	ZED S	Prom Bulturen of Connected Innie Concultante	ED SIGNATURE NAME (PRINT) TITLE DATE Rvan Hultgren of Kennedy/Jenks Consultants Date State Stat	
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RMO FI The Responsible Soli	ution		sdale, Az		3			ect: 405-			****		FOR SERVICE CA	LL	BF	RANCH	H MAN	NAGER		DO	C. EXP			DULED E WEE		RRITORY	REFI NU	ERENCE IMBER	
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VIOUS				9				9) T			MA	NIFEST	CODE SEQ		00	001	1		100		- up.ar u1101)	an imple	VISA		TOTAL I		HE AREA BEI	LOW	
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BNSF Wishram RIWP Addendum Soil and Water IDW

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Lustomer Name D.EAFWATEREN . LEARWATER ENVIR Corrier clear water envir UNIVERSE 18 Payagnt Type tradit been be Colltaine Manual Tiches# Hauryna Trokesë Charle # Pailing # 400/1886 113981MA (LADY - Evel Dil Impacked Soil Debris

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1071 1 111

Consumer Comments? We want to know. Please vall.

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Special Mise Each-	13/10	(III) Eac			1968 75 156,95	

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2 of 18 Wentchez Total Tax 16 Wighnan

Total Labor Hours

CLEARWATER ENV	CLEARWATER ENVIRONMENTAL SERVICES, Inc					D	aily Activity
Date: 12/11/201	8 Project #:	5573	Site Work I	Description	:	Wishram, WA	IDW Water
Purchase Order#							
tact: Shane De	gross		Company:		BNSF		
		PM		lan Tally			
	_	Super					
	= 2	Oper Tech					
	- •	10011					
Safety Eq	eeting et up / Daily I uipment Che tion Work Ins	ck	x X X				
0600 Loadout							
0730 Head t <mark>o Wishram, W/</mark> 0900 <mark>Onsite, loadup 8 55g</mark> :		ator					
1015 Drive yard to check f							
1030 Head back to office							
1200 Lunch							
1330 End of day							
EMPLOYEE NAME	START	END	LUNCH	STRAIGHT	OVER	TOTAL	
	TIME	TIME	HOURS	TIME	TIME	HOURS	
lan Tally	600	1330	0.5			7	
Ari Andra	de 630	1330	0.5			6.5	
	-						

13.5

Total Labor Hours

	ENVIRONMENTAL					<i>Da</i>	ily Activity L
Date: 12.12.18	Project #:	5573	Site Work I	Description	n:	IDW Water	
Purchase Order #		8					
tact: Ryan Hibbs S	icott Mcdonalo	,	Company:	BNSF Wis	hram		-
		PM					
		Super	-				
		Oper Tech	-				
Facility Safety	Meeting y Set up / Daily Ins Equipment Check ruction Work Inspe		X X X				
0600 loaded up from sl 0900 arrived t <mark>o wisham</mark>	hop, pre trip insp	rection, f	uel and left	to wishrar	n er in soft ar	ound	
1400 left wishram	, otalioa loadilig	10 01 0111	o or oon, 1 p	po, i wate	i iii ooit gi	Julia	
1600 arrived back to sho	op .						
6							
EMPLOYEE NAME	START	END	LUNCH	DRIVE	OVER	TOTAL	
	TIME	TIME	HOURS	TIME	TIME	HOURS	
		1600	0.5	4		0.5	
	600	1600				9.5	
	700	1600	0.5	4		8.5	
Ari Andrade Ryan Munson							

18

CLEARWATER ENVIRONMENTAL SERVICES, Inc

Total Labor Hours

Daily Activity Log

Date:	12/17/2018	Project #:	5573	Site Work [Description	1:	Wishram, WA Solidification	IDW Water
Purchase Order	#		8				Condition	
tact:	Scott Mcdor	nald		Company:		BNSF		
			PM		lan Tally			
			Super					
			Oper					
			Tech					
	Safety Meeti Facility Set	up / Daily li		X X X				
	Constructio			X				
	JOHOLI GOLIO		Poolion	لكا	į			
0600 Start solidi	fication of W	ishram IDV	V Water D	Ms				
	ifyed by end		· vialei D	1113				
1430 End of day		or day						
1-00 Ella ol uay								
EMBLOVEE	T	0745-	ENE	Line	070415115	0.455	7074	
EMPLOYEE NAME		START TIME	END TIME	LUNCH HOURS	STRAIGHT TIME	OVER TIME	TOTAL HOURS	
	lan Tally	600	1200	0.5	LIME	THALE	5.5	
	Ari Andrade	600	1430	0.5			8	
	Drake Repp		1430	0.5			8	
	Ryan Munso		1430	0			2.5	
				-		-	+	

24

Total Labor Hours

Date: 12.18.18	Project #:	5573	Site Work	Description:		idw water solic	lification
Purchase Order#	-						
tact: scott-alexand	der Mcdonald		Company:	BNSF Wish	ram		
		PM					
		Super	_				
		Oper	_				
		Tech	-				
			-	-			
Safet	ty Meeting		X				
Facili	ity Set up / Daily Ins		X				
	ty Equipment Check		X_				
Cons	struction Work Inspe	ection	X_				
930 started solidifica	ation process						
1100 made dump run	to hillsboro						
300 returned from land							
EMPLOYEE NAME	START	END	LUNCH	STRAIGHT	OVER	TOTAL	
	TIME	TIME	HOURS	TIME	TIME	HOURS	
Ari Andrade	930	1530	0.5			5.5	
Ryan Munson	930	1500	0.5			5	
an Tally	1030	1430	0.5			3.5	
Drake Repp	1030	1500	0.5			4	
		1					
				_			





Requested Facility: Chemical Waste Management (Hazardous Waste Multiple Generator Locations (Attach Locations) Request Certifications	The second secon	
A. GENERATOR INFORMATION (MATERIAL ORIGIN)	B. BILLING INFORMATION SAME	AS GENERATOR
1. Generator Name: BNSF Railway	1. Billing Name: BNSF Railway	
2. Site Address: 1 Railroad Avenue	2. Billing Address:605 Puyallup Avenue	
(City, State, ZIP) Wishram WA 98673	(City, State, ZIP) Tacoma WA 98421	
3. County: Klickitat	3. Contact Name: Shane DeGross	
4. Contact Name: Shane DeGross	4. Email: Shane.Degross@BNSF.com	
5. Email: Shane.Degross@BNSF.com	5. Phone: <u>(253)</u> 591-2567 6. Fax:	
6. Phone: <u>(253) 591-2567</u> 7. Fax:		☐ Yes ☑ No
8. Generator EPA ID: N/A	8. P.O. Number:	Ties Ties
9. State ID: 1 N/A	9. Payment Method:	redit Card
C. MATERIAL INFORMATION	D. REGULATORY INFORMATION	
1. Common Name: STAB01 - LNAPL Remediation Waste		☐ Yes* ☑ No
Describe Process Generating Material:	Code:	
Vacuum removal of diesel and oil range petroleum hydrocarbons (LNAPL) from three onsite monitoring wells.	Code: <u>x004</u>	Yes No
	3. Is this material non-hazardous due to Treatment, Delisting, or an Exclusion?	☐ Yes* ☑ No
2. Material Composition and Contaminants:	contains crearing ing recar code contained	☐ Yes* ☑ No
1. Diesel and Oil Range Petroleum Hydrocarbon 95-100 %		☐ Yes* ☐ No
2. Groundwater 0-5 %	,	☐ Yes* ☐ No
3.		☑ Yes* ☐ No
4.	8. NRC or State-regulated radioactive or NORM waste?	
Total comp. must be equal to or greater than 100% ≥100%	*If Yes, see Addendum (page 2) for additional question	-
3. State Waste Codes:	9. Contains PCBs? → If Yes, answer a, b and c.	☐ Yes ☑ No
4. Color: Various	a. Regulated by 40 CFR 761?	Yes No
5. Physical State at 70°F: ☐ Solid ☐ Liquid ☐ Other:	b. Remediation under 40 CFR 761.61 (a)?	Yes No
6. Free Liquid Range Percentage: 99 to 100 N/A		☐ Yes ☐ No
7. pH:toto	 Regulated and/or Untreated Medical/Infectious Waste? 	☐ Yes ☑ No
8. Strong Odor: Yes No Describe: petroleum hydrocarbon	11. Contains Asbestos?	☐ Yes ☑ No
9. Flash Point: □ <140°F ☑ 140°−199°F □ ≥200° □ N/A	→ If Yes: □ Non-Friable □ Non-Friable - Regulat	
E. ANALYTICAL AND OTHER REPRESENTATIVE INFORMATION	F. SHIPPING AND DOT INFORMATION	
1. Analytical attached ☑ Yes	One-Time Event □ Repeat Event/Ongoing Busine	155
Please identify applicable samples and/or lab reports:	Estimated Quantity/Unit of Measure: 1000	33
All samples in the analytical report are representative of the LNAPL	☐ Tons ☐ Yards ☐ Drums ☑ Gallons ☐ Other:	
waste.	Container Type and Size: <u>Tanker Truck</u>	
	4. USDOT Proper Shipping Name:	☑ N/A
2. Other information attached (such as MSDS)?	4. 03DOT FTOPEL SHIPPING Name.	——————————————————————————————————————
G. GENERATOR CERTIFICATION (PLEASE READ AND CERTIFY BY SIGNATURE) By signing this EZ Profile™ form, I hereby certify that all information submitted in this and all relevant information necessary for proper material characterization and to identify known from a sample that is representative as defined in 40 CFR 261 – Appendix 1 or by using a in the process or new analytical) will be identified by the Generator and be disclosed to Will I am an agent signing on behalf of the Generator, I have confirmed with the Generator that information contained in this Profile is accurate and complete.	wn and suspected hazards has been provided. Any analytical data attacl n equivalent method. All changes occurring in the character of the mate	hed was derived erial (i.e., changes
Name (Print): SHANE DEGROSS Date: 07/10/2019	Shane DeGross	
Title: Manager Environmental Remediation	2111110 2071000	

Company: BNSF Railway



EZ Profile™ Addendum

Profile Number: OR342506



Only complete this Addendum if prompted by responses on EZ Profile™ (page 1) or to provide additional information. Sections and question numbers correspond to EZ Profile™.

EZ Profile™.			
C. MATERIAL INFORMATION Describe Process Generating Material (Continued from page 1):	If more space is needed, please attach a	additional r	nanes
beschibe trocess deficituting Material (continued from page 1).	ii more space is needed, prease actually	radicional p	ouges
Material Composition and Contaminants (Continued from page 1):	If more space is needed, please attach a	additional r	2000
5.	ii more space is needed, pieuse detaeri	zaarcionai p	Juges
6.			
7.			
8.			
9.			
Total co	omposition must be equal to or greater than 100%	≥1009	%
D. REGULATORY INFORMATION			
Only questions with a "Yes" response in Section D on the EZ Profile™ fo	orm (page 1) need to be answered here.		
1. EPA Hazardous Waste			
a. Please list all USEPA listed and characteristic waste code numbers:			
b. Is the material subject to the Alternative Debris standards (40 CFR 268.4	l5)?	☐ Yes	
c. Is the material subject to the Alternative Soil standards (40 CFR 268.49)		Yes	□ N
d. Is the material exempt from Subpart CC Controls (40 CFR 264.1083)?		Yes	
→ If Yes, please check one of the following:			
☐ Waste meets LDR or treatment exemptions for organics (40 CFR 2			
☐ Waste contains VOCs that average <500 ppmw (CFR 264.1082(c	:)(1)) – will require annual update.		
2. State Hazardous Waste → Please list all state waste codes:			
3. For material that is Treated, Delisted, or Excluded $ ightarrow$ Please indicate the cat			
☐ Delisted Hazardous Waste ☐ Excluded Waste under 40 CFR 2			
	s Waste \rightarrow If checked, complete question 4.		
4. Underlying Hazardous Constituents → Please list all Underlying Hazardous	Constituents:		
5. Industries regulated under Benzene NESHAP include petroleum refineries, chem			
a. Are you a TSDF? \rightarrow If yes, please complete Benzene NESHAP questionna	aire. If not, continue.	Yes	
b. Does this material contain benzene?		Yes	
1. If yes, what is the flow weighted average concentration?			opmv
c. What is your facility's current total annual benzene quantity in Megagram	s?	-	
d. Is this waste soil from a remediation?		Yes	
1. If yes, what is the benzene concentration in remediation waste?			opmv
e. Does the waste contain >10% water/moisture?		☐ Yes	
f. Has material been treated to remove 99% of the benzene or to achieve <	TO ppmw?	☐ Yes	
g. Is material exempt from controls in accordance with 40 CFR 61.342?		☐ Yes	U N
→ If yes, specify exemption:	b aliana Abak Abia na aka akasana ia ankia ak ka		
h. Based on your knowledge of your waste and the BWON regulations, do yo	ou believe that this waste stream is subject to	☐ Yes	
treatment and control requirements at an off-site TSDF? 6. 40 CFR 63 GGGGG → Does the material contain <500 ppmw VOHAPs at the contain <500 ppmw VOHAPs at t	the point of determination?	☐ Yes	
7. CERCLA or State-Mandated clean up \rightarrow Please submit the Record of Decisio	•		
the evaluation for proper disposal. A "Determination of Acceptability" may be			
8. NRC or state regulated radioactive or NORM Waste → Please identify Isoto		.,	



Hazardous WAM Approval

Requested Management Facility: Chemical Waste Management (Hazardous Waste Facility)

Profile Number: OR342506	Waste Approval Expiration Date: 07/17/2020
APPROVAL DETAILS	
Hazardous Classification: State Hazardous	Profile Renewal: 🔲 Yes 🇹 No
Management Method: Solidification/Liquifix	
Generator Name: BNSF Railway	
Material Name: STAB01 - LNAPL Remediation Waste	
Management Facility Precautions, Special Handling Procedures or Limitation	on on approval:
Generator Conditions	
 An EPA form 8700-22 must be used for all hazardous ship your TSC. 	ments and may be ordered from an authorized vendor or
- Approval number must accompany shipment.	
- Drummed waste must be marked with profile number on top labeling under RCRA and/or DOT provisions	& side of the containers & bear only the appropriate
- Chemical Waste Management has all the necessary permits characterized and identified by this approved profile.	and licenses for the waste that has been
- Must meet applicable OSHA, DOT packaging, labeling, shi	pping and manifesting requirements per 49 CFR.
- The WM decision is based on specific parameters defined non-conforming in any way will need to be re-evaluated regulations. If alternative treatment is not available back to the generator.	and managed in accordance with all RCRA and State
- OR - Section 13 of the manifest will require Oregon sta	te code.
Must be scheduled. Please contact Bob Mulholland (rmul	oll@wm.com) or Tina Weiser (tweiser@wm.com).
WM Authorization Name: Leslie Fichera	Title: Waste Approval Manager
WM Authorization Signature: Leslie Fichera	Date: <u>07/17/2019</u>
Agency Authorization (if Required):	Date:

Ple	ase pr	int or type. (Form desig	gned for use on elite (12-pitch)	typewriter.)						m Approved.	OMB No.	2050-0039
1	1000	FORM HAZARPOUS VASTE MANIFEST	1. Generator ID Number			00 - 899	- 467	101		072	4 J	JK ·
	5. Ge	enerator's Name and Mailir BNSC Rails	ng Address			alor's Site Addres Railroad		nan mailing addn	ess)			
		605 Proall	lup Are			lishram		9673				
	Gene	erator's Phone: 25	3-591-2567			713K/W						
		ansporter 1 Company Nam	omental Sonis	**				U.S. EPA ID		30114		
	7. Tra	ansporter 2 Company Nam	ne service	<u></u>	-			U.S. EPA ID		30110	1	
И	R Do	esignated Facility Name an	nd Site Address				_	lua rossio				
	0. 50		Waste Manign	wd 1767	29 Cedar	Springs	Lank	U.S. EPA ID				
				Anin	ylon or 9	7812		DRO	088 4	५ घड	3	
		ity's Phone: 541 - 4	154 - 2930 ion (including Proper Shipping Nam	an Hannel Clare (D.M. arbay		40.0-4			Т	1	- H	
	9a. HM	and Packing Group (if a	any))	-		No.	Type	11. Total Quantity	12. Unit Wt./Vol.	13.	Waste Code	ıs
꽁		DIASEL 6	and Oil Rays	Actrolour Hy	docation					4004		
RAT						01	17	80	6			
GENERATOR		2.		111.65								
9							1 :					
		3								- 3		
		4.					1		-	0 x = 3		or =
	14. St	pecial Handling Instruction	ns and Additional Information									
		Truck = 2138	S	tate Hazard	lous West	< ×00	14		846	9		
		Prosile 4 or										
	15. 0	GENERATOR'S/OFFERO	R'S CERTIFICATION: I hereby de	eclare that the contents of thi	is consignment are fully	and accurately de	escribed above	by the proper sl	nipping nam	e, and are clas	sified, pack	aged,
	E	Exporter, I certify that the c	rded, and are in all respects in prop contents of this consignment confo	rm to the terms of the attache	ed EPA Acknowledgmer	nt of Consent.			. If export st	nipment and I a	ım the Prim	ary
	Gener	rator's/Offeror's Printed/Tur	imization statement identified in 40 ped Name		. Éignaluse	or (b) (if I am a sm	all quantity ger	nerator) is true.	-	Mon	th Day	Year
¥	PHI	an Hurgas	W OH BEHMEO	EBNSF CHHU	2013	The	4	-			7 2	A
I'EN	16, Int	ternational Shipments	Import to U.S.		Export from U.S.	Port of er				-		
	-	sporter signature (for export ansporter Acknowledgment				Date leav	ring U.S.:					
TRANSPORTER	Transp	porter 1 Printed/Typed Nan		- 4	Signature	11	1	111		Mont		Year
NSP	Transp	John Nil	Kirk		Signature	W	1//	/		Mont		Year
TRA					1					l work	II Day	rea
1	_	screpancy										
	18a. D 9. /	Sludge 15 b	unker oil App	raed to p	0.00	Residue		Partial Rej	ection	. [Full Reje	
	Mon	mager/8NS	/ KALIMANY KA	7-24-19	rocess as	lanifest Reference	e Number:	omay	par	Sman	e De G	-095/
<u>=</u>	18b. Al	Iternate Facility (or Genera	ator)					U.S. EPA ID N	lumber			
FAC	Facility	y's Phone						T				
	18c Si	ignature of Alternate Facilit	ty (or Generator)		3.4					Mon	ith Day	Year
DESIGNATED FACILITY	19. Ha:	zardous Waste Report Ma	anagement Method Codes (i.e., coo	des for hazardous wasta trea	ilment, disconsal, and re-	cycling systems)		-				
ES	1		2.	The Transfer William WGG	3.	-laura electua)		4.	-	-	-	
	_	100										
		signated Facility Owner or	r Operator: Certification of receipt o	nazardous materials cover	ed by the manifest exce Signature	pt as noted in Iter	n 18a			Mont	th Day	Year
1		Laun	Dulas		16	d				17	124	19
PA	rom f	8700-22 (Rev. 3-05) Pr	revious editions are obtolete		personal and a second	1 A 197 mg (m				Company of the same		

Washington State-Only Toxicity Designation Tool

This table is included in the full designation tool. Use this if you are only interested in the WA state-only toxicity designation of your waste. Only enter text in yellow fields.



WISHRAM - LNAPL

<- Start Here

Applicable State-Only Toxicity Waste Codes

Chemical	CAS No.	Concentration Weight %	Reference	Fish LC 50 mg/L	Rat Oral LD 50	Rat Inhalation LC 50	Rabbit Dermal LD 50	Toxic Category	Halogenated Organic Compound (HOC)?
Double check to make sure				< 0.01	< 0.5	< 0.02	< 2	х	
your CAS #'s are input correctly with dashes. If	Input CAS	Input as a percent. Include the % sign, e.g., 15.5%.	Toxicity database	0.01 - < 0.1	0.5 - < 5	0.02 - < 0.2	2 - < 20	Α	
the NO DATA error is still in the Chemical column,	number must include dashes, e.g., 108-88-3	To convert mg/kg to percentage, divide	information is from, e.g., RTECS or EcoTox	0.1 - < 1	5 - < 50	0.2 - < 2	20 - < 200	В	
contact your regional Ecology designation		mg/kg by 10,000 (input with % sign).		1 - < 10	50 - < 500	2 - < 20	200 - < 2,000	С	
contact.				10 - 100	500 - 5,000	20 - 200	2,000 - 20,000	D	
Copper	7440-50-8	0.000101%	RTECS and Ecotox	0.02				Α	
Nickel	7440-02-0	0.000153%	RTECS and Ecotox	0.05				Α	
Mercury	7439-97-6	0.000001%	RTECS, HODB,	0.01				Х	D,F,P,U,WP,
n-butylbenzene	104-51-8	0.001070%	Enntay					NO DATA	
Benzene, ethyl-	100-41-4	0.000010%	RTECS and Ecotox	14.00	3,500.0		5,000.00	D	D,F,P,U,WP,
Cumene	98-82-8	0.001250%	RTECS and Ecotox	6.32	1,400.0		10,627.20	С	D,F,P,U,WP,
p-Cymene	99-87-6	0.000528%	RTECS and Ecotox		3,200.0		10,545.00	D	
Naphthalene	91-20-3	0.001070%	RTECS and Ecotox	6.14	490.0		20,000.00	С	D,F,P,U,WP,
Benzene, propyl-	103-65-1	0.001590%	RTECS		6,040.0				
1,2,4-Trimethylbenzene	95-63-6	0.002250%	RTECS and Ecotox	7.72	5,000.0	18.00		С	
1,2,3-Trimethylbenzene NO DATA	526-73-8	0.003090%							
Xylene	1330-20-7	0.000204%	RTECS and Ecotox	3.30	1,300.0	21.71	1,700.00	С	D,F,P,U,WP,
o-Xylene	95-47-6	0.000068%	RTECS, HODB,	16.40	3,567.0			D	
Sec-Butylbenzene	135-98-8	0.001290%	KTECO, HOUD,	05.00	1,933.1		13,808.00	D	
tert-butylbenzene	98-06-6	0.000165%	Ecotov	65.00	3,045.0			D	
		0.012839%							

Equ	ivalent Co	ncentratio	n
	0.00%	х	
+	0.00%	Α	
+	0.00%	В	
+	1,000	С	
+	10,000	D	
Wa	0000% aste Code: I signation: I		

	Waste Code	Designation	Min %
	WT01	EHW	1%
	WT02	DW	0.01%
ı	WT02	DW or Special Waste	0.001%

Laboratory Results notes:

- No reference data for 1,2,3-trimethylbenzene
- Mercury was detected in the method blank for LNAPL samples. Results were qualified as non-detect, U, at the reporting limit. Value of 1/2 the reporting limit included in this tool.

Appendix I

Bank Monitoring Inspection Data

Monitoring Personnel	AR
Date	1/22/2016
Start Time	1105
End Time	1250
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	70 F Wind 5 mph from W Partly cloudy
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	159.21
Other Observations	

Monitoring Personnel	AR
Date	2/12/2016
Start Time	9:00
End Time	9:40
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	70 F Wind 0 mph Overcast/misty
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.96
Other Observations	

Monitoring Personnel	AR
Date	3/30/2016
Start Time	11:45
End Time	12:05
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	70 F Wind 0-5 mph Clear
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.91
Other Observations	

Monitoring Personnel	AR
Date	4/29/2016
Start Time	12:50
End Time	13:30
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	60 F Wind 20-30 mph Overcast
Water Conditions (calm, small riffles, choppy, etc.)	Very choppy
Pool Elevation (NOAA TDAO3)	159.14
Other Observations	

Monitoring Personnel	AR
Date	5/31/2016
Start Time	16:45
End Time	17:05
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	90 F Wind up to 10 mph Clear
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.61
Other Observations	Sunken fishing boat present in river adjacent to site

Monitoring Personnel	AR
Date	6/30/2016
Start Time	10:55
End Time	11:10
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	90 F Wind up to 20-25 mph Clear
Water Conditions (calm, small riffles, choppy, etc.)	Сһорру
Pool Elevation (NOAA TDAO3)	158.67
Other Observations	Sunken fishing boat present in river adjacent to site

Monitoring Personnel	JS
Date	8/1/2016 - 8/12/2016
Start Time	Daily during drilling activities
End Time	Daily during drilling activities
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	Yes. Sheen and oil droplets observed on 4 August 2016, sample of oil droplets was collected and submitted for analysis. Subsequent bank monitoring was performed from August 5th through August 12th. No additional oil droplet sheen was identified through 12 August 2016.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	Average daily temperatures between 67 - 80 F Clear
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.68-159.15
Other Observations	

Monitoring Personnel	AR
Date	9/16/2016
Start Time	16:30
End Time	16:50
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	90 F Clear
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.95
Other Observations	

Monitoring Personnel	JS
Date	10/10/2016 - 10/25/2016
Start Time	Daily during RI field activities
End Time	Daily during RI field activities
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	Yes. Oil droplet sheen was observed on the surface of the river on 13 and 14 October 2016. Sample of the oil droplets were collected and submitted for analysis. Sheen was not observed during subsequent inspections between 17 and 20 October 2016. Sheen was observed on 21 October 2016. No sample was collected. Sheen was not observed during subsequent inspections.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	Average daily temperatues between 49 and 56 F Clear
Water Conditions (calm, small riffles, choppy, etc.)	
Pool Elevation (NOAA TDAO3)	157.97 - 158.97
Other Observations	

Monitoring Personnel	JS/AR
Date	11/1/2016 - 11/18/2016
Start Time	Daily during RI field activities
End Time	Daily during RI field activities
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	Average temperature 42 F 0 inches precipitation
Water Conditions (calm, small riffles, choppy, etc.)	
Pool Elevation (NOAA TDAO3)	158.77
Other Observations	

Monitoring Personnel	JS
Date	12/12/2016 - 12/13/2016
Start Time	Daily during RI field activities
End Time	Daily during RI field activities
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	Average temperature 36 F 0.04 inches precipitation
Water Conditions (calm, small riffles, choppy, etc.)	
Pool Elevation (NOAA TDAO3)	159.11
Other Observations	

Monitoring Personnel	AR
Date	1/27/2017
Start Time	13:40
End Time	13:55
Start Location	Concrete Pad
End Location	WWTP Outfall
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	34 F No wind Clear
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.90
Other Observations	

Monitoring Personnel	AR
Date	2/24/2017
Start Time	14:15
End Time	
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	45 F No wind Clear
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.70
Other Observations	

Monitoring Personnel	AR
Date	3/16/2017
Start Time	12:40
End Time	
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	50 F Wind 10 mph from W Clear
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	156.20
Other Observations	

Monitoring Personnel	AR
Date	4/18/2017
Start Time	13:55
End Time	
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	70 F No wind Partly cloudy
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	158.20
Other Observations	Foam on water

Monitoring Personnel	AR
Date	5/15/2017
Start Time	10:45
End Time	11:05
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	70 F Wind 5-10 mph from W Partly cloudy
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	157.80
Other Observations	Foam on water

Monitoring Personnel	AR
Date	6/2/2017 and 6/23/2017
Start Time	9:50; 15:25
End Time	10:15; 15:45
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	85 F; 90 F Wind 5-10 mph from W; wind 10 mph from W Clear during both inspections
Water Conditions (calm, small riffles, choppy, etc.)	Calm; light ripples
Pool Elevation (NOAA TDAO3)	157.03; 158.25
Other Observations	

Monitoring Personnel	AR
Date	7/11/2017
Start Time	16:50
End Time	17:05
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	82 F Wind 15 mph from W
Water Conditions (calm, small riffles, choppy, etc.)	Light ripples
Pool Elevation (NOAA TDAO3)	158.18
Other Observations	

Monitoring Personnel	AR
Date	8/2/2017 - 8/5/2017
Start Time	Various
End Time	Various
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	 2 August 2017: Sheen, initially observed around 12 pm (noon), was visible from just east of the concrete slab (former pump house) to approximately 100 yards downstream to the southwest. The sheen included occasional patches approximately 3 inches wide by 1.5 feet (elongated in the upstream/downstream direction), as well as several smaller diffuse patches. The smallest patches were approximately 3 inches in diameter. One patch approximately 1 foot in diameter was observed with an oil droplet in the center. Oil sheen and an oil droplet samples were collected for laboratory analysis. Oil sheen or droplets were not observed after 2:30 pm; wind (from the east) had increased since noon. 3 August 2017: Sheen and oil droplets observed between approximately 1 pm and 4 pm in similar areas as on 2 August 2017. A sample of oil droplets with water was collected for laboratory analysis. 4 August 2017: No sheen observed at 8 am, noon, 2 pm, or at 4 pm, temperature ranged from
	80 °F in morning to 90-100 °F in afternoon, wind was from the west at approximately 15 to 20 mph, water surface was choppy. 5 August 2017: No sheen observed in morning (approximately 8 and 9 am), temperature 73 °F, wind was from the west at approximately 10 mph, water was somewhat choppy.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	73 - 110 F No wind when sheen was observed, up to 20mph wind when no sheen was observed
Water Conditions (calm, small riffles, choppy, etc.)	Calm to choppy
Pool Elevation (NOAA TDAO3)	158.46 - 158.86
Other Observations	

Monitoring Personnel	AR
Date	9/18/2017 - 9/21/2017
Start Time	Various
End Time	Various
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	18 and 19 September 2017: No sheen was observed. 20 September 2017: Sheen was observed starting at approximately 8 am, temperature was approximately 70°F, winds approximately 5 mph from the west. Approximately 5 patches of sheen were observed, each less than 5 feet from the shore and around 1 foot in diameter. Multiple small oil droplets were observed. Sheen was observed from approximately 30 feet west of the pump house pad extending approximately 100 feet west. Oil sheen was not observed during periodic monitoring throughout the day from approximately 9:30 am through 8 pm. Conditions were generally windier through the remainder of the day with periods of light rain, clouds and temperatures in the 50s and 60s °F. 21 September 2017: Bank inspection monitoring performed in the morning and no sheen was observed on the water surface. Temperature was approximately 50°F and windy.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	See above.
Water Conditions (calm, small riffles, choppy, etc.)	Calm to choppy
Pool Elevation (NOAA TDAO3)	159.09 - 159.13
Other Observations	

Monitoring Personnel	Steve Misnest
Date	10(19/17
Start Time	1340
End Time	1420
Start Location	Former pump house
End Location	west out fall
Sheen Observed? If yes, describe location and characteristics	No Sheen observed
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	und's-8 mph to east remp: 60°F cloudy 0.02 in per prior to inspection
Water Conditions (calm, small riffles, choppy, etc.)	small riffles
Pool Elevation (NOAA TDAO3)	159,22 USALE Forebay Elevation
, Other Observations	None

Monitoring Personnel	AR
Date	11/8/2017 and 11/29/2017 - 12/1/2017
Start Time	Various
End Time	Various
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No oil sheen or droplets were observed on the water surface of the Columbia River on 8 November 2017. Oil sheen was observed within an area of approximately a 10-inch diameter circle at approximately 1:30 pm and 2:30 pm on the water surface of the Columbia River on 29 November 2017. Oil sheen was not observed during the rest of the day on 29 November 2017, nor on the following two days (30 November 2017 and 1 December 2017). No oil sheen samples were collected due to the limited volume observed.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	38 F Wind 3 mph 0.13 inches precipitation
Water Conditions (calm, small riffles, choppy, etc.)	Calm to choppy
Pool Elevation (NOAA TDAO3)	158.79
Other Observations	

Monitoring Personnel	RVAN HILTGREN
Date	12/21/2017
Start Time 1035 pm	1035
End Time	1047, PERIODICANS UNTIL 1730 PULLING DAS
Start Location	EAST IX PLANT HOUSE + 2 CONLINETE
End Location	WATP OUTFAIL
	NO SAZEN OBSERVED IN MORNING (1035-1047) NOR THROUGHOUT THE BAY.
	CAST OBSERVATION AT APPROXIMETY 1730.
Sheen Observed? If yes, describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	WNW Imph, 35°F, cous, Wount, that Fug LIGHT BREEZE, NO PRECIPITATION
Water Conditions (calm, small riffles, choppy, etc.)	caun, were
Pool Elevation (NOAA TDAO3)	159.33 USACE AVERAGE FOREBRY EVEN.
Other Observations	

Monitoring Personnel	Rosan Hurghen
Date	12/22/2017
Start Time	0900
End Time	0915
Start Location	CAST OF ALMPHOUSE #2
End Location	WWTP OUTPHE
	NO SHEEN OBSERVED
Sheen Observed? If yes, describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	NO PRECEDENTION
Water Conditions (calm, small riffles, choppy, etc.)	CAM / Sman RIFFLES
Pool Elevation (NOAA TDAO3)	159 USACE Arrage Foreby Hevation
Other Observations	
,	

Monitoring Personnel	Alice Polainson
Date	1-18-17
Start Time	9:15 AM
End Time	9:40 An
Start Location	concrete and (former pump house)
End Location	Wisham WWTP outfall
Sheen Observed? If yes, describe location and characteristics	No.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	Wind $\approx 3-5$ ngh from N Tenp $\approx 45^{\circ}F$ Precip 0.1-0.2" in 24h, not currently raining overcost
Water Conditions (calm, small riffles, choppy, etc.)	calm, very small ripples
Pool Elevation (NOAA TDAO3)	158.91
Other Observations	None,

Monitoring Personnel	AR
Date	2/27/2018
Start Time	10:30
End Time	10:45
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	39 F Wind 0 mph Overcast
Water Conditions (calm, small riffles, choppy, etc.)	
Pool Elevation (NOAA TDAO3)	158.29
Other Observations	

Monitoring Personnel	AR
Date	3/26/2018
Start Time	
End Time	
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	
Water Conditions (calm, small riffles, choppy, etc.)	
Pool Elevation (NOAA TDAO3)	158.21
Other Observations	

Monitoring Personnel	AR
Date	4/26/2028
Start Time	9:45
End Time	10:05
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	50 F Wind 0 mph
Water Conditions (calm, small riffles, choppy, etc.)	Calm
Pool Elevation (NOAA TDAO3)	157.92
Other Observations	

Monitoring Personnel	Steve Misner
Date	5/15/18
Start Time	1300
End Time	1330
Start Location Fmr	Purp loc.
End Location	out Call wwith.
Shoon Observed 2 If you	No
Sheen Observed? If yes, describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	east at 25 mph, 85° F, Open Mist 24 hrs Clear.
Water Conditions (calm, small riffles, choppy, etc.)	small rifles to colm
Pool Elevation (NOAA TDAO3)	159.00
Other Observations	Pone

Monitoring Personnel	AR
Date	6/18/2018 - 6/28/2018
Start Time	Various
End Time	Various
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	20 June 2018: During pre-probing of sediment for Dart installation, as part of the ongoing nearshore investigation, sheen (possibly biogenic) was observed on the water surface at two locations just offshore of monitoring well WMW-17: one to the southeast (at 8:34 am) and one to the southwest (at 10:35 am) of WMW-17, both approximately 20 to 25 feet away from the shoreline. Sheen was observed as small, approximately 4 to 6-inch diameter areas in both locations. Oil sheen was not observed during the rest of the day on 20 June 2018, nor on 21 or 22 June 2018. No samples were collected for analysis. 24 June 2018: Oil sheen was observed at approximately 9:30 am and again around 10:30-11 am. Sunny, temperature approximately 70°F, no wind, water surface of Columbia River was calm. Sheen was observed on the river surface, approximately 2 feet from shore near well WMW-16, at approximately 9:30 am, one area with a 5-inch diameter and smaller areas with diameters less than 2 inches. At 10:30 am, an oil droplet approximately 0.5 inch in diameter surrounded by an area of sheen approximately 10 inches in diameter was observed from the boat performing the nearshore investigation work (approximately 20 feet from shore in the vicinity of WMW-17). Around 11 am, a diffuse patch of sheen approximately 4 feet in length and 2 inches in width was observed along the bank approximately 1 foot from the shore near well WMW-17. Oil sheen was not observed during the rest of the day on 24 June 2018, nor on 25, 26, or 28 June 2018. No samples were collected for analysis.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	67 - 95 F Wind 0 - 30 mph 0 inches precipitation
Water Conditions (calm, small riffles, choppy, etc.)	Calm to choppy (typically calm when sheen observed)
Pool Elevation (NOAA TDAO3)	158.37 - 159.46

Monitoring Personnel	AR
Date	6/18/2018 - 6/28/2018
Start Time	Various
Other Observations	

Monitoring Personnel	Steve Misner
Date	7126118
Start Time	1410
End Time	1430
Start Location	Four pump location
End Location	wwte outfall
	70
Sheen Observed? If yes, describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	wind Eat ~ 10-15mph Temp 100° F Clear, No pep prior 24 hours
Water Conditions (calm, small riffles, choppy, etc.)	moderate viffles to light chop
Pool Elevation (NOAA TDAO3)	
	None
Other Observations	

Monitoring Personnel	RH
Date	8/8/2018
Start Time	9:40
End Time	14:30
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	Sheen and oil droplets observed in mutiple disconnected locations between well WMW-18 to approximately 10 feet east of well WMW-17. At 9:50, starting approximately 10 feet east of well WMW-17 and extending 20 feet east, a 20-foot long by 0.5-foot wide area of sheen was observed approximately 20 feet south of shoreline. At 9:55 winds from west and movement of water, the sheen extent narrowed to approximately 20-feet by 0.25-feet. Sheen moved with river towards east. Approximately 10 feet east of well WMW-18 a 3-foot by 3-foot area of sheen was observed 5 feet south of the shoreline. In line with well WMW-18, multiple small areas of sheen approximately 6 inches in diameter were observed approximately 5 feet south of the shoreline. At 10:00 wind from the west/southwest moved water and sheen towards the shoreline, dispersing the sheen. By this time most of the larger areas of sheen were broken up into smaller areas. A sample was collected. At 14:30 sheen was observed near Former Pump House #2 approximately 20 feet east and west of the structure. Water was very calm, temperature 104 F.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	90 F Wind 4 mph from west 0 inches precipitation Clear/hazy sky
Water Conditions (calm, small riffles, choppy, etc.)	Calm, small riffles with wind
Pool Elevation (NOAA TDAO3)	158.76

Monitoring Personnel	RH
Date	8/8/2018
Start Time	9:40
Other Observations	

Monitoring Personnel	RH
Date	8/9/2018
Start Time	7:20
End Time	15:50
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	 7:20 - 7:30: No sheen or oil droplets observed between Former Pump House #2 and WWTP outfall to river. River level midway up the outfall pipe (higher than on 8/8/2018). River slightly choppy, wind approximately 8 mph from west. Clear, hazy sky. Temperature 77 F. 12:00: No sheen or oil droplets observed. Temperature 99 F with light breeze. Wind WNW 9 mph. Hazy skies. River water level high. 15:50: No sheen or oil droplets observed. Temperature 104 F with light breeze. Wind WNW 9 mph. Hazy skies. High water level, relatively clam water.
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	See above.
Water Conditions (calm, small riffles, choppy, etc.)	Calm, small riffles with wind
Pool Elevation (NOAA TDAO3)	159.18
Other Observations	

Monitoring Personnel	RH
Date	8/10/2018
Start Time	12:00
End Time	
Start Location	WWTP Outfall
End Location	Concrete Pad
Sheen Observed? If yes, describe location and characteristics	No sheen or oil droplets observed
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	90 F Wind 13 mph WNW 0 inches precipitation
Water Conditions (calm, small riffles, choppy, etc.)	Lightly choppy water
Pool Elevation (NOAA TDAO3)	158.86
Other Observations	

Monitoring Personnel	Ryan Hultgren
Date	09/20/18
Start Time	9:15:00 AM
End Time	9:25:00 AM
Start Location	Former Pump House #2 (near well WMW-18)
End Location	WWTP outfall to Columbia River
Sheen Observed? If yes, describe location and characteristics	No oil sheen or oil droplets observed
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	60 deg F, 10-20 mph from west, windy, partly cloudy / sunny
Water Conditions (calm, small riffles, choppy, etc.)	Very choppy water, moving from west to east (same direction as wind)
Pool Elevation (NOAA TDAO3)	The Dalles Dam Average Forebay Elevation 09/20/18: 159.00
Other Observations	Columbia River water level at bottom of WWTP outfall pipe

Monitoring Personnel	RET	
Date	10/17/18	
Start Time	0700	
End Time	0.723	
Start Location	NWTP outtout to commbia River	
End Location	Former pump house 2, near wmw-10	
	No	
Sheen Observed? If yes, describe location and characteristics		
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	40° F. no precip, wind ENE 2mph.	
Water Conditions (calm, small riffles, choppy, etc.)	Calm, slight wind moving water w to E mar berm	
Pool Elevation (NOAA TDAO3)		
	water well below outfall invert	
Other Observations		
2.4		

Monitoring Personnel	KT/BR	
Date	11/5/2018 - 11/7/2018	
Start Time	Daily during groundwater monitoring activities	
End Time	Daily during groundwater monitoring activities	
Start Location	WWTP Outfall	
End Location	Concrete Pad	
Sheen Observed? If yes, describe location and characteristics	No sheen or oil droplets observed	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	42 - 60 F Wind 2 - 13 mph 0 inches precipitation	
Water Conditions (calm, small riffles, choppy, etc.)	Very choppy	
Pool Elevation (NOAA TDAO3)	158.18 - 158.57	
Other Observations		

Monitoring Porgennel	IVTT 3 NL	
Monitoring Personnel Date	KET 2 MG	
	12 5 18	
Start Time	1520	
End Time	. 3	
Start Location	WTP outfall to Columbia	
End Location	Conc pad WMW-18	
	no sheen	
Sheen Observed? If yes, describe location and characteristics		
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	34° (loudy, wind ENE 10 mph, o in precip	
Water Conditions (calm, small riffles, choppy, etc.)	cuppy Ismall nittes	
Pool Elevation (NOAA TDAO3)		
Other Observations		

Monitoring Personnel	Matthew Grzegorzevski	
Date	422/19	
Start Time	11:00	
End Time	12:00	
Start Location	WWTP Ortfall to Columbia	
End Location	Concrete Pad WMW-18	
Sheen Observed? If yes, describe location and characteristics	No sheen	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	34°F, Partly Gunny, no precip, 4mph wind	
Water Conditions (calm, small riffles, choppy, etc.)	Swall riffles	
Pool Elevation (NOAA TDAO3)		
Other Observations .	USE: 59 inches below top of WWTP outfall pipe	

Monitoring Personnel	KET/MG
Date	3/1/19
Start Time	0800
End Time	1100
Start Location	Concrete pad by WMW-18
End Location	WWTP Outfall
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	33 F, light snow, wind 10mph ESE, cloudy
Water Conditions (calm, small riffles, choppy, etc.)	small riffles
Pool Elevation (NOAA TDAO3)	158.60
Other Observations	

Monitoring Personnel	Matthew Grzegorzewski
Date	Matthew Grzegorzewski 3-14-19
Start Time	930
End Time	1000
Start Location	WWTP outfull pipe
End Location	WMW - 21
	No sheen observed.
Sheen Observed? If yes, describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	34°F, gunny, 10% doud cover, calm
Water Conditions (calm, small riffles, choppy, etc.)	calm, minimal ripples
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	RYAN HULTGLEN	
Date	6/4/19	
Start Time	1600	
End Time	1615	
Start Location	NEAR RMO-Z; GO WEST TOWHOD GUTFAU THEN BACK TOWARD CAST	
End Location	COMMETE PUMPHOUSE #	
Sheen Observed? If yes, describe location and characteristics	NO SHEEN OBSCINCO	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours	STRONG WINDS BLOWING TO THE	
prior to inspection); cloud cover Water Conditions (calm, small riffles, choppy, etc.)	CHOPPY, WIND BLOWN TO EAST/ WORTHEAST TO SHOKE	
Pool Elevation (NOAA TDAO3)	WARY 158.94 (ANG FOREBAY CLEVITHE ALLS DAM)	
Other Observations	WHERE LEVEL COMMBIA RIVER YEAR BOTTOM OF WHITE OUT FAM PIPE (SEE PICTURES). DIDNOT MEASURE LEVEL DIRECTLY.	

A. Kdinger
7-22 and 7:23
7:22 - 11-16:50 723 - 10-10:10
7-22 1:15 7-23 10:10
~ MW-14
coracte pad
nove
winds 15 mgh & to BSE, ~ 90°F, no precipitation, mostly clear sky
choppy
none

Monitoring Personnel	Robinson	
Date	7-24-19	
Start Time	15:00	
End Time	15:15	
Start Location		
End Location	WMW 15 conorde pad	
Sheen Observed? If yes,	no	
describe location and characteristics		
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	~920F, winds 20mph	
Water Conditions (calm, small riffles, choppy, etc.)	clopps w/ whiteeps	
Pool Elevation (NOAA TDAO3)		
Other Observations		

Monitoring Personnel	Robinson
Date	7-25-19
Start Time	16:00 (and throughout a florown)
End Time	16:16
Start Location	
End Location	whw-15 concrok pad
4	
Sheen Observed? If yes, describe location and characteristics	NO
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	~950F, calm, clear
Water Conditions (calm, small riffles, choppy, etc.)	calm.
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	Robinson 7-76-19	
Date	7-76-19	
Start Time	7:45	
End Time	7:55	
Start Location	WMW-14	
End Location	WMW-14 Concrek pad	= 1
Sheen Observed? If yes, describe location and	NO	
characteristics		
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	~800 F, colon, clear sky	
Water Conditions (calm, small riffles, choppy, etc.)	small riples	
Pool Elevation (NOAA TDAO3)		, , , , , , , , , , , , , , , , , , , ,
	MAN /	
Other Observations	nore	

Monitoring Personnel	KET
Date	7/27/19
Start Time	0(055
End Time	0710
Start Location	conc. pad by wmw-18
End Location	WNTP OUTFALL to Columbia
Sheen Observed? If yes, describe location and characteristics	No sheepa
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	wind W 16 MPH 68 °F Oin precip Mostly sunnor
Water Conditions (calm, small riffles, choppy, etc.)	small riffles
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	EET
Date	7/10/19
Start Time	1475
End Time	1440
Start Location	WMW-14
End Location	conc-pad by WMW-18
Sheen Observed? If yes, describe location and characteristics	No Sheen Observed
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	85°F SUNNY Wind W 6 Mph O in precip
Water Conditions (calm, small riffles, choppy, etc.)	calm
Pool Elevation (NOAA TDAO3)	
Other Observations	

	I.V. a
Monitoring Personnel	RET
Date	7/29/19
Start Time	0940
End Time	1000
Start Location	WMW-18
End Location	WMW-14
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	68°F Wina W 7mph o" preap Sunny
Water Conditions (calm, small riffles, choppy, etc.)	small riffles
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	LYET
Date	818119
Start Time	0755
End Time	0910
Start Location	WMW-18
End Location	WMW-10
Sheen Observed? If yes, describe location and characteristics	NO
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	15 mph to E, 70°F, slight precip during inspection, cloudy
Water Conditions (calm, small riffles, choppy, etc.)	Choppy
Pool Elevation (NOAA TDAO3)	
Other Observations	

Mariana Danasa da	
Monitoring Personnel	VE I
Date	819/19
Start Time	1200
End Time	1210
Start Location	MWM-18
End Location	WMW-14
Sheen Observed? If yes, describe location and characteristics	Ne
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	slightly breezy, ~ 85° F, no precip, sunny
Water Conditions (calm, small riffles, choppy, etc.)	small nffles
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	451
Date	80/12/19
Start Time	1420
End Time	14 40
Start Location	WMW-10
End Location	WWW-18
Sheen Observed? If yes, describe location and characteristics	No
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	82°F, Wind WNW 9 mph, no precip,
Water Conditions (calm, small riffles, choppy, etc.)	calm
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	KET
Date	8/19/19
Start Time	1430
End Time	1445
Start Location	WMW-14
End Location	WMW-18
	No
Sheen Observed? If yes, describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	SUNNY WIND WITMPH, ho precip,
Water Conditions (calm, small riffles, choppy, etc.)	small riffles + wake from boats
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	Biloria Gronzalez
Date	09/23/2019
Start Time	1310
End Time	1340
Start Location	MW-14
End Location	MW-18
÷ .	No sheen observed.
Sheen Observed? If yes, describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	uindy, overcast, 63°F, rain previous day, wind
Water Conditions (calm, small riffles, choppy, etc.)	choppy water.
Pool Elevation (NOAA TDAO3)	
Other Observations	

Monitoring Personnel	Giona Gionzalez
Date	1/1/2/19
Start Time	1200 - 1220
End Time	
Start Location	WMW-23
End Location	WMW-14
Sheen Observed? If yes,	No sheen
describe location and characteristics	
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	Moderate wind speed in NW director appox 50°F, clauds wisome breakage, light precipitation in AM
Water Conditions (calm, small riffles, choppy, etc.)	moderate ripples
Pool Elevation (NOAA TDAO3)	
	none
Other Observations	

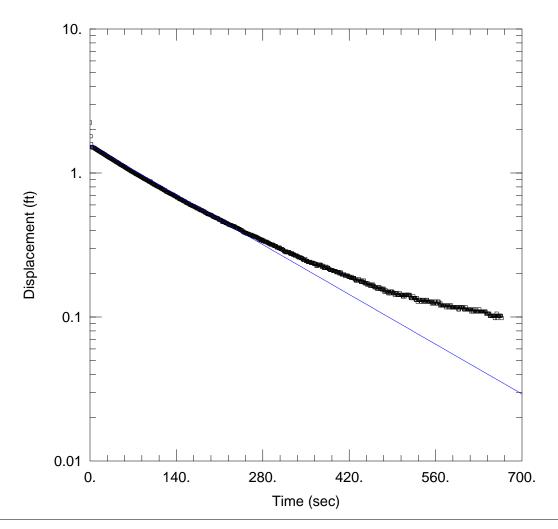
Monitoring Personnel	67/049 GUONZAIEZ
Date	11/13/19
Start Time	1300
End Time	1315
Start Location	WMW-23
End Location	WMW-14
Sheen Observed? If yes, describe location and characteristics	No sheen
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	strong winds and very enoppy water wind direction NW, temp appox 45°F
Water Conditions (calm, small riffles, choppy, etc.)	choppy water
Pool Elevation (NOAA TDAO3)	
Other Observations	none

		1
Monitoring Personnel	610V10 570Y7a107	
Date	11 19 19	
Start Time	IDIO	
End Time	1040	
Start Location	WMW-23	
End Location	WMW-14	
	nosheen	
Sheen Observed? If yes, describe location and characteristics		
Weather: wind speed/direction; temperature (degrees F); precipitation (amount 24 hours prior to inspection); cloud cover	little mind, NW direction, aboutly + slightly toggy.	
Water Conditions (calm, small riffles, choppy, etc.)	calm light nipples	
Pool Elevation (NOAA TDAO3)		
	Bidfilm from WMW-23+0 WMWZ(approx 15 yards	
Other Observations	columbia over -very stringy -very stringy -milky white -silky -nings -nings	-sheer

Appendix J

Slug Test Aqtesolv Outputs





Data Set: N:\...\RMD-1_1F.aqt

Date: 11/19/18 Time: 11:34:53

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 2.241 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

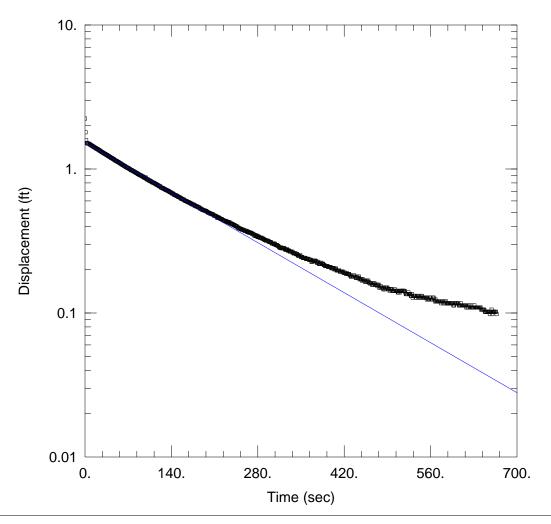
Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 5.396E-6 ft/sec y0 = 1.563 ft



Data Set: N:\...\RMD-1_1F.aqt

Date: 11/19/18 Time: 11:35:16

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 2.241 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

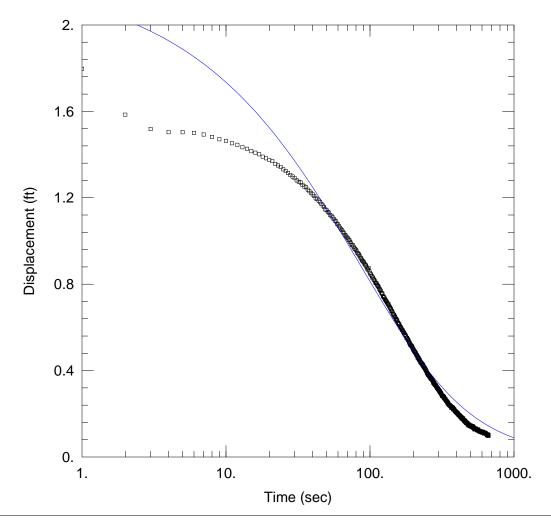
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 7.189E-6 ft/sec

y0 = 1.523 ft



Data Set: N:\...\RMD-1_1F.aqt

Date: 11/19/18 Time: 11:36:56

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft

WELL DATA (RMD-1)

Initial Displacement: 2.241 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

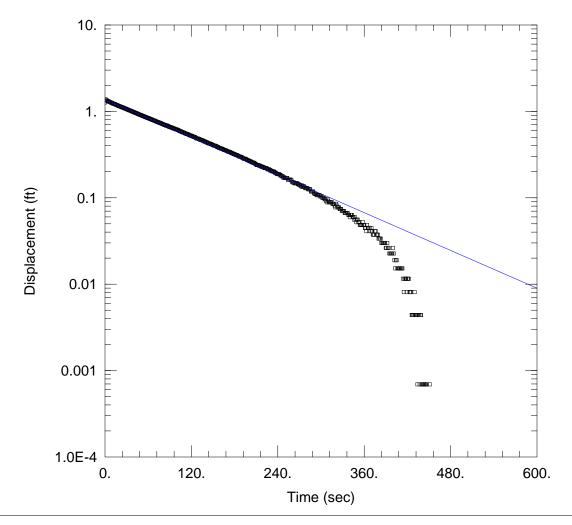
= 3.548E-6 ft/sec

Kz/Kr = 1.

Kr

Solution Method: KGS Model

 $= 0.003059 \text{ ft}^{-1}$



Data Set: N:\...\RMD-1_2R.aqt

Date: 11/19/18 Time: 11:32:35

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.269 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

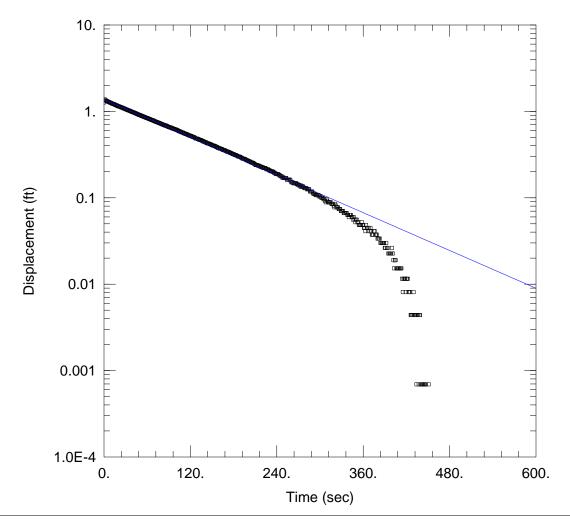
Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 7.959E-6 ft/secy0 = 1.378 ft



Data Set: N:\...\RMD-1_2R.aqt

Date: 11/19/18 Time: 11:32:52

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.269 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

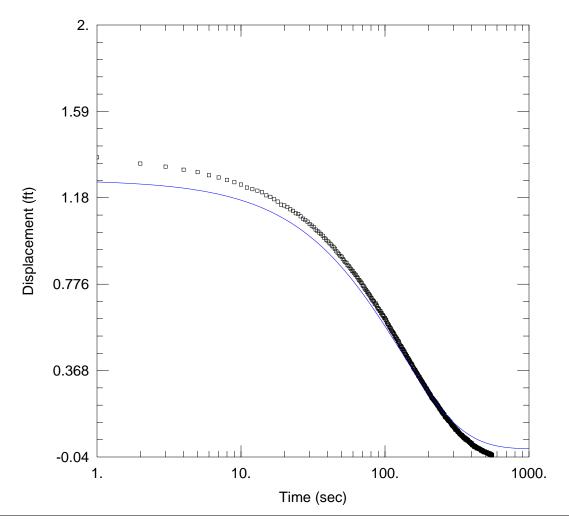
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 1.056E-5 ft/sec

y0 = 1.378 ft



Data Set: N:\...\RMD-1_2R.aqt

Date: 11/19/18 Time: 11:33:41

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft

WELL DATA (RMD-1)

Initial Displacement: 1.269 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

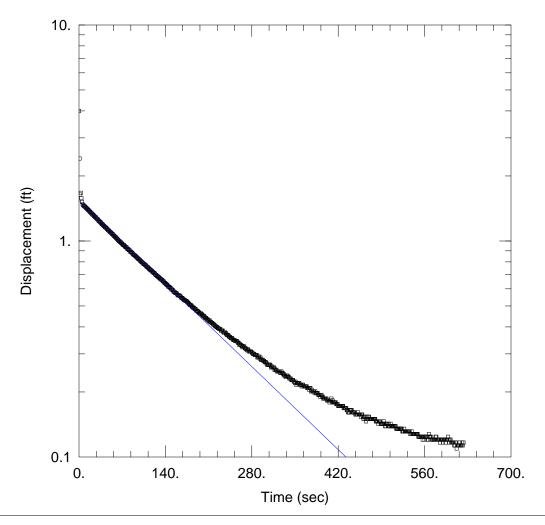
= 8.68E-6 ft/sec

Kz/Kr = 1.

Kr

Solution Method: KGS Model

 $= 3.906E-12 \text{ ft}^{-1}$



Data Set: N:\...\RMD-1_3F.aqt

Date: 11/19/18 Time: 11:29:53

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 3.995 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

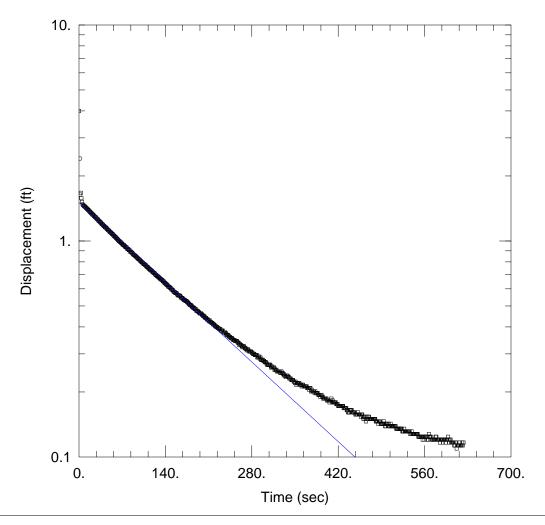
Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 5.998E-6 ft/sec y0 = 1.539 ft



Data Set: N:\...\RMD-1_3F.aqt

Date: 11/19/18 Time: 11:30:14

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 3.995 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

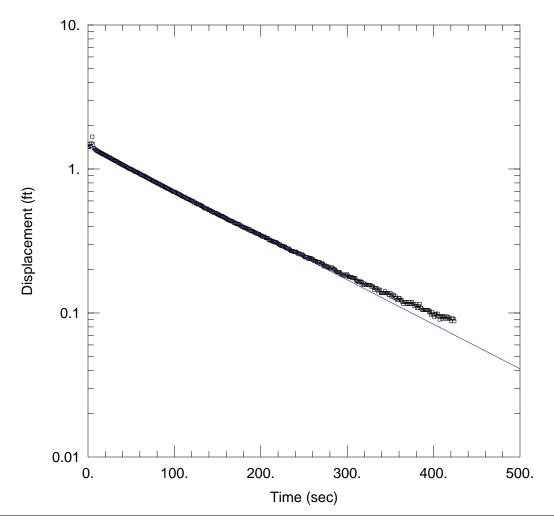
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 7.634E-6 ft/sec

y0 = 1.505 ft



Data Set: N:\...\RMD-1_4R.aqt

Date: 11/19/18 Time: 11:27:55

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.42 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

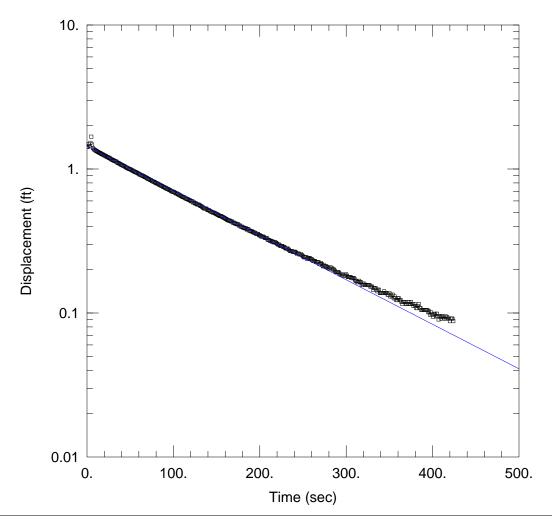
Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 6.752E-6 ft/sec y0 = 1.437 ft



Data Set: N:\...\RMD-1_4R.aqt

Date: 11/19/18 Time: 11:28:17

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.42 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

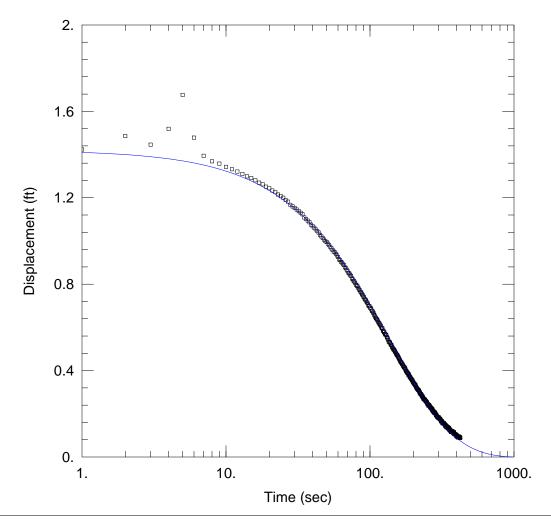
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 8.955E-6 ft/sec

y0 = 1.436 ft



Data Set: N:\...\RMD-1_4R.aqt

Date: 11/19/18 Time: 11:28:47

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft

WELL DATA (RMD-1)

Initial Displacement: 1.42 ft

Static Water Column Height: 29.83 ft

Total Well Penetration Depth: 29.83 ft Casing Radius: 0.083 ft

Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

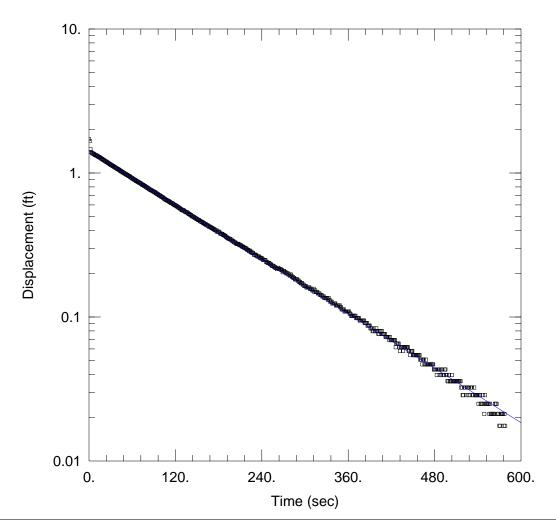
Aquifer Model: Unconfined

Solution Method: KGS Model

= 7.776E-6 ft/sec Kr

 $= 3.906E-12 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\RMD-1_5F_BR.aqt

Date: 10/19/18 Time: 14:27:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.72 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

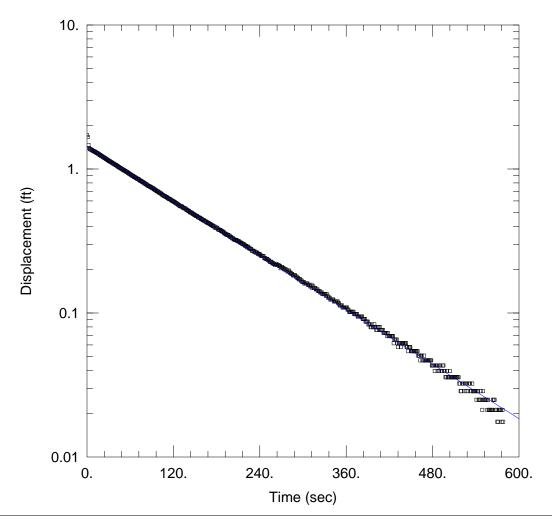
Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 6.878E-6 ft/secy0 = 1.428 ft



Data Set: N:\...\RMD-1_5F_HV.aqt

Date: 10/19/18 Time: 14:25:02

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.72 ft

Total Well Penetration Depth: 29.83 ft

Total Well Perlettation Depth. 29.03 II

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

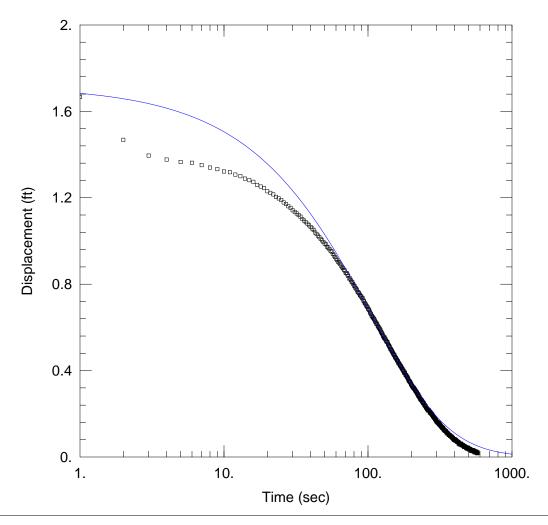
Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 9.124E-6 ft/sec y0 = 1.428 ft



Data Set: N:\...\RMD-1_5F_KGS.aqt

Date: 10/19/18 Time: 15:48:49

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft

WELL DATA (RMD-1)

Initial Displacement: 1.72 ft

. <u>1.72</u> IL

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

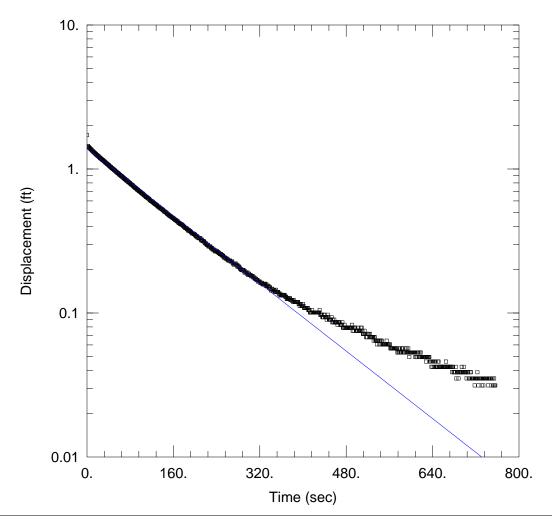
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 8.336E-6 ft/sec

 $Kz/Kr = \overline{1}$.

Ss = $2.204E-5 \text{ ft}^{-1}$



Data Set: N:\...\RMD-1_BR.aqt

Date: 10/19/18 Time: 10:56:30

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.72 ft

Total Well Penetration Depth: 29.83 ft

Total Well Perietration Depth. 29.03

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

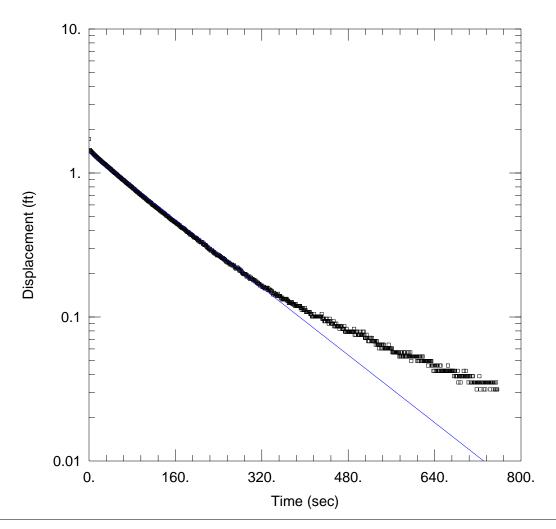
Screen Length: 15. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 6.405E-6 ft/sec y0 = 1.389 ft



Data Set: N:\...\RMD-1_6R_HV.aqt

Date: 10/19/18 Time: 14:18:02

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-1)

Initial Displacement: 1.72 ft

Total Well Penetration Depth: 29.83 ft

Casing Radius: 0.083 ft

Static Water Column Height: 29.83 ft

Screen Length: 15. ft Well Radius: 0.125 ft

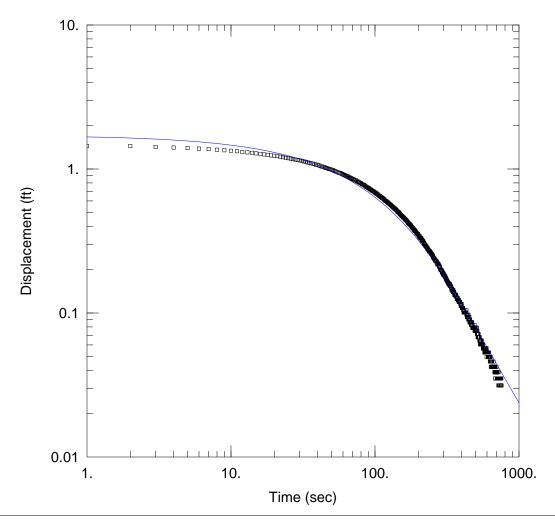
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 8.495E-6 ft/sec

y0 = 1.389 ft



Data Set: N:\...\RMD-1.aqt

Date: 10/19/18 Time: 10:55:29

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-1 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 29.83 ft

WELL DATA (RMD-1)

Initial Displacement: 1.72 ft

Static Water Column Height: 29.83 ft

Total Well Penetration Depth: 29.83 ft

Screen Length: 15. ft

Casing Radius: 0.083 ft

Well Radius: 0.125 ft

SOLUTION

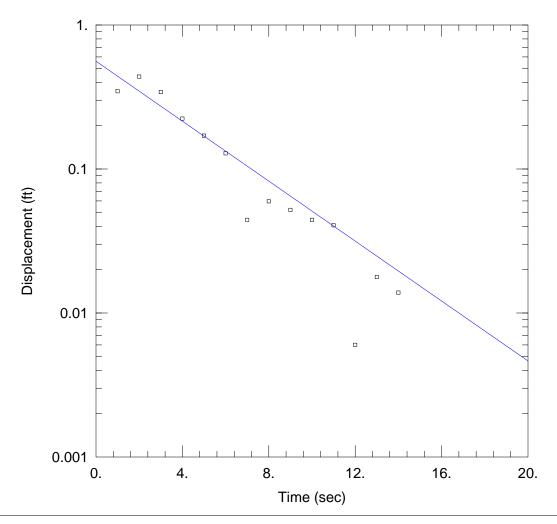
Aquifer Model: Unconfined

Solution Method: KGS Model

= 7.742E-6 ft/secKr

 $= 8.749E-5 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\RMD-4-1F.aqt

Date: 11/12/18 Time: 15:15:03

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.344 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

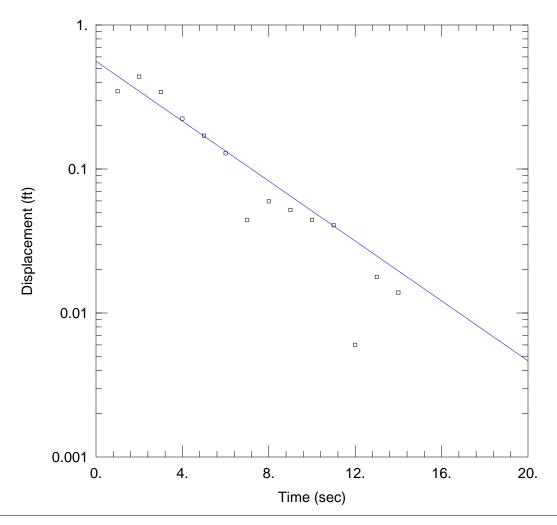
Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001629 ft/sec y0 = 0.56 ft



Data Set: N:\...\RMD-4-1F.aqt

Date: 11/12/18 Time: 15:15:38

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: <u>BNSF Railway Company</u>

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.344 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

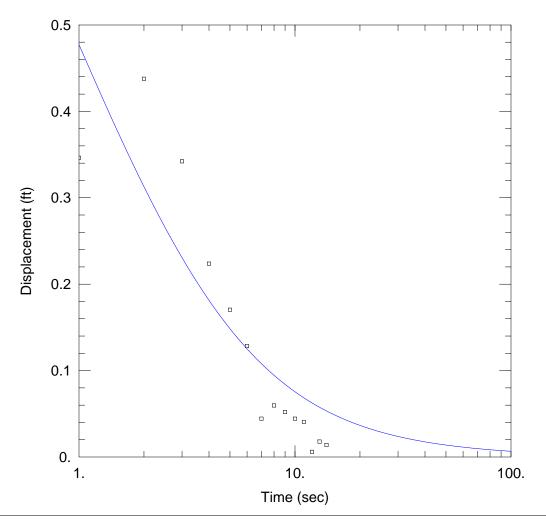
Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002093 ft/sec y0 = 0.5598 ft



Data Set: N:\...\RMD-4-1F.aqt

Date: 11/12/18 Time: 15:16:05

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft

WELL DATA (RMD-4)

Initial Displacement: 1.344 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

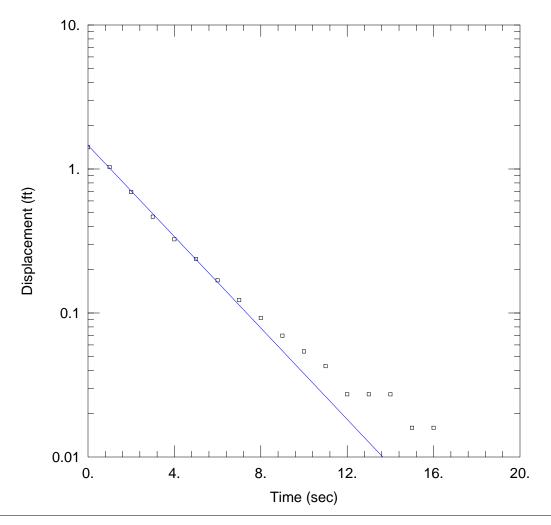
Aquifer Model: Unconfined

= 0.000166 ft/secKr

Kz/Kr = 1.

Solution Method: KGS Model

 $= 0.001932 \text{ ft}^{-1}$



Data Set: N:\...\RMD-4-2R.aqt

Date: 11/12/18 Time: 15:14:06

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: <u>BNSF Railway Company</u>

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.417 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

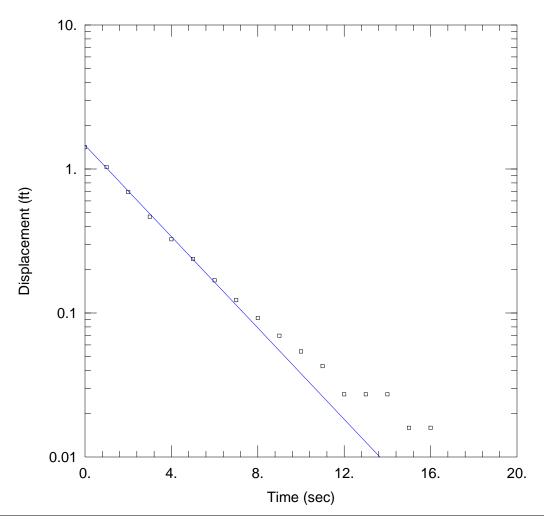
Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0002483 ft/sec y0 = 1.46 ft



Data Set: N:\...\RMD-4-2R.aqt

Date: 11/12/18 Time: 15:13:46

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.417 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

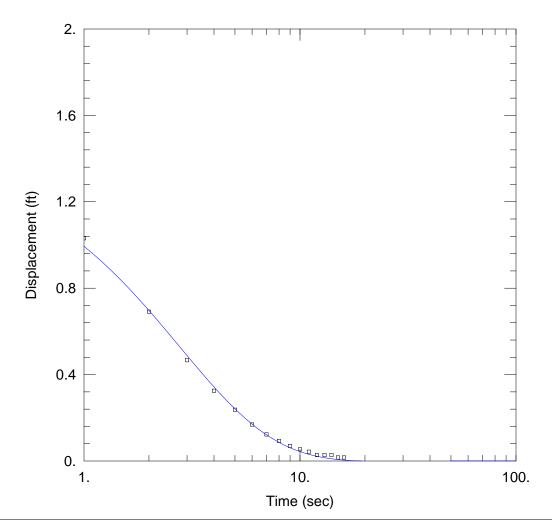
Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.000319 ft/sec y0 = 1.459 ft



Data Set: N:\...\RMD-4-2R.aqt

Date: 11/12/18 Time: 15:13:26

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft

WELL DATA (RMD-4)

Initial Displacement: 1.417 ft

1.417

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

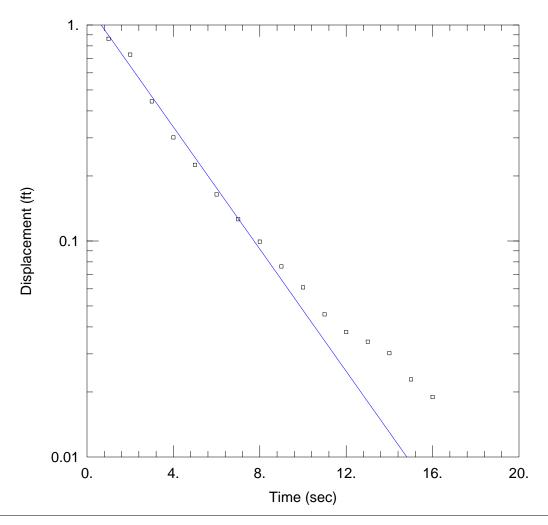
Aquifer Model: Unconfined

Kr = 0.0002747 ft/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $1.985E-12 \text{ ft}^{-1}$



Data Set: N:\...\RMD-4-3F.aqt

Date: 11/12/18 Time: 15:08:45

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.184 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

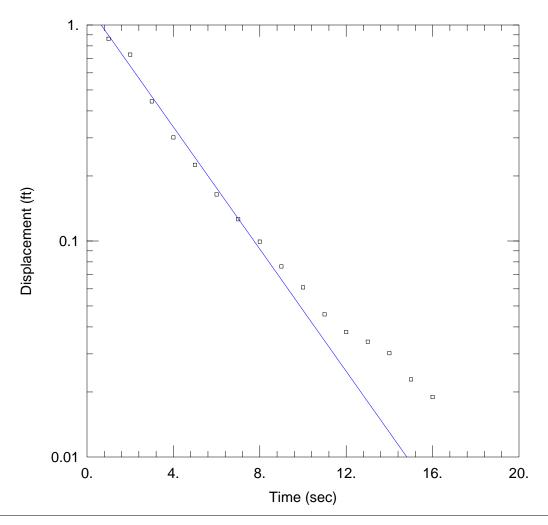
Screen Length: <u>20.</u> ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0002212 ft/sec y0 = 1.238 ft



Data Set: N:\...\RMD-4-3F.aqt

Date: 11/12/18 Time: 15:09:03

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.184 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

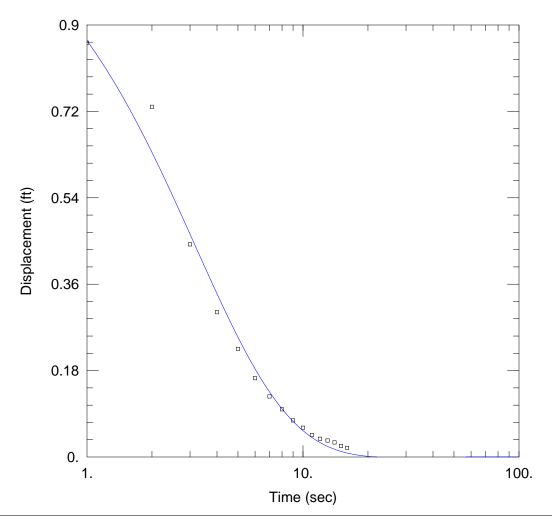
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002844 ft/sec

y0 = 1.238 ft



Data Set: N:\...\RMD-4-3F.aqt

Date: 11/12/18 Time: 15:09:45

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft

WELL DATA (RMD-4)

Initial Displacement: 1.184 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

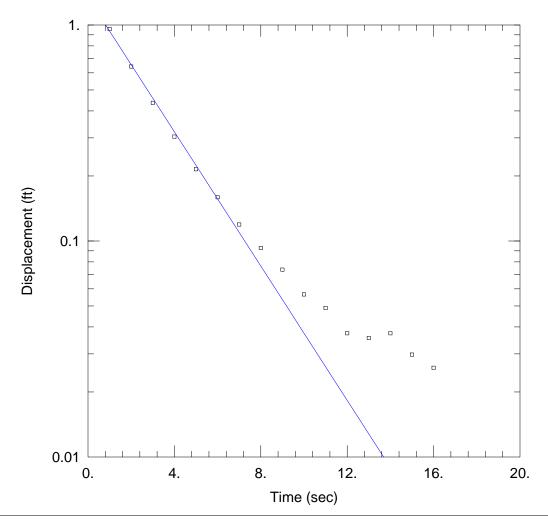
Aquifer Model: Unconfined

= 0.0002413 ft/sec Kr

Kz/Kr = 1.

Solution Method: KGS Model

 $= 1.985E-12 \text{ ft}^{-1}$



Data Set: N:\...\RMD-4-4R.aqt

Date: 11/12/18 Time: 15:05:35

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.368 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

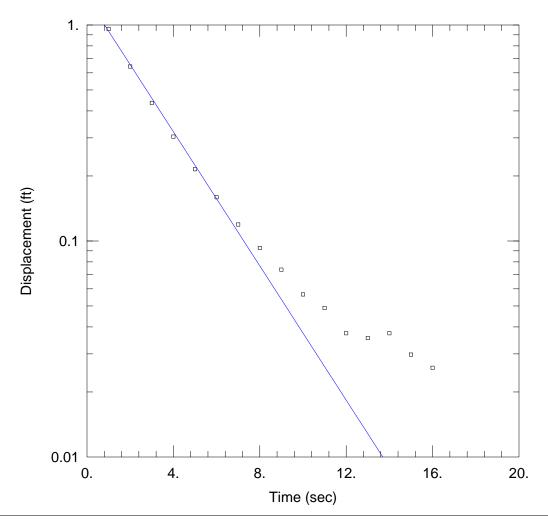
Screen Length: <u>20.</u> ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0002432 ft/sec y0 = 1.339 ft



Data Set: N:\...\RMD-4-4R.aqt

Date: 11/12/18 Time: 15:05:14

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.368 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

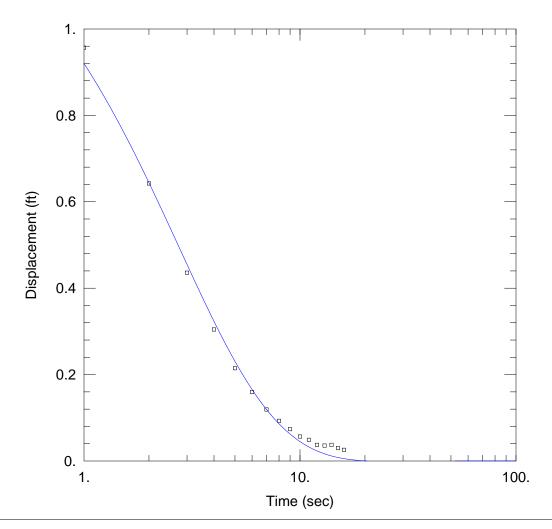
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0003125 ft/sec

y0 = 1.338 ft



Data Set: N:\...\RMD-4-4R.aqt

Date: 11/12/18 Time: 15:04:50

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft

WELL DATA (RMD-4)

Initial Displacement: 1.368 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

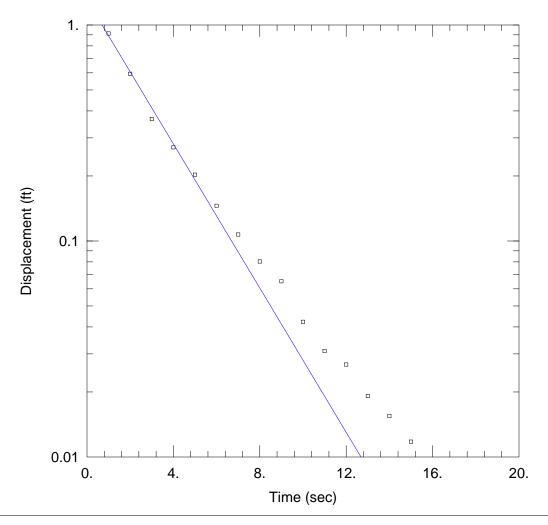
Aquifer Model: Unconfined

= 0.0002805 ft/sec Kr

Kz/Kr = 1.

Solution Method: KGS Model

 $= 5.239E-7 \text{ ft}^{-1}$



Data Set: N:\...\RMD-4-5F.aqt

Date: 11/12/18 Time: 14:56:00

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.368 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: <u>20.</u> ft Well Radius: 0.25 ft

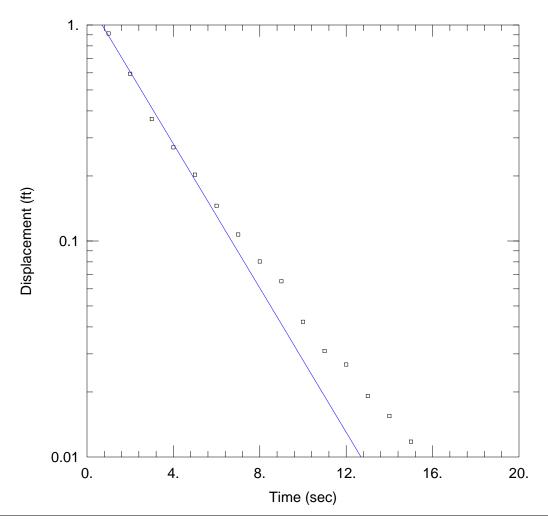
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0002611 ft/sec

y0 = 1.307 ft



Data Set: N:\...\RMD-4-5F.aqt

Date: 11/12/18 Time: 14:56:22

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.368 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

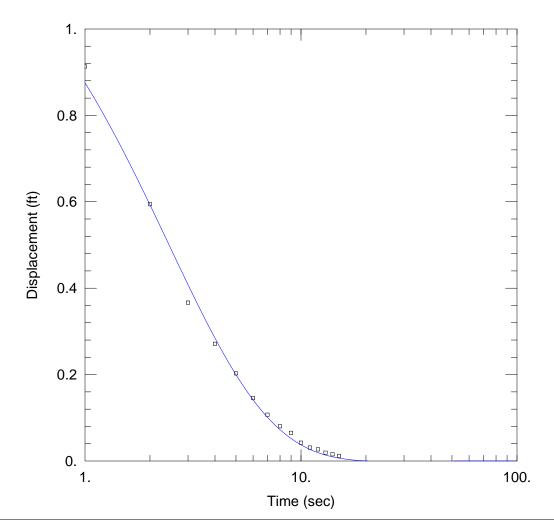
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0003357 ft/sec

y0 = 1.307 ft



Data Set: N:\...\RMD-4-5F.aqt

Date: 11/12/18 Time: 14:56:46

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft

WELL DATA (RMD-4)

Initial Displacement: 1.368 ft

Static Water Column Height: 50.37 ft

Total Well Penetration Depth: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

Casing Radius: 0.083 ft

SOLUTION

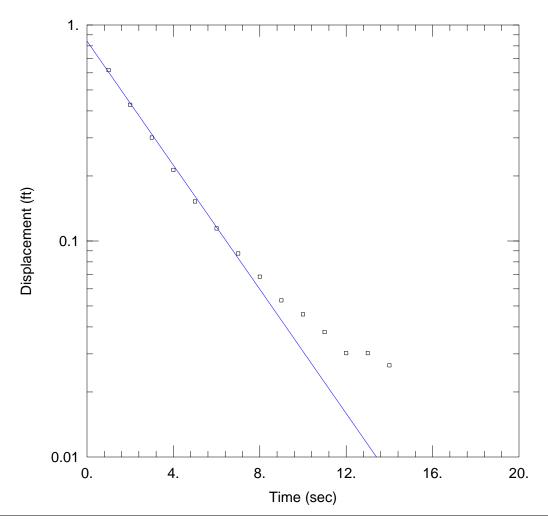
Aquifer Model: Unconfined

Solution Method: KGS Model

= 0.0003055 ft/secKr

 $= 9.38E-7 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\RMD-4-6R.aqt

Date: 11/12/18 Time: 14:58:13

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.121 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

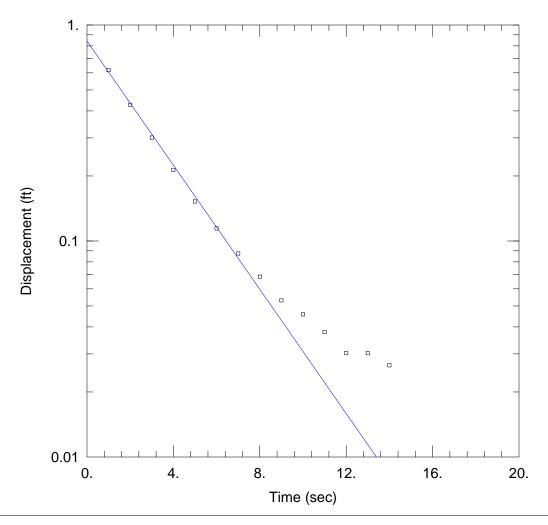
Screen Length: <u>20.</u> ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0002248 ft/sec y0 = 0.8417 ft



Data Set: N:\...\RMD-4-6R.aqt

Date: 11/12/18 Time: 14:58:30

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-4)

Initial Displacement: 1.121 ft

Total Well Penetration Depth: 50.37 ft

Total Well Perietration Depth. 50.31

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: <u>20.</u> ft Well Radius: 0.25 ft

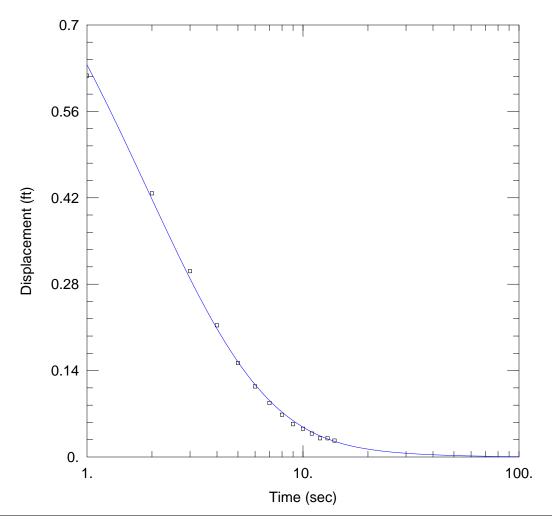
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002891 ft/sec

y0 = 0.8419 ft



Data Set: N:\...\RMD-4-6R.aqt

Date: 11/12/18 Time: 14:59:01

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: RMD-4 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 50.37 ft

WELL DATA (RMD-4)

Initial Displacement: 1.121 ft

Total Well Penetration Depth: 50.37 ft

Casing Radius: 0.083 ft

Static Water Column Height: 50.37 ft

Screen Length: 20. ft Well Radius: 0.25 ft

SOLUTION

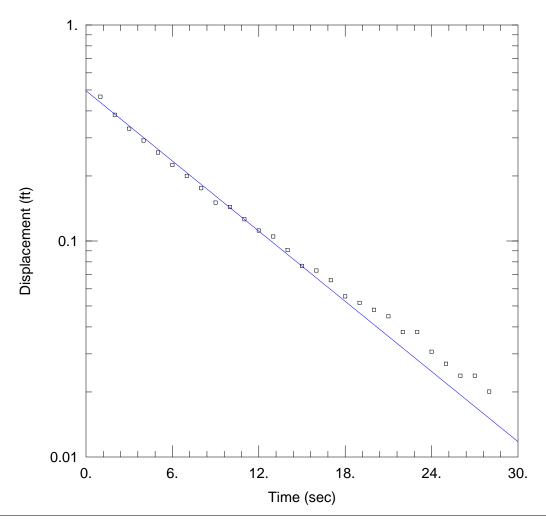
Aquifer Model: Unconfined

= 0.0002856 ft/sec Kr

Kz/Kr = 1.

Solution Method: KGS Model

 $= 1.514E-5 \text{ ft}^{-1}$



Data Set: N:\...\WMW-5_1F.aqt

Date: 11/12/18 Time: 15:28:22

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 1.095 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

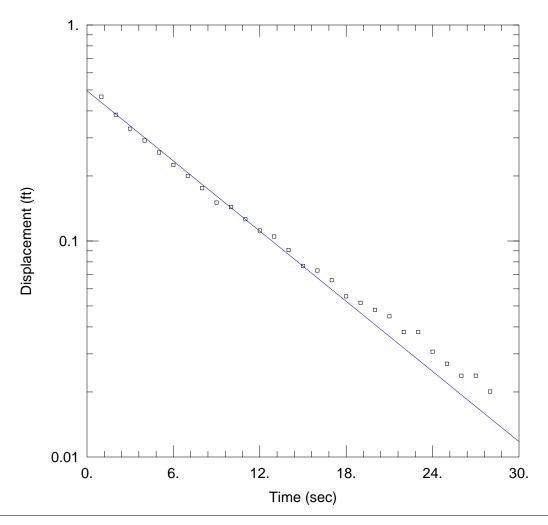
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001308 ft/sec

y0 = 0.4957 ft



Data Set: N:\...\WMW-5_1F.aqt

Date: 11/12/18 Time: 15:28:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 1.095 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

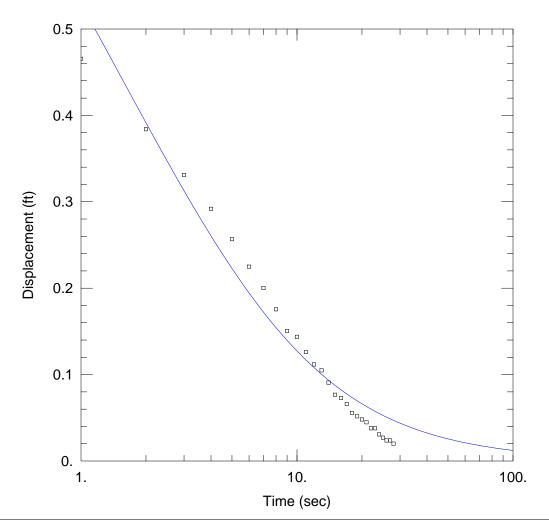
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0001882 ft/sec

y0 = 0.4956 ft



Data Set: N:\...\WMW-5_1F.aqt

Date: 11/12/18 Time: 15:27:47

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: <u>1696120</u>

Location: Wishram Railyard, Washington

Test Well: $\frac{WMW-5}{2016}$

AQUIFER DATA

Saturated Thickness: 14.51 ft

WELL DATA (WMW-5)

Initial Displacement: 1.095 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

SOLUTION

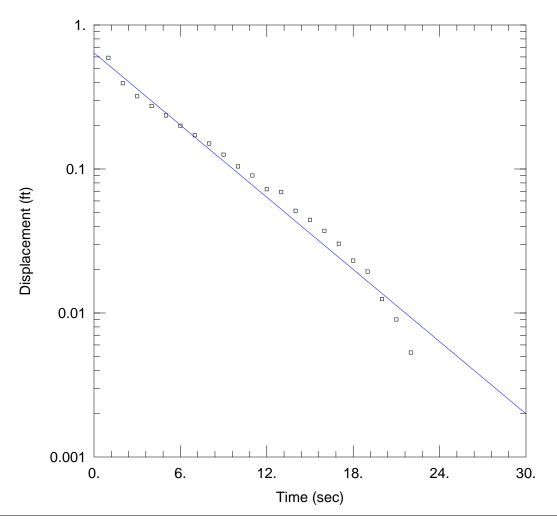
Aquifer Model: Unconfined

Kr = 0.0001455 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = 0.004829 ft^{-1}



Data Set: N:\...\WMW-5_2R.aqt

Date: 11/12/18 Time: 15:29:55

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 2.245 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

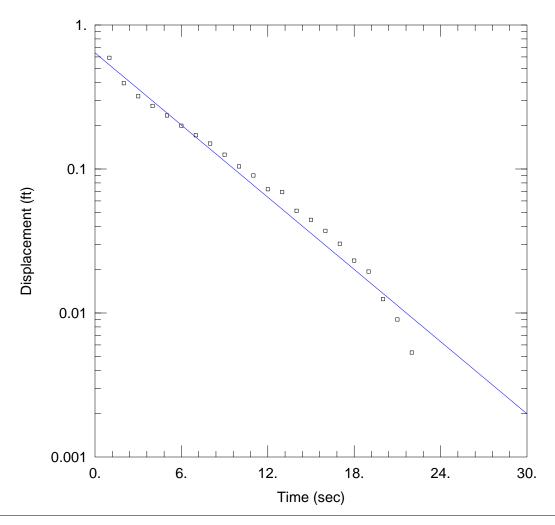
Screen Length: 10. ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0002019 ft/secy0 = 0.6402 ft



Data Set: N:\...\WMW-5_2R.aqt

Date: 11/12/18 Time: 15:30:17

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 2.245 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

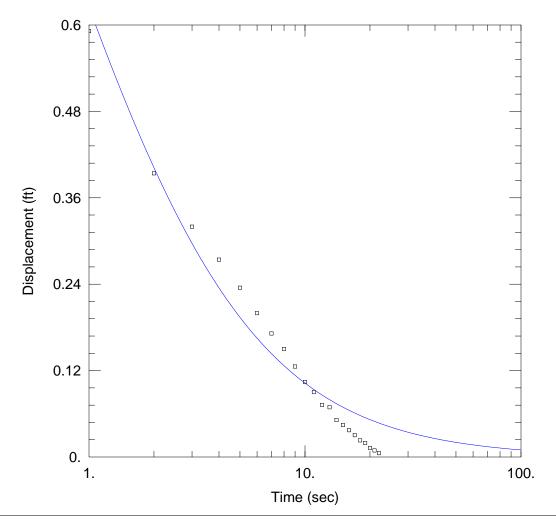
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002904 ft/sec

y0 = 0.6402 ft



Data Set: N:\...\WMW-5_2R.aqt

Date: 11/12/18 Time: 15:30:43

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: <u>1696120</u>

Location: Wishram Railyard, Washington

Test Well: $\frac{WMW-5}{2016}$

AQUIFER DATA

Saturated Thickness: 14.51 ft

WELL DATA (WMW-5)

Initial Displacement: 2.245 ft

Total Well Penetration Depth: 14.51 ft

Cooling Dodings 0.000 #

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

SOLUTION

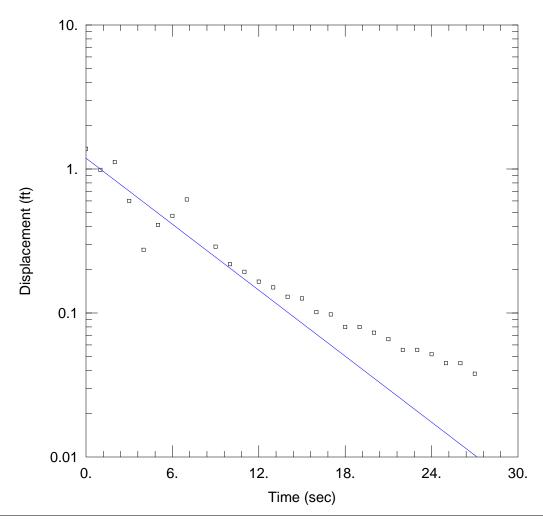
Aquifer Model: Unconfined

Kr = 0.0003517 ft/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.00811 ft^{-1}



Data Set: N:\...\WMW-5_3F.aqt

Date: 11/12/18 Time: 15:31:49

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 1.381 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

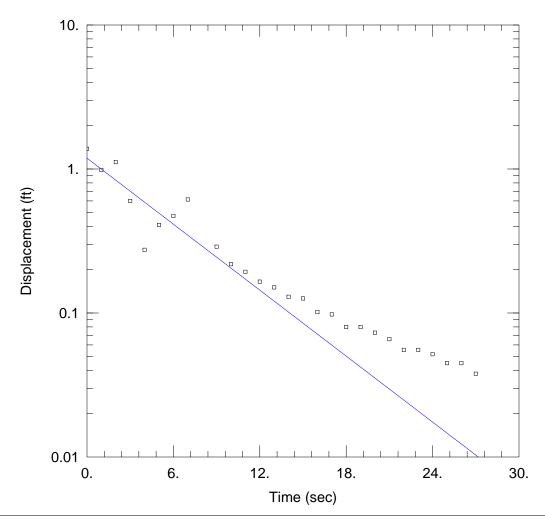
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001846 ft/sec

y0 = 1.188 ft



Data Set: N:\...\WMW-5_3F.aqt

Date: 11/12/18 Time: 15:32:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 1.381 ft

Casing Radius: 0.083 ft

Total Well Penetration Depth: 14.51 ft

Screen Length: 10. ft

Well Radius: 0.25 ft

SOLUTION

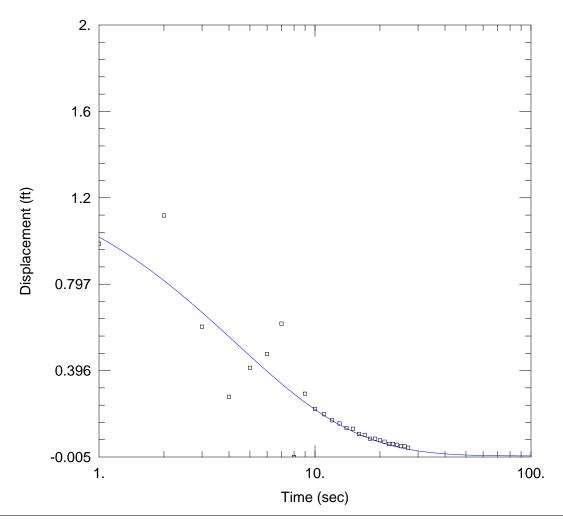
Aquifer Model: Unconfined

Solution Method: Hvorslev

Static Water Column Height: 14.51 ft

K = 0.0002654 ft/sec

y0 = 1.188 ft



Data Set: N:\...\WMW-5_3F.aqt

Date: 11/12/18 Time: 15:32:31

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft

WELL DATA (WMW-5)

Initial Displacement: 1.381 ft

Static Water Column Height: 14.51 ft

Total Well Penetration Depth: 14.51 ft

Screen Length: 10. ft

Casing Radius: 0.083 ft

Well Radius: 0.25 ft

SOLUTION

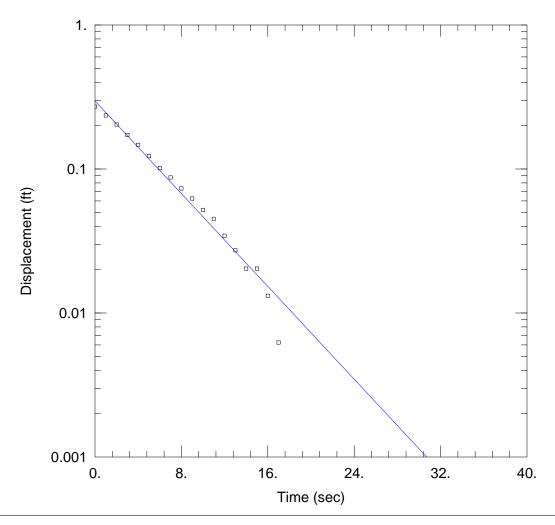
Aquifer Model: Unconfined

Solution Method: KGS Model

= 0.0002287 ft/sec Kr

 $= 5.373E-5 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\WMW-5_4R.aqt

Date: 11/12/18 Time: 15:34:33

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 0.2711 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

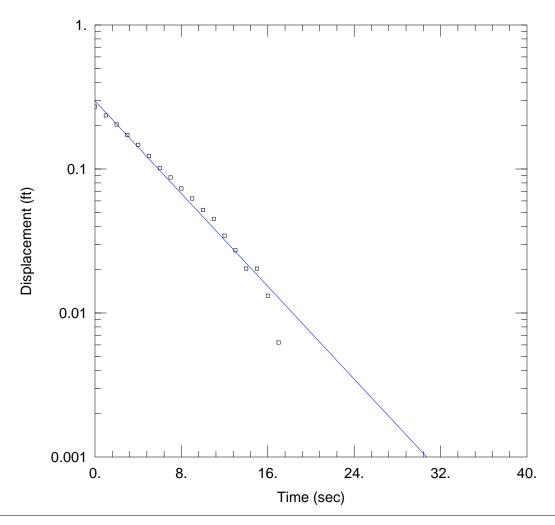
Screen Length: 10. ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001945 ft/secy0 = 0.2967 ft



Data Set: N:\...\WMW-5_4R.aqt

Date: 11/12/18 Time: 15:35:00

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 0.2711 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

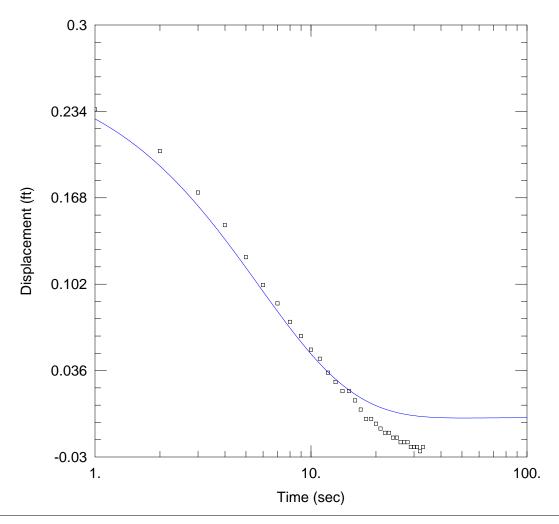
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002797 ft/sec

y0 = 0.2966 ft



Data Set: N:\...\WMW-5_4R.aqt

Date: 11/12/18 Time: 15:35:21

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft

WELL DATA (WMW-5)

Initial Displacement: 0.2711 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

SOLUTION

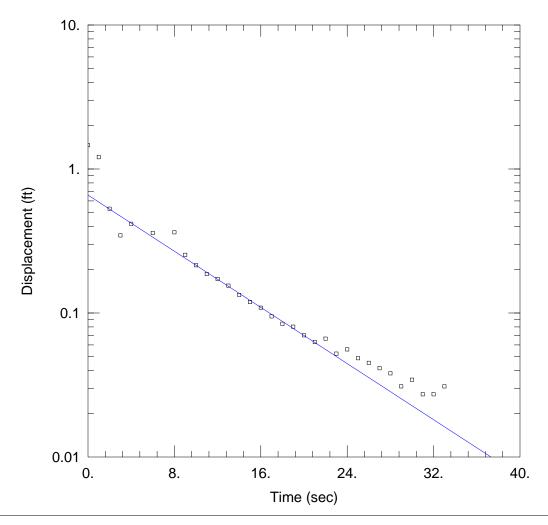
Aquifer Model: Unconfined

= 0.0002109 ft/sec Kr

Kz/Kr = 1.

Solution Method: KGS Model

 $= 1.429E-11 \text{ ft}^{-1}$



Data Set: N:\...\WMW-5_5F.aqt

Date: 11/12/18 Time: 15:41:16

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 1.463 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

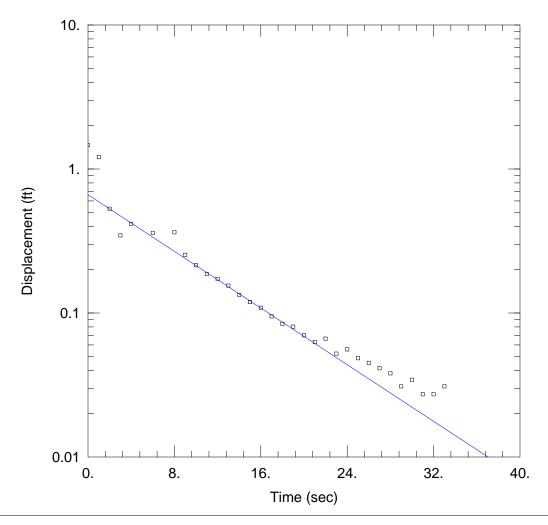
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001177 ft/sec

y0 = 0.6584 ft



Data Set: N:\...\WMW-5_5F.aqt

Date: 11/12/18 Time: 15:42:37

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 1.463 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

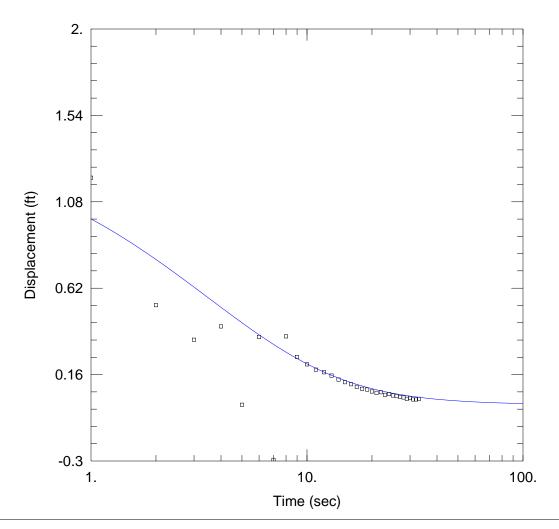
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0001709 ft/sec

y0 = 0.6623 ft



Data Set: N:\...\WMW-5_5F.aqt

Date: 11/12/18 Time: 15:43:00

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: $\frac{WMW-5}{2016}$

AQUIFER DATA

Saturated Thickness: 14.51 ft

WELL DATA (WMW-5)

Initial Displacement: 1.463 ft

1.403 11

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

SOLUTION

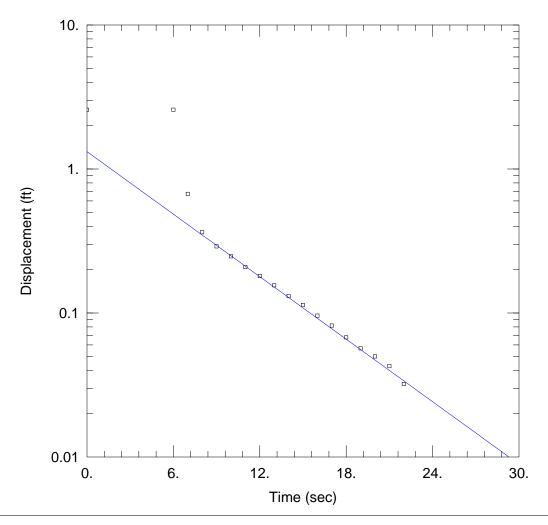
Aquifer Model: Unconfined

Kr = 0.0002048 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

 $Ss = 0.0002562 \text{ ft}^{-1}$



Data Set: N:\...\WMW-5_6R.aqt

Date: 11/12/18 Time: 15:44:08

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 2.578 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

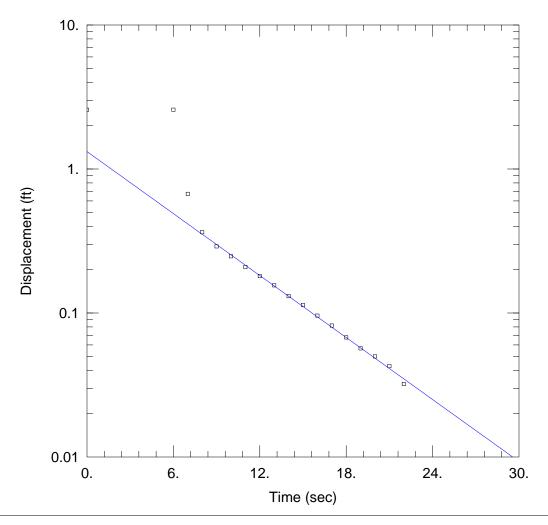
Screen Length: 10. ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001748 ft/secy0 = 1.319 ft



Data Set: N:\...\WMW-5_6R.aqt

Date: 11/12/18 Time: 15:44:32

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-5)

Initial Displacement: 2.578 ft

Total Well Penetration Depth: 14.51 ft

Casing Radius: 0.083 ft

Static Water Column Height: 14.51 ft

Screen Length: 10. ft Well Radius: 0.25 ft

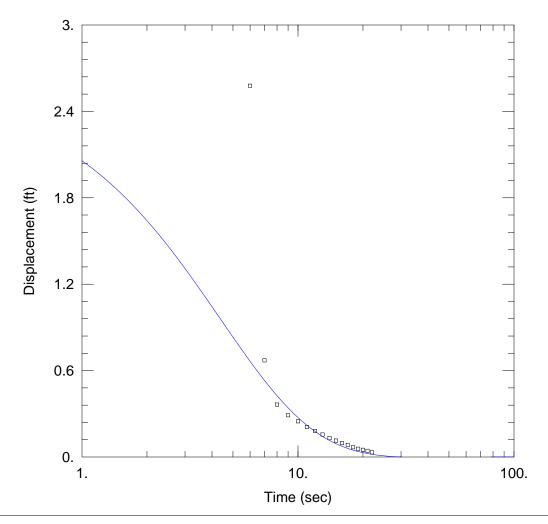
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002494 ft/sec

y0 = 1.32 ft



Data Set: N:\...\WMW-5_6R.aqt

Date: 11/12/18 Time: 15:45:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-5 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 14.51 ft

WELL DATA (WMW-5)

Initial Displacement: 2.578 ft

Screen Length: 10. ft

Total Well Penetration Depth: 14.51 ft Casing Radius: 0.083 ft Well Radius: 0.25 ft

SOLUTION

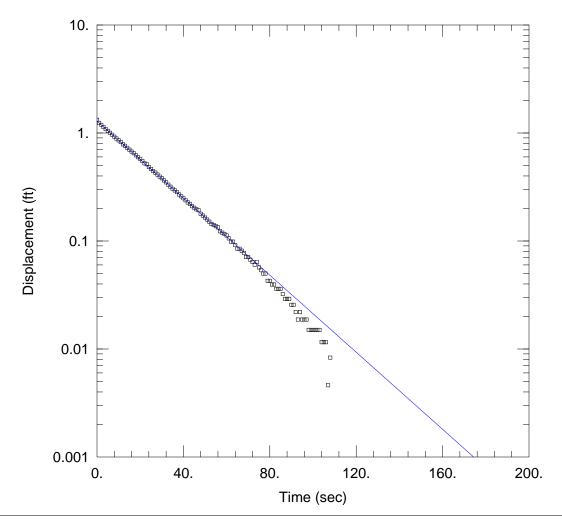
Aquifer Model: Unconfined

Solution Method: KGS Model $= 1.429E-11 \text{ ft}^{-1}$

Static Water Column Height: 14.51 ft

= 0.000277 ft/sec Kr

Kz/Kr = 1.



Data Set: N:\...\WMW-7_1R.aqt

Date: 11/13/18 Time: 09:08:49

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-7)

Initial Displacement: 1.324 ft

Total Well Penetration Depth: 7.72 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

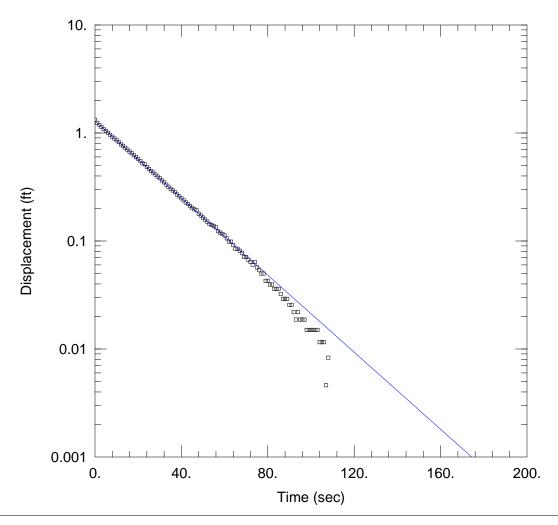
Screen Length: 7.72 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 4.756E-5 ft/sec y0 = 1.29 ft



Data Set: N:\...\WMW-7_1R.aqt

Date: 11/13/18 Time: 09:09:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-7)

Initial Displacement: 1.324 ft

Total Well Penetration Depth: 7.72 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

Screen Length: 7.72 ft Well Radius: 0.25 ft

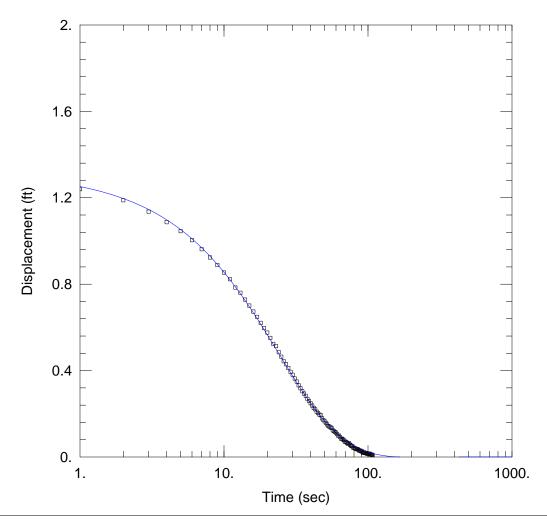
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 9.71E-5 ft/sec

y0 = 1.29 ft



Data Set: N:\...\WMW-7_1R.aqt

Date: 11/13/18 Time: 09:09:24

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft

WELL DATA (WMW-7)

Initial Displacement: 1.324 ft

Total Well Penetration Depth: 7.72 ft

Cooing Doding, 0.002 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

Screen Length: 7.72 ft Well Radius: 0.25 ft

SOLUTION

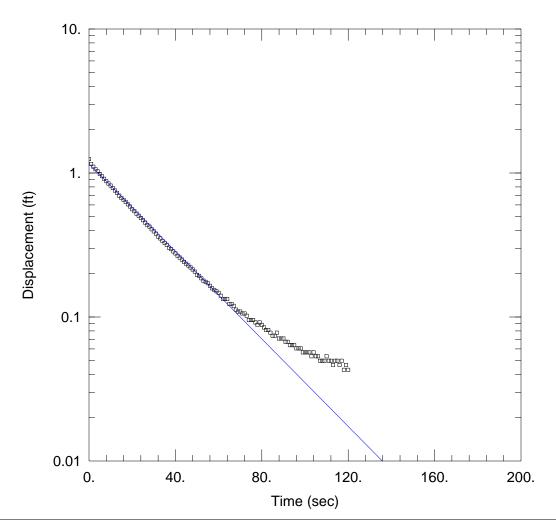
Aquifer Model: Unconfined

Kr = 5.312E-5 ft/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $8.202E-6 \text{ ft}^{-1}$



Data Set: N:\...\WMW-7_2R.aqt

Date: 11/13/18 Time: 09:07:03

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-7)

Initial Displacement: 1.249 ft

Total Well Penetration Depth: 7.72 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

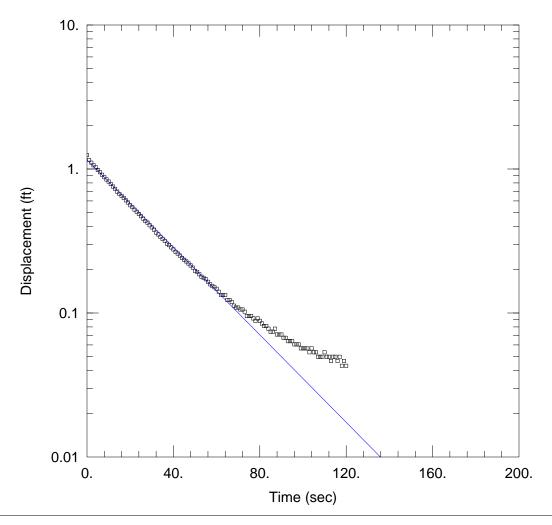
Screen Length: 7.72 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 4.052E-5 ft/sec y0 = 1.158 ft



Data Set: N:\...\WMW-7_2R.aqt

Date: 11/13/18 Time: 09:07:21

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-7)

Initial Displacement: 1.249 ft

Total Well Penetration Depth: 7.72 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

Screen Length: 7.72 ft Well Radius: 0.25 ft

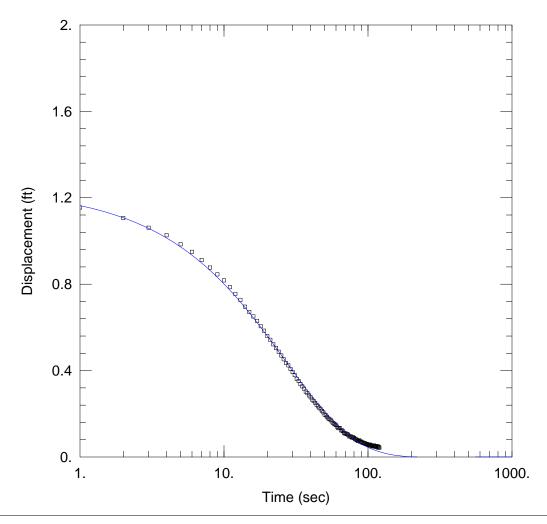
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 8.271E-5 ft/sec

y0 = 1.158 ft



Data Set: N:\...\WMW-7_2R.aqt

Date: 11/13/18 Time: 09:07:41

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft

WELL DATA (WMW-7)

Initial Displacement: 1.249 ft

Static Water Column Height: 7.72 ft

Total Well Penetration Depth: 7.72 ft

Screen Length: 7.72 ft Well Radius: 0.25 ft

Casing Radius: 0.083 ft

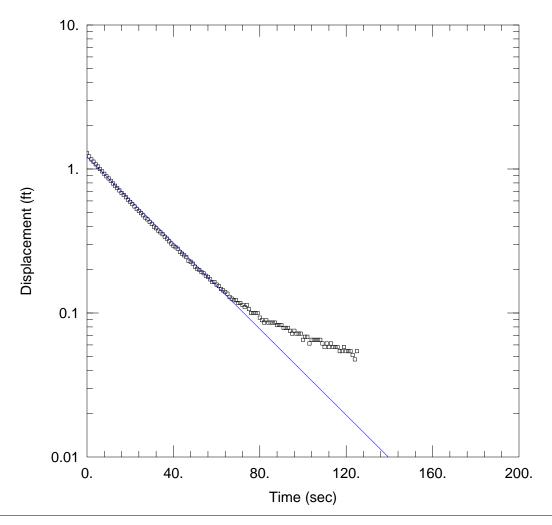
SOLUTION

Aquifer Model: Unconfined

Solution Method: KGS Model

= 4.663E-5 ft/sec Kr

 $= 4.658E-5 \text{ ft}^{-1}$



Data Set: N:\...\WMW-7_3R.aqt

Date: 11/13/18 Time: 09:11:24

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-7)

Initial Displacement: 1.287 ft

Total Well Penetration Depth: 7.72 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

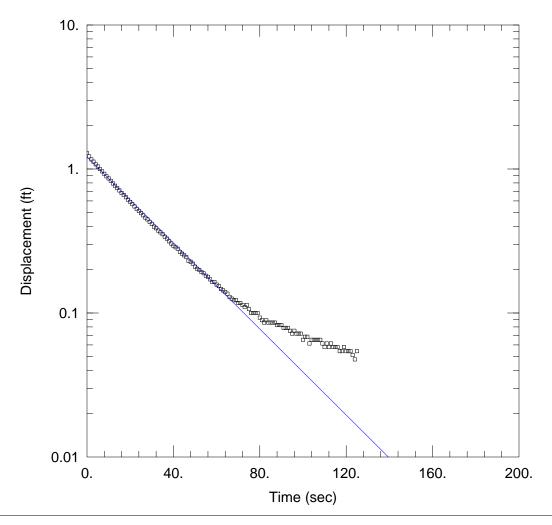
Screen Length: 7.72 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 3.983E-5 ft/sec y0 = 1.212 ft



Data Set: N:\...\WMW-7_3R.aqt

Date: 11/13/18 Time: 09:11:50

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-7)

Initial Displacement: 1.287 ft

Total Well Penetration Depth: 7.72 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

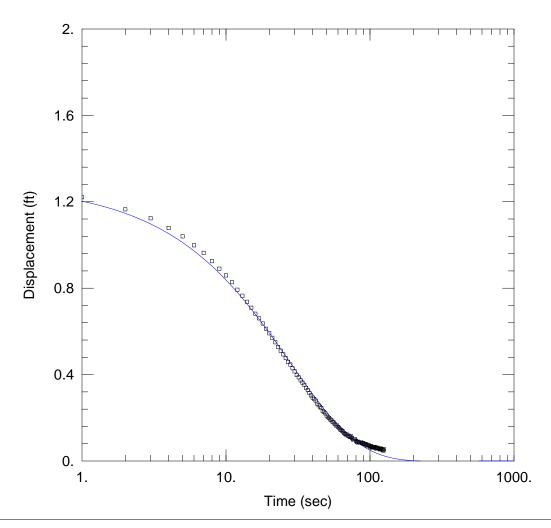
Screen Length: 7.72 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 8.131E-5 ft/secy0 = 1.212 ft



Data Set: N:\...\WMW-7_3R.aqt

Date: 11/13/18 Time: 09:12:14

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-7 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 7.72 ft

WELL DATA (WMW-7)

Initial Displacement: 1.287 ft

Total Well Penetration Depth: 7.72 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.72 ft

Screen Length: 7.72 ft Well Radius: 0.25 ft

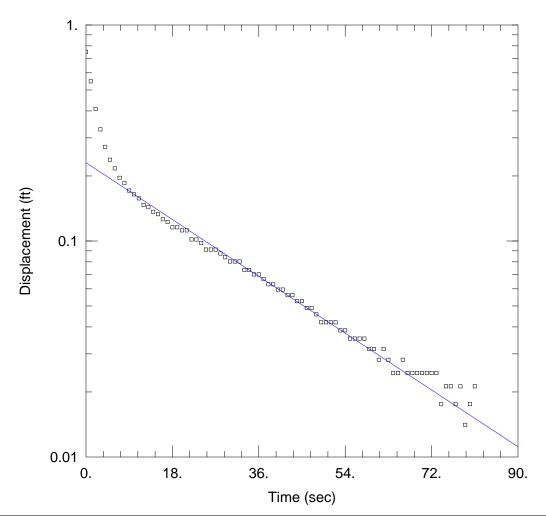
SOLUTION

Aquifer Model: Unconfined

= 4.512E-5 ft/sec

Kr Kz/Kr = 1. Solution Method: KGS Model

 $= 4.368E-5 \text{ ft}^{-1}$



Data Set: N:\...\WMW-9_1R.aqt

Date: 11/13/18 Time: 09:21:47

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: $\frac{WMW-9}{2016}$

AQUIFER DATA

Saturated Thickness: 12.27 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-9)

Initial Displacement: 0.7513 ft

Total Well Penetration Depth: 12.27 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

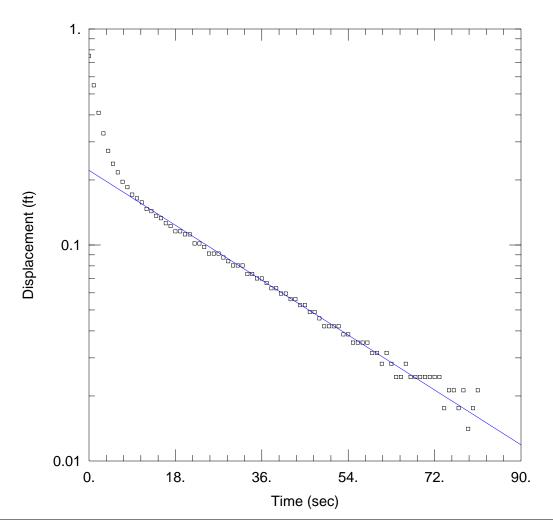
Screen Length: 12.27 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 2.814E-5 ft/sec y0 = 0.2303 ft



Data Set: N:\...\WMW-9_1R.aqt

Date: 11/13/18 Time: 09:22:58

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-9)

Initial Displacement: 0.7513 ft

Total Well Penetration Depth: 12.27 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

Screen Length: 12.27 ft Well Radius: 0.25 ft

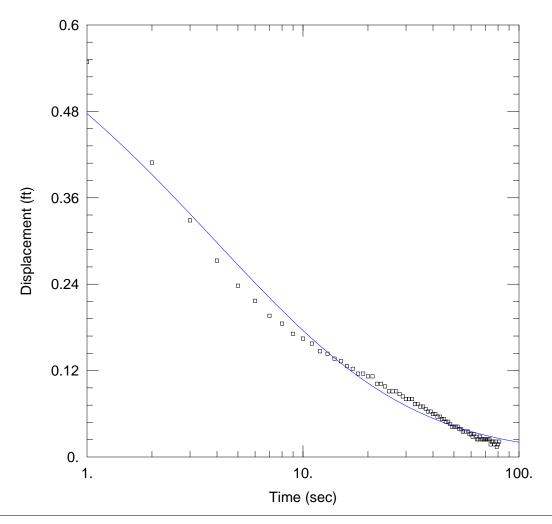
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 4.836E-5 ft/sec

y0 = 0.2216 ft



Data Set: N:\...\WMW-9_1R.aqt

Date: 11/13/18 Time: 09:23:19

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft

WELL DATA (WMW-9)

Initial Displacement: 0.7513 ft

Total Well Penetration Depth: 12.27 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

Screen Length: 12.27 ft Well Radius: 0.25 ft

SOLUTION

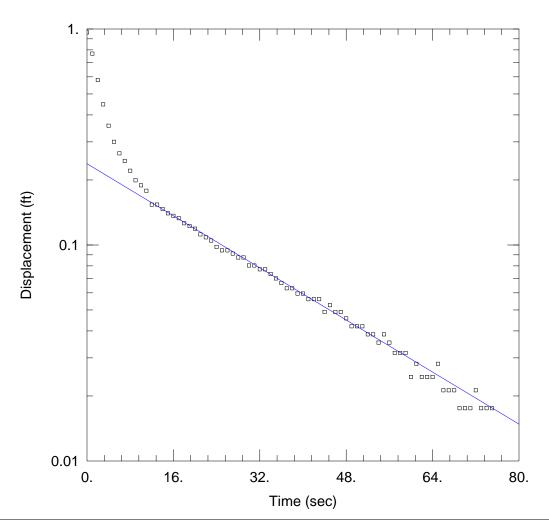
Aquifer Model: Unconfined

= 4.975E-5 ft/sec Kr

Kz/Kr = 1.

Solution Method: KGS Model

 $= 0.003638 \text{ ft}^{-1}$



Data Set: N:\...\WMW-9_2R.aqt

Date: 11/13/18 Time: 09:24:23

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-9)

Initial Displacement: 0.9642 ft

Total Well Penetration Depth: 12.27 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

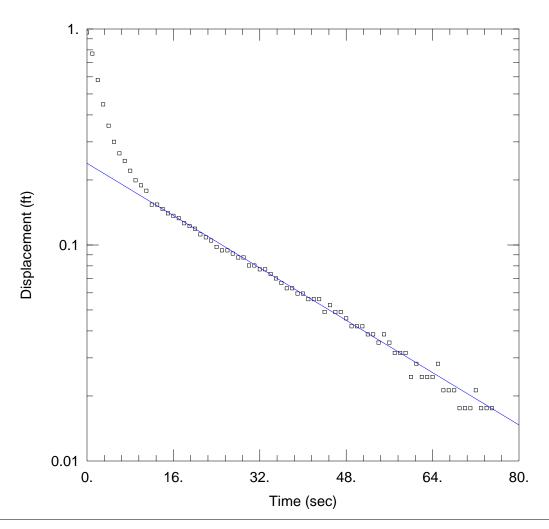
Screen Length: 12.27 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 2.902E-5 ft/secy0 = 0.2378 ft



Data Set: N:\...\WMW-9_2R.aqt

Date: 11/13/18 Time: 09:24:47

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-9)

Initial Displacement: 0.9642 ft

Static Water Column Height: 12.27 ft

Total Well Penetration Depth: 12.27 ft

Screen Length: 12.27 ft Well Radius: 0.25 ft

Casing Radius: 0.083 ft

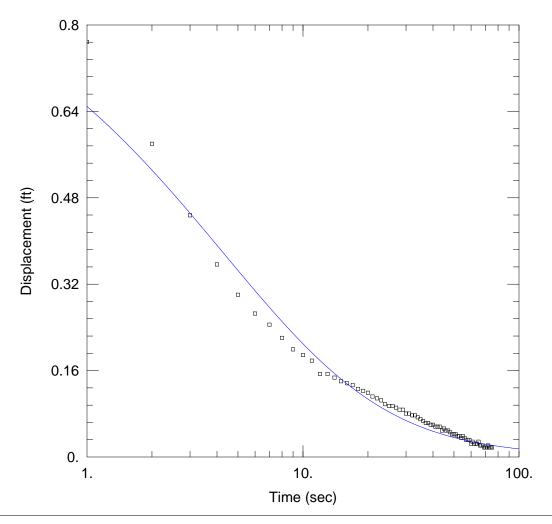
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 5.186E-5 ft/sec

y0 = 0.2389 ft



Data Set: N:\...\WMW-9_2R.aqt

Date: 11/13/18 Time: 09:25:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft

WELL DATA (WMW-9)

Initial Displacement: 0.9642 ft

Total Well Penetration Depth: 12.27 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

Screen Length: 12.27 ft Well Radius: 0.25 ft

SOLUTION

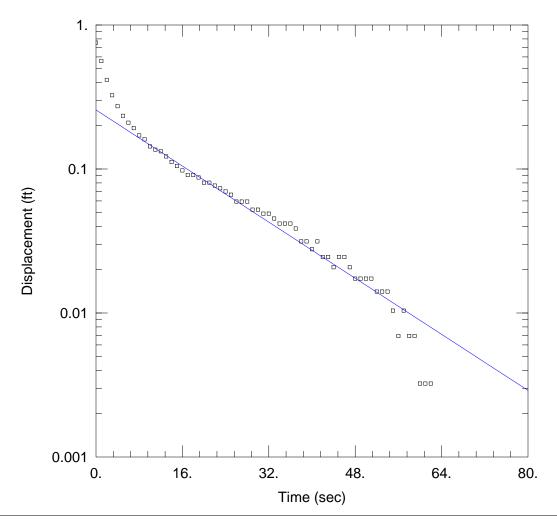
Aquifer Model: Unconfined

Kr = 8.054E-5 ft/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.00113 ft^{-1}



Data Set: N:\...\WMW-9_3R.aqt

Date: 11/13/18 Time: 09:25:59

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-9)

Initial Displacement: 0.7546 ft

Total Well Penetration Depth: 12.27 ft

Cooling Dodings 0.002 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

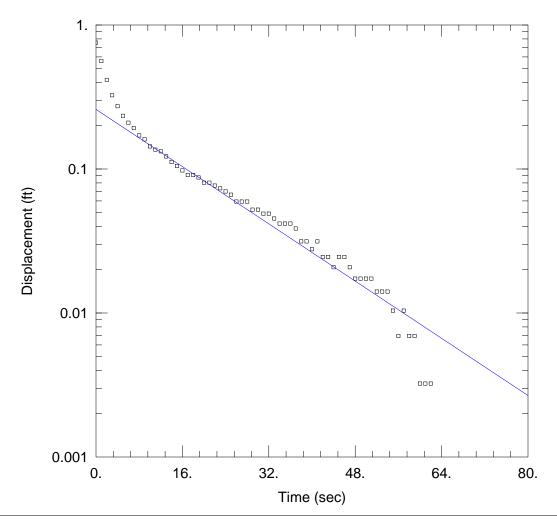
Screen Length: 12.27 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 4.687E-5 ft/sec y0 = 0.2568 ft



Data Set: N:\...\WMW-9_3R.aqt

Date: 11/13/18 Time: 09:26:37

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-9)

Initial Displacement: 0.7546 ft

Total Well Penetration Depth: 12.27 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

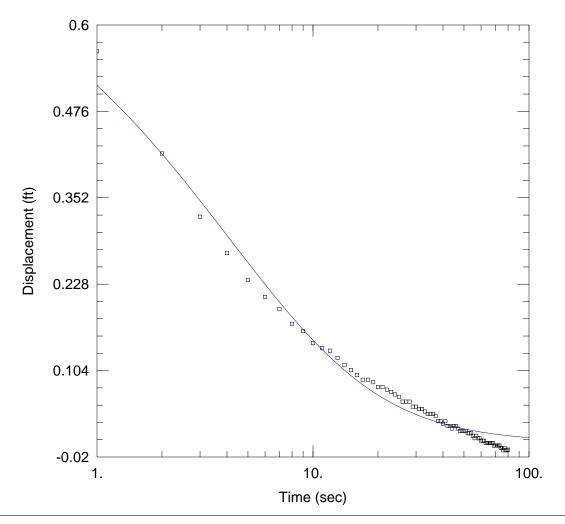
Screen Length: 12.27 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 8.505E-5 ft/sec y0 = 0.2592 ft



Data Set: N:\...\WMW-9_3R.aqt

Date: 11/13/18 Time: 09:33:39

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-9 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.27 ft

WELL DATA (WMW-9)

Initial Displacement: 0.7546 ft

Total Well Penetration Depth: 12.27 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.27 ft

Screen Length: 12.27 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

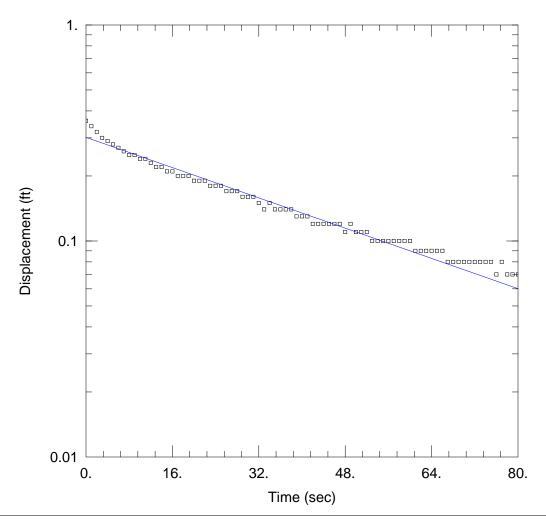
= 0.0001036 ft/sec

Kz/Kr = 1.

Kr

Solution Method: KGS Model

 $= 0.000633 \text{ ft}^{-1}$



Data Set: N:\...\WMW-15_1R.aqt

Date: 11/13/18 Time: 09:53:18

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-15)

Initial Displacement: 0.36 ft

Total Well Penetration Depth: 12.18 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.18 ft

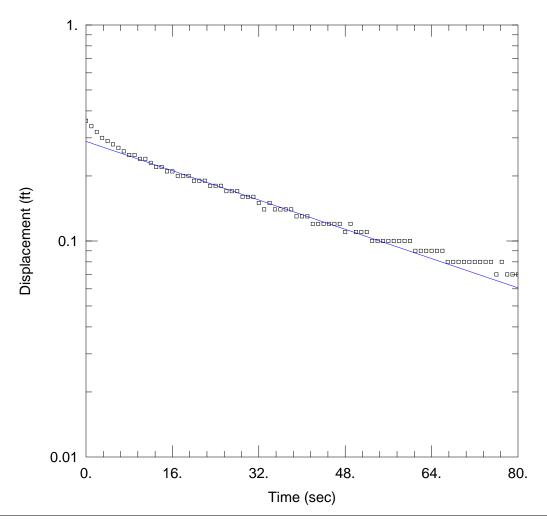
Screen Length: 12.18 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.695E-5 ft/sec y0 = 0.3018 ft



Data Set: N:\...\WMW-15_1R.aqt

Date: 11/13/18 Time: 09:54:37

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-15)

Initial Displacement: 0.36 ft

Total Well Penetration Depth: 12.18 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.18 ft

Screen Length: 12.18 ft Well Radius: 0.25 ft

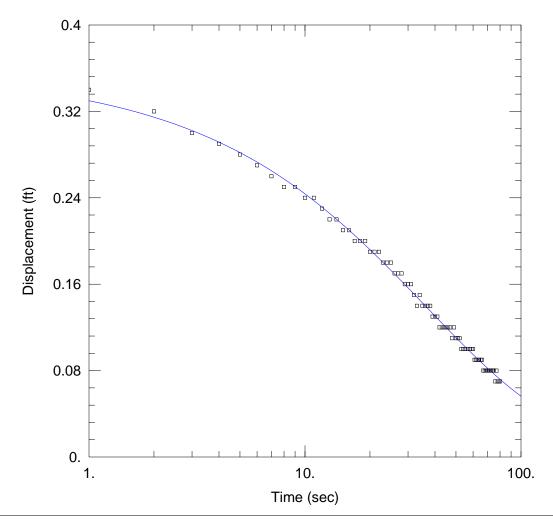
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 2.924E-5 ft/sec

y0 = 0.289 ft



Data Set: N:\...\WMW-15_1R.aqt

Date: 11/13/18 Time: 09:55:00

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft

WELL DATA (WMW-15)

Initial Displacement: 0.36 ft

.. <u>0.30</u> II

Total Well Penetration Depth: 12.18 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.18 ft

Screen Length: 12.18 ft Well Radius: 0.25 ft

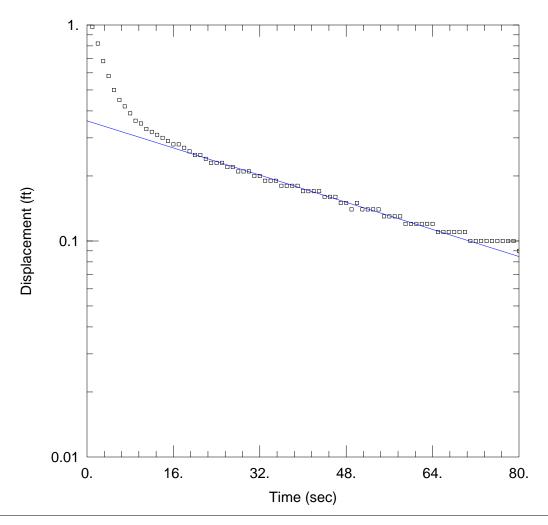
SOLUTION

Aquifer Model: Unconfined

Solution Method: $\underline{\mathsf{KGS}\;\mathsf{Model}}$

Kr = 1.475E-5 ft/sec

Ss = 0.000289 ft^{-1}



Data Set: N:\...\WMW-15_2R.aqt

Date: 11/13/18 Time: 09:58:21

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-15)

Initial Displacement: 1.1 ft

Total Well Penetration Depth: 12.18 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.18 ft

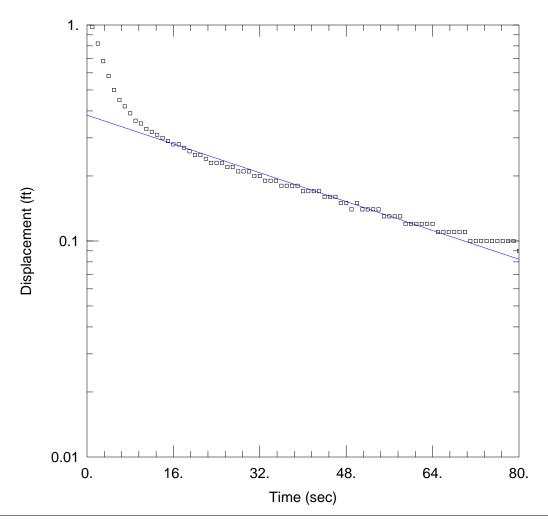
Screen Length: 12.18 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.52E-5 ft/sec y0 = 0.3599 ft



Data Set: N:\...\WMW-15_2R.aqt

Date: 11/13/18 Time: 10:00:35

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-15)

Initial Displacement: 1.1 ft

Total Well Penetration Depth: 12.18 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.18 ft

Screen Length: 12.18 ft Well Radius: 0.25 ft

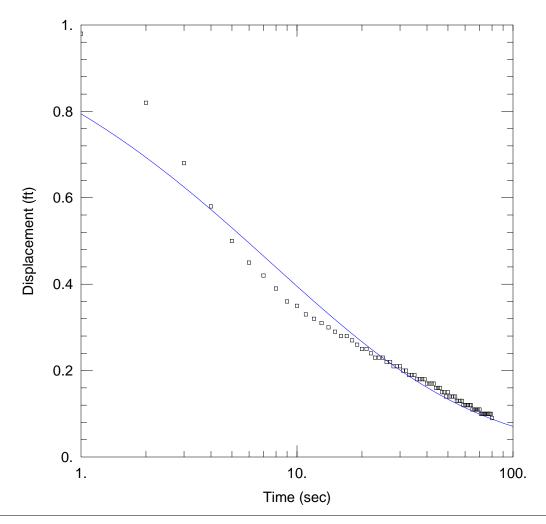
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 2.876E-5 ft/sec

y0 = 0.3822 ft



Data Set: N:\...\WMW-15_2R.aqt

Date: 11/13/18 Time: 10:07:27

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: <u>1696120</u>

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft

WELL DATA (WMW-15)

Initial Displacement: 1.1 ft

Ctatic V

Total Well Penetration Depth: 12.18 ft

Static Water Column Height: 12.18 ft

Casing Radius: 0.083 ft

Screen Length: 12.18 ft Well Radius: 0.25 ft

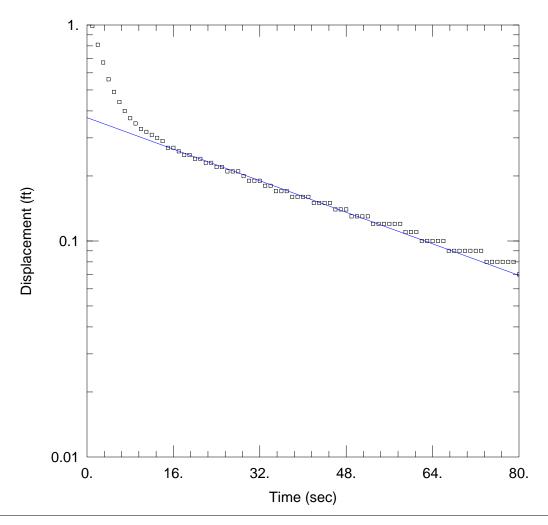
SOLUTION

Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 2.108E-5 ft/sec

Ss = 0.004848 ft^{-1}



Data Set: N:\...\WMW-15_3R.aqt

Date: 11/13/18 Time: 10:08:46

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-15)

Initial Displacement: 1.28 ft

Total Well Penetration Depth: 12.18 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.18 ft

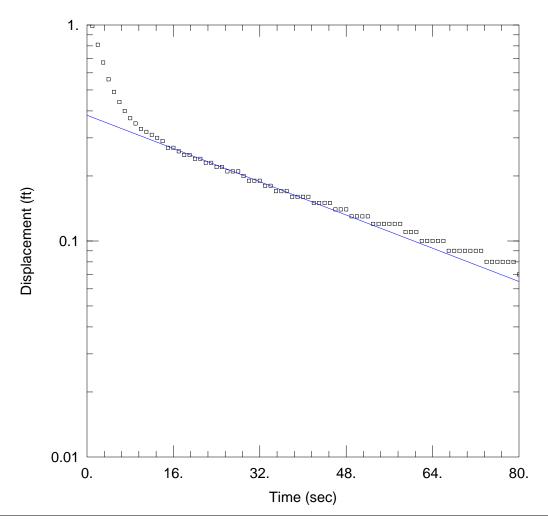
Screen Length: 12.18 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.767E-5 ft/sec y0 = 0.3724 ft



Data Set: N:\...\WMW-15_3R.aqt

Date: 11/13/18 Time: 10:09:15

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-15)

Initial Displacement: 1.28 ft

Casing Radius: 0.083 ft

Total Well Penetration Depth: 12.18 ft

: 12.18 ft

Static Water Column Height: 12.18 ft

Screen Length: 12.18 ft Well Radius: 0.25 ft

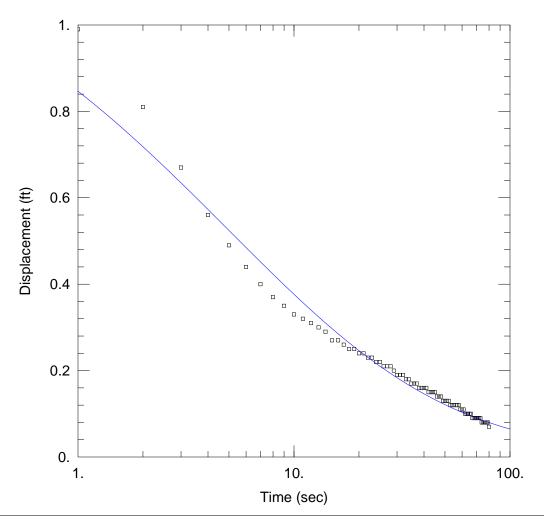
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 3.318E-5 ft/sec

y0 = 0.3819 ft



Data Set: N:\...\WMW-15_3R.aqt

Date: 11/13/18 Time: 10:09:37

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.18 ft

WELL DATA (WMW-15)

Initial Displacement: 1.28 ft

Total Well Penetration Depth: 12.18 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.18 ft

Screen Length: 12.18 ft Well Radius: 0.25 ft

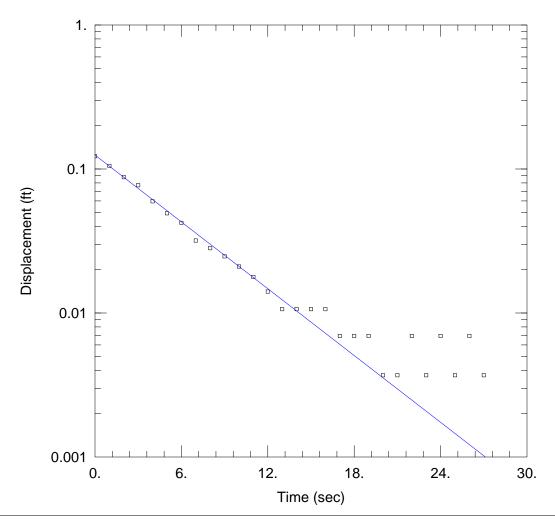
SOLUTION

Aquifer Model: Unconfined

Solution Method: KGS Model

= 2.519E-5 ft/sec Kr

 $= 0.007024 \text{ ft}^{-1}$



Data Set: N:\...\WMW-18_1R.aqt

Date: 11/13/18 Time: 10:13:50

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-18)

Initial Displacement: 0.1226 ft

Total Well Penetration Depth: 12.61 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.61 ft

Screen Length: 12.61 ft Well Radius: 0.25 ft

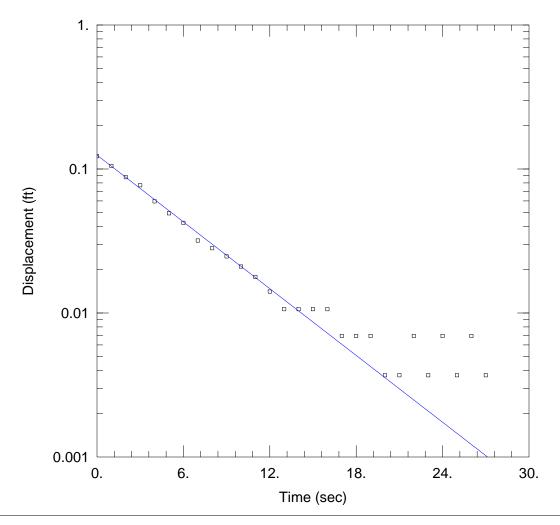
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.000146 ft/sec

y0 = 0.1249 ft



Data Set: N:\...\WMW-18_1R.aqt

Date: 11/13/18 Time: 10:14:13

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-18)

Initial Displacement: 0.1226 ft

Static Water Column Height: 12.61 ft

Total Well Penetration Depth: 12.61 ft

Screen Length: 12.61 ft Well Radius: 0.25 ft

Casing Radius: 0.083 ft

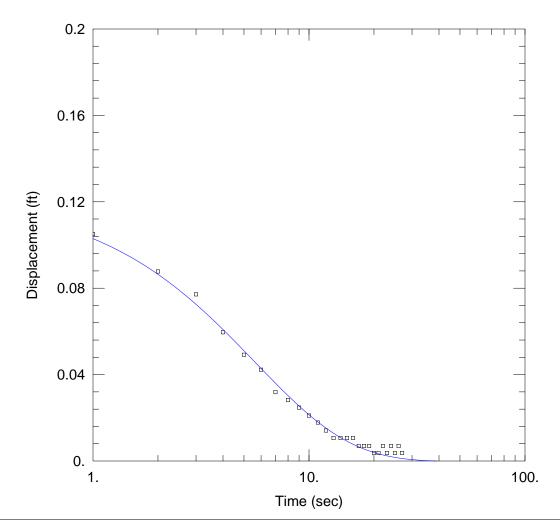
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002576 ft/sec

y0 = 0.1248 ft



Data Set: N:\...\WMW-18_1R.aqt

Date: 11/13/18 Time: 10:14:34

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft

WELL DATA (WMW-18)

Initial Displacement: 0.1226 ft

Total Well Penetration Depth: 12.61 ft

Screen Length: 12.61 ft

Static Water Column Height: 12.61 ft

Casing Radius: 0.083 ft

Well Radius: 0.25 ft

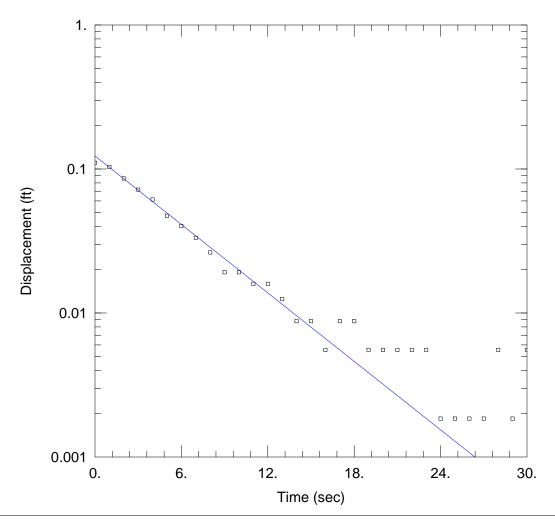
SOLUTION

Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 0.0001571 ft/sec

Ss = $1.111E-11 \text{ ft}^{-1}$



Data Set: N:\...\WMW-18_2R.aqt

Date: 11/13/18 Time: 10:15:20

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-18)

Initial Displacement: 0.1104 ft

Total Well Penetration Depth: 12.61 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.61 ft

Screen Length: 12.61 ft Well Radius: 0.25 ft

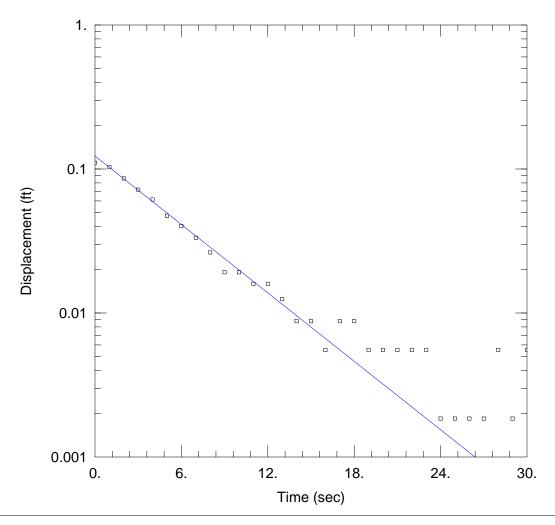
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001496 ft/sec

y0 = 0.1231 ft



Data Set: N:\...\WMW-18_2R.aqt

Date: 11/13/18 Time: 10:17:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-18)

Initial Displacement: 0.1104 ft

Total Well Penetration Depth: 12.61 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.61 ft

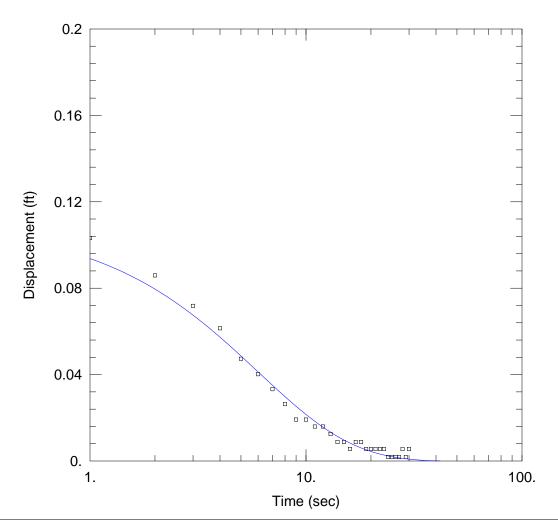
Screen Length: 12.61 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.000264 ft/sec y0 = 0.1231 ft



Data Set: N:\...\WMW-18_2R.aqt

Date: 11/13/18 Time: 10:17:29

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15 Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft

WELL DATA (WMW-18)

Initial Displacement: 0.1104 ft

Static Water Column Height: 12.61 ft

Total Well Penetration Depth: 12.61 ft

Screen Length: 12.61 ft

Casing Radius: 0.083 ft

Well Radius: 0.25 ft

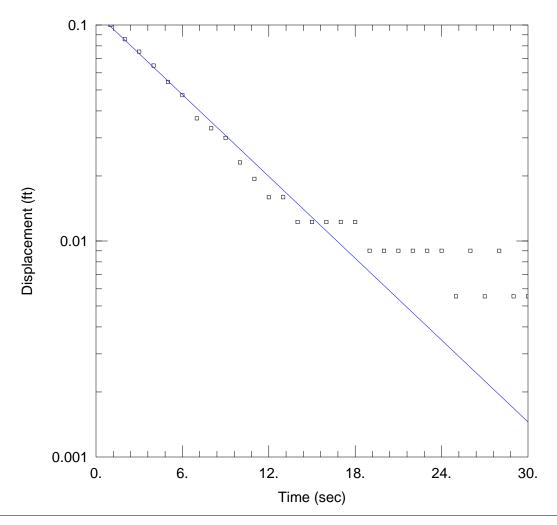
SOLUTION

Aquifer Model: Unconfined

Solution Method: KGS Model

= 0.000147 ft/secKr

 $= 1.111E-11 \text{ ft}^{-1}$



Data Set: N:\...\WMW-18_3R.aqt

Date: 11/13/18 Time: 10:19:34

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-18)

Initial Displacement: 0.1104 ft

Total Well Penetration Depth: 12.61 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.61 ft

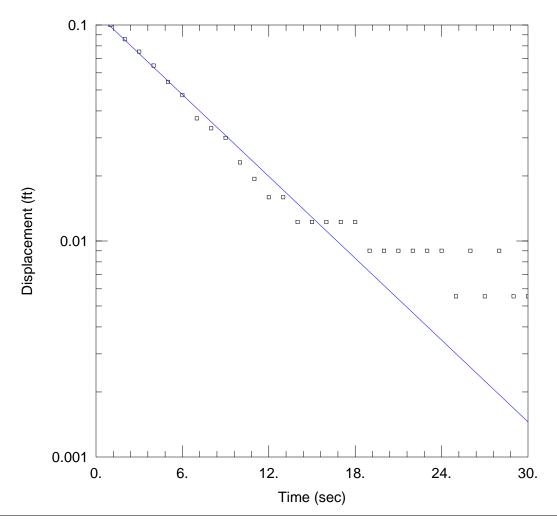
Screen Length: 12.61 ft Well Radius: 0.25 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001192 ft/sec y0 = 0.1139 ft



Data Set: N:\...\WMW-18_3R.aqt

Date: 11/13/18 Time: 10:20:14

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1696120

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-18)

Initial Displacement: 0.1104 ft

Total Well Penetration Depth: 12.61 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.61 ft

Screen Length: 12.61 ft Well Radius: 0.25 ft

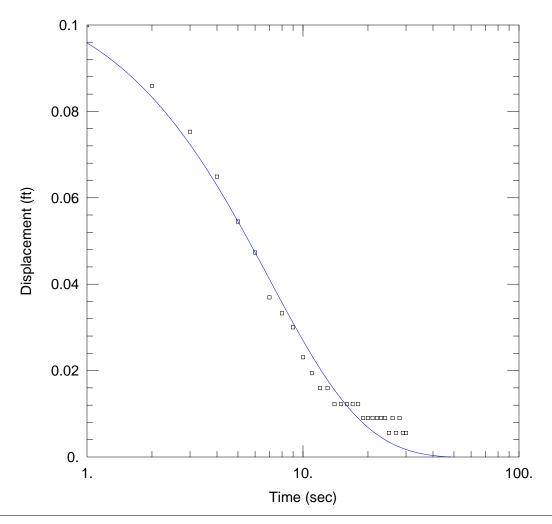
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002104 ft/sec

y0 = 0.1139 ft



Data Set: N:\...\WMW-18_3R.aqt

Date: 11/13/18 Time: 10:20:36

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: <u>1696120</u>

Location: Wishram Railyard, Washington

Test Well: WMW-15
Test Date: 2016

AQUIFER DATA

Saturated Thickness: 12.61 ft

WELL DATA (WMW-18)

Initial Displacement: 0.1104 ft

Total Well Penetration Depth: 12.61 ft

Casing Radius: 0.083 ft

Static Water Column Height: 12.61 ft

Screen Length: 12.61 ft Well Radius: 0.25 ft

SOLUTION

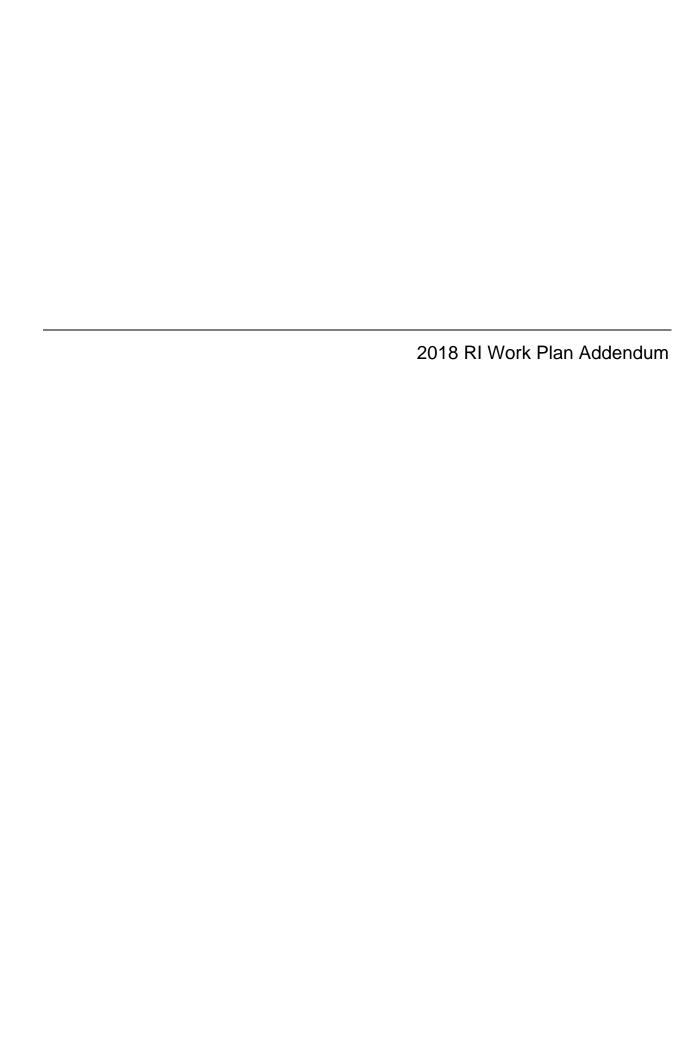
Aquifer Model: Unconfined

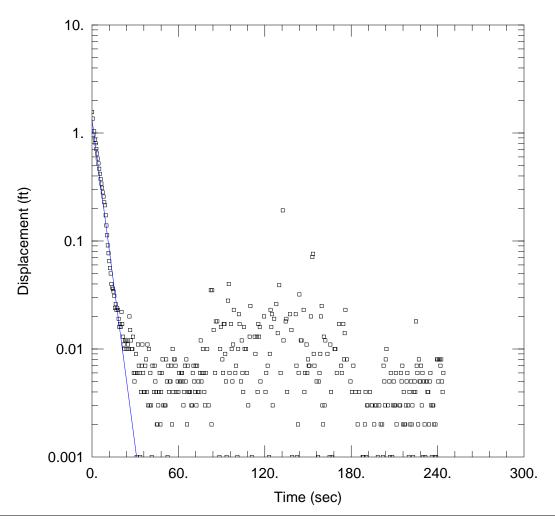
Kr = 0.0001265 ft/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $1.111E-11 \text{ ft}^{-1}$





TEST 1 - FALLING

Data Set: N:\...\RMD-06-1F.aqt

Date: 10/05/18 Time: 14:29:23

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants

Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.89 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 1.566 ft

Static Water Column Height: 47.89 ft

Total Well Penetration Depth: 47.89 ft

Screen Length: 20. ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

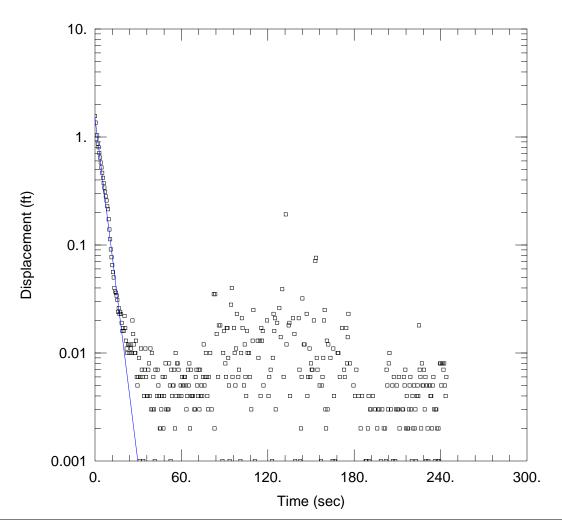
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001799 ft/sec

y0 = 1.336 ft



TEST 1 - FALLING

Data Set: N:\...\RMD-06-1F.aqt

Date: <u>10/05/18</u> Time: <u>14:27:45</u>

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants

Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: $\frac{\text{RMD-06}}{\text{8/28/18}}$

AQUIFER DATA

Saturated Thickness: 47.89 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 1.566 ft

Static Water Column Height: 47.89 ft

Total Well Penetration Depth: 47.89 ft

Screen Length: 20. ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

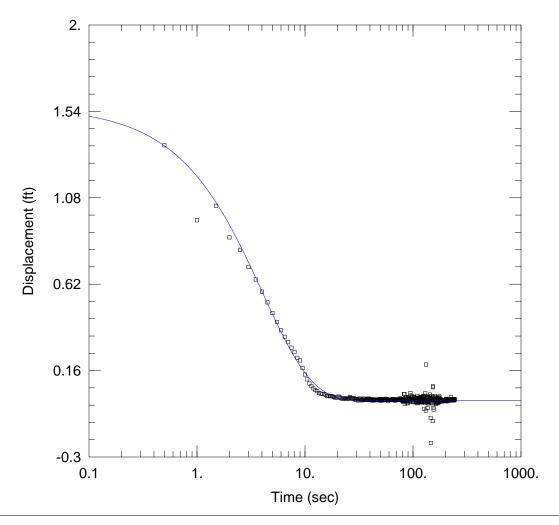
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.000244 ft/sec

y0 = 1.489 ft



TEST 1 - FALLING

Data Set: N:\...\RMD-06-1F.aqt

Date: 10/05/18 Time: 14:27:01

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.89 ft

WELL DATA (RMD-06)

Initial Displacement: 1.566 ft

Static Water Column Height: 47.89 ft

Total Well Penetration Depth: 47.89 ft

Screen Length: 20. ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

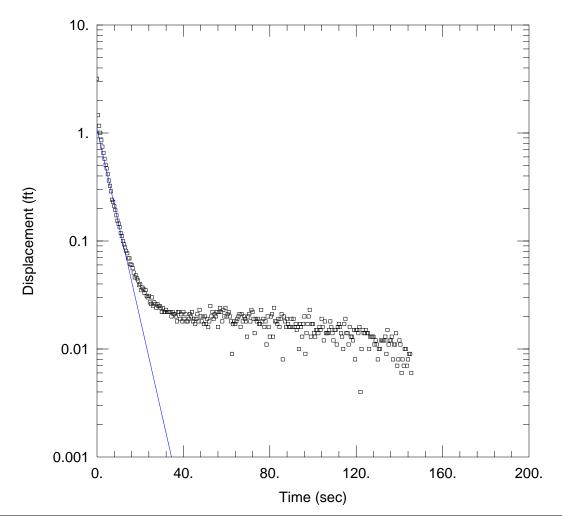
SOLUTION

Aquifer Model: Unconfined

Solution Method: KGS Model

= 0.0002166 ft/sec Kr

 $= 6.158E-7 \text{ ft}^{-1}$



TEST 2 - RISING

Data Set: N:\...\RMD-06-2R.aqt

Date: 10/05/18 Time: 14:25:24

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 3.174 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

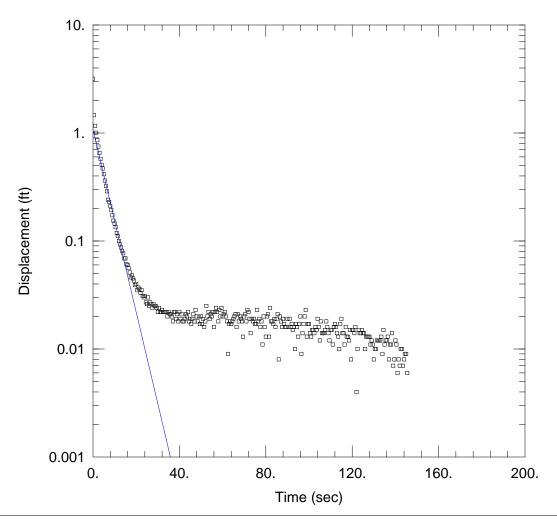
Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001571 ft/sec y0 = 1.096 ft



TEST 2 - RISING

Data Set: N:\...\RMD-06-2R.aqt

Date: 10/05/18 Time: 14:24:49

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 3.174 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

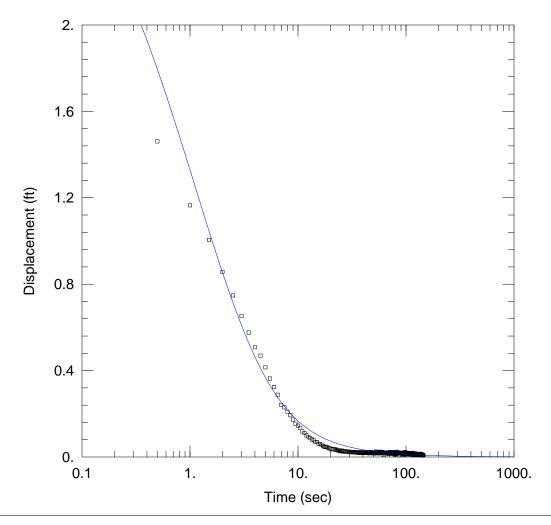
Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0001936 ft/sec y0 = 1.08 ft



TEST 2 - RISING

Data Set: N:\...\RMD-06-2R.aqt

Date: 10/05/18 Time: 14:04:08

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft

WELL DATA (RMD-06)

Initial Displacement: 3.174 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

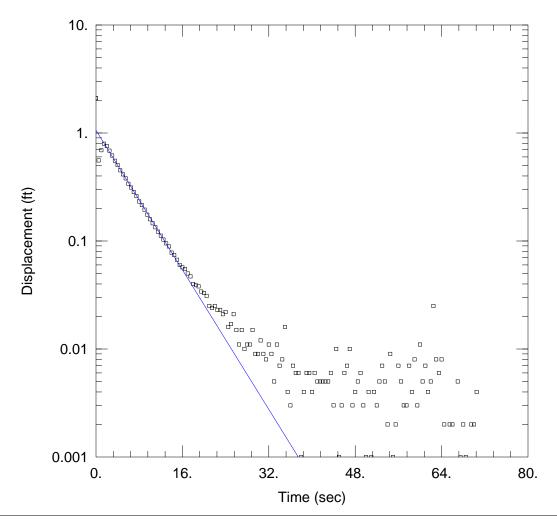
Aquifer Model: Unconfined

Kr = 0.0002133 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = 0.002088 ft^{-1}



TEST 3 - FALLING

Data Set: N:\...\RMD-06-3F.aqt

Date: 10/05/18 Time: 14:02:17

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.89 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 2.094 ft

Total Well Penetration Depth: 47.89 ft

Static Water Column Height: 47.89 ft

Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

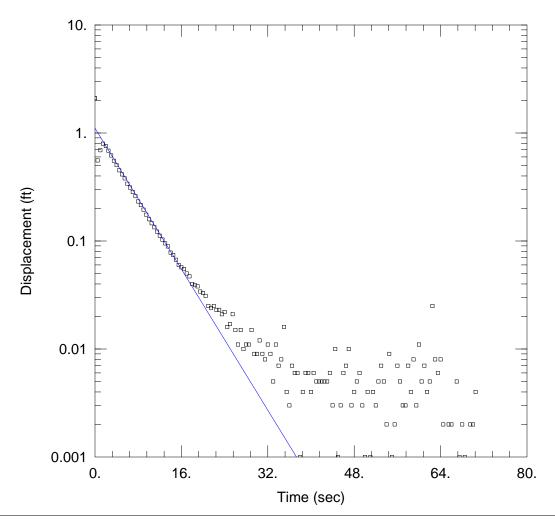
Aquifer Model: Unconfined

Casing Radius: 0.083 ft

Solution Method: Bouwer-Rice

K = 0.000144 ft/sec

y0 = 1.058 ft



TEST 3 - FALLING

Data Set: N:\...\RMD-06-3F.aqt

Date: 10/05/18 Time: 14:01:54

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.89 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 2.094 ft

Static Water Column Height: 47.89 ft

Total Well Penetration Depth: 47.89 ft

Screen Length: 20. ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

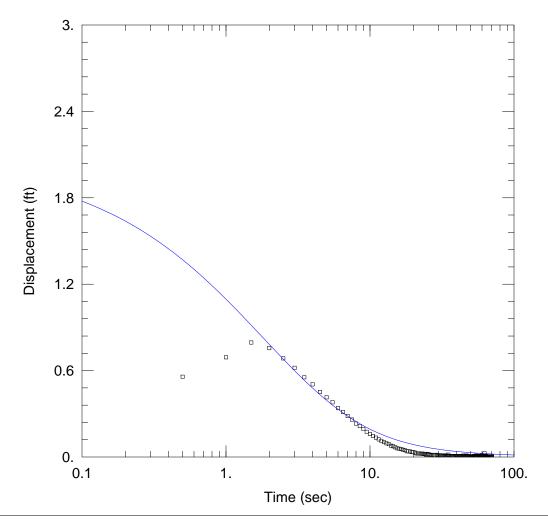
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0001866 ft/sec

y0 = 1.106 ft



TEST 3 - FALLING

Data Set: N:\...\RMD-06-3F.aqt

Date: 10/05/18 Time: 14:00:44

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: $\frac{\text{RMD-06}}{\text{8/28/18}}$

AQUIFER DATA

Saturated Thickness: 47.89 ft

WELL DATA (RMD-06)

Initial Displacement: 2.094 ft

2.094 II

Total Well Penetration Depth: 47.89 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.89 ft

Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

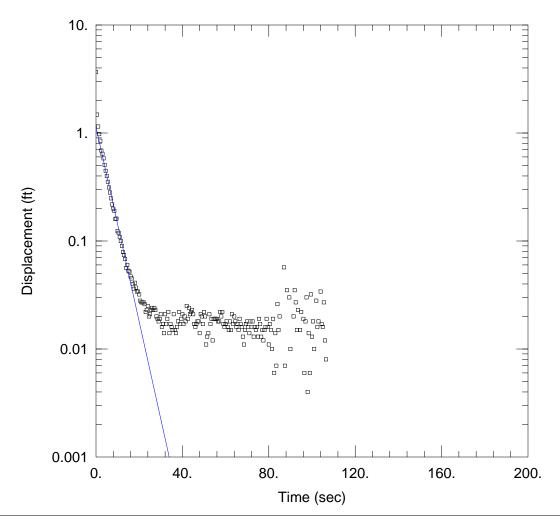
= 0.0001311 ft/sec

 $Kz/Kr = \overline{1}$.

Kr

Solution Method: KGS Model

Ss = 0.002088 ft^{-1}



TEST 4 - RISING

Data Set:

Date: 10/05/18 Time: 13:43:55

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 3.668 ft

Casing Radius: 0.083 ft

Total Well Penetration Depth: 47.9 ft

Static Water Column Height: 47.9 ft

Screen Length: 20. ft Well Radius: 0.125 ft

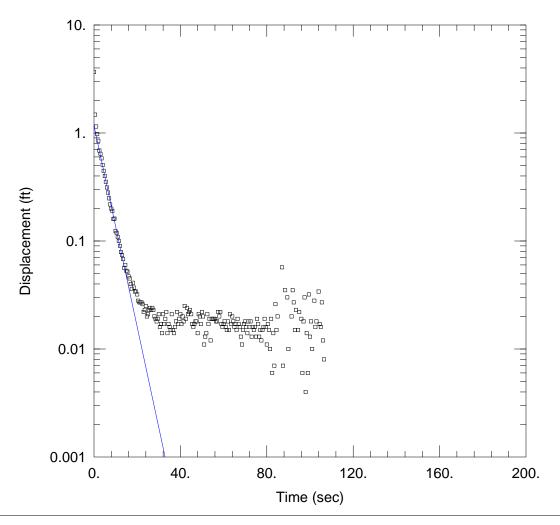
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.001127 ft/sec

y0 = 1.137 ft



TEST 4 - RISING

Data Set:

Date: 10/05/18 Time: 13:45:34

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants

Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 3.668 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

Screen Length: 20. ft Well Radius: 0.125 ft

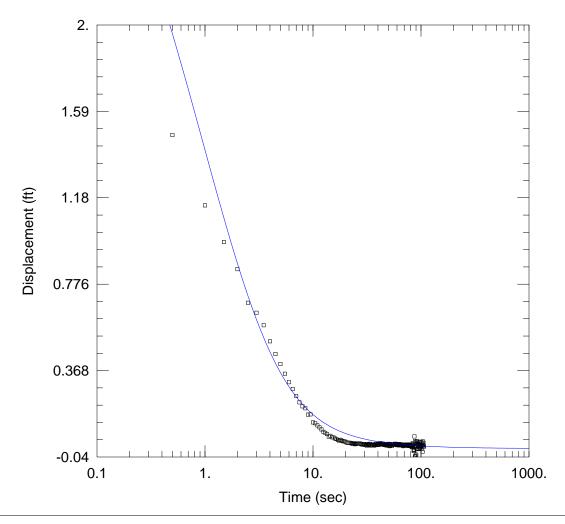
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0001876 ft/sec

y0 = 1.169 ft



TEST 4 - RISING

Data Set:

Date: 10/05/18 Time: 13:47:32

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: <u>BNSF Railway Company</u>

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft

WELL DATA (RMD-06)

Initial Displacement: 3.668 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

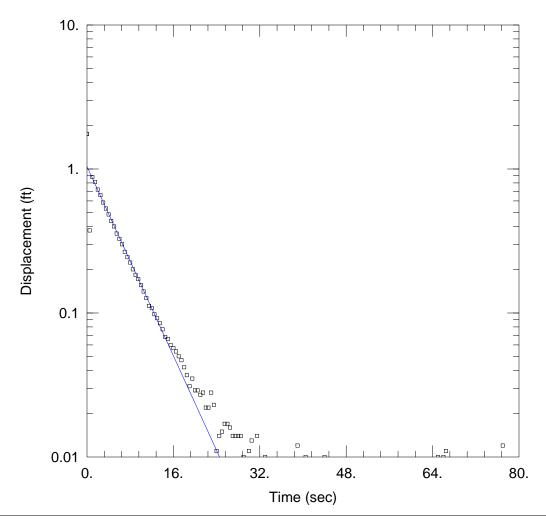
Aquifer Model: Unconfined

Kr = 0.0002494 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = 0.002088 ft^{-1}



TEST 5 - FALLING

Data Set: N:\...\RMD-06-5F.aqt

Date: 10/05/18 Time: 14:38:29

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: $\frac{\text{RMD-06}}{\text{8/28/18}}$

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 1.753 ft

Total Well Penetration Depth: 47.89 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

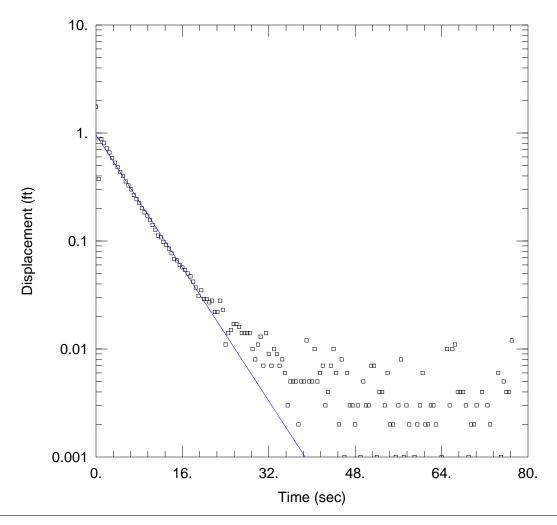
Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.001026 ft/sec y0 = 1.04 ft



TEST 5 - FALLING

Data Set: N:\...\RMD-06-5F.aqt

Date: 10/05/18 Time: 14:38:58

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 1.753 ft

Total Well Penetration Depth: 47.89 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

Screen Length: 20. ft Well Radius: 0.125 ft

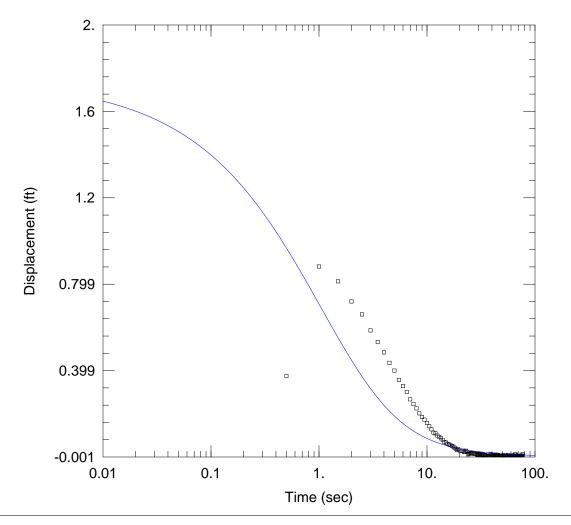
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.000155 ft/sec

y0 = 0.9598 ft



TEST 5 - FALLING

Data Set: N:\...\RMD-06-5F.aqt

Date: 10/05/18 Time: 14:46:21

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft

WELL DATA (RMD-06)

Initial Displacement: 1.753 ft

1.755 IL

Total Well Penetration Depth: 47.89 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

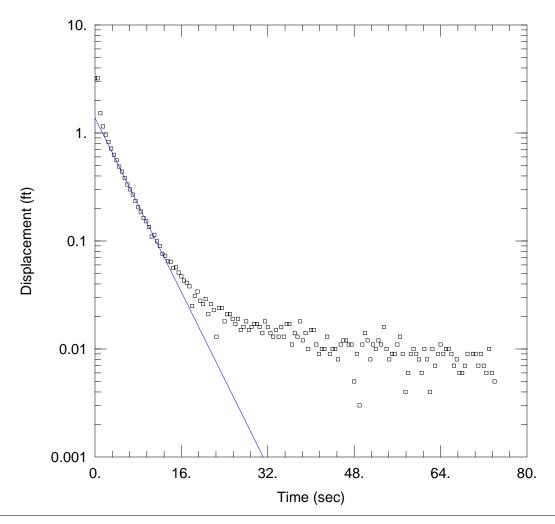
Aquifer Model: Unconfined

Kr = 0.0002285 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = 0.002088 ft^{-1}



TEST 6 - RISING

Data Set:

Date: 10/05/18 Time: 14:52:03

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: $\frac{RMD-06}{8/28/18}$

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 3.207 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

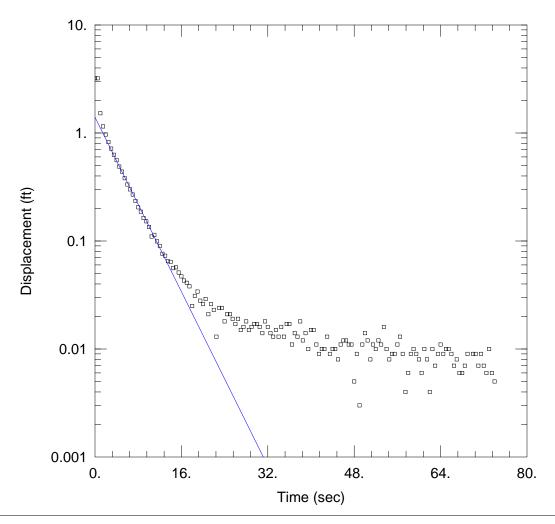
Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.001259 ft/sec y0 = 1.378 ft



TEST 6 - RISING

Data Set:

Date: 10/05/18 Time: 14:52:55

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: RMD-06
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 47.9 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (RMD-06)

Initial Displacement: 3.207 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: 47.9 ft

Screen Length: 20. ft Well Radius: 0.125 ft

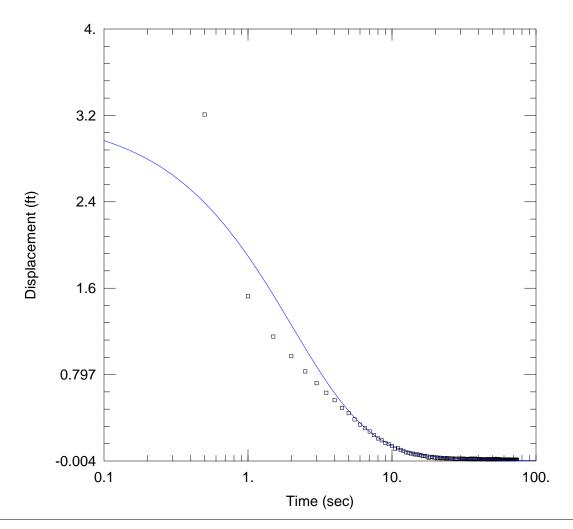
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0002031 ft/sec

y0 = 1.398 ft



TEST 6 - RISING

Data Set:

Date: 10/05/18 Time: 14:53:39

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: $\frac{RMD-06}{8/28/18}$

AQUIFER DATA

Saturated Thickness: 47.9 ft

WELL DATA (RMD-06)

Initial Displacement: 3.207 ft

Total Well Penetration Depth: 47.9 ft

Casing Radius: 0.083 ft

Static Water Column Height: $\underline{47.9}$ ft

Screen Length: 20. ft Well Radius: 0.125 ft

SOLUTION

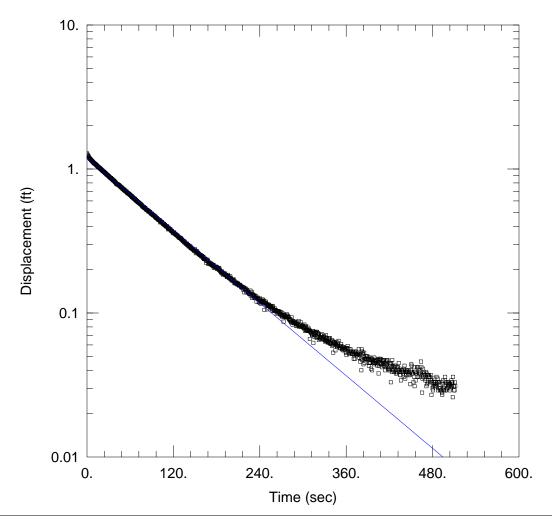
Aquifer Model: Unconfined

Kr = 0.0003215 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = $1.802E-5 \text{ ft}^{-1}$



WELL TEST ANALYSIS

Data Set: N:\...\WMW-20-1.aqt

Date: 10/03/18 Time: 11:45:53

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-20 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.966 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-20)

Initial Displacement: 1.284 ft

Total Well Penetration Depth: 3.966 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.966 ft

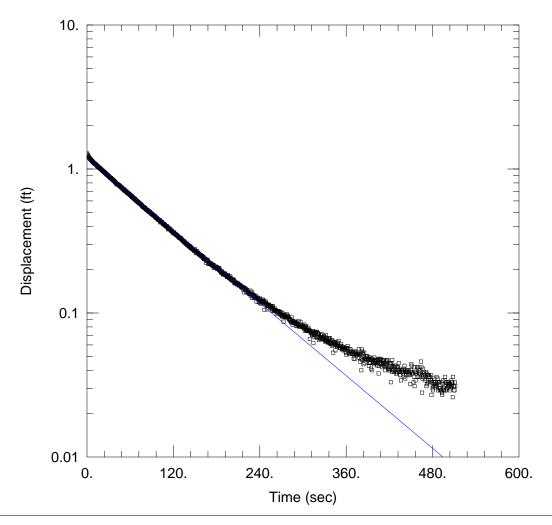
Screen Length: 3.966 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 2.2E-5 ft/sec y0 = 1.194 ft



WELL TEST ANALYSIS

Data Set: N:\...\WMW-20-1.aqt

Date: 10/03/18 Time: 11:47:49

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-20 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.966 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-20)

Initial Displacement: 1.284 ft

Total Well Penetration Depth: 3.966 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.966 ft

Screen Length: 3.966 ft Well Radius: 0.125 ft

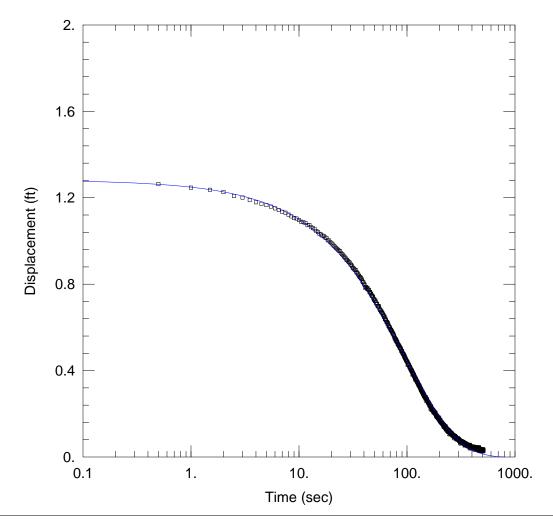
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 4.451E-5 ft/sec

y0 = 1.193 ft



WELL TEST ANALYSIS

Data Set: N:\...\WMW-20-1.aqt

Date: 10/03/18 Time: 11:49:30

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-20</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 3.966 ft

WELL DATA (WMW-20)

Initial Displacement: 1.284 ft

Static Water Column Height: 3.966 ft

Total Well Penetration Depth: 3.966 ft

Screen Length: 3.966 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

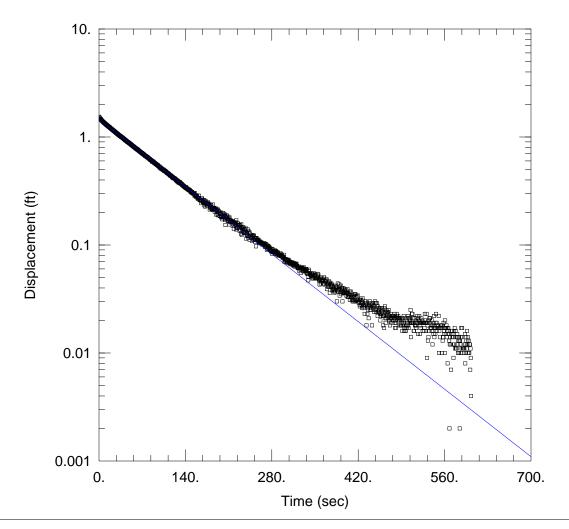
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 2.527E-5 ft/sec

Ss = $0.0003504 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\WMW-20-2.aqt

Date: 10/03/18 Time: 12:06:14

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-20 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.444 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-20)

Initial Displacement: 1.536 ft

Static Water Column Height: 3.444 ft Screen Length: 3.444 ft

Total Well Penetration Depth: 3.444 ft

Well Radius: 0.125 ft

Casing Radius: 0.083 ft

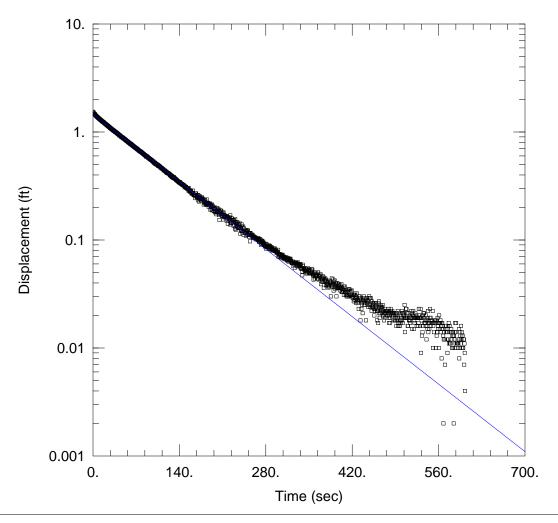
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 2.568E-5 ft/sec

y0 = 1.464 ft



Data Set: N:\...\WMW-20-2.aqt

Date: 10/03/18 Time: 12:11:47

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-20 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.444 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-20)

Initial Displacement: 1.536 ft

Total Well Penetration Depth: 3.444 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.444 ft

Screen Length: 3.444 ft Well Radius: 0.125 ft

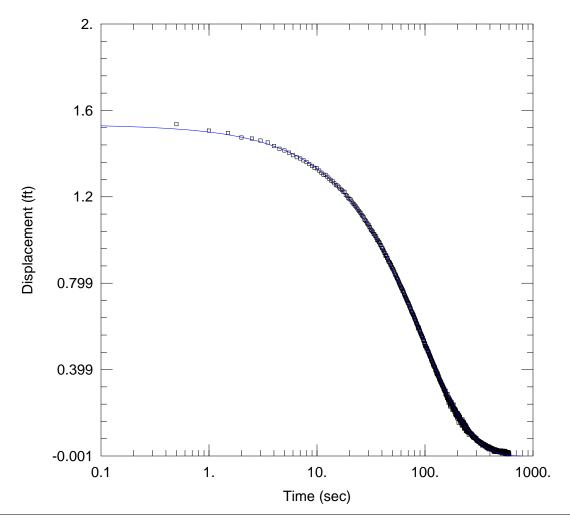
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 5.448E-5 ft/sec

y0 = 1.464 ft



Data Set: N:\...\WMW-20-2.aqt

Date: 10/03/18 Time: 12:12:49

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-20</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 3.444 ft

WELL DATA (WMW-20)

Initial Displacement: 1.536 ft

Static Water Column Height: 3.444 ft

Total Well Penetration Depth: 3.444 ft

Screen Length: 3.444 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

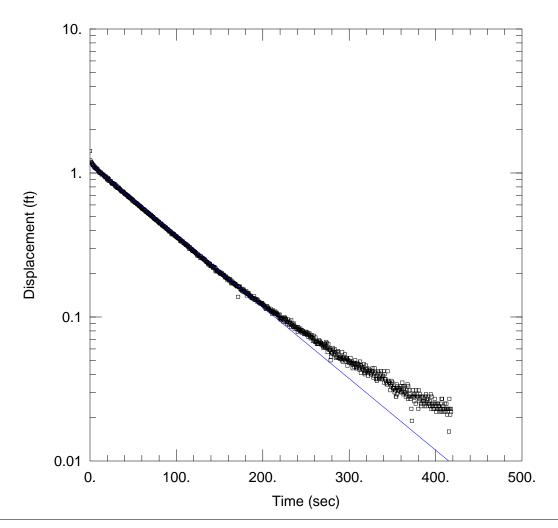
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 2.916E-5 ft/sec

Ss = $0.0002449 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set:

Date: 10/03/18 Time: 12:24:46

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-20 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.969 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-20)

Initial Displacement: 1.421 ft

Total Well Penetration Depth: 3.969 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.969 ft

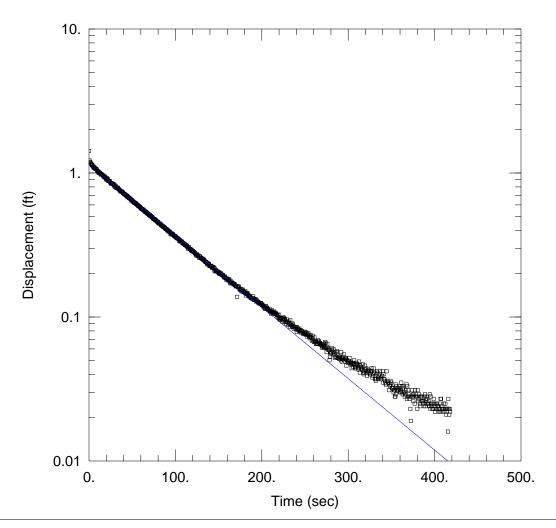
Screen Length: 3.969 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 2.598E-5 ft/sec y0 = 1.152 ft



Data Set:

Date: 10/03/18 Time: 12:26:12

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-20 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.969 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-20)

Initial Displacement: 1.421 ft

Total Well Penetration Depth: 3.969 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.969 ft

Screen Length: 3.969 ft Well Radius: 0.125 ft

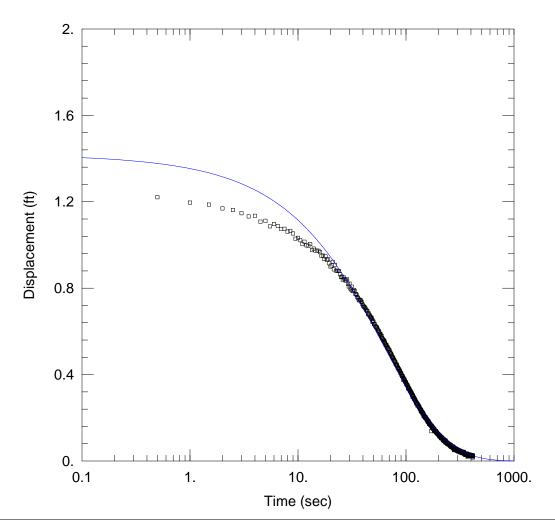
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 5.256E-5 ft/sec

y0 = 1.152 ft



Data Set: N:\...\WMW-20-3.aqt

Date: 10/03/18 Time: 12:27:49

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-20</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 3.969 ft

WELL DATA (WMW-20)

Initial Displacement: 1.421 ft

Static Water Column Height: 3.969 ft

Total Well Penetration Depth: 3.969 ft

Screen Length: 3.969 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

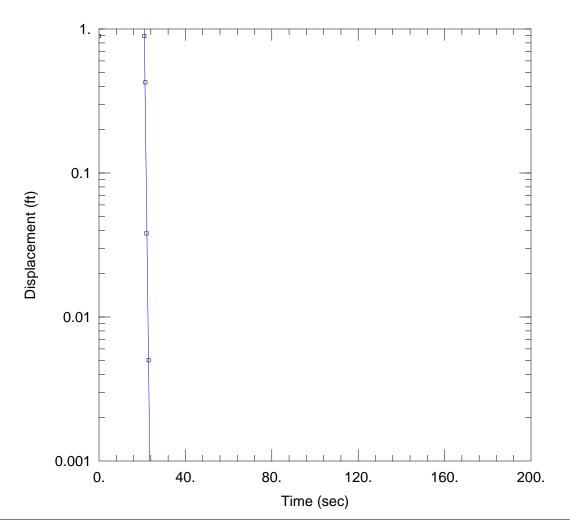
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 3.267E-5 ft/sec

Ss = 0.001186 ft^{-1}

Kz/Kr = 1.



Data Set:

Date: 10/03/18 Time: 12:36:56

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-22 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 4.496 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-22)

Initial Displacement: 0.893 ft

Total Well Penetration Depth: 4.496 ft

Casing Radius: 0.083 ft

Static Water Column Height: 4.496 ft

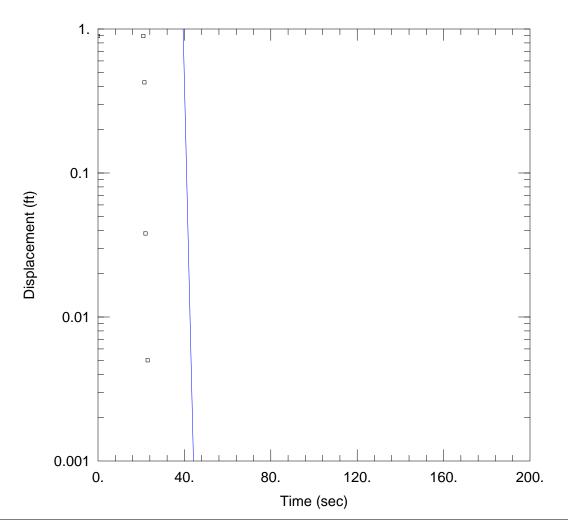
Screen Length: 4.496 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.00568 ft/secy0 = 6.427E + 24 ft



Data Set: N:\...\WMW-22-1.aqt

Date: 10/03/18 Time: 12:39:26

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-22 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 4.496 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-22)

Initial Displacement: 0.893 ft

Total Well Penetration Depth: 4.496 ft

Casing Radius: 0.083 ft

Static Water Column Height: 4.496 ft

Screen Length: 4.496 ft Well Radius: 0.125 ft

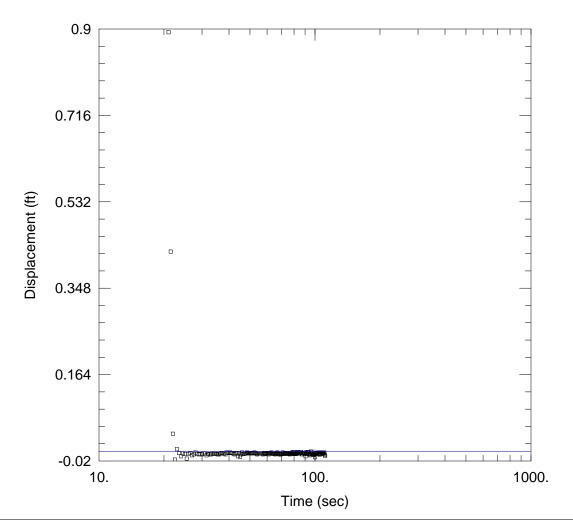
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.005881 ft/sec

y0 = 6.427E + 24 ft



Data Set: N:\...\WMW-22-1.aqt

Date: 10/03/18 Time: 12:40:27

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-22</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 4.496 ft

WELL DATA (WMW-22)

Initial Displacement: 0.893 ft

Static Water Column Height: 4.496 ft

Total Well Penetration Depth: 4.496 ft

Screen Length: 4.496 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

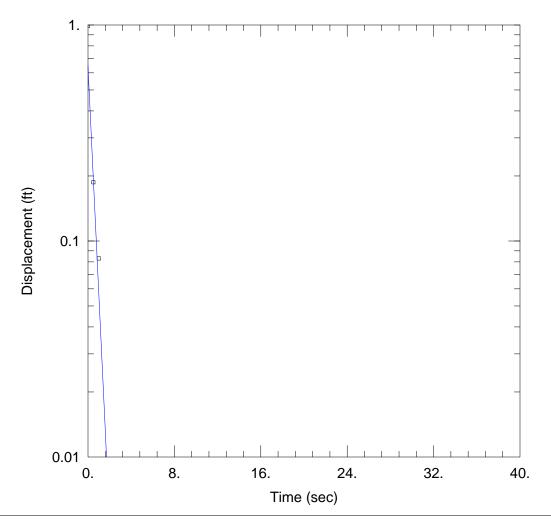
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 0.002887 ft/sec

Ss = $2.981E-10 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set:

Date: 10/03/18 Time: 12:50:52

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-22 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 4.504 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-22)

Initial Displacement: 0.99 ft

Total Well Penetration Depth: 4.504 ft

Casing Radius: 0.083 ft

Static Water Column Height: 4.504 ft

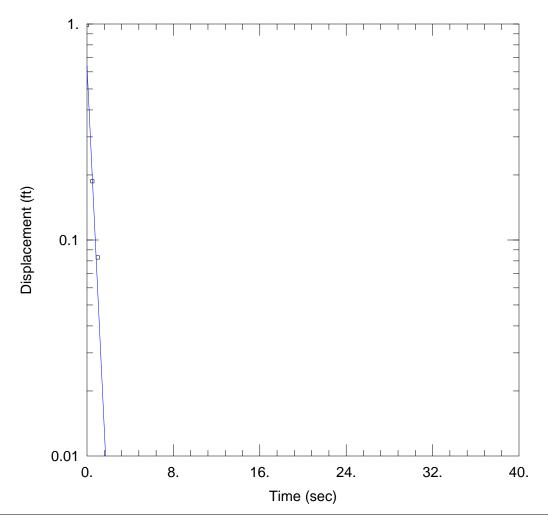
Screen Length: 4.504 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.005046 ft/secy0 = 0.6415 ft



Data Set:

Date: 10/03/18 Time: 12:51:44

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-22
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 4.504 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-22)

Initial Displacement: 0.99 ft

5.99 ft Static Water Column Height: 4.504 ft

Total Well Penetration Depth: 4.504 ft

Screen Length: 4.504 ft Well Radius: 0.125 ft

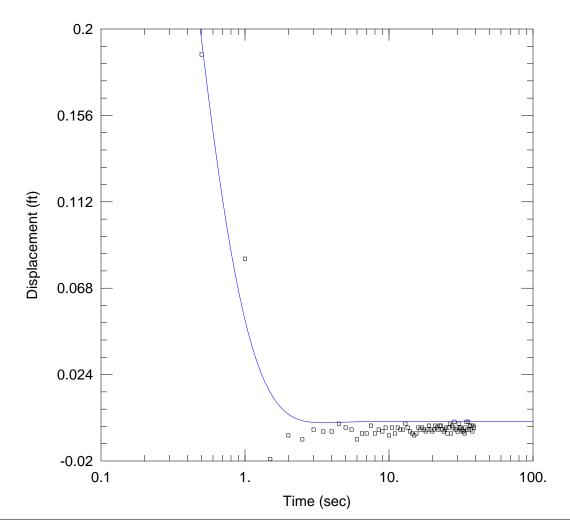
Casing Radius: 0.083 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.009802 ft/sec y0 = 0.6406 ft



Data Set:

Date: 10/03/18 Time: 12:52:47

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-22</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 4.504 ft

WELL DATA (WMW-22)

Initial Displacement: 0.99 ft

Static Water Column Height: 4.504 ft

Total Well Penetration Depth: 4.504 ft

Screen Length: 4.504 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

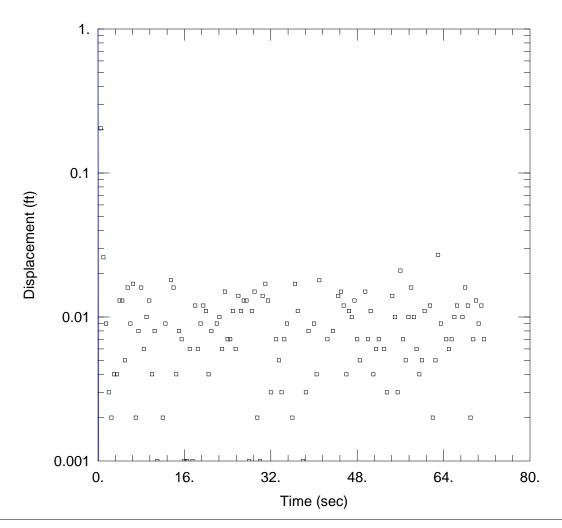
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 0.007497 ft/sec

Ss = $0.0003653 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\WMW-22-3.aqt

Date: 10/03/18 Time: 13:06:00

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-22 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 4.502 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-22)

Initial Displacement: 1.231 ft

Casing Radius: 0.083 ft

Total Well Penetration Depth: 4.502 ft

Screen Length: 4.502 ft

Well Radius: 0.125 ft

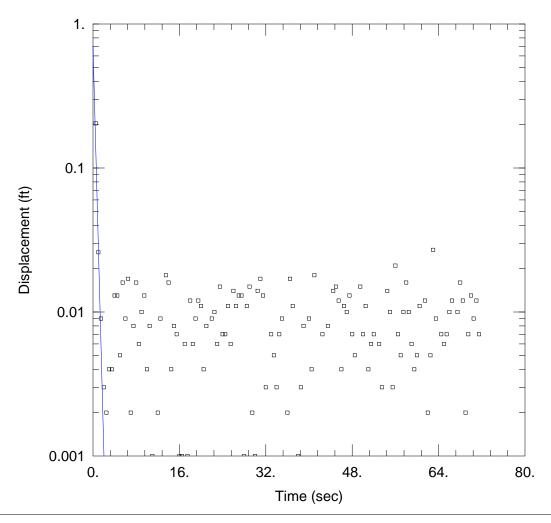
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

Static Water Column Height: 4.502 ft

K = 0.2221 ft/secy0 = 1. ft



Data Set: N:\...\WMW-22-3.aqt

Date: 10/03/18 Time: 13:06:30

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-22 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 4.502 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-22)

Initial Displacement: 1.231 ft

Total Well Penetration Depth: 4.502 ft

Casing Radius: 0.083 ft

Static Water Column Height: 4.502 ft

Screen Length: 4.502 ft Well Radius: 0.125 ft

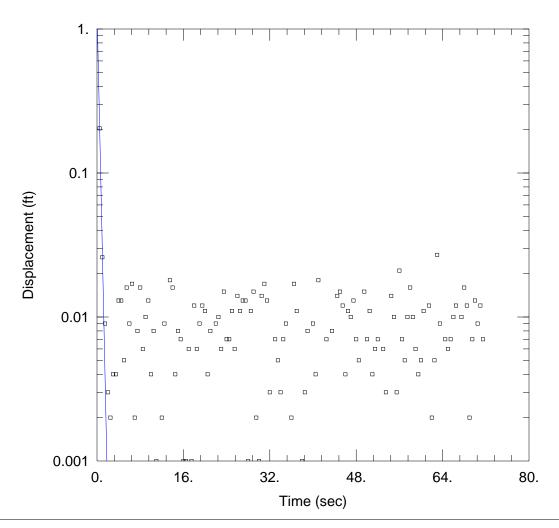
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.006729 ft/sec

y0 = 0.7044 ft



Data Set: N:\...\WMW-22-3.aqt

Date: 10/03/18 Time: 13:07:08

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-22 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 4.502 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-22)

Initial Displacement: 1.231 ft

Total Well Penetration Depth: 4.502 ft

Casing Radius: 0.083 ft

502 ft Screen Length: <u>4.502</u> ft

Well Radius: <u>0.125</u> ft

Static Water Column Height: 4.502 ft

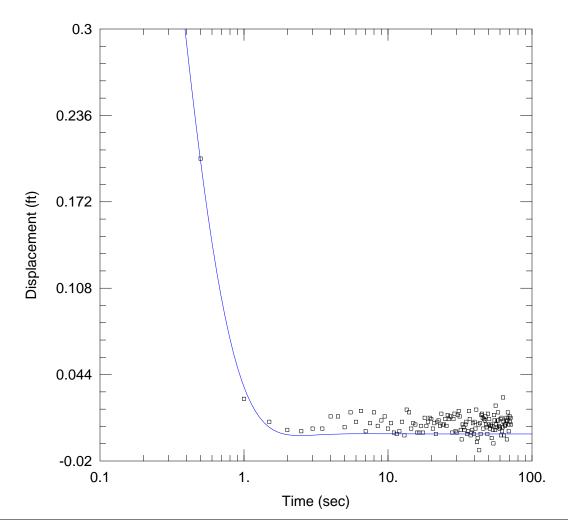
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.01622 ft/sec

y0 = 1.508 ft



Data Set: N:\...\WMW-22-3.aqt

Date: 10/03/18 Time: 13:07:57

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: <u>1896120*04</u>

Location: Wishram Railyard, Washington

Test Well: <u>WMW-22</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 4.502 ft

WELL DATA (WMW-22)

Initial Displacement: 1.231 ft

1 ft Static Water Column Height: 4.502 ft

Total Well Penetration Depth: 4.502 ft

Screen Length: 4.502 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

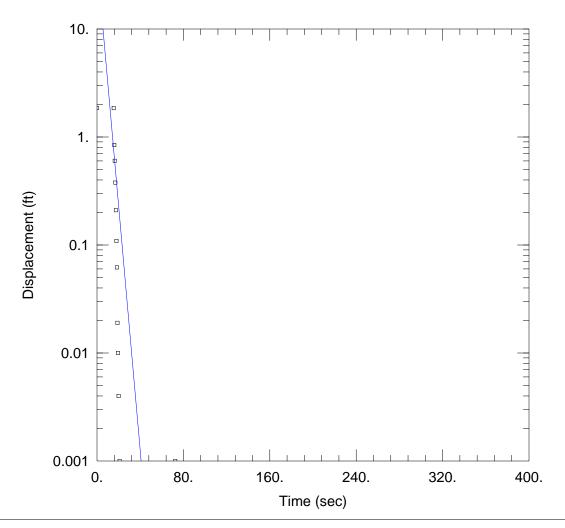
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 0.008231 ft/sec

Ss = $2.247E-11 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\WMW-23-1.aqt

Date: 10/03/18 Time: 13:18:05

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23
Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.566 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-23)

Initial Displacement: 1.852 ft

Static Water Column Height: 7.566 ft

Total Well Penetration Depth: 7.566 ft

Screen Length: 7.566 ft Well Radius: 0.125 ft

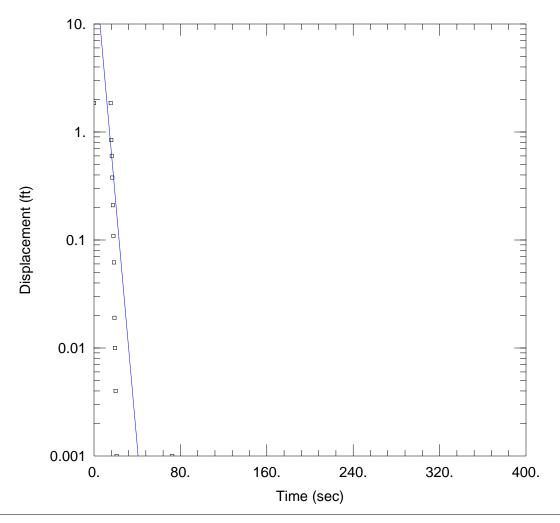
Casing Radius: 0.083 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0003736 ft/sec y0 = 42.69 ft



Data Set: N:\...\WMW-23-1.aqt

Date: <u>10/03/18</u> Time: <u>13:18:45</u>

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-23</u> Test Date: <u>8/29/18</u>

AQUIFER DATA

Saturated Thickness: 7.566 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-23)

Initial Displacement: 1.852 ft

2 ft Static Water Column Height: 7.566 ft

Total Well Penetration Depth: 7.566 ft

Screen Length: 7.566 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

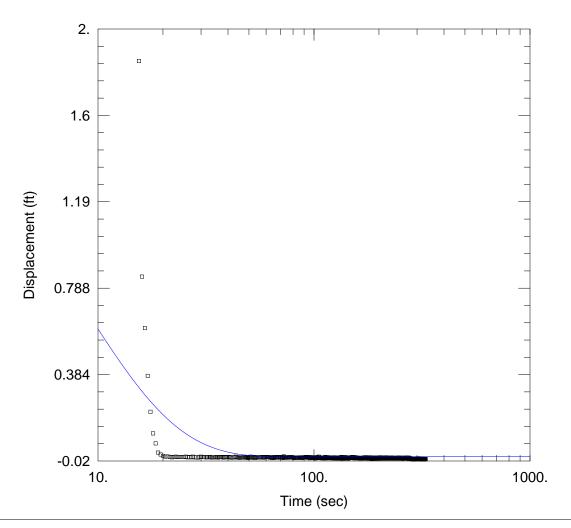
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.0006291 ft/sec

y0 = 42.69 ft



Data Set: N:\...\WMW-23-1.aqt

Date: 10/03/18 Time: 13:20:26

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.566 ft

WELL DATA (WMW-23)

Initial Displacement: 1.852 ft

Static Water Column Height: 7.566 ft

Total Well Penetration Depth: 7.566 ft

Screen Length: 7.566 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

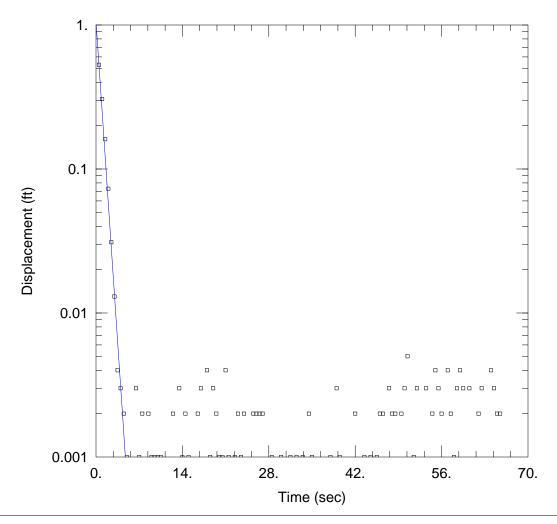
Aquifer Model: Unconfined

Solution Method: KGS Model

= 0.0001781 ft/sec Kr

 $= 1.322E-11 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\WMW-23-2.aqt

Date: 10/03/18 Time: 13:27:09

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.638 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-23)

Initial Displacement: 1.644 ft

Total Well Penetration Depth: 7.638 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.638 ft

Screen Length: 7.638 ft Well Radius: 0.125 ft

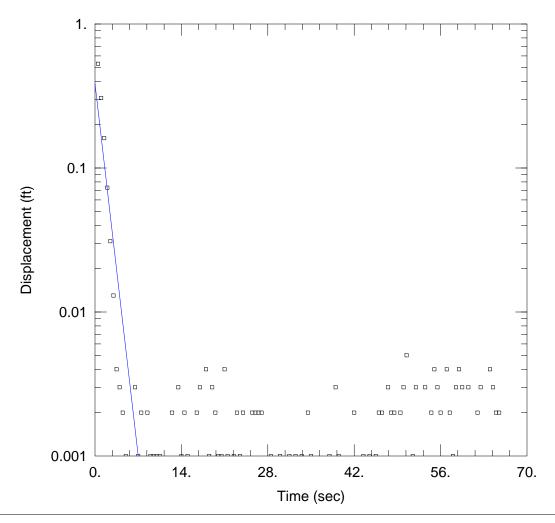
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.002086 ft/sec

y0 = 1.076 ft



Data Set: N:\...\WMW-23-2.aqt

Date: 10/03/18 Time: 13:28:07

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.638 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-23)

Initial Displacement: 1.644 ft

Total Well Penetration Depth: 7.638 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.638 ft Screen Length: 7.638 ft

Well Radius: 0.125 ft

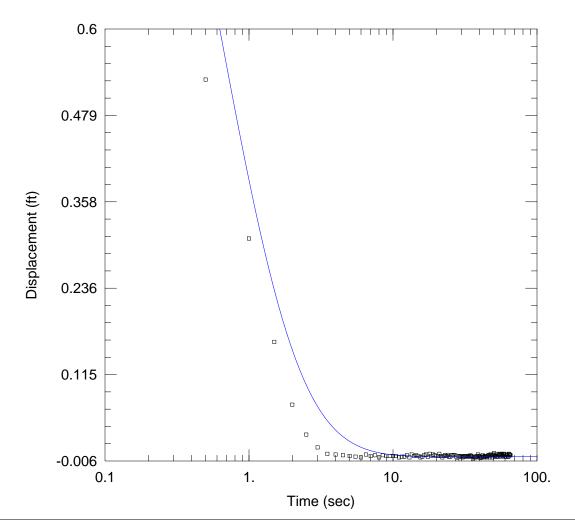
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.002031 ft/sec

y0 = 0.3847 ft



Data Set: N:\...\WMW-23-2.aqt

Date: 10/03/18 Time: 13:29:36

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23
Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.638 ft

WELL DATA (WMW-23)

Initial Displacement: 1.644 ft

644 ft Static Wa

Total Well Penetration Depth: 7.638 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.638 ft Screen Length: 7.638 ft

Well Radius: <u>0.125</u> ft

SOLUTION

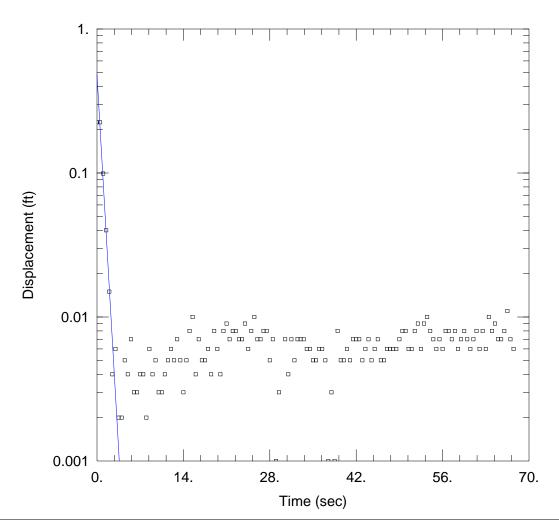
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 0.002031 ft/sec

Ss = 0.000373 ft^{-1}

Kz/Kr = 1.



Data Set: N:\...\WMW-23-3.aqt

Date: 10/03/18 Time: 13:37:55

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.634 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-23)

Initial Displacement: 0.225 ft

Total Well Penetration Depth: 7.634 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.634 ft

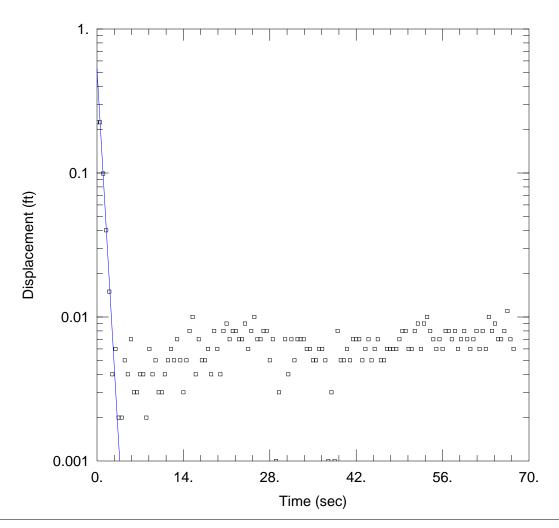
Screen Length: 7.634 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.002431 ft/secy0 = 0.4804 ft



Data Set: N:\...\WMW-23-3.aqt

Date: 10/03/18 Time: 13:38:37

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants
Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23
Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.634 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-23)

Initial Displacement: 0.225 ft

Static Water Column Height: 7.634 ft

Total Well Penetration Depth: 7.634 ft

Screen Length: 7.634 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

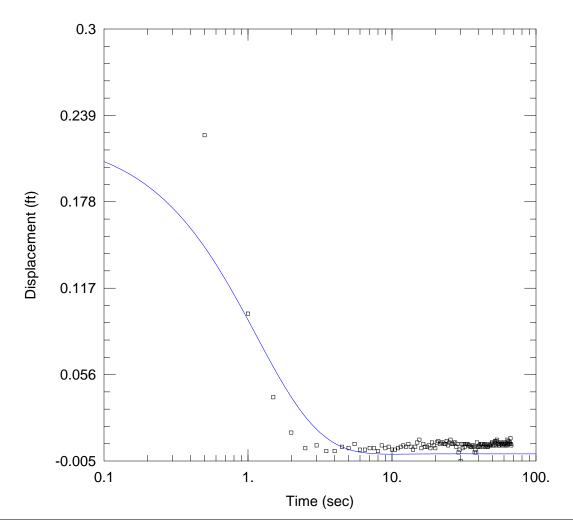
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 0.00407 ft/sec

y0 = 0.5287 ft



Data Set: N:\...\WMW-23-3.aqt

Date: 10/03/18 Time: 13:39:50

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 7.634 ft

WELL DATA (WMW-23)

Initial Displacement: 0.225 ft

Total Well Penetration Depth: 7.634 ft

Casing Radius: 0.083 ft

Static Water Column Height: 7.634 ft

Screen Length: 7.634 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

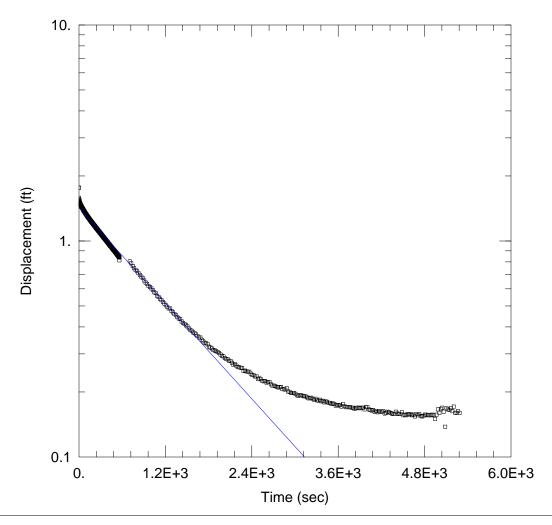
Solution Method: KGS Model

= 0.001355 ft/sec

 $= 1.31E-11 \text{ ft}^{-1}$

Kz/Kr = 1.

Kr



Data Set: N:\...\WMW-26-1.aqt

Date: 10/03/18 Time: 14:07:31

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.615 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-26)

Initial Displacement: 1.765 ft

Total Well Penetration Depth: 3.615 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.615 ft

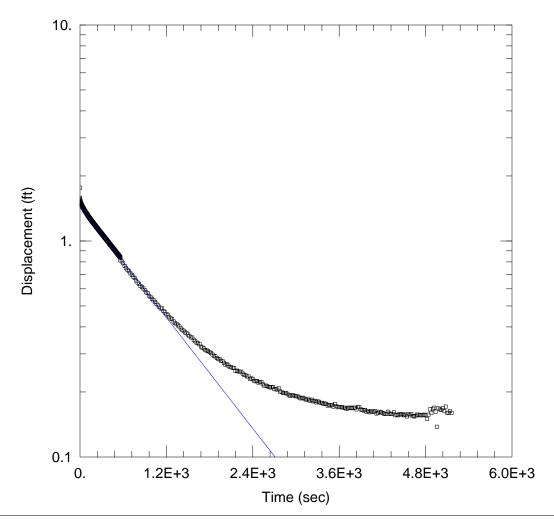
Screen Length: 3.615 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 2.052E-6 ft/sec y0 = 1.424 ft



TEST 1 REV

Data Set:

Date: 10/05/18 Time: 07:58:29

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.615 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-26)

Initial Displacement: 1.765 ft

Total Well Penetration Depth: 3.615 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.615 ft

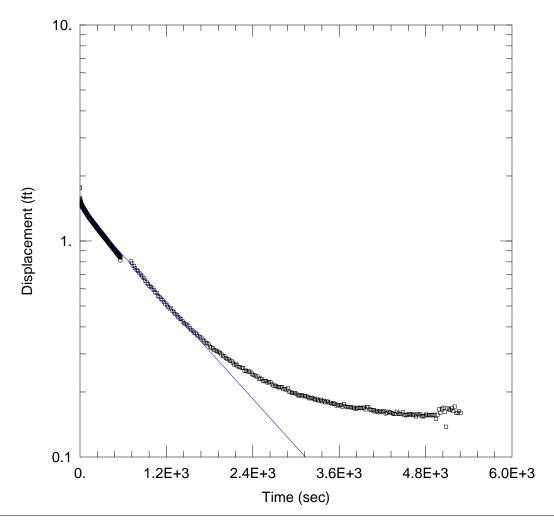
Screen Length: 3.615 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 2.384E-6 ft/sec y0 = 1.442 ft



Data Set: N:\...\WMW-26-1.aqt

Date: 10/03/18 Time: 14:08:08

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.615 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-26)

Initial Displacement: 1.765 ft

Total Well Penetration Depth: 3.615 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.615 ft

Screen Length: 3.615 ft Well Radius: 0.125 ft

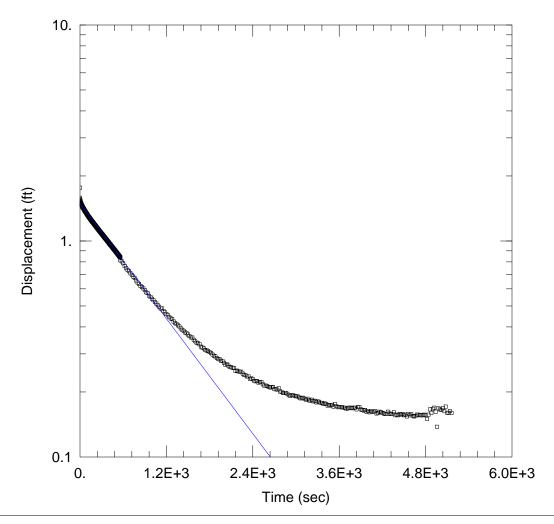
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 4.284E-6 ft/sec

y0 = 1.424 ft



TEST 1 REV

Data Set:

Date: 10/05/18 Time: 07:59:13

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.615 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-26)

Initial Displacement: 1.765 ft

Total Well Penetration Depth: 3.615 ft

Casing Radius: 0.083 ft

Static Water Column Height: 3.615 ft

Screen Length: 3.615 ft Well Radius: 0.125 ft

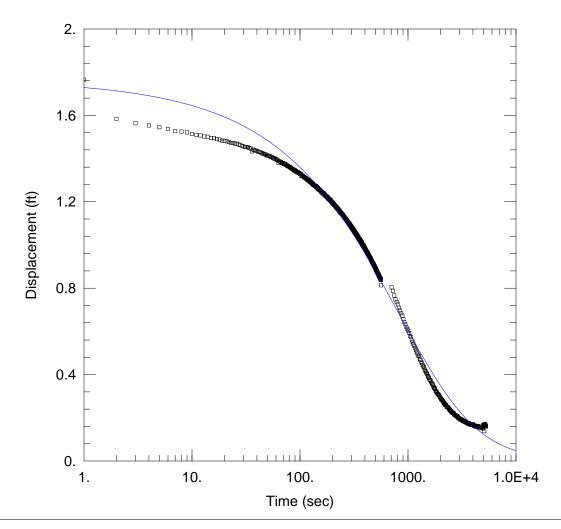
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 5.158E-6 ft/sec

y0 = 1.489 ft



Data Set: N:\...\WMW-26-1.aqt

Date: 10/03/18 Time: 14:16:27

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-23 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.615 ft

WELL DATA (WMW-26)

Initial Displacement: 1.765 ft

Static Water Column Height: 3.615 ft

Total Well Penetration Depth: 3.615 ft

Screen Length: 3.615 ft

Casing Radius: 0.083 ft

Well Radius: 0.125 ft

SOLUTION

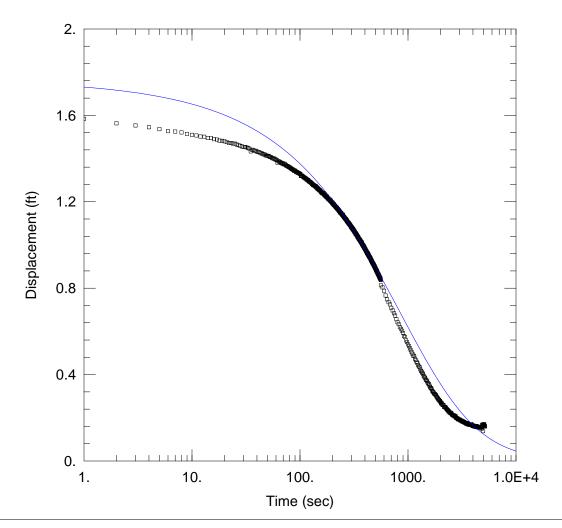
Aquifer Model: Unconfined

Solution Method: KGS Model

= 1.568E-6 ft/sec Kr

 $= 0.01161 \text{ ft}^{-1}$ Ss

Kz/Kr = 1.



TEST 1 REV

Data Set:

Date: 10/05/18 Time: 08:00:09

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 3.615 ft

WELL DATA (WMW-26)

Initial Displacement: 1.765 ft

Static Water Column Height: 3.615 ft

Total Well Penetration Depth: 3.615 ft

Screen Length: 3.615 ft

Casing Radius: 0.083 ft

Well Radius: 0.125 ft

SOLUTION

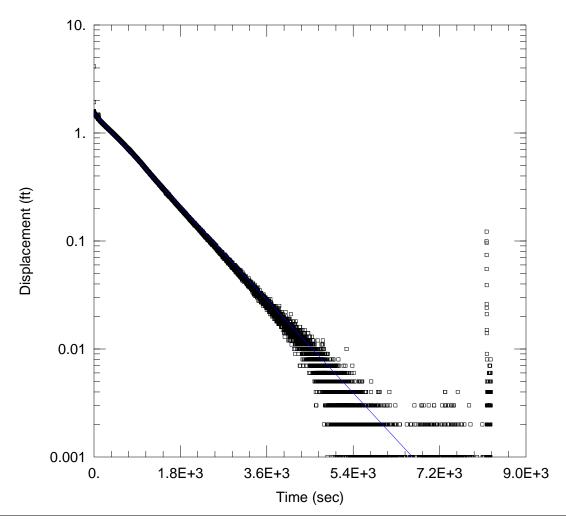
Aquifer Model: Unconfined

Solution Method: KGS Model

= 1.58E-6 ft/sec Kr

 $= 0.009991 \text{ ft}^{-1}$

Kz/Kr = 1.



Data Set: N:\...\WMW-26-2.aqt

Date: 10/03/18 Time: 14:23:02

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 5.779 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-26)

Initial Displacement: 4.128 ft

Total Well Penetration Depth: 5.779 ft

Casing Radius: 0.083 ft

Static Water Column Height: 5.779 ft

Screen Length: 5.779 ft Well Radius: 0.125 ft

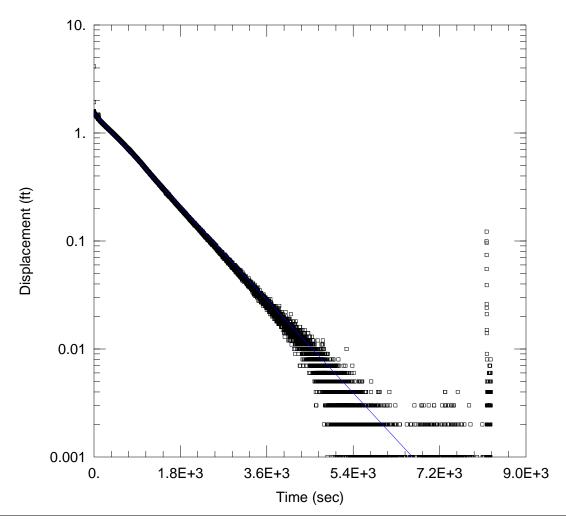
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.93E-6 ft/sec

y0 = 1.527 ft



Data Set: N:\...\WMW-26-2.aqt

Date: 10/03/18 Time: 14:23:55

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-26</u> Test Date: <u>8/29/18</u>

AQUIFER DATA

Saturated Thickness: 5.779 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-26)

Initial Displacement: 4.128 ft

Total Well Penetration Depth: 5.779 ft

Casing Radius: 0.083 ft

Static Water Column Height: 5.779 ft

Screen Length: <u>5.779</u> ft Well Radius: 0.125 ft

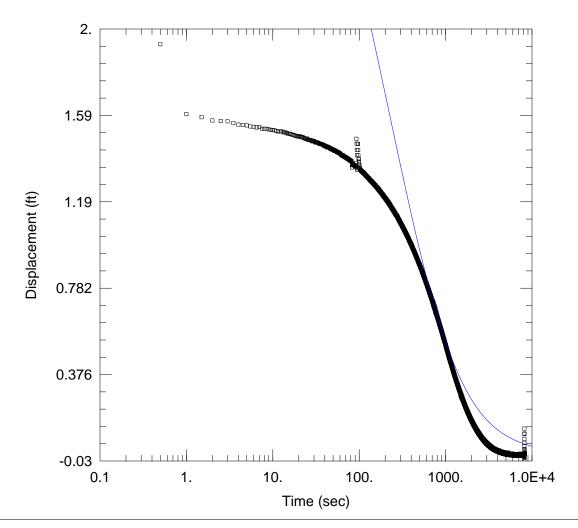
SOLUTION

Aquifer Model: Unconfined

Solution Method: <u>Hvorslev</u>

K = 3.489E-6 ft/sec

y0 = 1.527 ft



Data Set: N:\...\WMW-26-2.aqt

Date: 10/03/18 Time: 14:37:29

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-26</u> Test Date: <u>8/29/18</u>

AQUIFER DATA

Saturated Thickness: 5.779 ft

WELL DATA (WMW-26)

Initial Displacement: 4.128 ft

Static Water Column Height: 5.779 ft

Total Well Penetration Depth: 5.779 ft

Screen Length: <u>5.779</u> ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

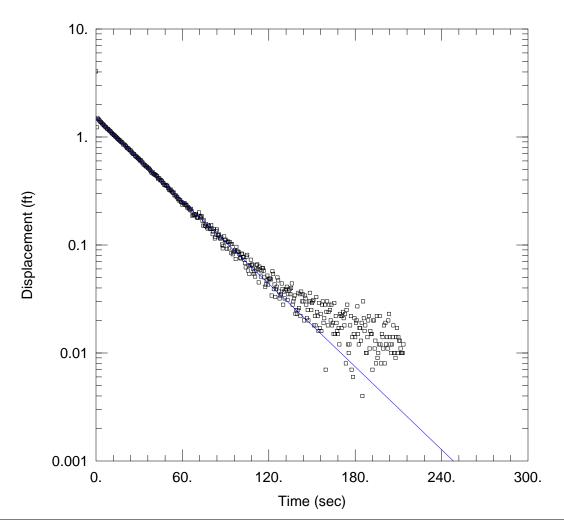
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 2.614E-6 ft/sec

Ss = 0.0173 ft^{-1}

Kz/Kr = 1.



Data Set: N:\...\WMW-28-1.aqt

Date: 10/03/18 Time: 14:44:17

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.817 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-28)

Initial Displacement: 4.043 ft

Total Well Penetration Depth: 6.817 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.817 ft

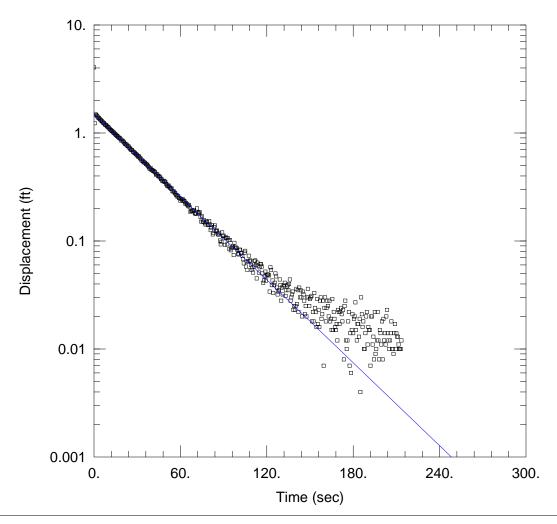
Screen Length: 6.817 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 4.562E-5 ft/sec y0 = 1.499 ft



Data Set: N:\...\WMW-28-1.aqt

Date: 10/03/18 Time: 14:44:52

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.817 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-28)

Initial Displacement: 4.043 ft

Total Well Penetration Depth: 6.817 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.817 ft

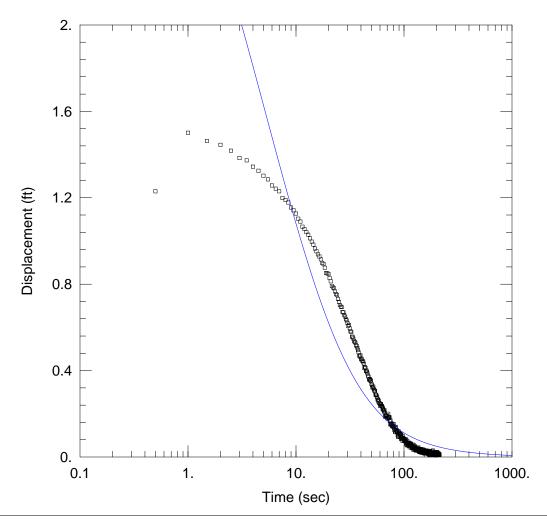
Screen Length: 6.817 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 7.889E-5 ft/secy0 = 1.499 ft



Data Set: N:\...\WMW-28-1.aqt

Date: 10/03/18 Time: 14:46:38

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.817 ft

WELL DATA (WMW-28)

Initial Displacement: 4.043 ft

Total Well Penetration Depth: 6.817 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.817 ft

Screen Length: <u>6.817</u> ft Well Radius: 0.125 ft

SOLUTION

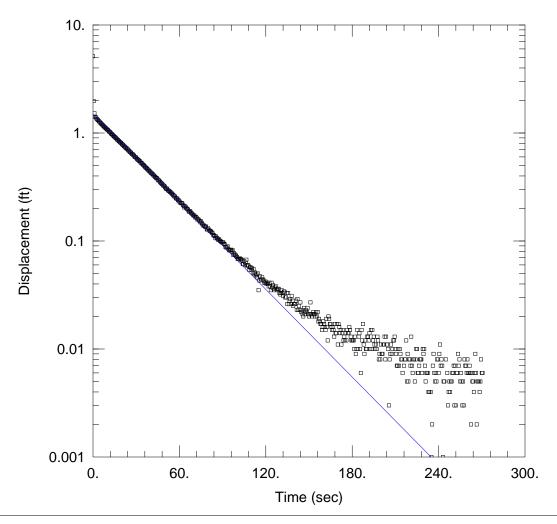
Aquifer Model: Unconfined

Solution Method: $\underline{\mathsf{KGS}\;\mathsf{Model}}$

Kr = 9.249E-5 ft/sec

Ss = 0.01467 ft^{-1}

Kz/Kr = 1.



Data Set: N:\...\WMW-28-2.aqt

Date: 10/03/18 Time: 14:52:06

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.8 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-28)

Initial Displacement: 5.137 ft

Total Well Penetration Depth: 6.8 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.8 ft

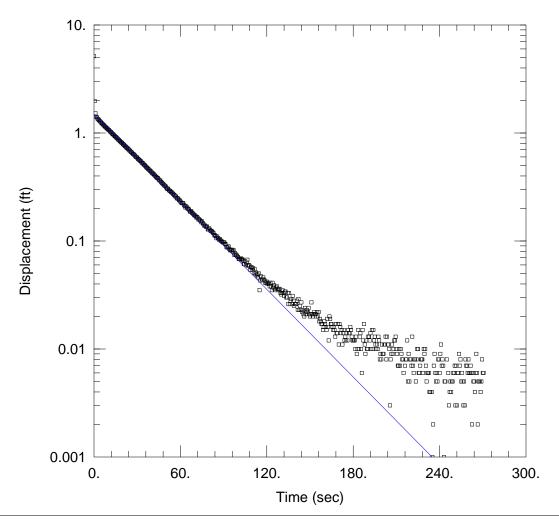
Screen Length: 6.8 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 4.83E-5 ft/sec y0 = 1.495 ft



Data Set: N:\...\WMW-28-2.aqt

Date: 10/03/18 Time: 14:52:50

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.8 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-28)

Initial Displacement: 5.137 ft

Total Well Penetration Depth: 6.8 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.8 ft

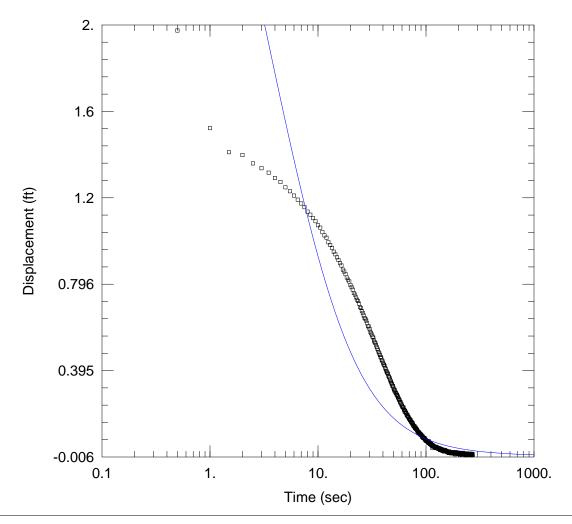
Screen Length: <u>6.8</u> ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 8.357E-5 ft/sec y0 = 1.495 ft



Data Set: N:\...\WMW-28-2.aqt

Date: 10/03/18 Time: 14:55:41

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-26
Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.8 ft

WELL DATA (WMW-28)

Initial Displacement: 5.137 ft

Total Well Penetration Depth: 6.8 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.8 ft

Screen Length: <u>6.8</u> ft Well Radius: 0.125 ft

SOLUTION

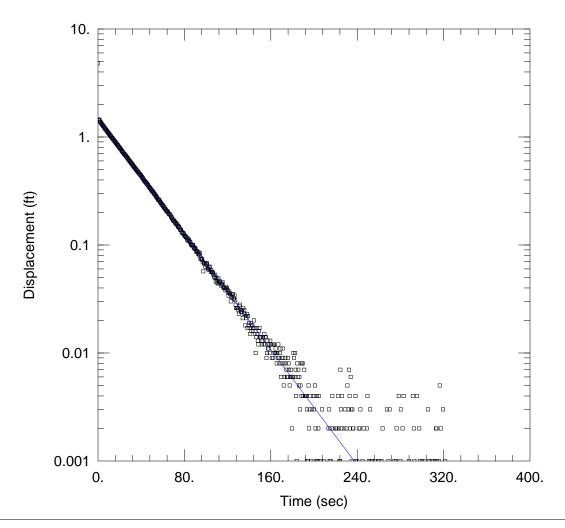
Aquifer Model: Unconfined

Kr = 0.0001545 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = 0.01471 ft^{-1}



Data Set: N:\...\WMW-28-3.aqt

Date: 10/05/18 Time: 08:07:25

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-28 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.791 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-28)

Initial Displacement: 4.806 ft

Total Well Penetration Depth: 6.791 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.791 ft

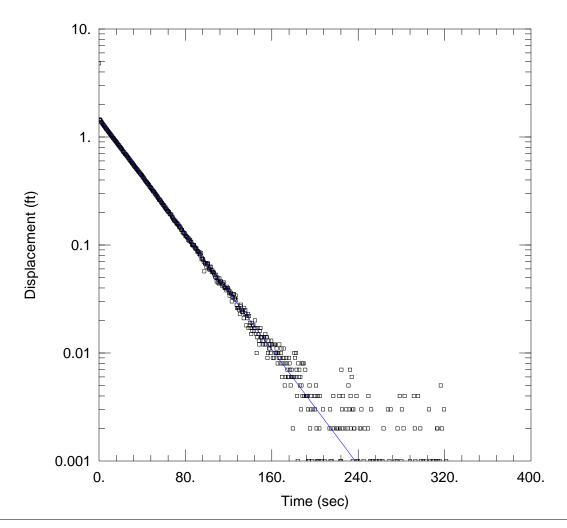
Screen Length: 6.791 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 4.774E-5 ft/secy0 = 1.472 ft



Data Set: N:\...\WMW-28-3.aqt

Date: 10/05/18 Time: 08:10:03

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-28 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.791 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-28)

Initial Displacement: 4.806 ft

Total Well Penetration Depth: 6.791 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.791 ft

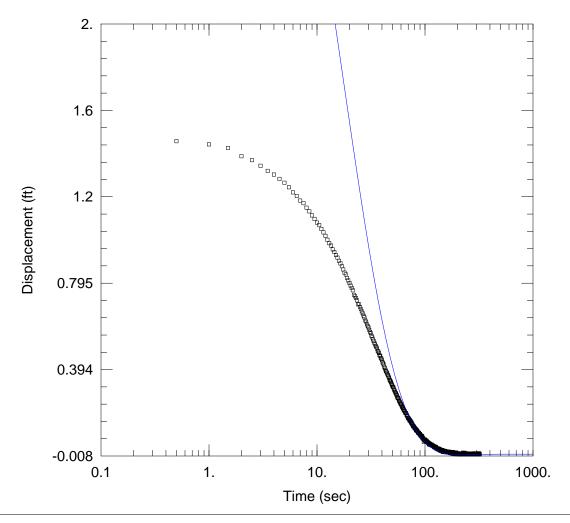
Screen Length: 6.791 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 8.264E-5 ft/sec y0 = 1.472 ft



Data Set: N:\...\WMW-28-3.aqt

Date: 10/05/18 Time: 08:11:38

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-28</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 6.791 ft

WELL DATA (WMW-28)

Initial Displacement: 4.806 ft

Total Well Penetration Depth: 6.791 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.791 ft

Screen Length: <u>6.791</u> ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

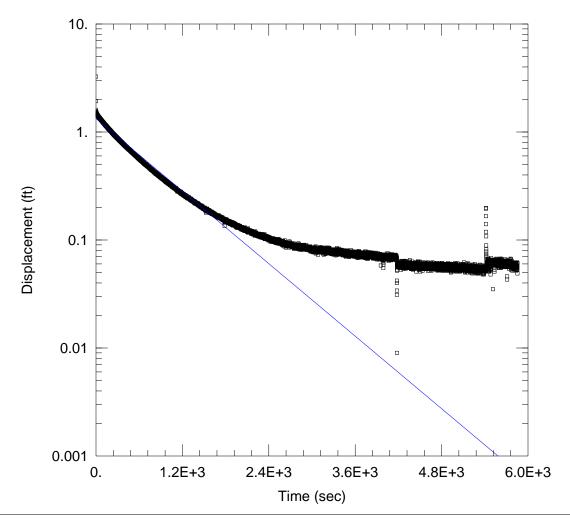
= 9.128E-5 ft/sec

Solution Method: KGS Model

Kz/Kr = 1.

Kr

Ss = $0.0001473 \text{ ft}^{-1}$



Data Set: N:\...\WMW-30-1.aqt

Date: 10/05/18 Time: 08:34:07

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-30 Test Date: 8/28/18

AQUIFER DATA

Saturated Thickness: 6.453 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-30)

Initial Displacement: 3.259 ft

Total Well Penetration Depth: 6.453 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.453 ft

Screen Length: 6.453 ft Well Radius: 0.125 ft

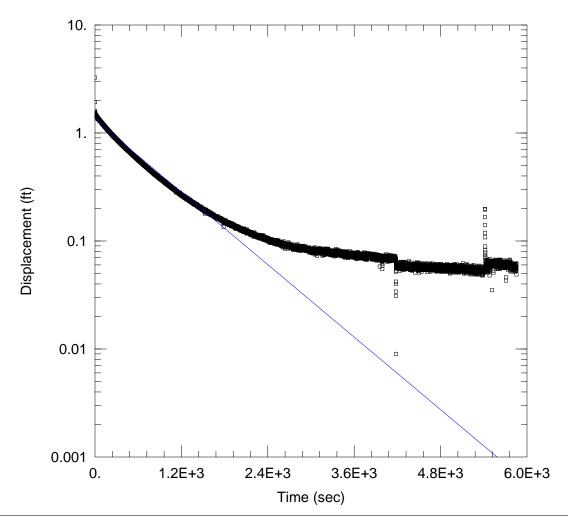
SOLUTION

Aquifer Model: Unconfined

K = 2.077E-6 ft/sec

Solution Method: Bouwer-Rice

y0 = 1.329 ft



Data Set: N:\...\WMW-30-1.aqt

Date: 10/05/18 Time: 08:35:23

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: $\frac{WMW-30}{8/28/18}$

AQUIFER DATA

Saturated Thickness: 6.453 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-30)

Initial Displacement: 3.259 ft

Total Well Penetration Depth: 6.453 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.453 ft

Screen Length: <u>6.453</u> ft Well Radius: 0.125 ft

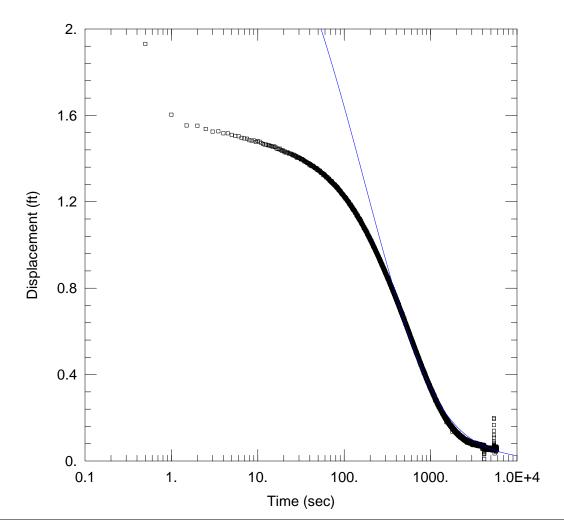
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 3.643E-6 ft/sec

y0 = 1.329 ft



Data Set: N:\...\WMW-30-1.aqt

Date: 10/05/18 Time: 08:41:35

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-30</u> Test Date: <u>8/28/18</u>

AQUIFER DATA

Saturated Thickness: 6.453 ft

WELL DATA (WMW-30)

Initial Displacement: 3.259 ft

Static Water Column Height: 6.453 ft

Total Well Penetration Depth: 6.453 ft

Screen Length: <u>6.453</u> ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

SOLUTION

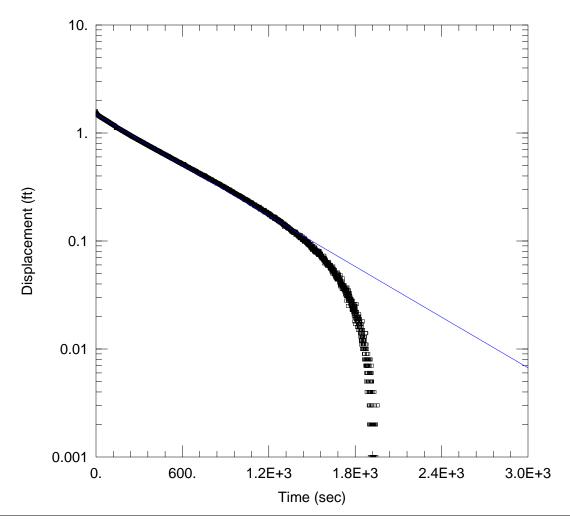
Aquifer Model: Unconfined

Solution Method: KGS Model

Kr = 2.929E-6 ft/sec

Ss = 0.0155 ft^{-1}

Kz/Kr = 1.



Data Set:

Date: 10/05/18 Time: 10:30:50

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-30 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.56 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-30)

Initial Displacement: 1.588 ft

Total Well Penetration Depth: 6.56 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.56 ft

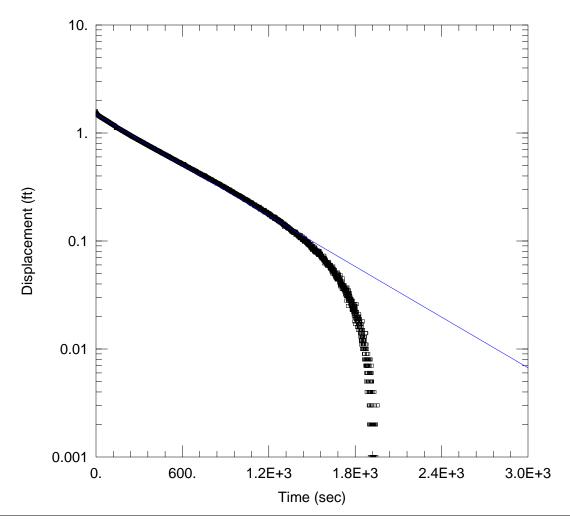
Solution Method: Bouwer-Rice

Screen Length: 6.56 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

K = 2.868E-6 ft/sec y0 = 1.484 ft



Data Set: N:\...\WMW-30-2.aqt

Date: 10/05/18 Time: 10:31:33

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-30 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.56 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-30)

Initial Displacement: 1.588 ft

Total Well Penetration Depth: 6.56 ft

Static Water Column Height: 6.56 ft

Screen Length: 6.56 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

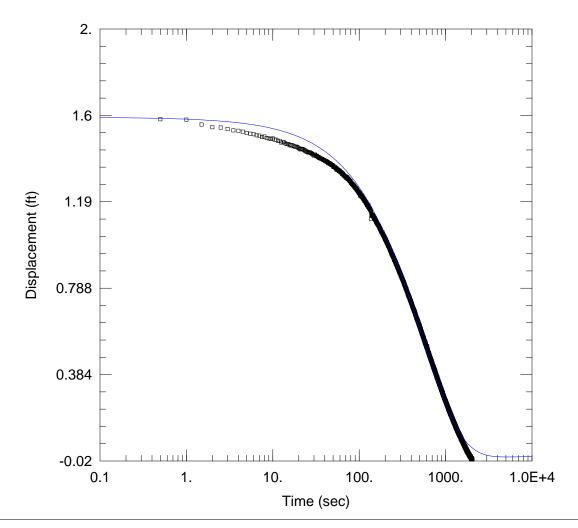
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 5.009E-6 ft/sec

y0 = 1.484 ft



Data Set: N:\...\WMW-30-2.aqt

Date: 10/05/18 Time: 10:33:02

PROJECT INFORMATION

Company: <u>Kennedy/Jenks Consultants</u> Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-30</u> Test Date: <u>8/29/18</u>

AQUIFER DATA

Saturated Thickness: 6.56 ft

WELL DATA (WMW-30)

Initial Displacement: 1.588 ft

Total Well Penetration Depth: 6.56 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.56 ft

Screen Length: <u>6.56</u> ft Well Radius: 0.125 ft

SOLUTION

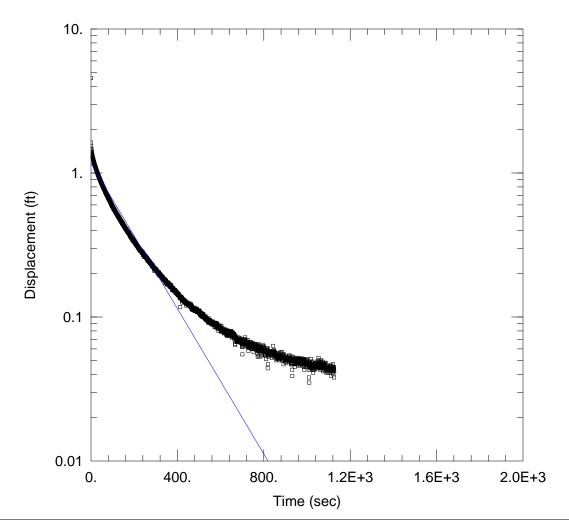
Aquifer Model: Unconfined

Kr = 3.348E-6 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = $5.294E-5 \text{ ft}^{-1}$



Data Set: N:\...\WMW-31-1.aqt

Date: 10/05/18 Time: 10:38:56

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-31 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.473 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-31)

Initial Displacement: 4.561 ft

Casing Radius: 0.083 ft

Total Well Penetration Depth: 6.473 ft

Static Water Column Height: 6.473 ft

Screen Length: 6.473 ft Well Radius: 0.125 ft

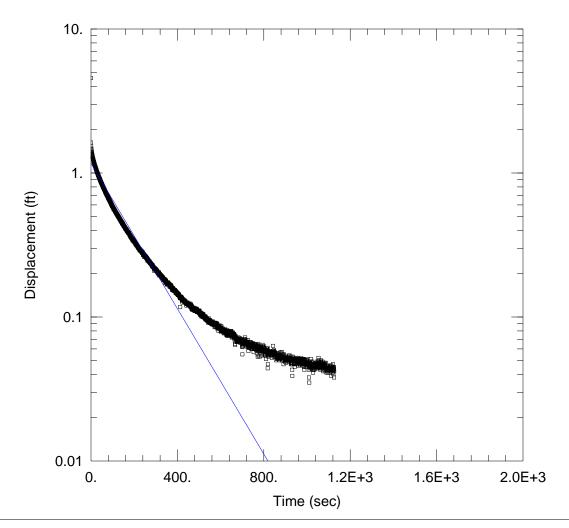
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 9.345E-6 ft/sec

y0 = 1.167 ft



Data Set: N:\...\WMW-31-1.aqt

Date: 10/05/18 Time: 10:39:34

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-31</u> Test Date: <u>8/29/18</u>

AQUIFER DATA

Saturated Thickness: 6.473 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-31)

Initial Displacement: 4.561 ft

Total Well Penetration Depth: 6.473 ft

etration Depth. <u>6.473</u> i

Casing Radius: 0.083 ft

Static Water Column Height: 6.473 ft

Screen Length: <u>6.473</u> ft Well Radius: 0.125 ft

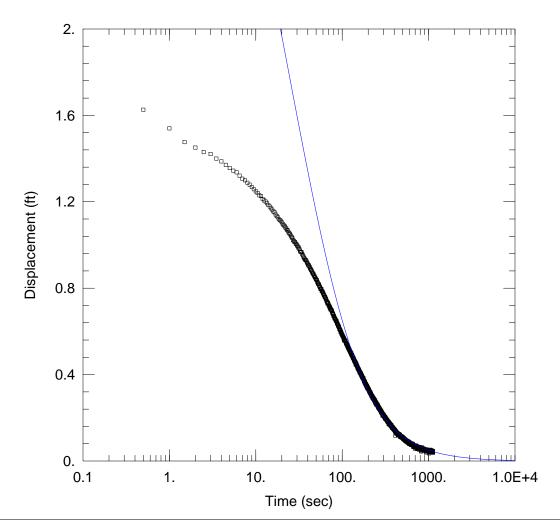
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 1.638E-5 ft/sec

y0 = 1.167 ft



Data Set: N:\...\WMW-31-1.aqt

Date: 10/05/18 Time: 10:42:18

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-31
Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.473 ft

WELL DATA (WMW-31)

Initial Displacement: 4.561 ft

Total Well Penetration Depth: 6.473 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.473 ft

Screen Length: <u>6.473</u> ft Well Radius: 0.125 ft

SOLUTION

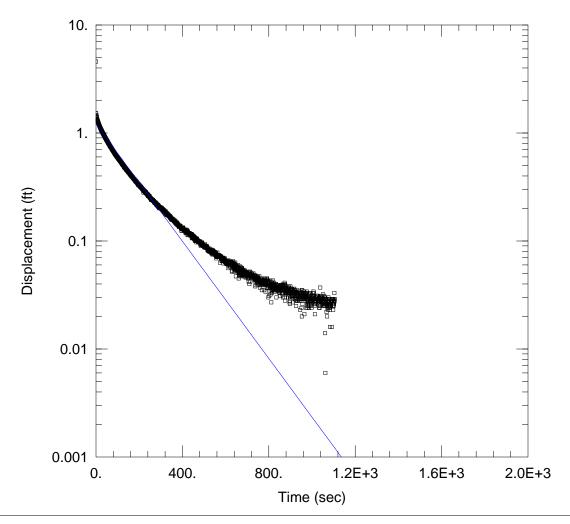
Aquifer Model: Unconfined

Kr = 2.109E-5 ft/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = 0.01545 ft^{-1}



Data Set: N:\...\WMW-31-2.aqt

Date: 10/05/18 Time: 10:46:35

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-31 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.46 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-31)

Initial Displacement: 4.582 ft

Total Well Penetration Depth: 6.46 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.46 ft

Solution Method: Bouwer-Rice

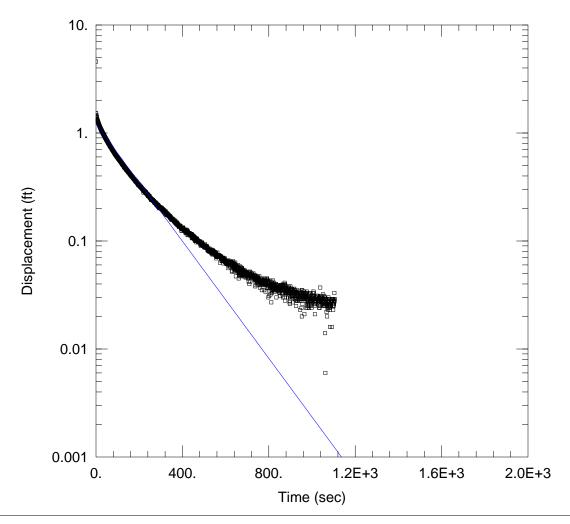
Screen Length: 6.46 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

K = 1.007E-5 ft/sec

y0 = 1.212 ft



Data Set: N:\...\WMW-31-2.aqt

Date: 10/05/18 Time: 10:47:30

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-31 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.46 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-31)

Initial Displacement: 4.582 ft

Static Water Column Height: 6.46 ft

Total Well Penetration Depth: 6.46 ft

Screen Length: 6.46 ft Well Radius: 0.125 ft

Casing Radius: 0.083 ft

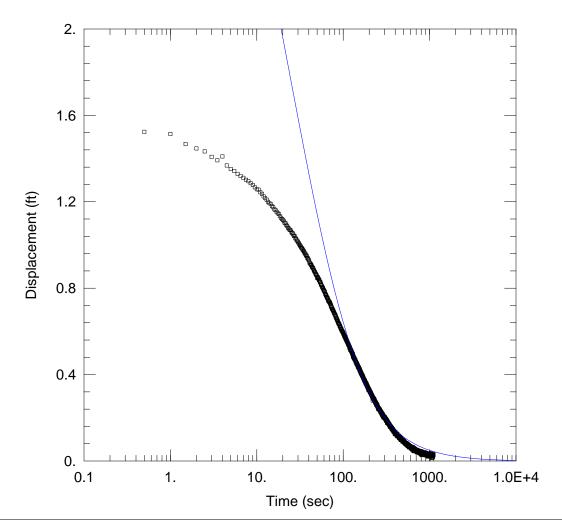
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 1.765E-5 ft/sec

y0 = 1.212 ft



Data Set: N:\...\WMW-31-2.aqt

Date: 10/05/18 Time: 11:20:08

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-31</u> Test Date: <u>8/29/18</u>

AQUIFER DATA

Saturated Thickness: 6.46 ft

WELL DATA (WMW-31)

Initial Displacement: 4.582 ft

Total Well Penetration Depth: 6.46 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.46 ft

Screen Length: <u>6.46</u> ft Well Radius: 0.125 ft

SOLUTION

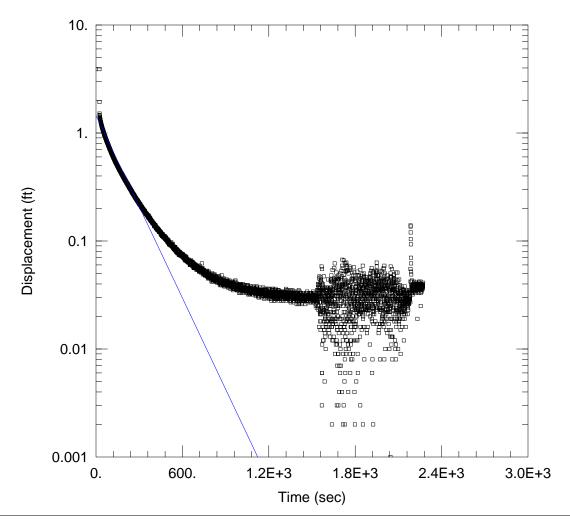
Aquifer Model: Unconfined

Kr = 2.152E-5 ft/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.01548 ft^{-1}



TEST 3

Data Set: N:\...\WMW-31-3.aqt

Date: 10/05/18 Time: 11:26:41

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-31 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.476 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-31)

Initial Displacement: 3.894 ft

Total Well Penetration Depth: 6.476 ft

Static Water Column Height: 6.476 ft Screen Length: 6.476 ft

Well Radius: 0.125 ft

SOLUTION

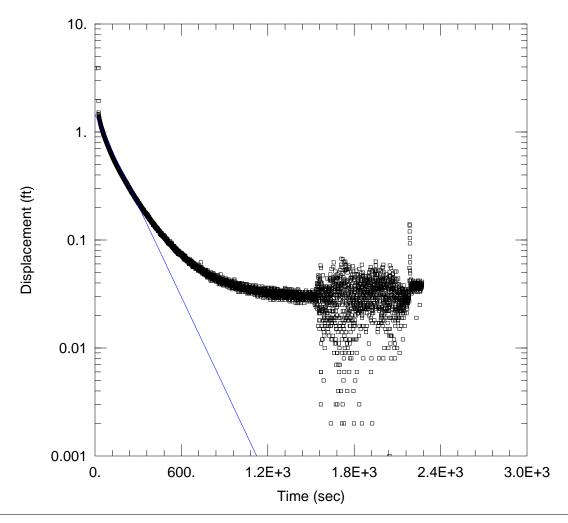
Aquifer Model: Unconfined

Casing Radius: 0.083 ft

Solution Method: Bouwer-Rice

K = 1.043E-5 ft/sec

y0 = 1.453 ft



TEST 3

Data Set: N:\...\WMW-31-3.aqt

Date: 10/05/18 Time: 11:27:10

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: <u>WMW-31</u> Test Date: <u>8/29/18</u>

AQUIFER DATA

Saturated Thickness: 6.476 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (WMW-31)

Initial Displacement: 3.894 ft

Total Well Penetration Depth: 6.476 ft

Casing Radius: 0.083 ft

Static Water Column Height: 6.476 ft

Screen Length: <u>6.476</u> ft Well Radius: 0.125 ft

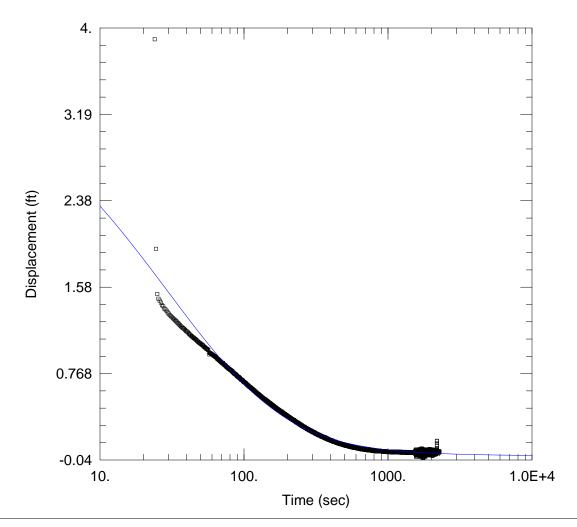
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 1.828E-5 ft/sec

y0 = 1.453 ft



TEST 3

Data Set: N:\...\WMW-31-3.aqt

Date: 10/05/18 Time: 11:28:46

PROJECT INFORMATION

Company: Kennedy/Jenks Consultants Client: BNSF Railway Company

Project: 1896120*04

Location: Wishram Railyard, Washington

Test Well: WMW-31 Test Date: 8/29/18

AQUIFER DATA

Saturated Thickness: 6.476 ft

WELL DATA (WMW-31)

Initial Displacement: 3.894 ft

Total Well Penetration Depth: 6.476 ft Casing Radius: 0.083 ft

Screen Length: 6.476 ft Well Radius: 0.125 ft

SOLUTION

Aquifer Model: Unconfined

= 1.713E-5 ft/sec Kr

Kz/Kr = 1.

Solution Method: KGS Model

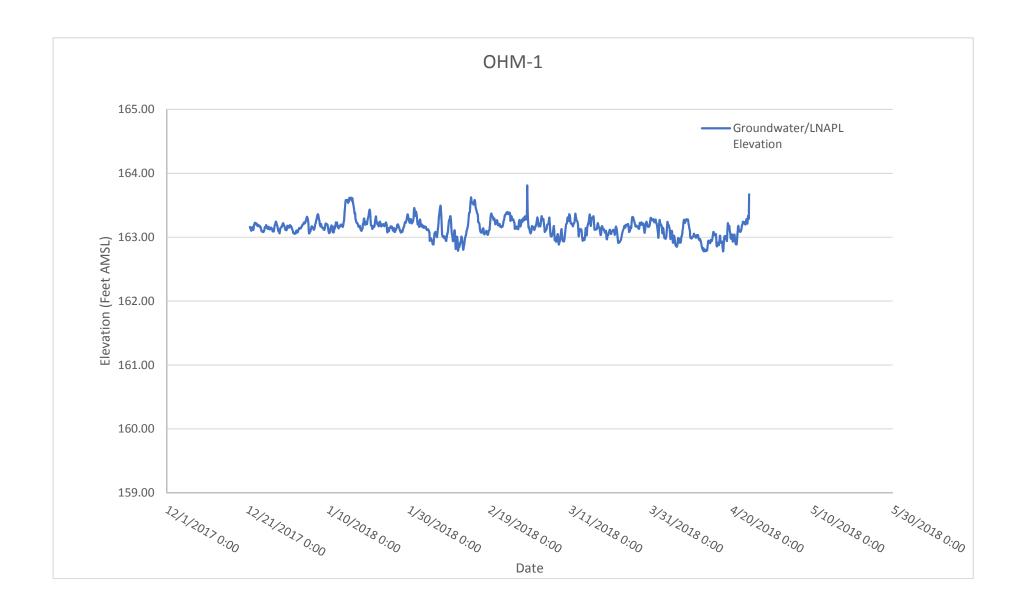
Static Water Column Height: 6.476 ft

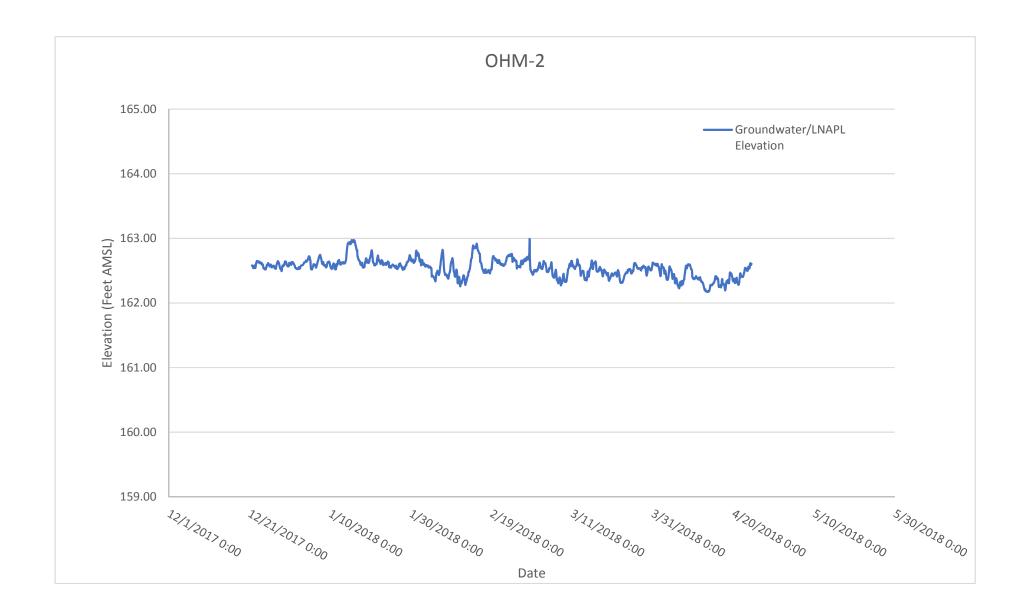
 $= 0.01544 \text{ ft}^{-1}$

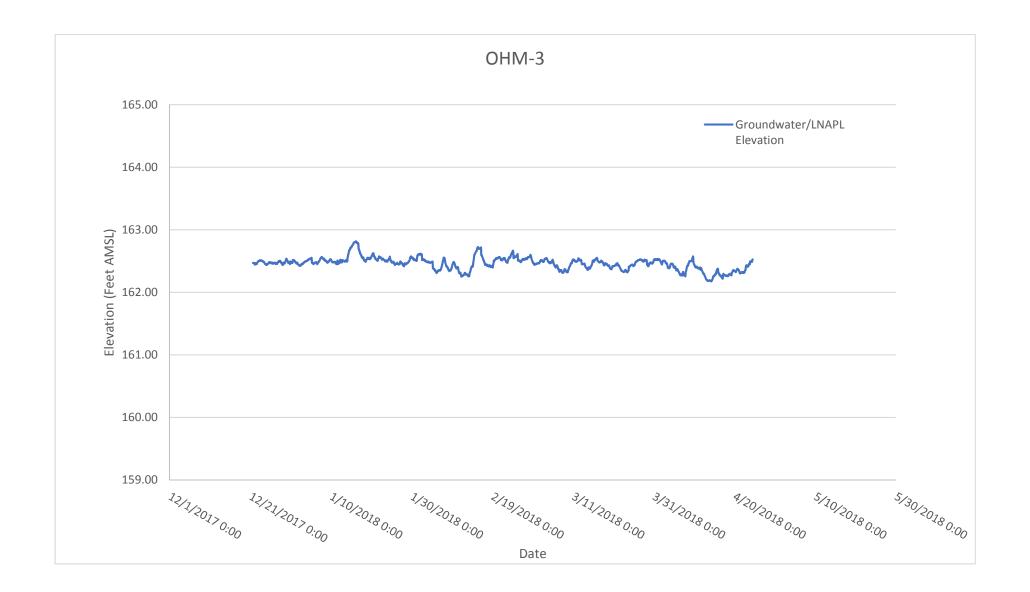
Appendix K

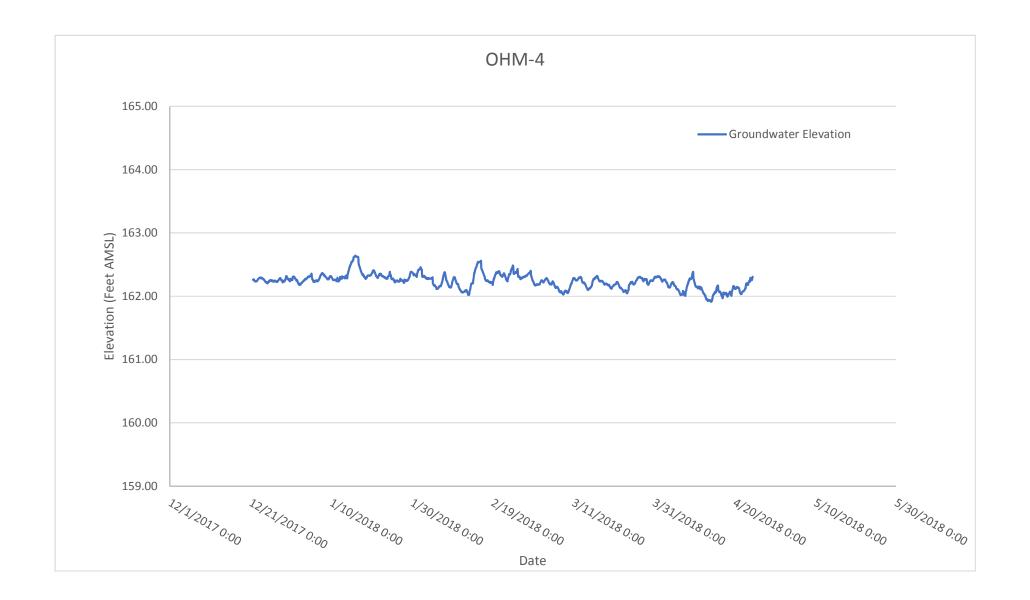
Transducer Data Plots

OHM-1 Pressure Transducer Data December 2017 Through April 2018

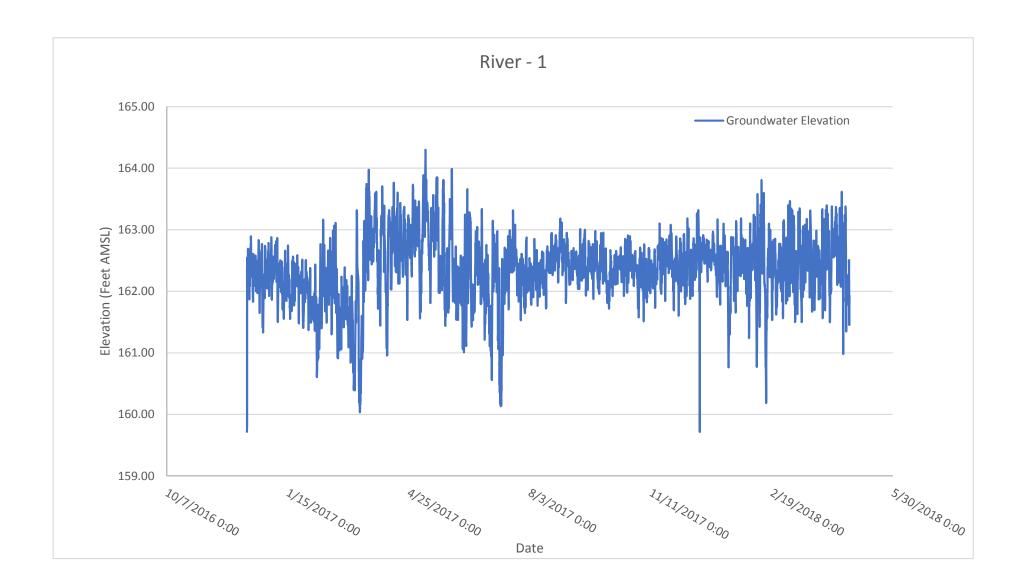




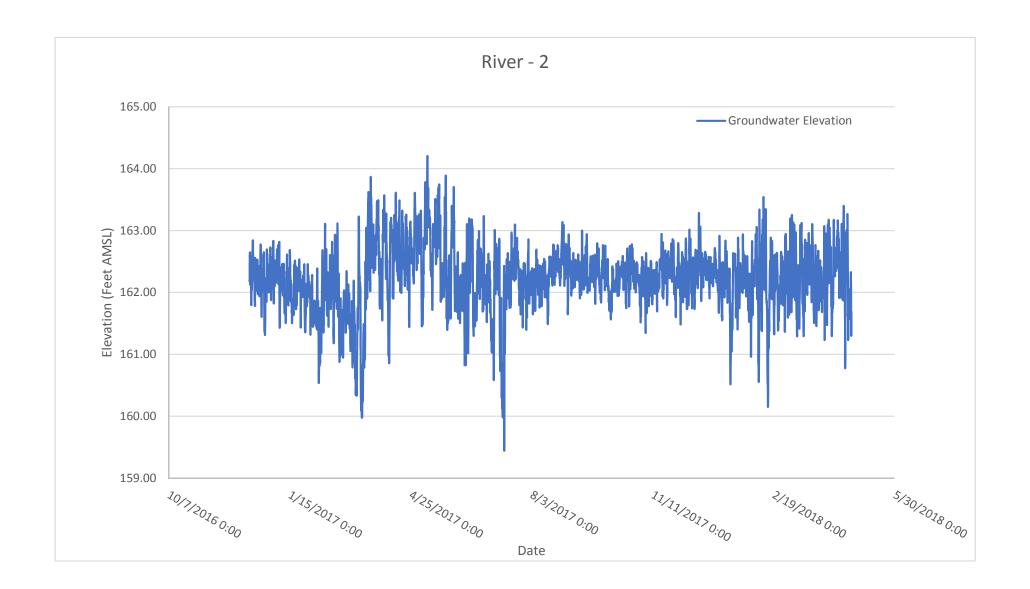




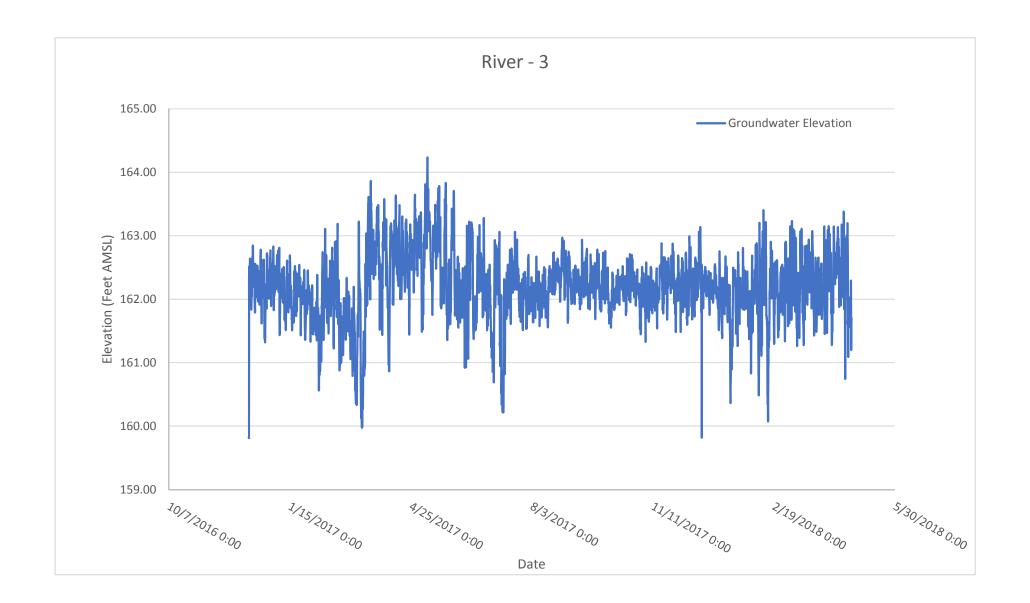
River - 1 Pressure Transducer Data December 2016 Through April 2018



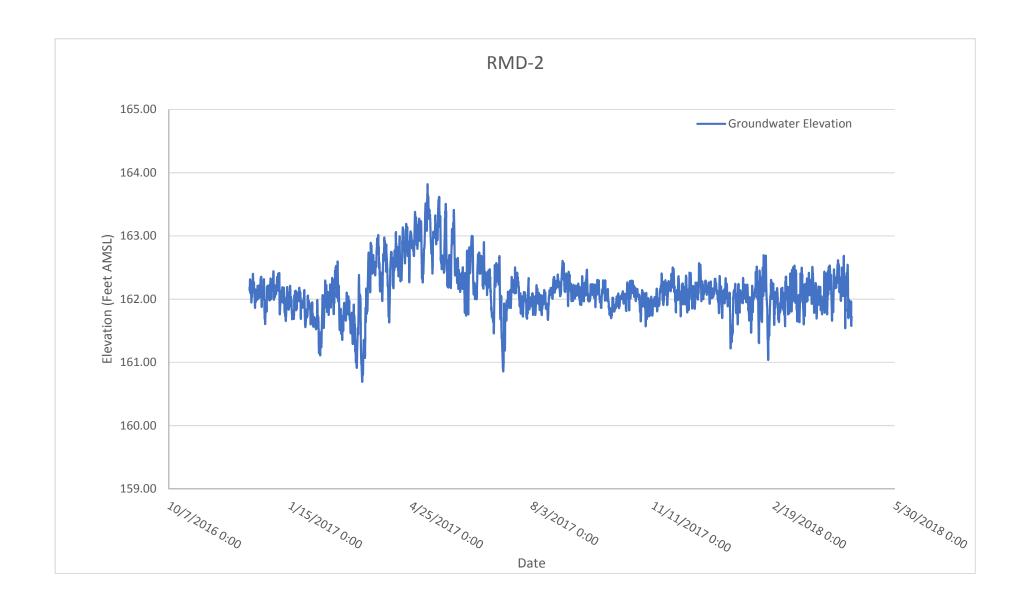
River - 2 Pressure Transducer Data December 2016 Through April 2018



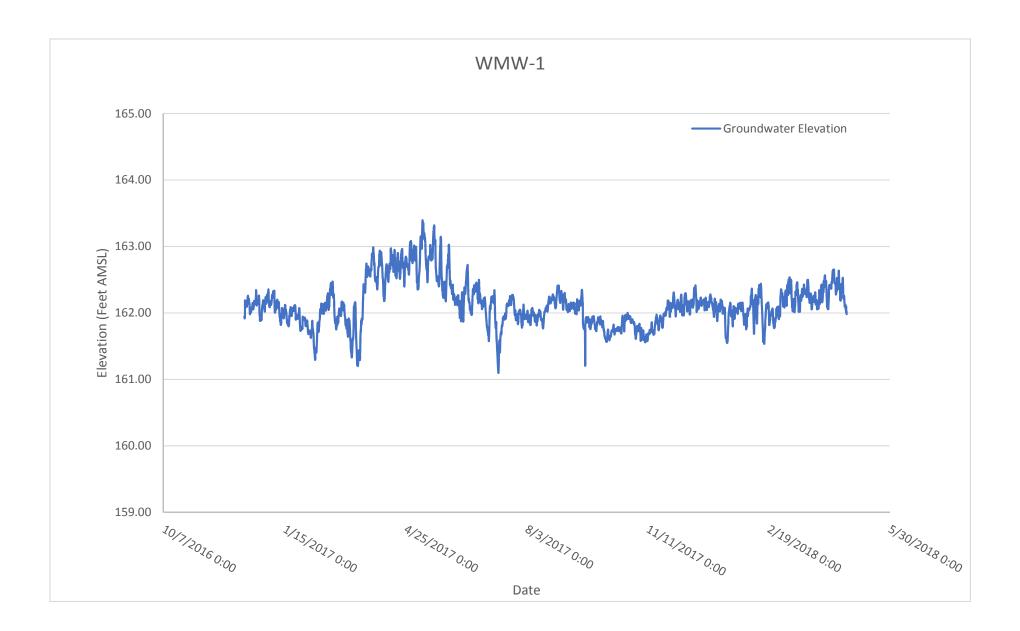
River - 3 Pressure Transducer Data December 2016 Through April 2018



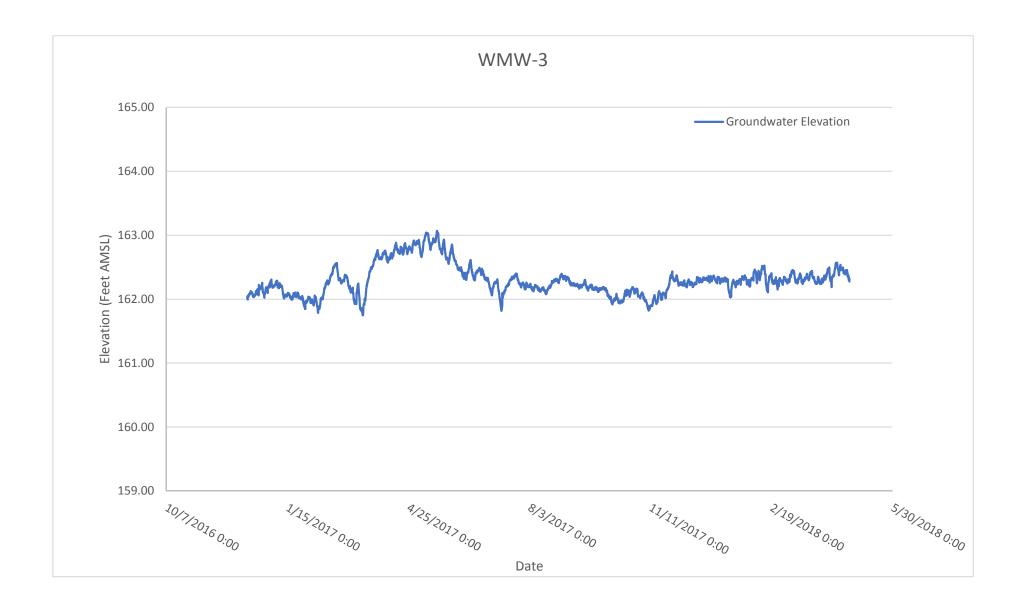
RMD-2 Pressure Transducer Data December 2016 Through April 2018



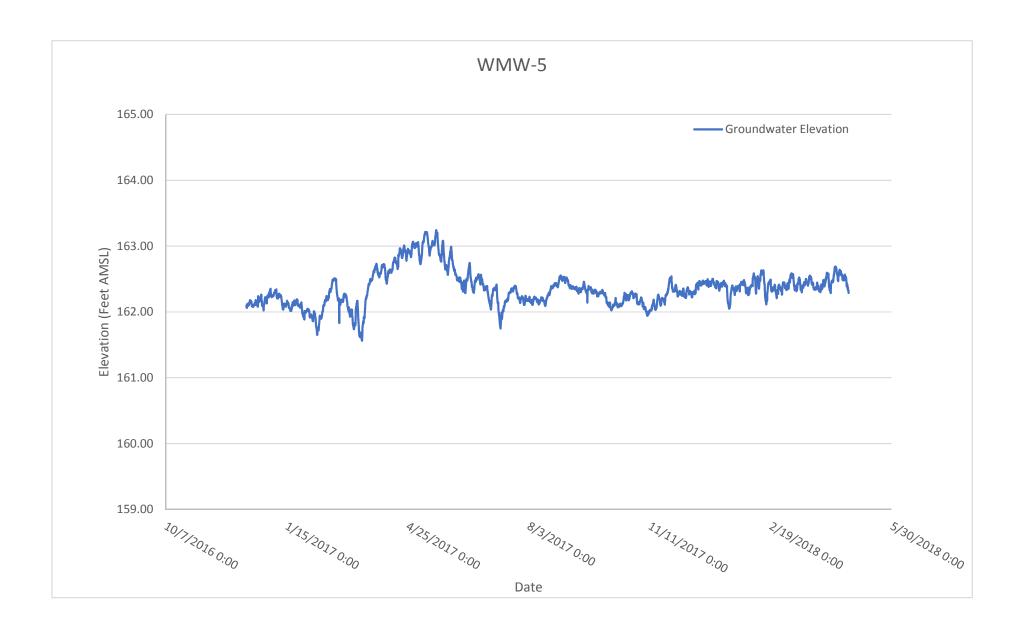
WMW-1 Pressure Transducer Data December 2016 Through April 2018

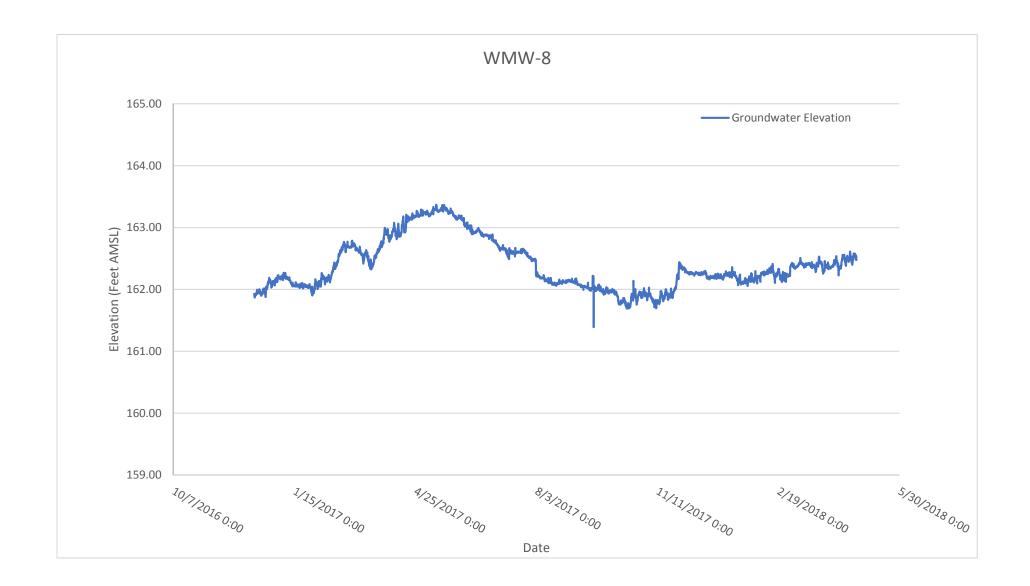


WMW-3 Pressure Transducer Data December 2016 Through April 2018

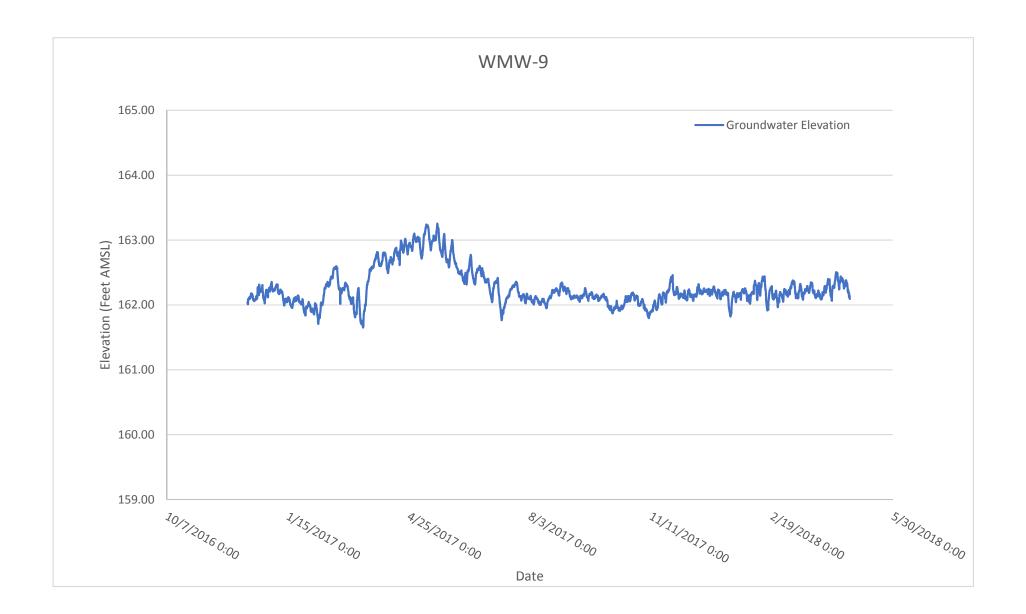


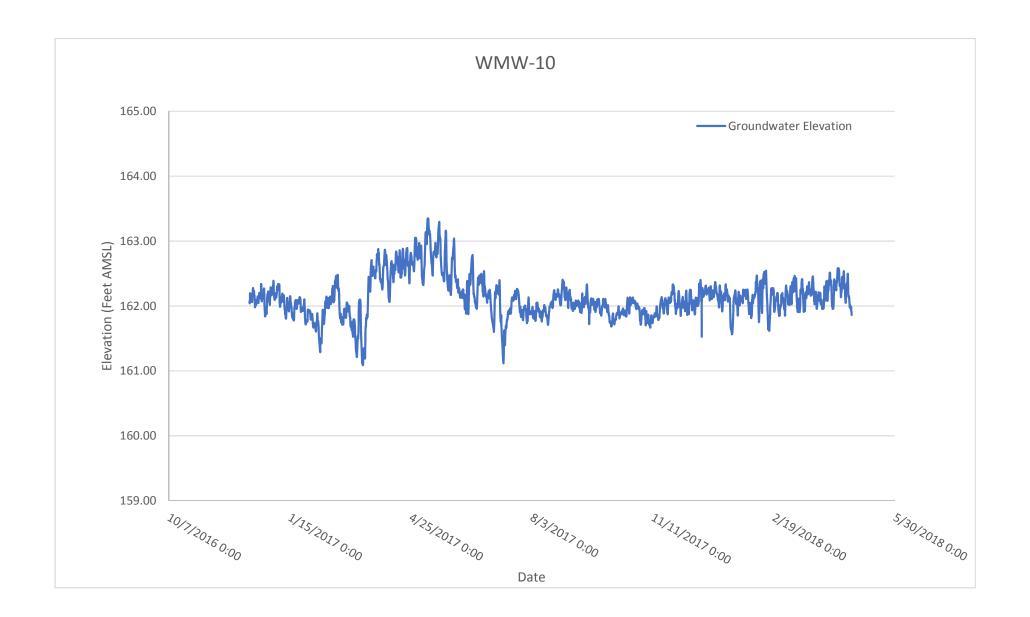
WMW-5 Pressure Transducer Data December 2016 Through April 2018

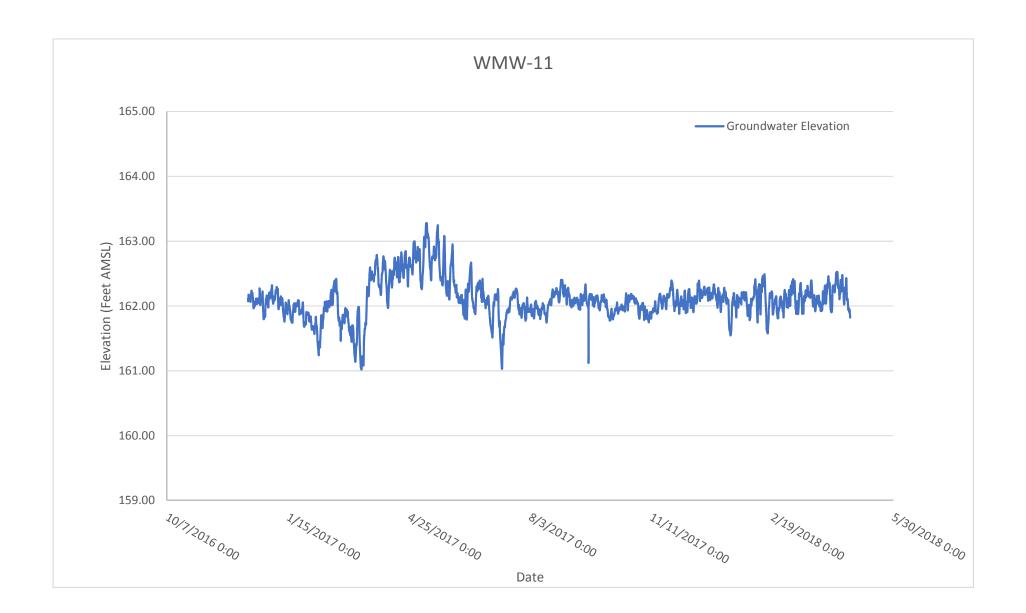


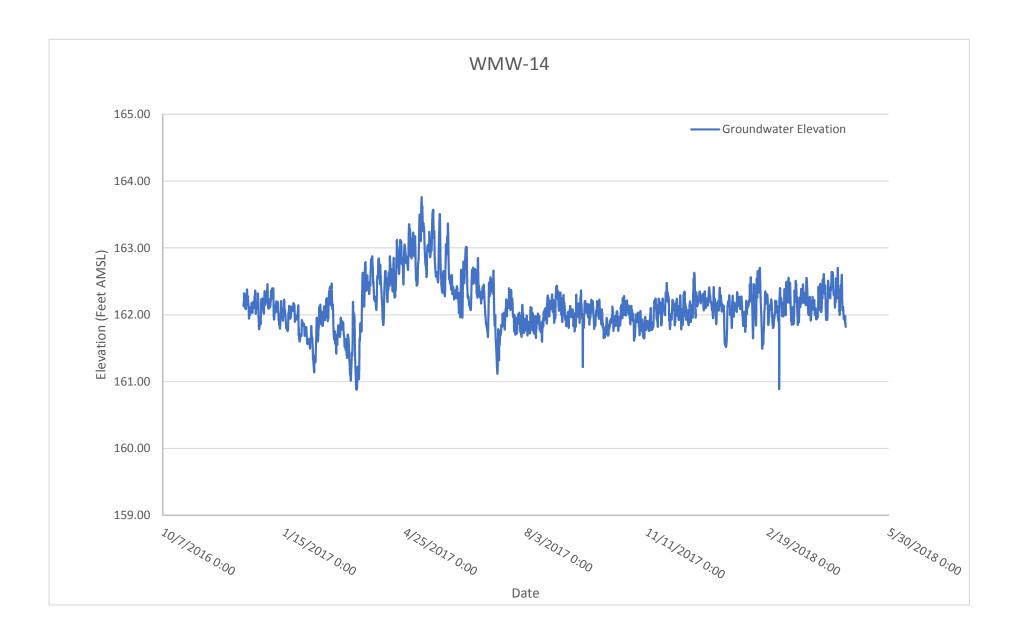


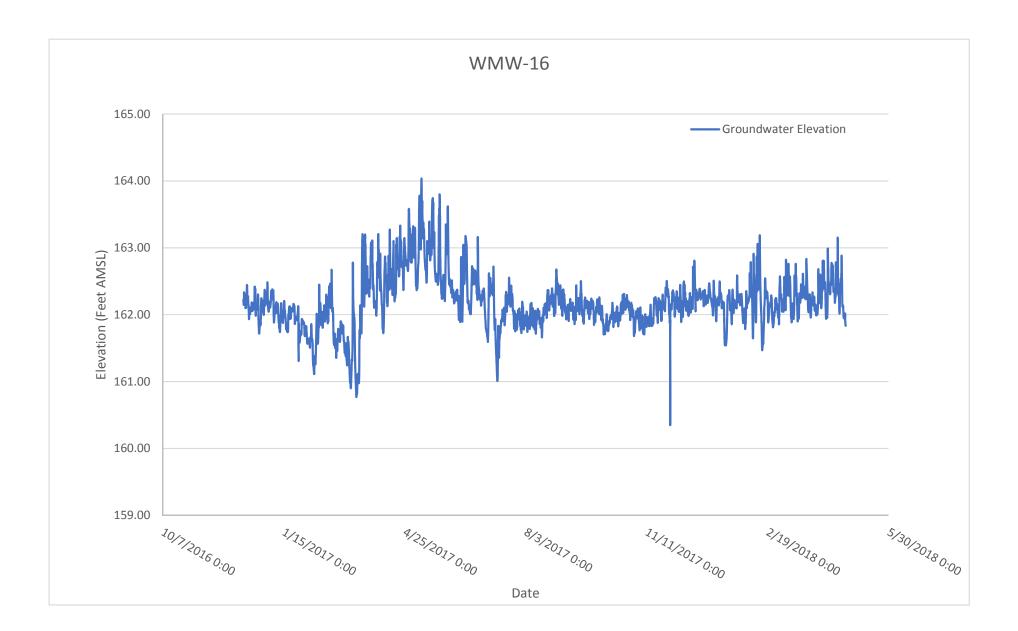
WMW-9 Pressure Transducer Data December 2016 Through April 2018

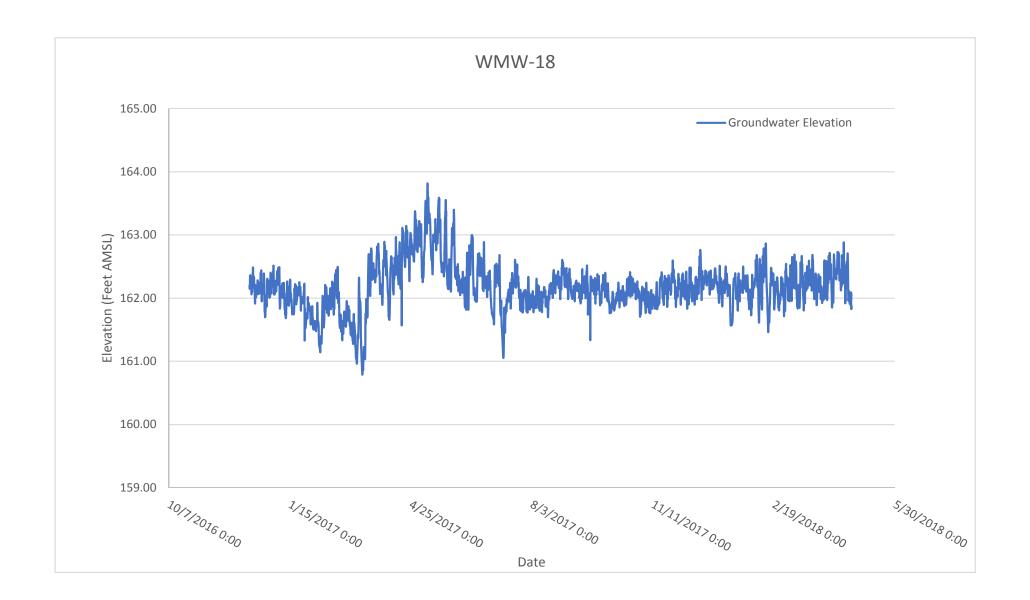


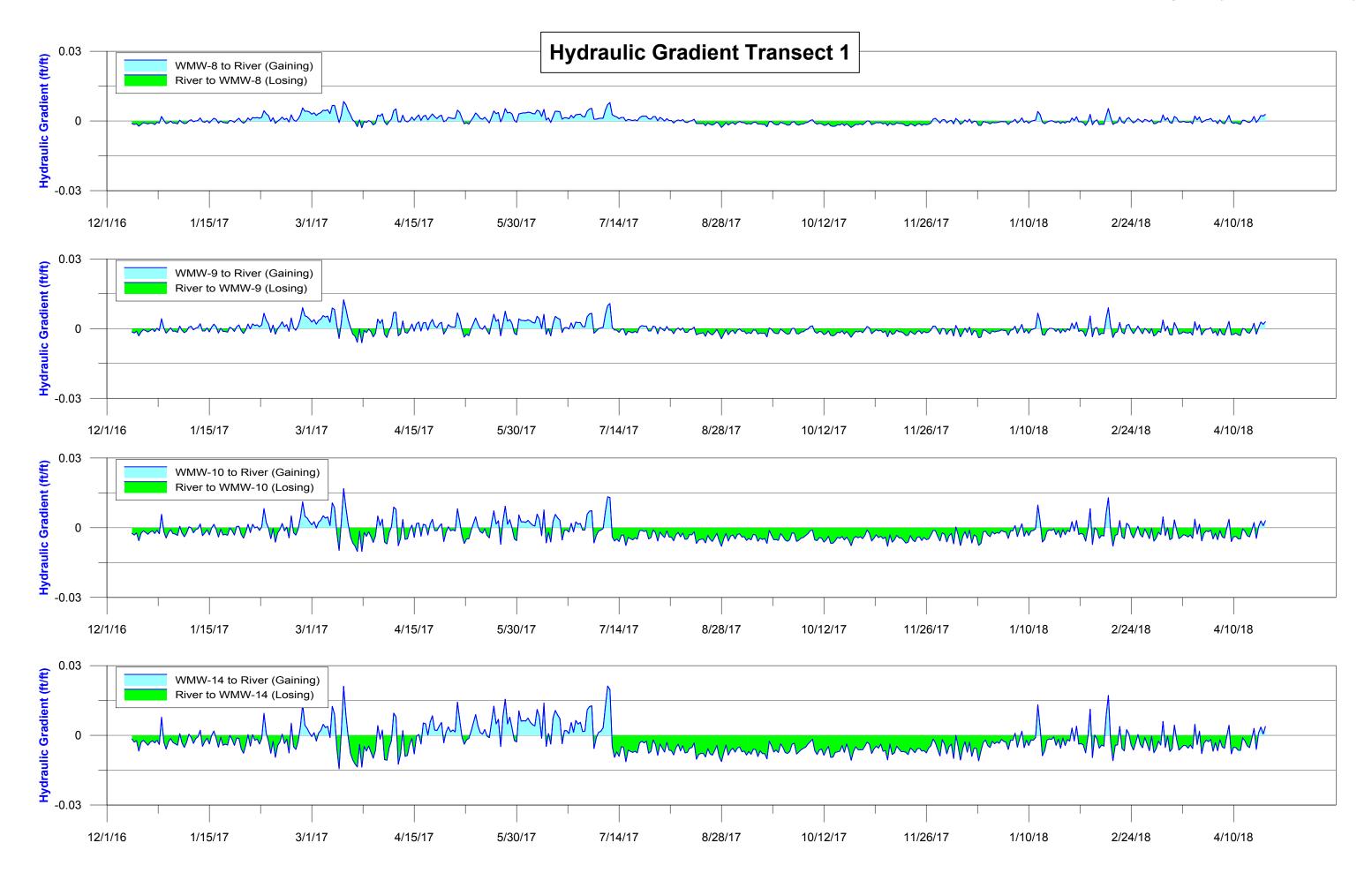


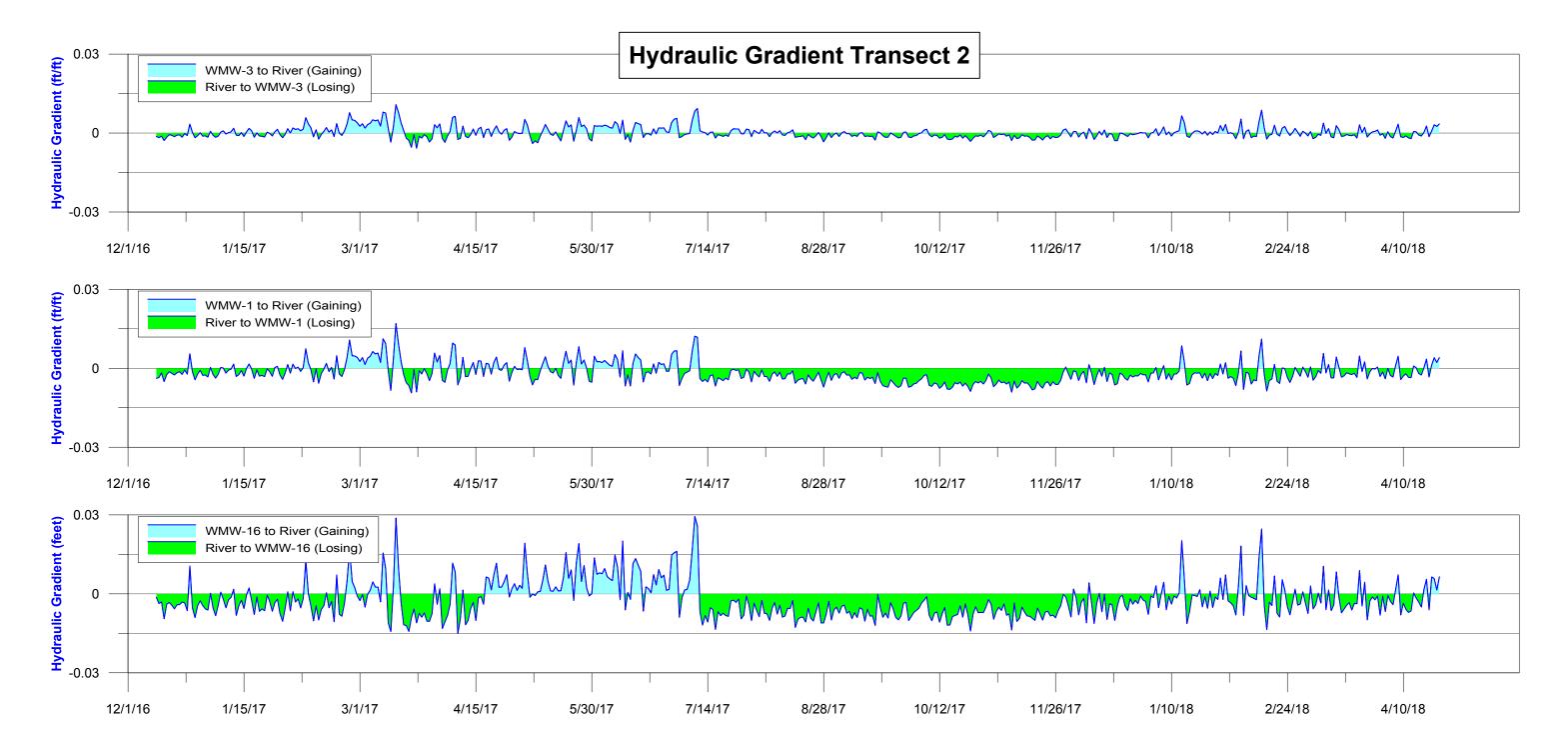


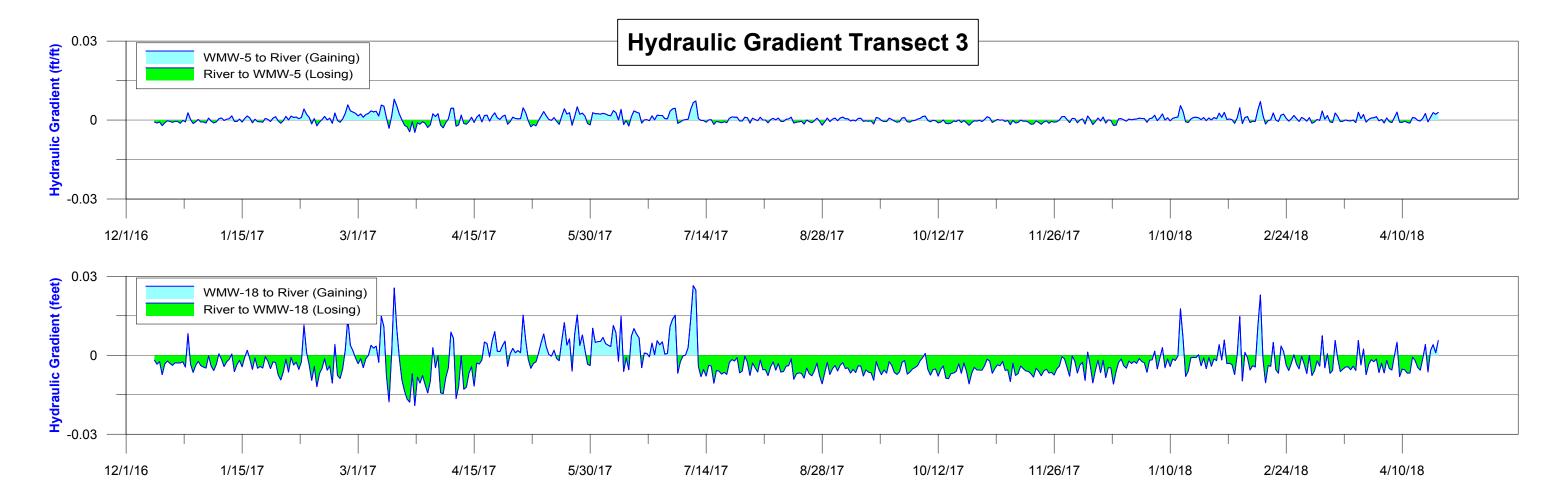












Appendix L

Hydraulic Gradient Analysis and Data Plots

Appendix L

Analysis of Groundwater and River Transducer Data

Introduction

Beginning in December 2016, transducer pressure data – convertible into hydraulic heads – were collected every two hours from three river locations as well as from multiple monitoring well locations (WMW-1, WMW-3, WMW-5, WMW-8, WMW-9, WMW-10, WMW-11, WMW-14, WMW-16, and WMW-18). Given the temporal resolution, these data sets provide a means for quantitative analysis regarding groundwater flow direction, with respect to the river, as a function of time. However, groundwater-riparian hydraulic interactions can entail both attenuation and lag in river water level fluctuations before a given water level perturbation (e.g., Figure 1) reaches a nearby monitoring well. To address the issue of the migration of "peaks" and "troughs" in the river impacting groundwater elevation on different time scales, a one-dimensional linear model with a periodic boundary condition was employed to partially correct out the effects of lag and attenuation (Van Wijk and de Vries, 1963), expressed as Equation-1:

$$h(x,t) = \bar{h} + A \frac{\left[sin\left(\omega t - \frac{x}{d}\right)\right]}{exp\left(\frac{x}{d}\right)}$$

where h is the hydraulic head, x the distance from the river bank to a monitoring point, ω the radial frequency (= $2\pi/T$, where T is the period), and d the damping distance as given by Equation-2:

$$d = \sqrt{\frac{2D}{\omega}} = \sqrt{\frac{2Kb}{S_y \omega}}$$

Here, D is the aquifer hydraulic diffusivity, K the hydraulic conductivity, b the aquifer thickness, and Sy the specific yield. The above relationship is subject to idealizing assumptions pertaining to a homogeneous aquifer, one-dimensional flow between the river and groundwater, and no additional source/sinks for groundwater other than the river itself.

The complex nature of the fluctuating boundary condition imposed by the river elevation itself requires an additional analytical component to inform Equation-1. Because the boundary condition employed by Equation-1 is sinusoidal, the complex river elevation behavior in time can be approximated using a Fourier series, which adds the terms of sine and cosine series over a large range of frequencies to mimic the observed behavior (Equation-3):

$$y = a_0 + \sum_{j=1}^{J} \left[a_j \cos\left(\frac{2\pi jt}{T}\right) + b_j \sin\left(\frac{2\pi jt}{T}\right) \right]$$

A Fourier series consisting of an arbitrary number of terms can be fit to the data using a general linear regression model, so that the coefficients in the Fourier series (e.g., a and b values, or the associated amplitudes for each frequency) can be determined that minimize the error between observation and predictions. Because Equation-1, the groundwater pressure signal perturbation relationship is linear, multiple solutions for different frequencies, as expressed by a Fourier series, can simply be superimposed to calculate the idealized response in groundwater elevation at a certain distance and time.

Results and Discussion

A Fourier series fit to the time-dependent average elevations calculated from the three river transducers from the data set spanning April 2017 through March 2018 is shown on Figure 2 for the first 100 days of that time period. The series was fit using 120 terms, effectively including perturbations with frequencies larger than approximately three days and excluding shorter "spikes" in the data. This represents the source term used in Equation-1.

Assuming an average hydraulic conductivity of 10 ft/day (based in part upon slug test results obtained from a subset of the instrumented wells), a specific yield of 0.1, and an average aquifer saturated thickness of 40 feet, simulated groundwater elevations associated with the observed river elevations are compared with groundwater transducer data on Figures 3 through 12. With the predicted values as a reference, higher-than-modeled groundwater elevations imply net flow toward the river from a given monitoring well location, whereas lower-than-modeled observations imply net flow away from the river.

Monthly averaged observed and modeled river and groundwater elevations are summarized in Tables L-1A and L-1B. The monthly averaged groundwater elevations, minus the corresponding monthly average river elevations across the monitoring well locations, are shown in Table L-2A. By this data-only metric, negative numbers imply flow away from the river, or a losing stream condition, whereas positive numbers imply a gaining stream condition. In comparison, average measured groundwater elevations, minus corresponding average modeled elevations, are shown in Table L-2B. As noted, negative values, or lower-than-modeled groundwater elevations, imply a losing stream condition, whereas positive values, or higher-than-modeled groundwater elevations, imply a gaining stream condition.

The approaches summarized in Tables L-2A and L-2B are in good agreement and indicate a losing stream condition during the summer and fall months across all well locations, and a gaining stream condition in the spring months for a majority of the wells. Overall, across all wells and the entire year, a losing condition is encountered more often than a gaining one.

Example average groundwater elevation distributions for implied gaining conditions (June) and losing conditions (November) are shown on Figures 13 and 14. With the inclusion of the river

transducer data and locations, the overall reversal of flow directions, as indicated by Tables L-2A and 2B, is apparent.

Reference

W. Van Wijk and D. de Vries, 1963. Periodic temperature variations in a homogeneous soil, in *Physics of Plant Environment* (W.R. van Wijk, ed.), North-Holland Publishing, Amsterdam.

TABLE L-1A AND L-1B

MONTHLY MEASURED AND MODELLED RIVER AND GROUNDWATER ELEVATIONS BNSF Wishram Railyard, Wishram, Washington

Table L-1A: Monthly Average Measured River and Groundwater Elevations

Month	River	WMW-1	WMW-3	WMW-5	WMW-8	WMW-9	WMW-10	WMW-11	WMW-14	WMW-16	WMW-18
Apr	162.68	162.70	162.74	162.77	163.04	162.80	162.63	162.56	162.64	162.64	162.58
May	162.75	162.76	162.84	162.95	163.24	162.95	162.75	162.69	162.93	162.93	162.86
Jun	162.17	162.23	162.43	162.47	162.94	162.49	162.25	162.16	162.40	162.38	162.31
Jul	162.04	161.94	162.20	162.19	162.60	162.16	161.93	161.90	161.96	161.99	162.01
Aug	162.31	162.05	162.22	162.27	162.16	162.13	162.01	162.04	161.99	162.06	162.11
Sep	162.34	162.01	162.22	162.36	162.04	162.14	162.03	162.09	162.02	162.11	162.15
Oct	162.26	161.79	162.07	162.19	161.87	162.04	161.93	162.00	161.96	162.02	162.06
Nov	162.27	161.82	162.06	162.17	161.94	162.07	161.94	162.01	161.97	162.03	162.07
Dec	162.37	162.14	162.28	162.35	162.25	162.18	162.11	162.13	162.12	162.23	162.21
Jan	162.17	162.02	162.27	162.37	162.19	162.14	162.09	162.06	162.09	162.15	162.14
Feb	162.21	162.03	162.32	162.40	162.24	162.19	162.12	162.08	162.12	162.20	162.18
Mar	162.33	162.25	162.32	162.42	162.39	162.21	162.17	162.13	162.18	162.26	162.23

Table L-1B: Monthly Average Modeled River and Groundwater Elevations

Month	River	WMW-1	WMW-3	WMW-5	WMW-8	WMW-9	WMW-10	WMW-11	WMW-14	WMW-16	WMW-18
Apr	162.68	162.58	162.49	162.46	162.42	162.53	162.60	162.61	162.64	162.64	162.63
May	162.76	162.72	162.67	162.65	162.61	162.70	162.73	162.74	162.75	162.75	162.75
Jun	162.17	162.26	162.33	162.36	162.39	162.30	162.24	162.23	162.21	162.20	162.21
Jul	162.03	162.06	162.12	162.14	162.19	162.09	162.05	162.05	162.04	162.04	162.04
Aug	162.31	162.28	162.26	162.25	162.24	162.27	162.29	162.29	162.30	162.30	162.30
Sep	162.35	162.35	162.36	162.35	162.35	162.36	162.35	162.35	162.35	162.35	162.35
Oct	162.25	162.27	162.28	162.29	162.29	162.28	162.27	162.27	162.26	162.26	162.26
Nov	162.27	162.27	162.27	162.27	162.28	162.27	162.27	162.27	162.27	162.27	162.27
Dec	162.37	162.35	162.34	162.34	162.33	162.35	162.36	162.36	162.36	162.36	162.36
Jan	162.17	162.22	162.25	162.26	162.28	162.24	162.21	162.20	162.19	162.19	162.19
Feb	162.21	162.21	162.22	162.23	162.24	162.22	162.21	162.21	162.21	162.21	162.21
Mar	162.33	162.32	162.30	162.30	162.29	162.31	162.32	162.33	162.33	162.33	162.33

Note:

All data results presented in elevation units of feet above mean sea level.

TABLE L-2A AND L-2B

MONTHLY AVERAGE RIVER VERSUS GROUNDWATER ELEVATIONS BNSF Wishram Railyard, Wishram, Washington

Table L-2A: Monthly Average Measured Groundwater Elevation Minus River Elevation

Month	WMW-1	WMW-3	WMW-5	WMW-8	WMW-9	WMW-10	WMW-11	WMW-14	WMW-16	WMW-18
Apr	0.02	0.07	0.10	0.37	0.13	-0.05	-0.12	-0.04	-0.03	-0.09
May	0.01	0.09	0.20	0.49	0.19	0.00	-0.06	0.18	0.17	0.10
Jun	0.06	0.26	0.30	0.76	0.32	0.07	-0.02	0.23	0.20	0.14
Jul	-0.10	0.17	0.16	0.56	0.12	-0.11	-0.13	-0.08	-0.05	-0.02
Aug	-0.26	-0.10	-0.04	-0.16	-0.19	-0.31	-0.27	-0.33	-0.25	-0.20
Sep	-0.33	-0.13	0.01	-0.31	-0.20	-0.31	-0.26	-0.32	-0.23	-0.19
Oct	-0.46	-0.19	-0.07	-0.39	-0.21	-0.32	-0.25	-0.30	-0.24	-0.19
Nov	-0.45	-0.21	-0.10	-0.33	-0.20	-0.33	-0.26	-0.30	-0.24	-0.19
Dec	-0.22	-0.09	-0.02	-0.12	-0.19	-0.25	-0.24	-0.24	-0.13	-0.15
Jan	-0.15	0.10	0.20	0.02	-0.03	-0.08	-0.11	-0.08	-0.02	-0.03
Feb	-0.19	0.11	0.18	0.03	-0.03	-0.09	-0.14	-0.09	-0.02	-0.04
Mar	-0.08	-0.01	0.09	0.05	-0.12	-0.16	-0.21	-0.15	-0.07	-0.10

Table L-2B: Monthly Average Measured Groundwater Minus Modeled Groundwater Elevation

Month	WMW-1	WMW-3	WMW-5	8-WMW	WMW-9	WMW-10	WMW-11	WMW-14	WMW-16	WMW-18
Apr	0.12	0.25	0.31	0.62	0.28	0.03	-0.05	0.00	0.00	-0.05
May	0.04	0.16	0.30	0.64	0.25	0.02	-0.05	0.18	0.18	0.11
Jun	-0.03	0.09	0.12	0.55	0.19	0.01	-0.08	0.19	0.17	0.10
Jul	-0.13	0.08	0.05	0.41	0.06	-0.13	-0.15	-0.08	-0.05	-0.03
Aug	-0.23	-0.04	0.02	-0.09	-0.14	-0.28	-0.25	-0.31	-0.24	-0.19
Sep	-0.34	-0.14	0.00	-0.31	-0.22	-0.32	-0.26	-0.33	-0.24	-0.20
Oct	-0.48	-0.22	-0.10	-0.42	-0.24	-0.34	-0.26	-0.31	-0.25	-0.20
Nov	-0.45	-0.21	-0.10	-0.33	-0.20	-0.32	-0.26	-0.29	-0.24	-0.19
Dec	-0.21	-0.06	0.01	-0.08	-0.17	-0.24	-0.23	-0.24	-0.13	-0.15
Jan	-0.20	0.02	0.10	-0.10	-0.09	-0.12	-0.14	-0.10	-0.04	-0.06
Feb	-0.18	0.10	0.17	0.00	-0.03	-0.09	-0.13	-0.09	-0.01	-0.03
Mar	-0.07	0.02	0.12	0.10	-0.10	-0.16	-0.20	-0.15	-0.07	-0.10

Notes:

Values in Table L-2A represent measured (Table L-1A) monthly average groundwater elevations minus monthly average river elevations. Results are presented in units of feet.

Values in Table L-2B represent measured (Table L-1A) minus modeled (Table L-1B) monthly average groundwater elevations.

Cell shading indicates the following conditions with respect to the Columbia River.

Losing stream condition (negative result from groundwater elevation minus river elevation)
Gaining stream condition (positive result from groundwater elevation minus river elevation)

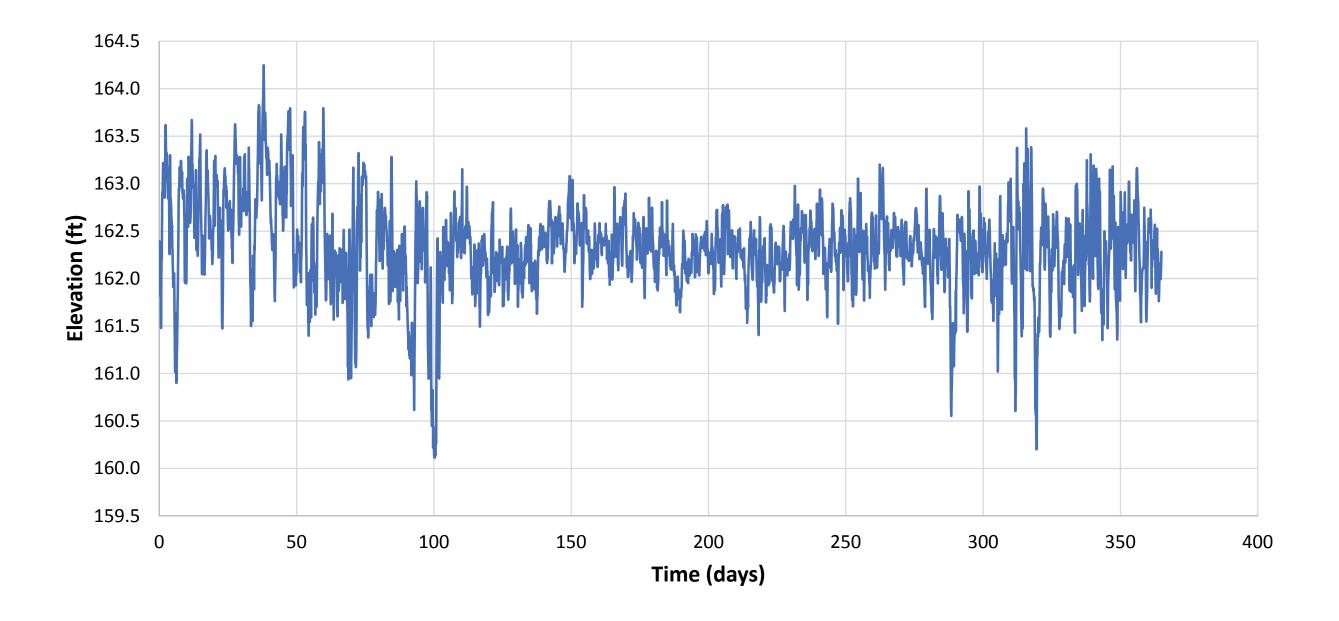


Figure 1: Average River Elevation (ft above MSL), April 2017 – March 2018

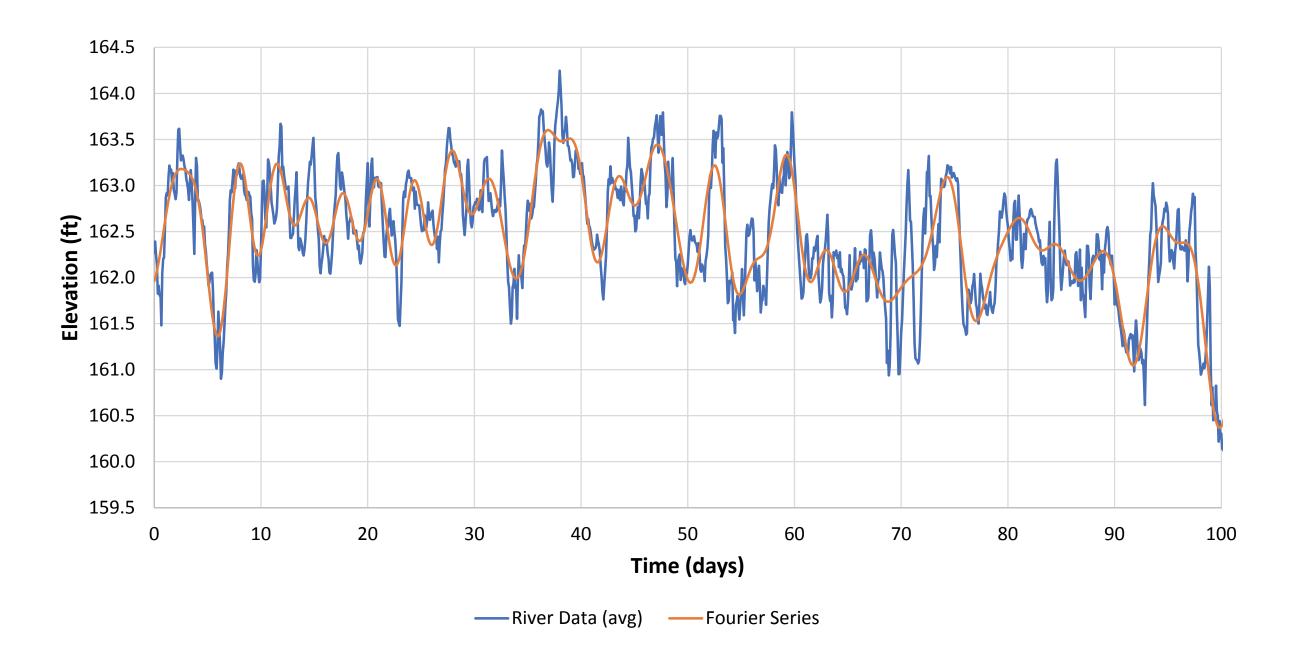


Figure 2: Average River Elevation (ft above MSL) and Fourier Series Approximation for First 100 days

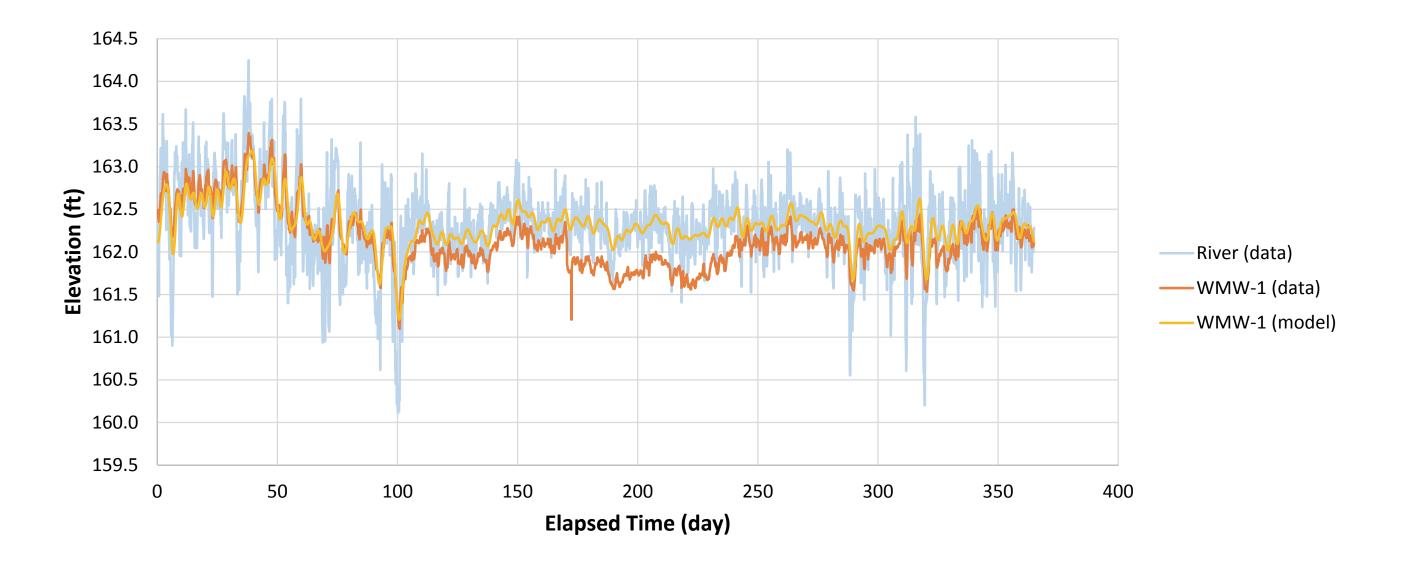


Figure 3: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-1 with Average River Elevation

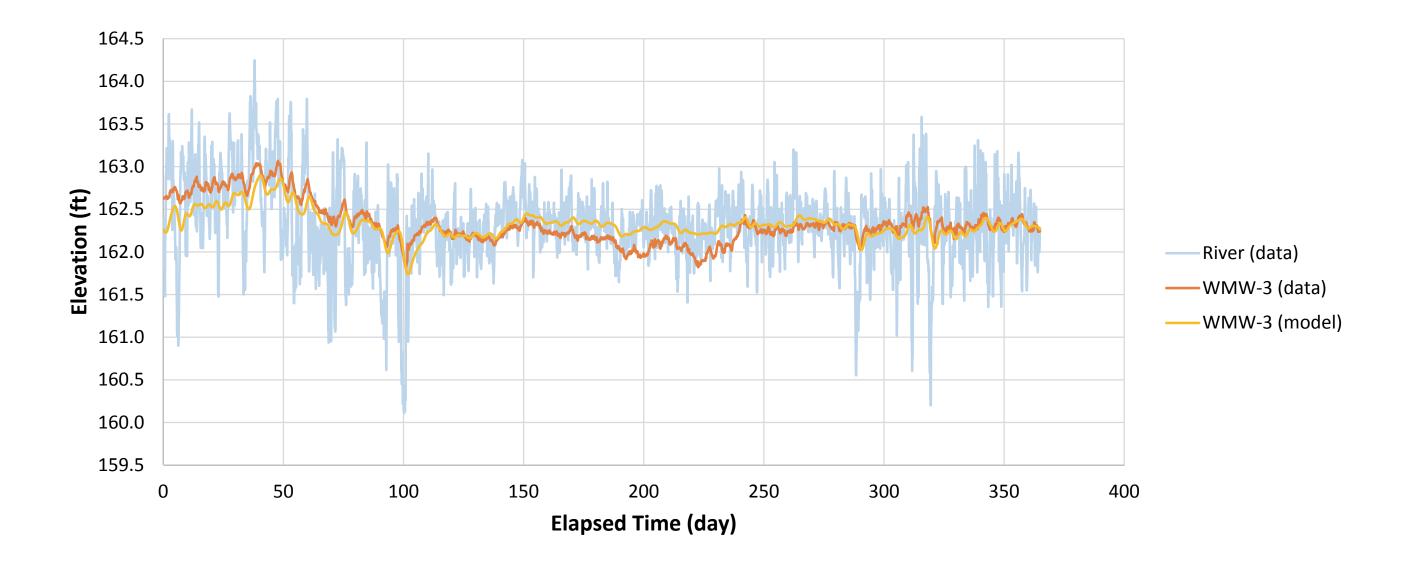


Figure 4: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-3 with Average River Elevation

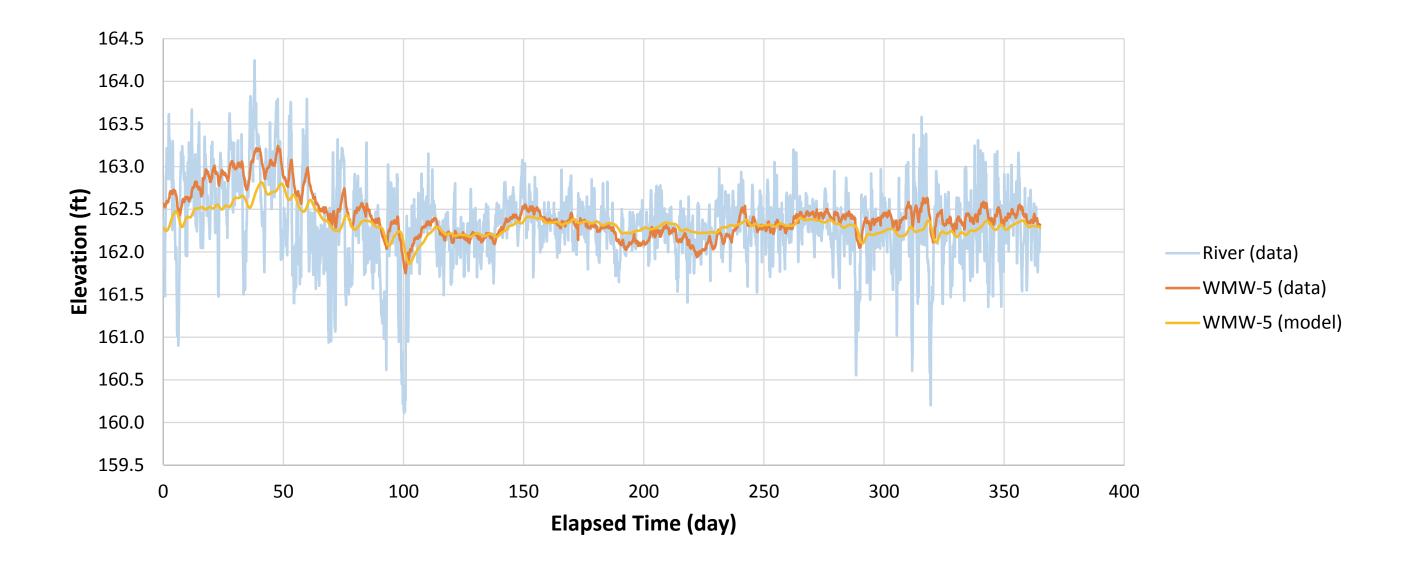


Figure 5: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-5 with Average River Elevation

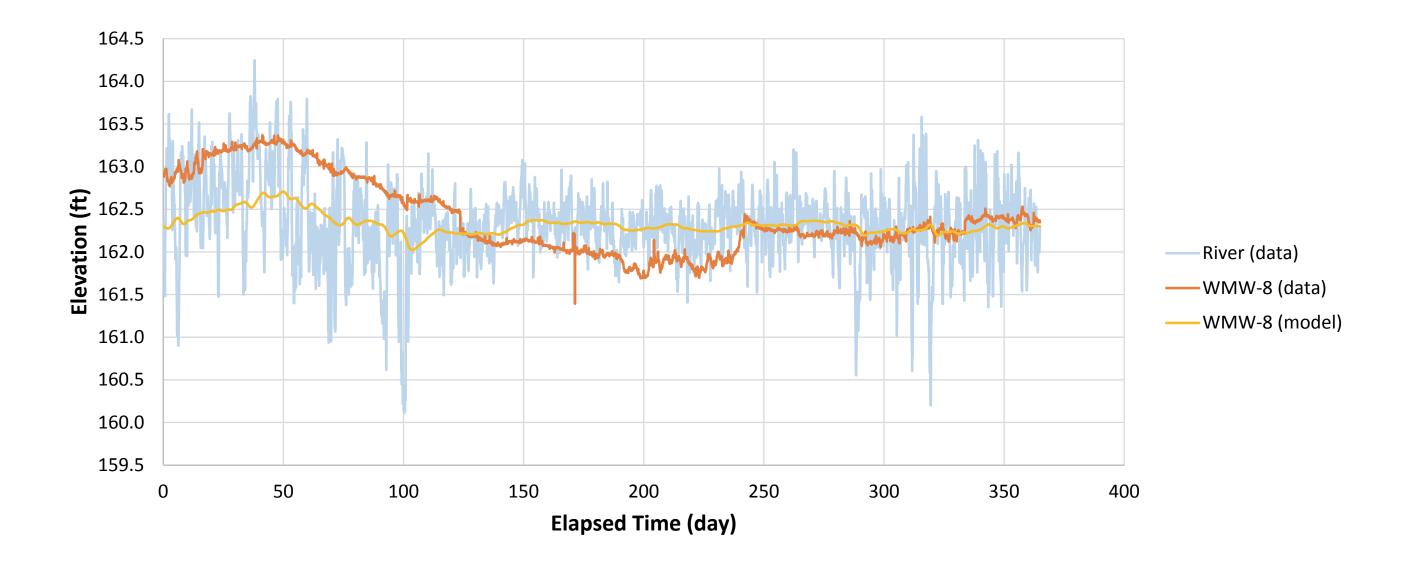


Figure 6: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-8 with Average River Elevation

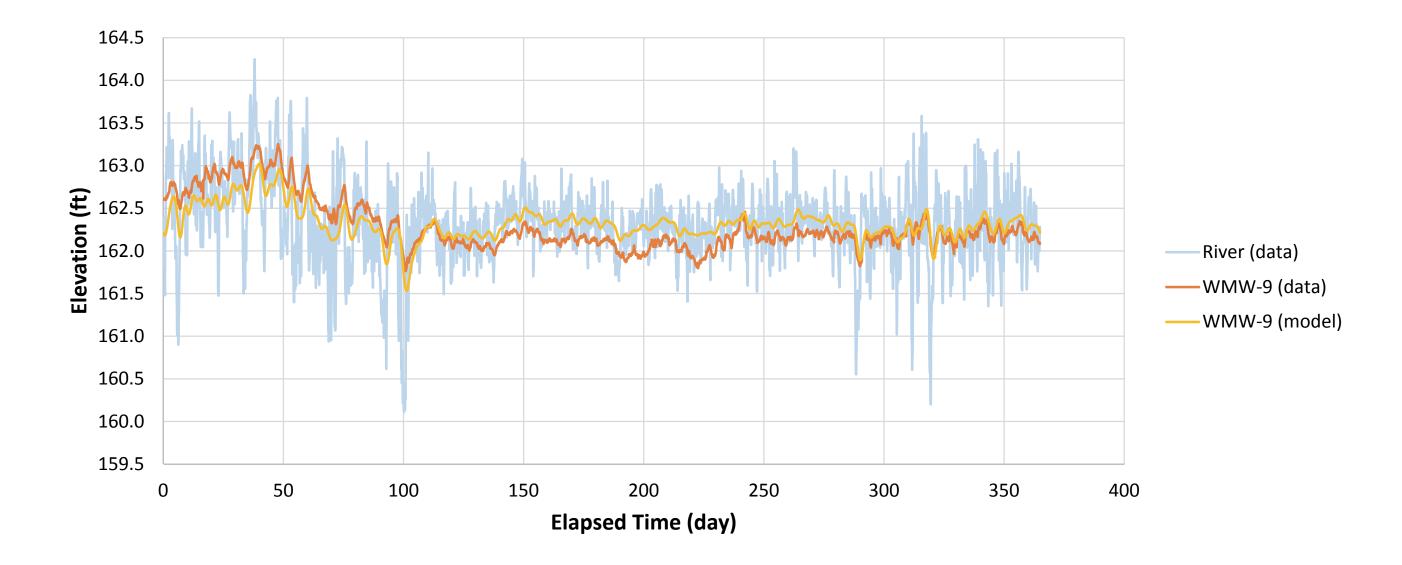


Figure 7: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-9 with Average River Elevation

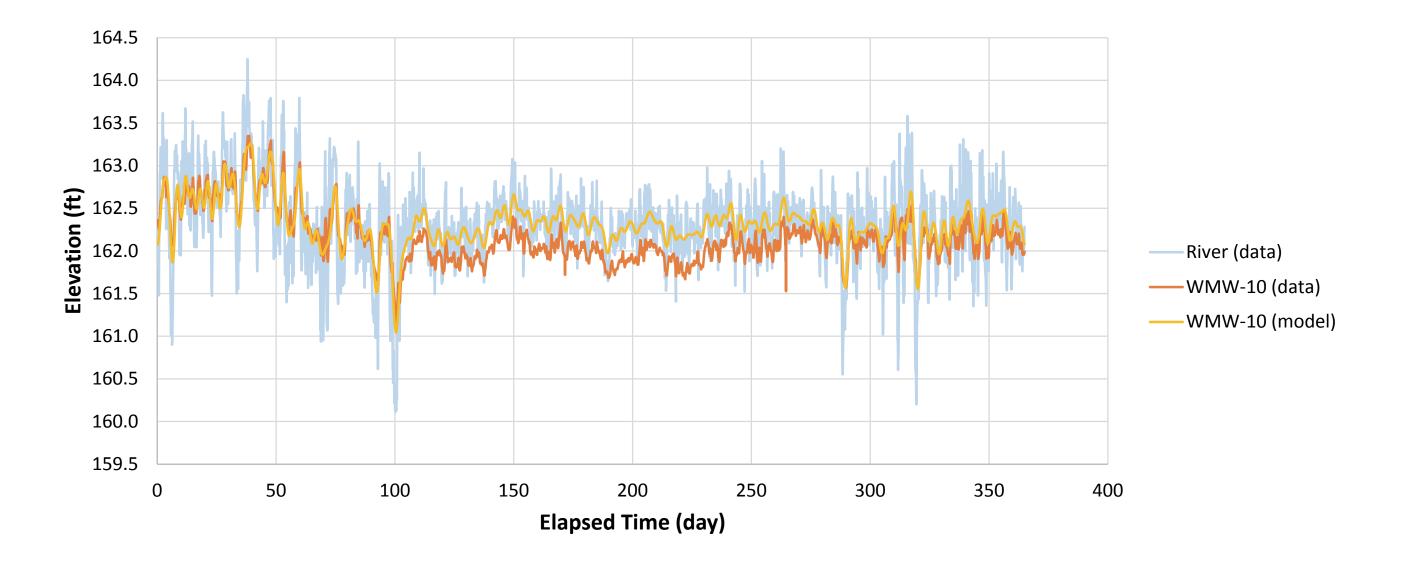


Figure 8: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-10 with Average River Elevation

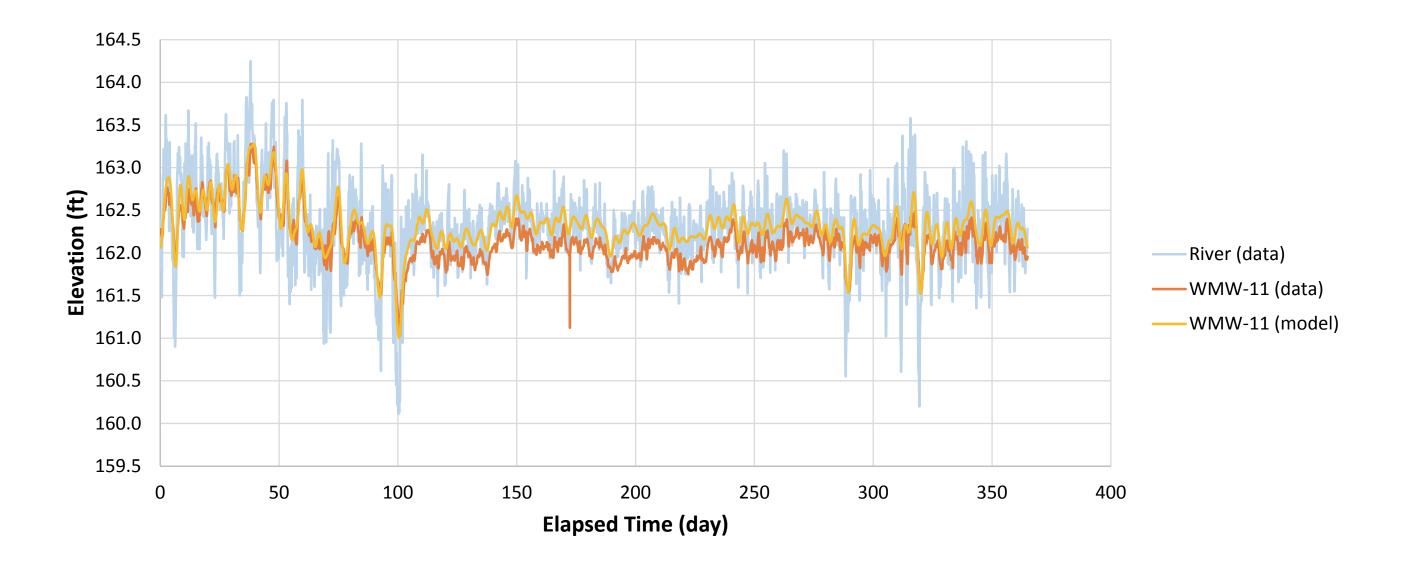


Figure 9: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-11 with Average River Elevation

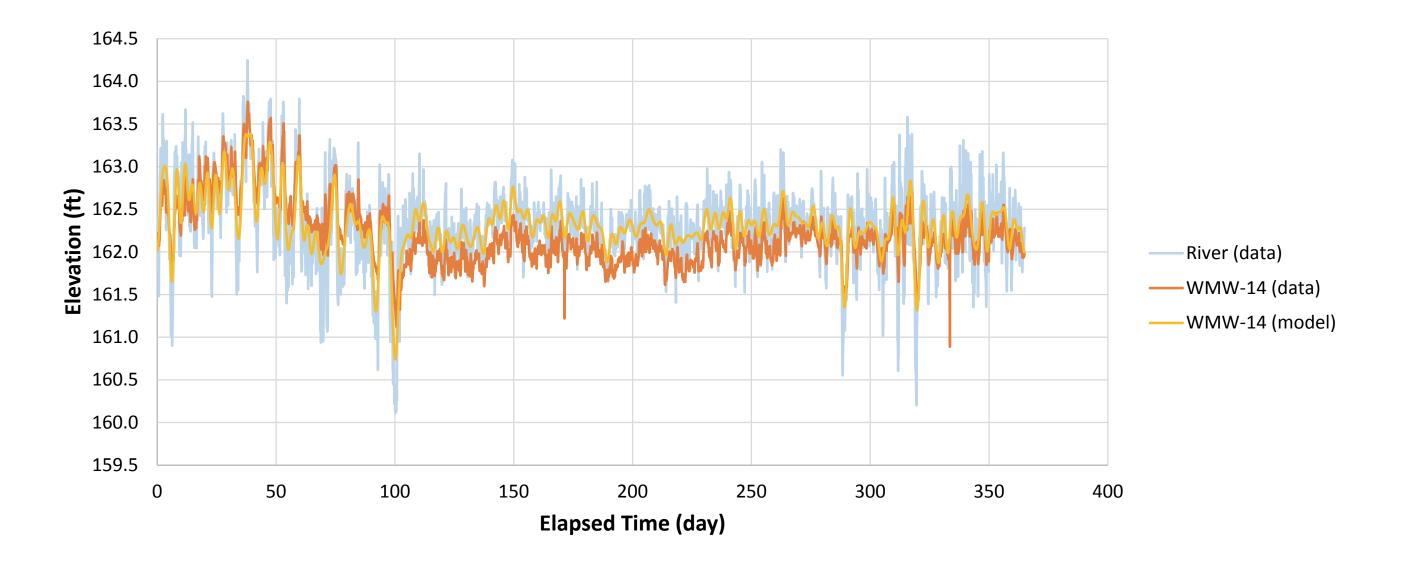


Figure 10: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-14 with Average River Elevation

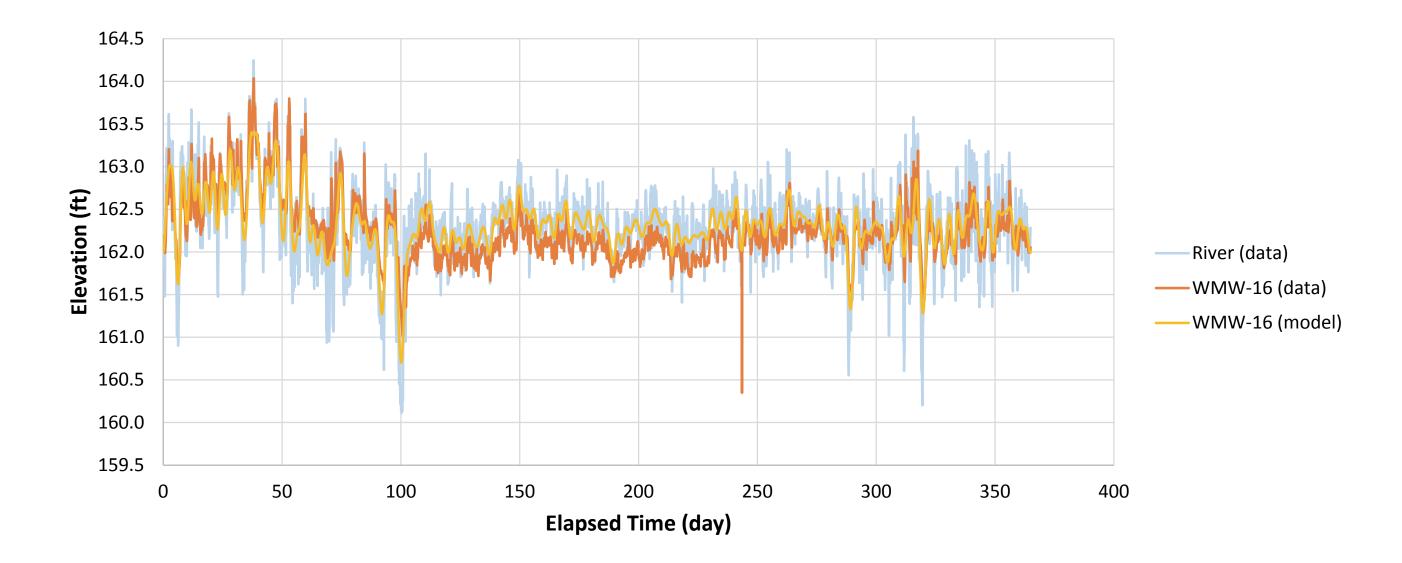


Figure 11: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-1 with Average River Elevation

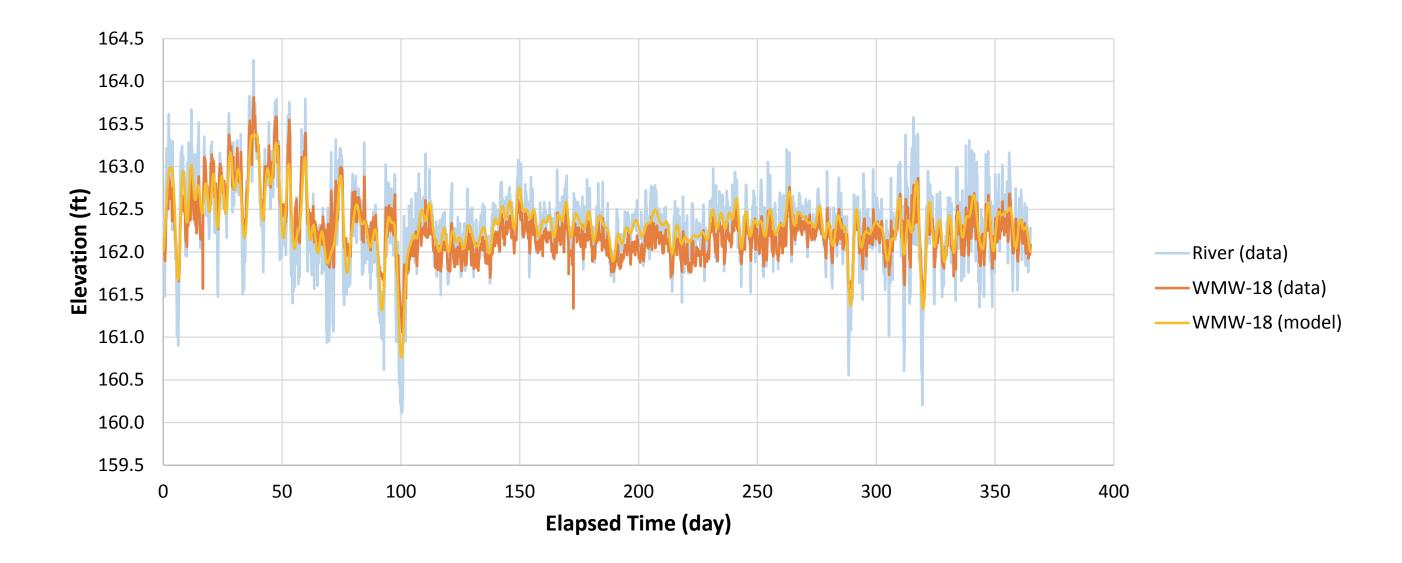
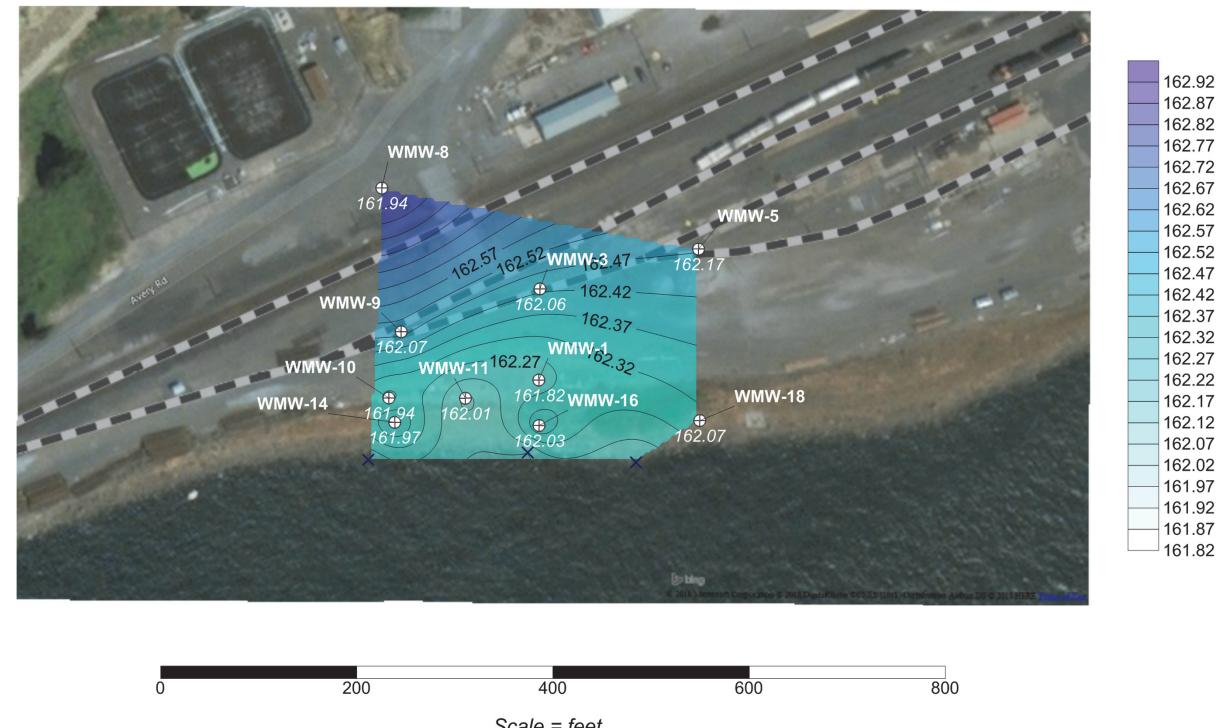
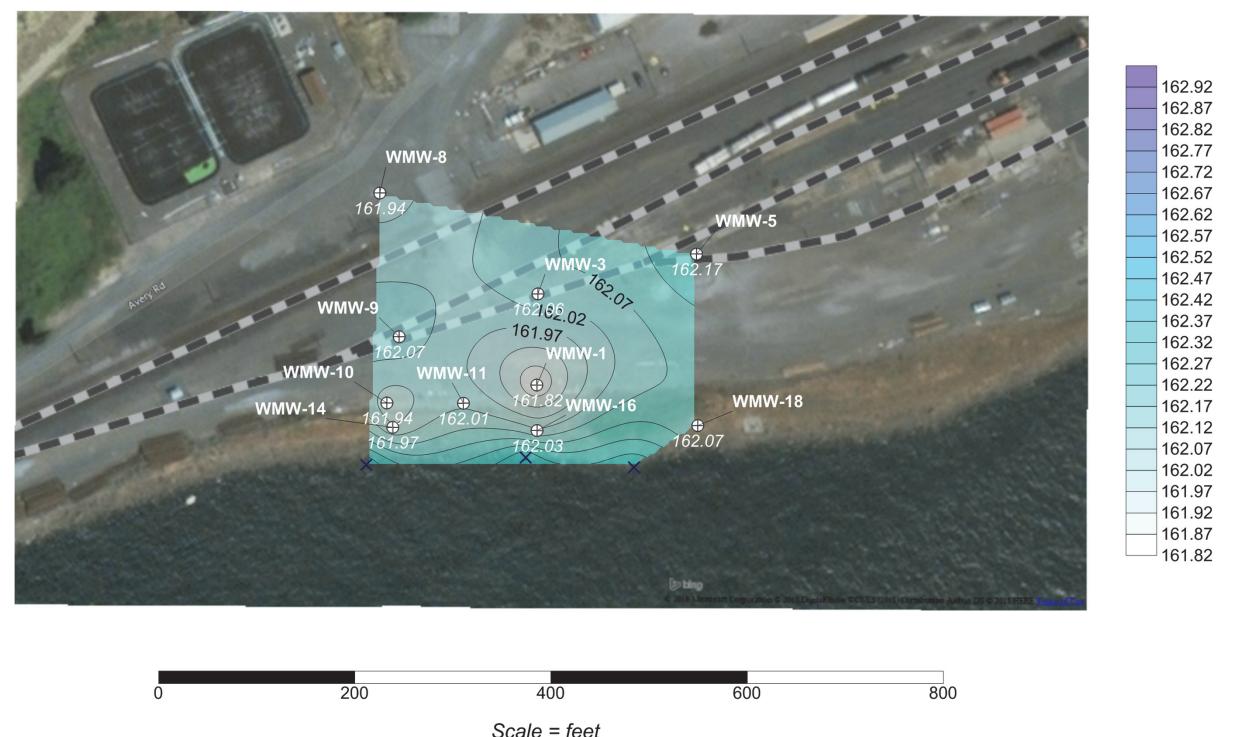


Figure 12: Comparison of Observed and Modeled Groundwater Elevation (ft above MSL) at WMW-18 with Average River Elevation



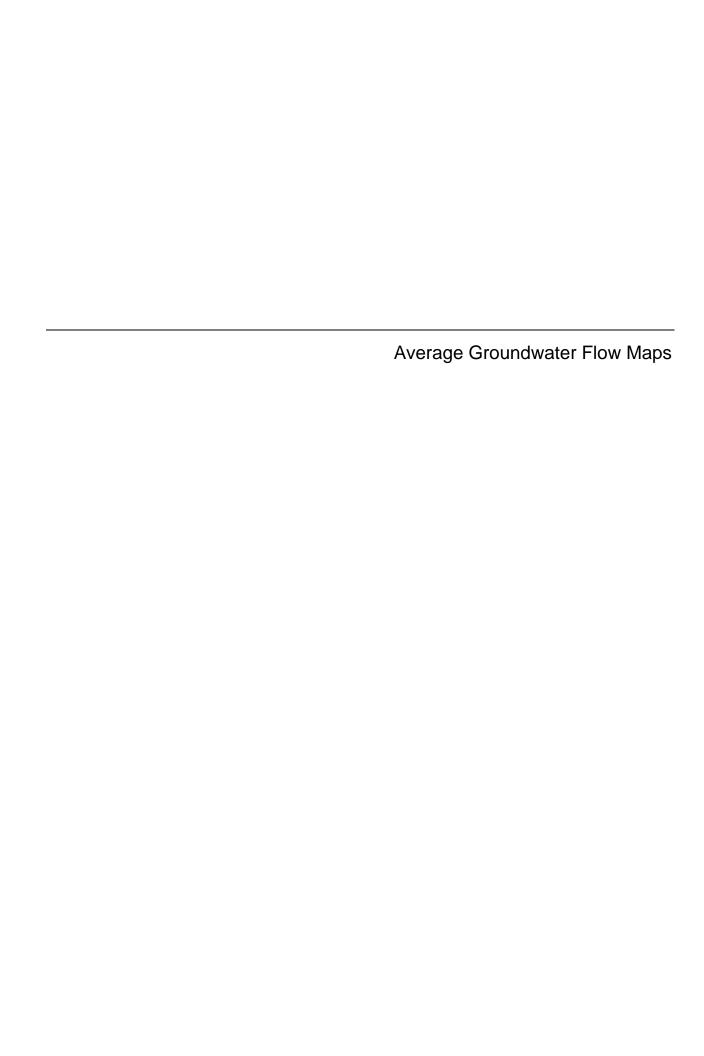
Scale = feet
Figure 13: Interpolated Averaged Groundwater Elevations (ft above MSL) in June 2017:
Apparent Gaining Stream Condition



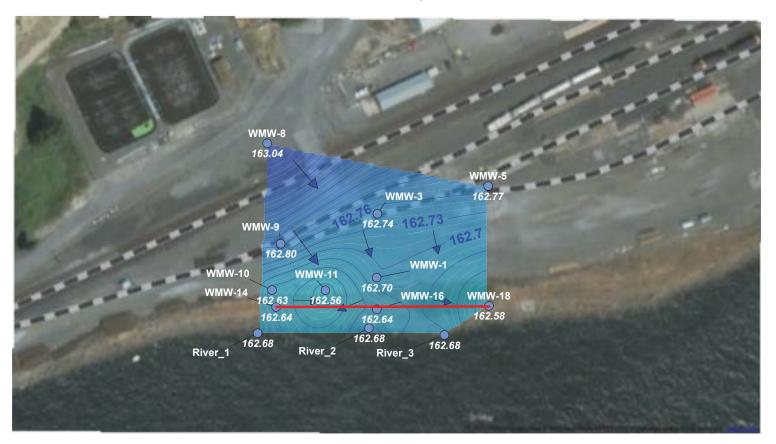
Scale = feet
Figure 14: Interpolated Averaged Groundwater Elevations (ft above MSL) in November 2017:
Apparent Losing Stream Condition

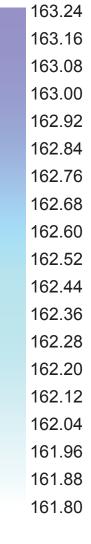
Appendix M

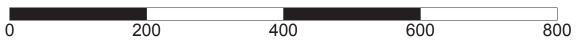
Groundwater Maps



April 2017

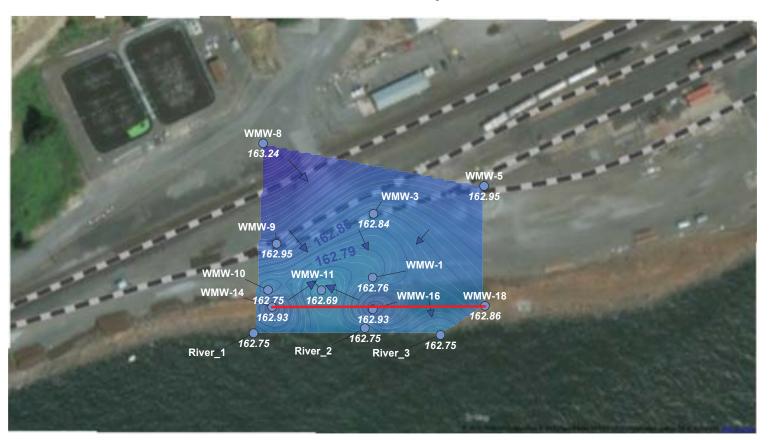


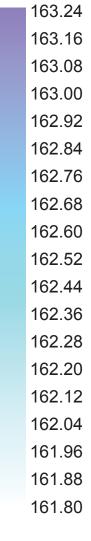


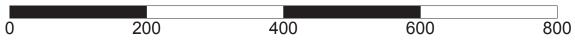


Scale = feet

May 2017



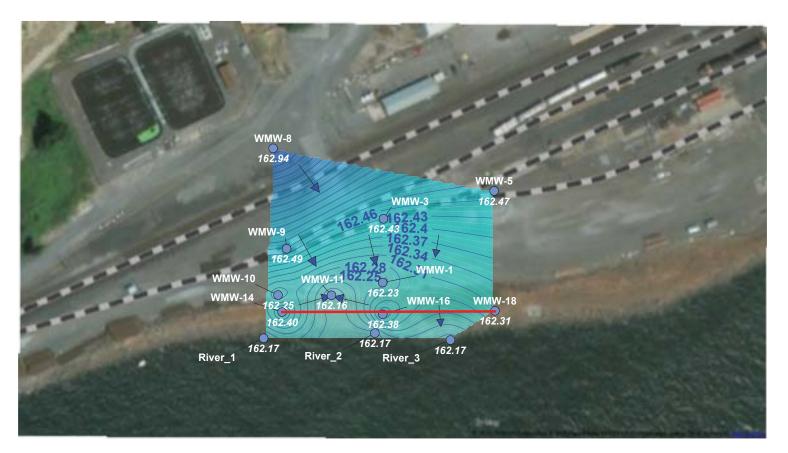


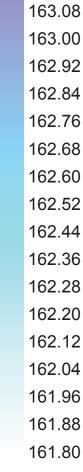


Monthly Average Groundwater Scale = feet

Elevation Maps

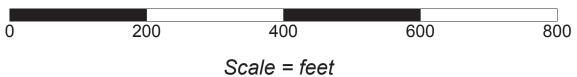
June 2017



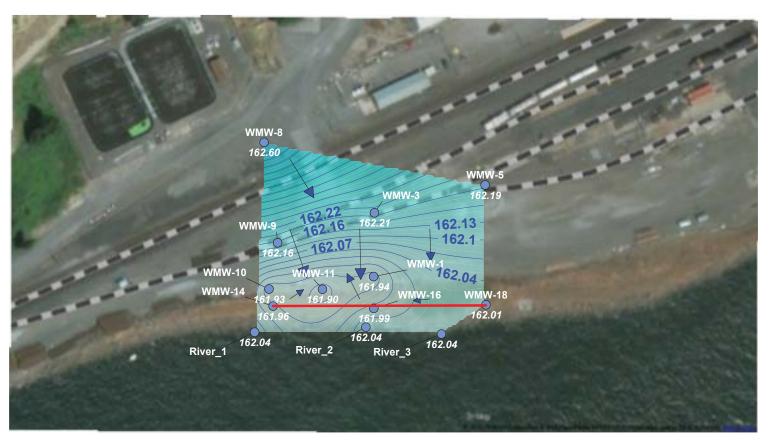


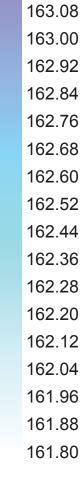
163.24

163.16



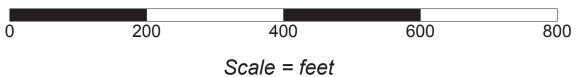
July 2017



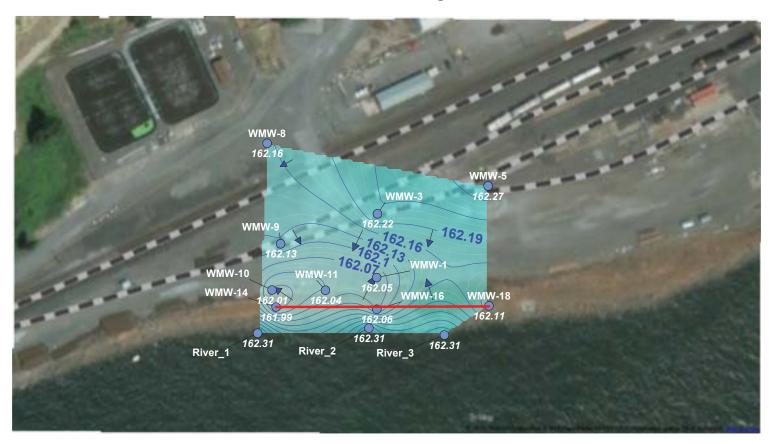


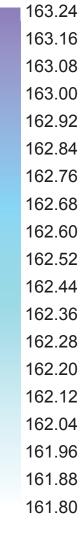
163.24

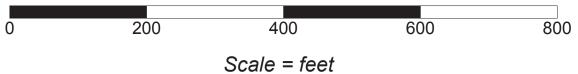
163.16



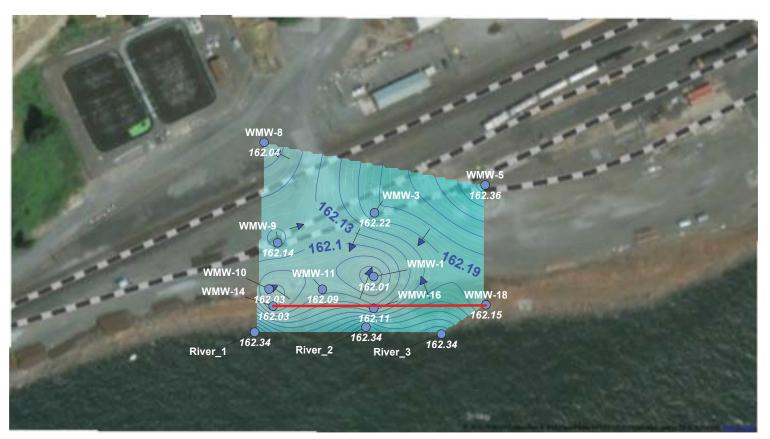
August 2017

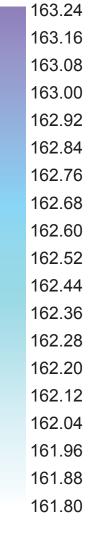


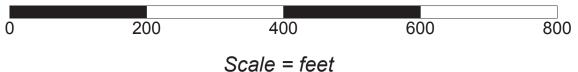




September 2017

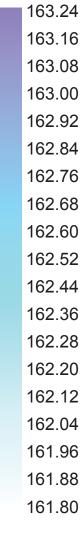


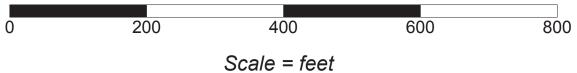




October 2017

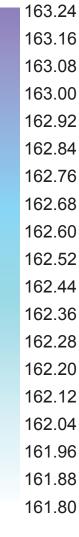


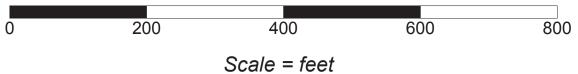




November 2017

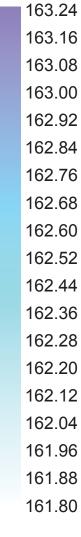


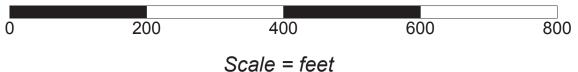




December 2017

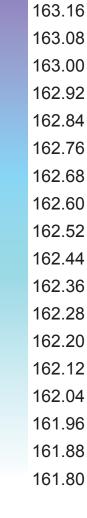




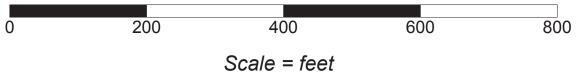


January 2018



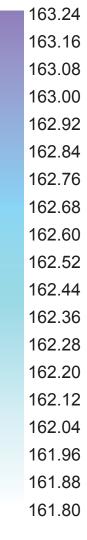


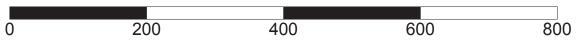
163.24



February 2018

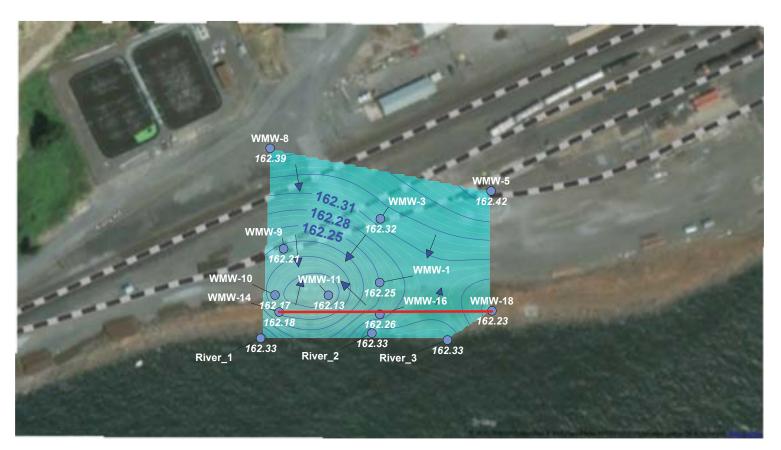


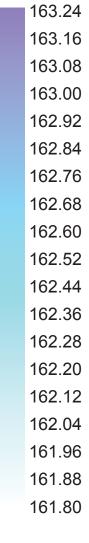


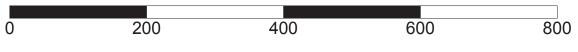


Scale = feet

March 2018

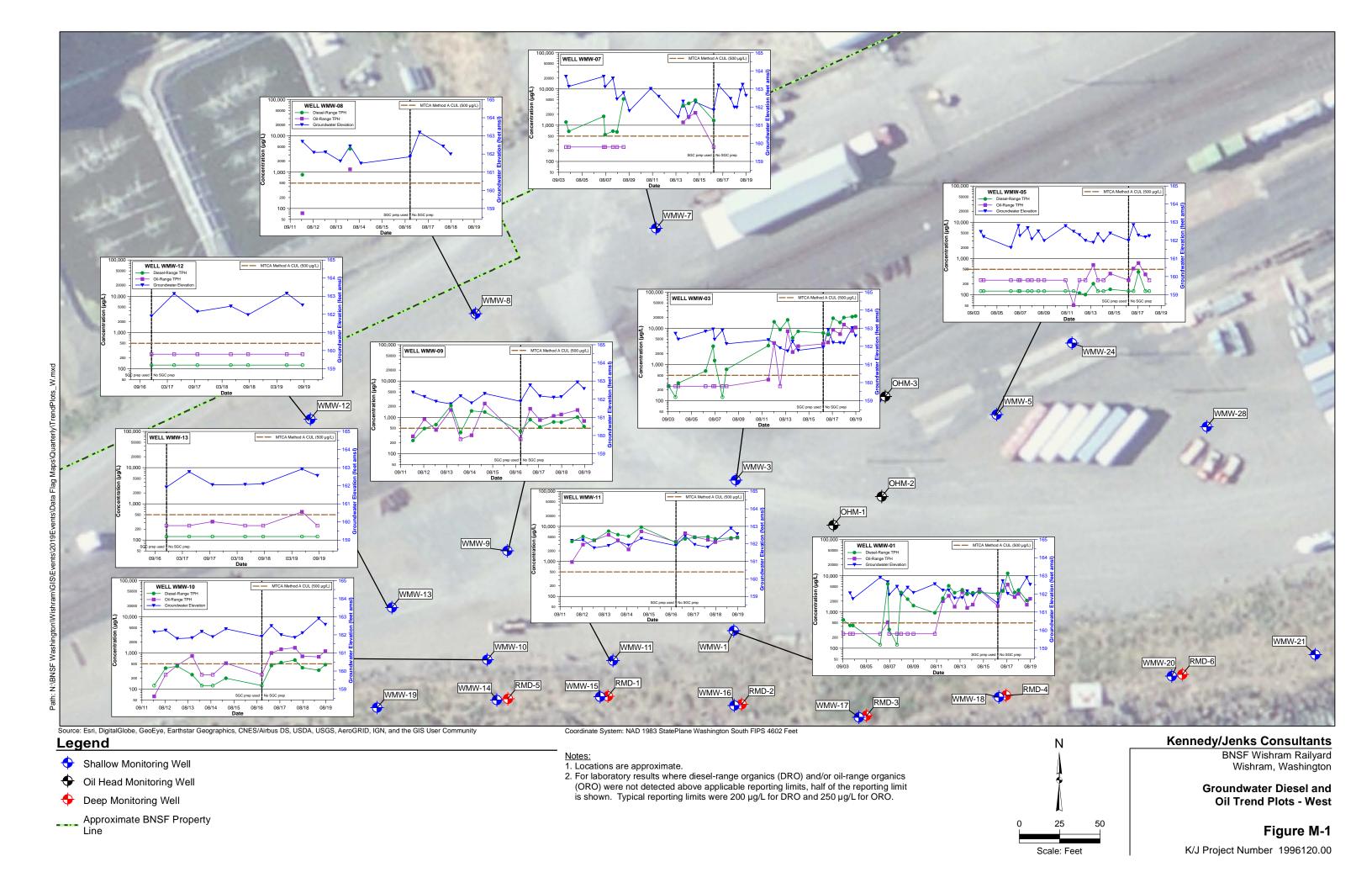


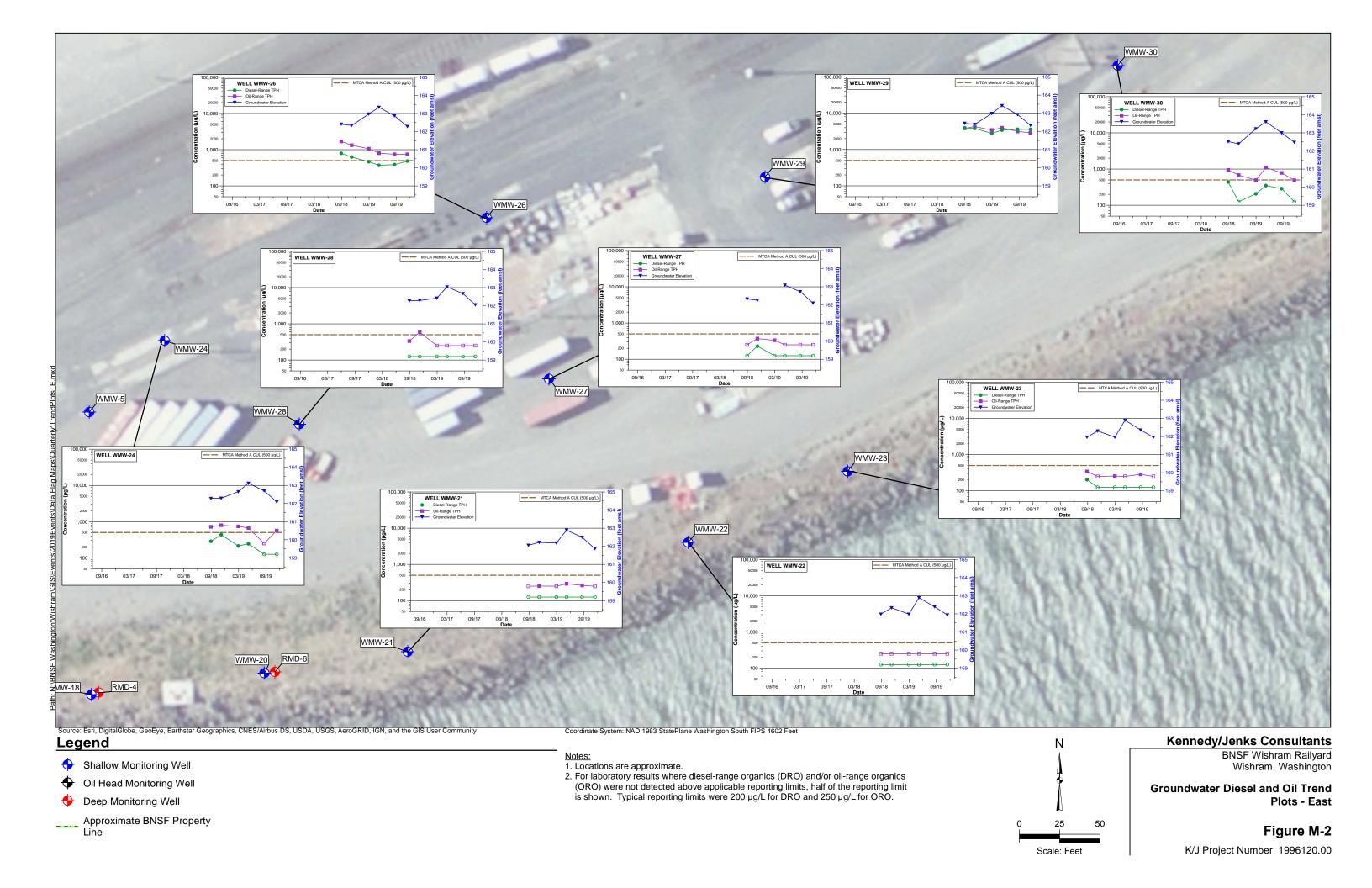




Scale = feet







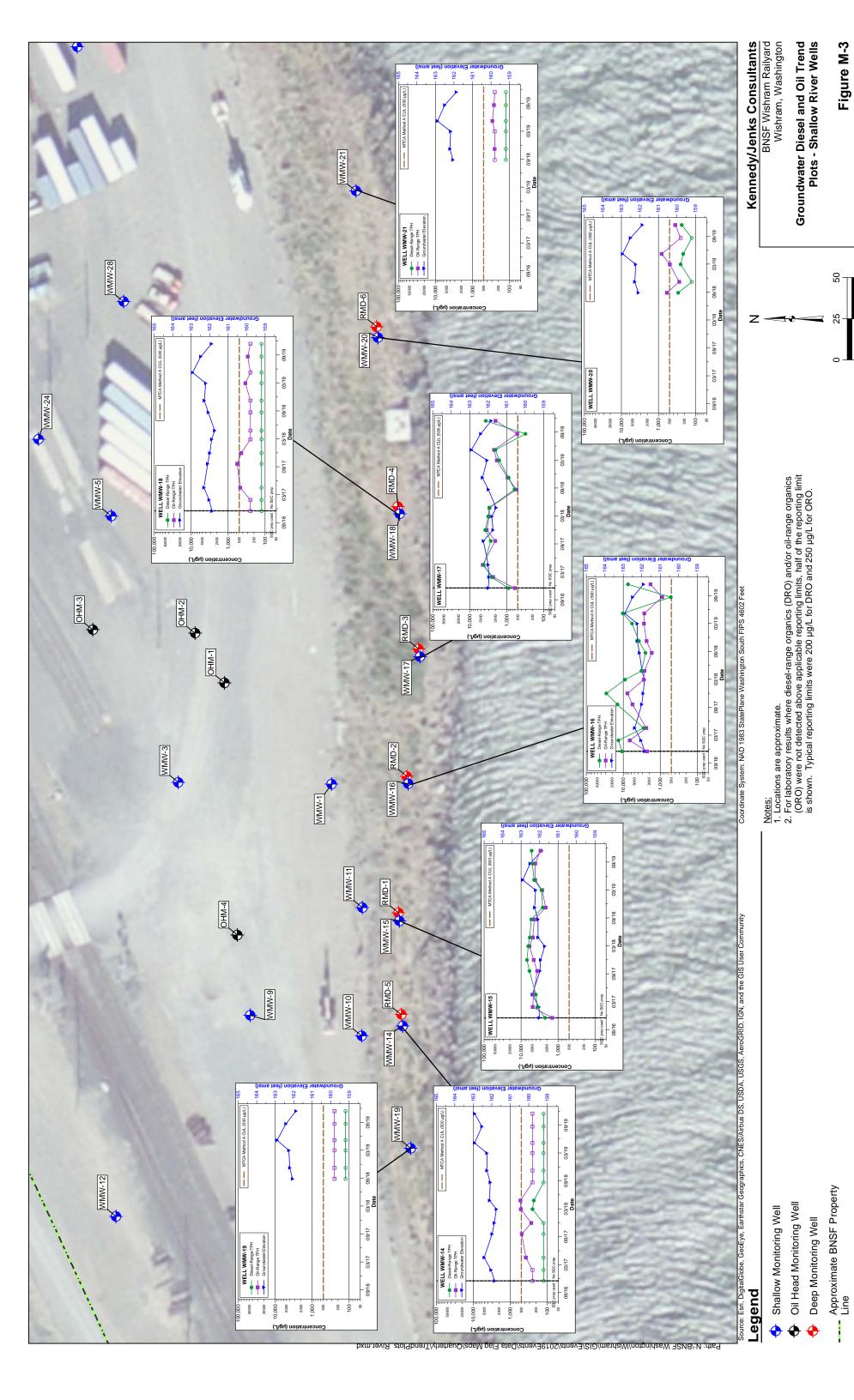


Figure M-3

K/J Project Number 1996120.00

Scale: Feet

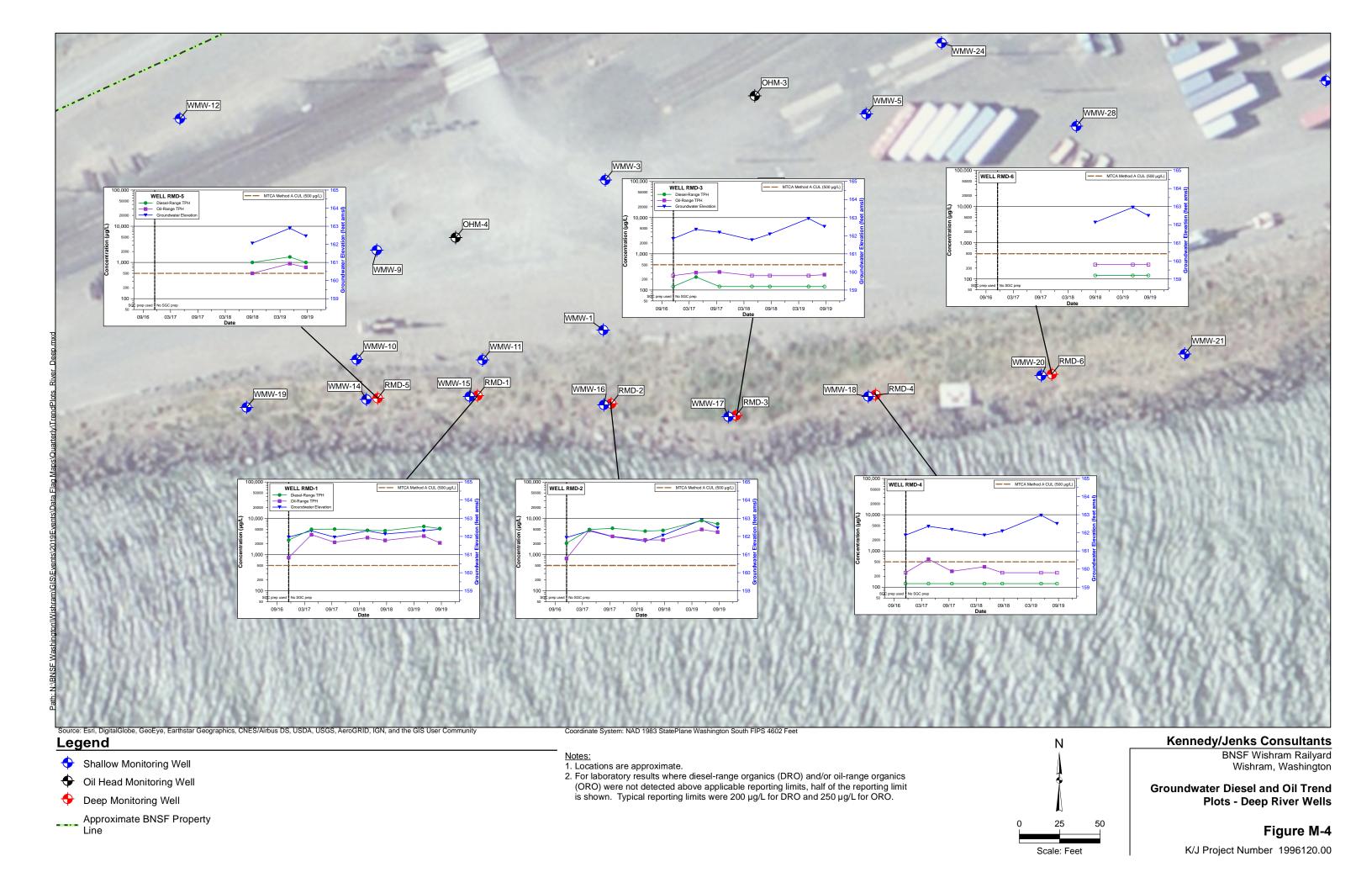
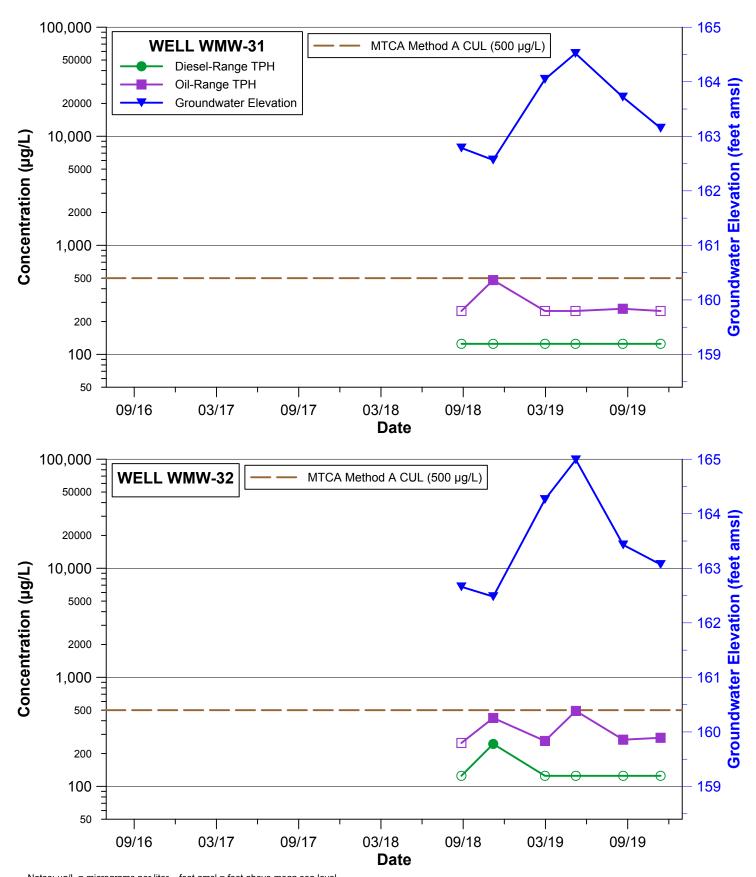


FIGURE M-5
DIESEL- AND OIL-RANGE ORGANICS IN GROUNDWATER TREND CHARTS
BNSF Wishram Railyard, Wishram, Washington



Notes: $\mu g/L = micrograms$ per liter. feet amsl = feet above mean sea level. Filled symbols indicate detected concentrations. Open symbols indicate not detected (ND) results, shown as 125 $\mu g/L$ for diesel- and 250 $\mu g/L$ for oil-range organics, which are half the maximum historical reporting limits. Groundwater samples were analyzed by NWTPH-Dx without silica gel cleanup preparation (SGC prep).

Appendix N

Former Water Wells Assessment

Monthly Progress Report BNSF Track Switching Facility (Agreed Order DE12897) Wishram, Washington

Ecology Manager:

BNSF Manager:

Prepared by Kennedy/Jenks Consultants:

Reporting Period:

Date Submitted:

John Mefford

Shane DeGross

Ryan Hultgren

1 through 30 September 2018

15 October 2018

BNSF Railway Company (BNSF) is conducting a remedial investigation (RI) and feasibility study (FS) for the BNSF Track Switching Facility in Wishram, Washington (aka Wishram Railyard, FSID 1625461). The work is being conducted with Ecology oversight under Agreed Order No. DE 12897 (AO). This progress report is being submitted pursuant to Paragraph VII.H of the AO.

Progress Made During This Reporting Period

- On 14 September 2018, BNSF submitted the August 2018 Monthly Progress Report to Ecology.
- On 19 September 2018, BNSF (and its consultants Kennedy/Jenks Consultants and Jacobs)
 met with Ecology and the representatives of the Yakama Nation to discuss the Conceptual
 Site Model (CSM) and status of ongoing activities conducted under the RI Work Plan
 Addendum and Nearshore Sediment Initial Investigation Work Plan.
 - On 21 September 2018, Ecology transmitted to BNSF via email a copy of meeting minutes prepared by Ecology for the 19 September meeting. BNSF provided comments back to Ecology via email on 24 September 2018.
 - On 28 September 2018, BNSF submitted to Ecology via email electronic versions of the slide presentation files from the 19 September 2018 meeting.
- On 19 and 20 September 2018, Kennedy/Jenks Consultants performed bank inspection monitoring. Observations are summarized under the Bank Inspection Results section.
- On 20 September 2018, attempts were made to locate former water supply Well #1 which was reportedly abandoned on 20 December 1928, according to historical railroad documents.
 - An area of approximately 30 feet long (west to east) by 20 feet wide (north to south) by depths ranging from 2 to 3 feet below ground surface (bgs) was excavated with a track-mounted excavator in the vicinity of a former pump house and approximate location of the former well. The excavated area included soil, blackberry bushes and grasses, assorted concrete debris (broken up pieces of concrete footings, slabs, etc.), and metallic debris. A mounded area with concrete and large bolts was also broken up and cleared. No evidence of Well #1 was observed in the excavated area. The excavation was backfilled with excavated materials and the surface compacted with the excavator bucket. See attached photographs.
 - An area of approximately 10 feet long (north to south) by 6 feet wide (west to east) near a suspected former utility pole, based on a historical aerial photograph from 1951, was also excavated to a depth of approximately 4 feet bgs. This area was approximately 30 feet west of the suspected Well #1 location. A concrete footing for a 3-foot diameter metal pipe structure was exposed, however, no evidence of Well #1 was observed. See attached photographs.
 - BNSF, Kennedy/Jenks, and Jacobs observed excavation activities; excavated soil was monitored by Jacobs for cultural artifacts.

Monthly Progress Report BNSF Track Switching Facility (Agreed Order DE12897) Wishram, Washington

Deviations from the Work Plan

 Section 3.2.1 of the RI Work Plan Addendum indicated that deep monitoring wells RMD-5 and RMD-6 would be installed using 0.040-inch slotted casing. The slot size was a typographical error; the wells were installed with 0.020-inch slotted casing, consistent with existing deep monitoring wells RMD-1 through RMD-4.

Bank Inspection Results

 No oil sheen or droplets were observed on the water surface of the Columbia River during bank inspections conducted on 19 and 20 September 2018. Photographs were taken, and a written log was prepared.

Key Activities/Schedule for Next Reporting Period

- Conduct monthly bank monitoring.
- Continue upland RI addendum activities including assessment of former water supply wells, validation of field and laboratory results, evaluation of the field and laboratory results with respect to the RI objectives (defining the nature and extent of site-related impacts in the uplands area) and begin preparation of the Draft RI Report.
- Continue inundated lands initial investigation activities including data validation of laboratory results and evaluation of the field and laboratory data with respect to the initial investigation objectives and begin preparation of the Draft Inundated Lands Initial Investigation Report.
- Begin preparation of the cultural resources monitoring report for the RIWP Addendum and initial investigation activities.
- BNSF will continue to assist with coordinating schedules between Ecology, BNSF and the Yakama Nation for a meeting to discuss the uplands RI data in advance of preparing the Draft RI Report. An agenda will be provided by BNSF in advance of the meeting.
- Submit data collected during RIWP Addendum and inundated lands initial investigation field
 activities to Ecology's EIM system. Following data validation and verification, survey data and
 well construction information (as applicable) and laboratory analytical results from soil,
 reconnaissance groundwater, monitoring well groundwater, and sediment samples will be
 uploaded to EIM. Laboratory analytical reports will also be submitted to Ecology.

Potential Problems Identified and Suggested Resolutions

• No potential problems were encountered during this reporting period.

Deliverables Submitted This Reporting Period

None.

EIM Results Submitted This Reporting Period

None.

Kennedy/Jenks Consultants

Monthly Progress Report BNSF Track Switching Facility (Agreed Order DE12897) Wishram, Washington









Kennedy/Jenks Consultants

Monthly Progress Report BNSF Track Switching Facility (Agreed Order DE12897) Wishram, Washington









Appendix O

Desktop Review of Potable Water Sources



The Dep The Department of Ecology does NOT Warranty the Data and/or the Information on this Well Report.

nit:	8664 STATE OF WASHINGTON DEPARTMENT OF CONSERV DIVISION OF WATER RESOUR	ATION	
VELL			.
lecord	by Driller		
Source	Driller's Record		
Locatio	n: State of WASHINGTON		
Con	mtyKlickitat		
Are	ea		
Ma	p		
S.W.	14 SW 14 sec 7 T. 2 N. R 15 E.E. W	Diagram of	Section
Drilling	Co Riebe Well Drilling		
Ad	dress 1503 E. Nob Hill Blvd. Ya	kima, W	ash.,
Me	thod of Drilling rotary Date		, 19
	Coffield & Sons		
Ad	dress Box 58, Wishram, Washingtourface, datum 550 ft above	on 986	73
Corrs-	101 Date March 8 , 1968	From	То
CORRE- LATION	Material	From (feet)	To (feet)
CORRE- LATION	l	From (feet)	To (feet)
CORRE- LATION	Material	From (feet)	To (feet)
CORRE- LATION	Material Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if repod-surface datum unless otherwise indicated. Correlate se. Following log of materials, list all casings, perforation	From (feet) necessary, in orticl, Give d with stratigras, S. reens, etc.	To (feet)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but a trapbrase as the water-bearing, so state and record static level if repud-surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation IRRIGATION & MUNICIPAL	From (feet) necessary, in orted. Give dwith stratigras, streams, etc.	To (feet)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports and surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation. IRRIGATION & MINICIPAL No well log available from 0 to	From (feet) necessary, in orted. Give dwith stratigras, streams, etc.	To (feet) parenthese lepths in feaching columns.)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports are datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation. IRRIGATION & MUNICIPAL. No well log available from 0' to Basalt, broken heavily creviced.	From (feet) necessary, in orted. Give dwith stratigras, streams, etc.	To (feet) parenthese lepths in feaching columns.)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if repaid-surface datum unless otherwise indicated. Correlate see Following log of materials, list all casings, perforation IRRIGATION & MINICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the	From (feet) necessary, in orted. Give dwith stratigras, streams, etc.	To (feet) parenthese lepths in feaching columns.)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if repaid-surface datum unless otherwise indicated. Correlate see Following log of materials, list all casings, perforation IRRIGATION & MINICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the	From (feet) necessary, in orted. Give dwith stratigras, streams, etc.	To (feet) parenthese lepths in feaching columns.)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports of the surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation. IRRIGATION & MINICIPAL. No well log available from 0' to basalt, broken heavily creviced black and gary, water in the broken basalt.	From (feet) necessare, in ortel. Give dwith stratigras, screens, etc. o. 98!	To (feet) parenthese lepths in feaching columns.)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports and surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation IRRIGATION & MINICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the broken basalt Casing: +1' to 240' Seal: original 8" casing in planump: Myers, Ses 1500 8 Stage	From (feet) necessary, in orted, Give dwith stratigrals, streens, etc. o 98! 98	narenthese epths in feather columns)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports a surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation IRRIGATION & MUNICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the broken basalt Casing: +1' to 240' Seal: original 8" casing in place pump: Myers, Ses 1500 8 Stage Bailer test: 150 gpm with 164'	From (feet) necessary, in orted, Give dwith stratigrals, streens, etc. o 98! 98	narenthese epths in feather columns)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports and surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation IRRIGATION & MINICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the broken basalt Casing: +1' to 240' Seal: original 8" casing in planump: Myers, Ses 1500 8 Stage	From (feet) necessary, in orted, Give dwith stratigrals, streens, etc. o 98! 98	narenthese epths in feather columns)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports a surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation IRRIGATION & MUNICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the broken basalt Casing: +1' to 240' Seal: original 8" casing in place pump: Myers, Ses 1500 8 Stage Bailer test: 150 gpm with 164'	From (feet) necessary, in orted, Give dwith stratigrals, streens, etc. o 98! 98	narenthese epths in feather columns)
CORRE- LATION	MATERIAL Inscribe driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports a surface datum unless otherwise indicated. Correlate see. Following log of materials, list all casings, perforation IRRIGATION & MUNICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the broken basalt Casing: +1' to 240' Seal: original 8" casing in place pump: Myers, Ses 1500 8 Stage Bailer test: 150 gpm with 164'	From (feet) necessary, in orted, Give dwith stratigrals, streens, etc. o 98! 98	narenthese epths in feather columns)
CORRE- LATION	material driller's terminology literally but paraphrase as ial water-bearing, so state and record static level if reports of surface datum unless otherwise indicated. Correlate see Following log of materials, list all casings, perforation. IRRIGATION & MINICIPAL No well log available from 0' to Basalt, broken heavily creviced black and gary, water in the broken basalt. Casing: +1' to 240' Seal: original 8" casing in planum: Myers, Ses 1500 8 Stage Bailer test: 150 gpm with 164' Temp. 54°	From (feet) necessary, in orted, Give dwith stratigrals, streens, etc. o 98! 98	narenthese epths in feather columns)







Location marked on air photo (please attach)

Well Tagging Form

Unique Well Tag No: AFC-873 RECORD VERIFICATION (check / one) Well Report available (please attach this form to the well report and submit it to the Ecology Regional Office near Verification inconclusive Wishram Water Sys Well Report not available Wellownership ie different from Wellereport To Dirst Name: Last Name: treet Address: State: LOCATION OF WELL IE DIFFERENT FROM WELL REPORTS Z ell Address: FOR AGENCY USE ONLY **GPS** Topographic Map. ngitude Survey Computer generated evation at land surface _feet/meters (circle one) Digital Altimeter Topographic Map Additional information, if available: Other Location marked on topographic map (please attach)

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				ST	ATE OF	W	\SH	INGTO)N				

Start Card No. W25804 Water Right Permit No. M/A

(1) OWHER: Name P.U.D. / WISHRAM 919 Address	WISHRAM, WA 98673-
(2) LOCATION OF WELL: County ELICKITAT (2a) STREET ADDRESS OF WELL (or nearest address) SAME	- SE 1/4 HE 1/4 Sec 18 T 2N N., R 15E WH
(2) DRADACER CCE. MINICIPAL	(10) WELL LOG
(4) TYPE OF WORK: Owner's Number of well (If more than one) NEW WELL Method: HOTARY (5) DIMENSIONS: Diameter of well 8 inches Drilled 550 ft. Depth of completed well 550 ft.	Formation: Describe by color, character, size of materia and structure, and show thickness of aquifers and the kanna nature of the material in each stratum penetrated, the material in each stratum penetrated in the material in the material in each stratum penetrated in the material i
(5) DIMENSIONS: Diameter of well 8 inches Drilled 550 ft. Depth of completed well 550 ft.	at least one entry for each change in formation.
(6) CONSTRUCTION DETAILS: Casing installed: 8 Dia. from -1 ft. to 29 ft. WELDED Dia. from ft. to ft. Dia. from ft. to ft.	SAND BROWN BASALT , FRACTURED BROWN & GRAY BASALT , MEDIUM GRAY BASALT , MEDIUM #ARD GRAY BASALT , HERD GRAY BASALT , HARD TO BLACK BASALT , POROUS , WATER BEARING CRAY BASALT , POROUS , WATER BEARING CRAY BASALT , POROUS , WATER BEARING 210
Perforations: NO Type of perforator used SIZE of perforations in. by in. perforations from ft. to ft. perforations from ft. to ft. perforations from ft. to ft.	GRAY BASALT , POROUS , MEDIUM HARD 430 GRAY BASALT , HARD 440 GRAY BASALT GREEN SEAMS 455 HARD W/ MATER BEARING 455 GRAY BASALT , HARD 475
Screens: NO Hanufacturer's Name Type Model No. Diam. slot size from ft. to ft. Diam. slot size from ft. to ft.	GRAT BASALT GREEN SBAMS 535, WATER BEARING, HARD 535
Gravel packed: NO Size of gravel Gravel placed from ft. to ft.	
Surface seal: YES To what depth? 30 ft. Material used in seal CRMENT & BENTO. Did any strata contain unusable water? NO Type of water? Depth of strata ft. Method of sealing strata off	
(7) PUMP: Manufacturer's Mame Type H.P.	DEPARTMENT OF BUILDING OF SECTION
(8) WATER LEVELS: Land-surface elevation above mean sea level ft. Static level 147 ft. below top of well Date 10/25/93 Artesian Pressure lbs. per square inch Date Artesian water controlled by	Work started 10/19/93 Completed 10/25/93
(9) WELL TESTS: Drawdown is amount water level is lowered below static level. Was a pump test made? NO If yes, by whom? Yield: gal./min with ft. drawdown after hrs.	WELL CONSTRUCTOR CERTIFICATION: I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials use and the information reported above are true to my best knowledge and belief.
Recovery data Time Water Level Time Water Level Time Water Level	NAME M-K WELL DRILLING CO. (Person, firm, or corporation) (Type or print)
Date of test / / Bailer test gal/min. ft. drawdown after hrs. Air test 250 gal/min. w/ stem set at 540 ft. for 1 hrs. Artesian flow g.p.m. Date	ADDRESS BOX 470 DALLESPORT, WA. [SIGNED] License No. 833 & 834 & Contractor's
Temperature of water Was a chemical analysis made? NO	Registration No. MKDRIC134PR Date 10/25/93

Artesian flow

WATER WELL REPORT
Original & 1st copy - Ecology, 2st copy - owner, 3st copy - driller
ECOLOGY Construction/Decommission ("x" in circle)
Construction
Decommission ORIGINAL INSTALLATION
Notice of Intent Number
PROPOSED USE: Domestic Industrial Municipal DeWater Inrigation Test Well Other
TYPE OF WORK: Owner's number of well (if more than one)
■ New well □ Reconditioned Method : □ Dug □ Bored □ Driven □ Deepened □ Cable • Rotary □ Jetted
DIMENSIONS: Diameter of well 10 inches, drilled 453 ft.
Depth of completed well 450_fl.
CONSTRUCTION DETAILS
Casing ■ Welded 16 " Diam. from +1.2 ft. to 68 ft. Installed: □ Liner installed 10 " Diam. from 42 ft. to 423 ft. □ Threaded 10 " Diam. From 448 ft. to 450 ft.
Perforations: Yes No
Type of perforator used
200.00
SIZE of perfs in. by in. and no. of perfs from ft. to ft.
Screens: Yes No K-Pac Location Manufacturer's Name Alloy Machine
Type V-shaped wire wrap Model No. 10PS 304 SS
Diam. 10" Slot size .040 from 423 ft. to 448 ft.
Diam. Slot size from ft. to ft.
Gravel/Filter packed: Yes No Size of gravel/sand Pea* Materials placed from 412 ft. to 453 ft.
Surface Seat: Yes No To what depth? 68** ft.
Material used in seal Cement
Did any strata contain unusable water?
Type of water? Depth of strata
Method of sealing strata off
PUMP: Manufacturer's Name
Туре: Н.Р.
WATER LEVELS: Land-surface elevation above mean sea levelft.
Static level 84 ft. below top of well Date 7-19-17
Artesian pressure lbs. per square inch Date
Artesian water is controlled by (cap, valve, etc.)
WELL TESTS: Drawdown is amount water level is lowered below static level
Was a pump test made? Yes No If yes, by whom? SWS
Yield: 300 gal/min, with 9.4 ft, drawdown after 24 hrs.
Yield: gal/min, with fl. drawdown after hrs. Yield: gal/min, with fl. drawdown after hrs.
Recovery data (time taken as zero when pump turned off) (water level measured from well top to water level)
Time Water Level Time Water Level Time Water Level
0 95.4 1000 89.79
10 94,12
100 93.04
Date of test 7-19-17
Bailer test gal./min, with ft. drawdown after hrs.
region for Burning with in mandown site; ins.
Airtest gal/min. with stem set at fl. for hrs.

Temperature of water 74 Was a chemical analysis made? Yes No

CURRENT

ter Right Permit No. CG4-GWC6528-A	*200	
perty Owner Name PUD No 1 of Klickitat Co	untv	
The state of the s	<u> </u>	w/sup
Street Address At the end of Smith Road		
Wishram County Klickitat		
ation <u>SE 1/4-1/4 NW 1/4 Sec 17 Twn 2N R</u> t, r Still REQUIRED)	0	
Lat/Long		
	/Sec	
Long Deg Long M	in/Sec	·
Tax parcel No. (Required) 02151700000100 CONSTRUCTION OR DECOMMISSIO Formation: Describe by color, character, size of n	aterial and st	ructure,
and the kind and nature of the material in each str least one entry for each change of information. (U		
SHEETS IF NECESSARY.)	JULIANIAN	~. 4F1D
MATERIAL	FROM	TO
Soil, sandy loam, brown, occasional rock	0	13
Soil, silty loam with some sandy brown dry powder	13	17
Soil, silty loam, brown, packed with some gravel 4" minus	17	23
Rock, brown and grey, medium, fractured, broken, weathered	23	31
Rock, grey, medium	31	37
Sand, tan and dark grey, fine, packed	37	49
Gravel, 1" minus, some sand, tan and dark grey	49	57
Baselt, grey, medium hard	57	60
Basalt, grey, hard	60	68
Basalt, grey, hard, fractured	68	71
Basalt, dark grey, hard, fractured, vesicular	71	27
Basalt, grey, hard	77	227
Basalt, grey, hard, some fractures	227	257
Chystone, blackish grey, medium hard, with clay, grey	257	262
Clay, bineish grey, medum soft	262	280
Sand, grey, medium, with wood and some comentation	280	292 430
Siltstone, grey, hard	430	434
Basalt, black, medium, fractured, vesicular, broken	434	441
Basalt, dark grey, medium hard, vesicular, fractured Basalt, brown, medium, broken, vesic., w/ clay, firm, light green		445
Basalt, grey,medium, broken, vescular	445	448
Basalt, grey, hard	448	453
*10/20 CSSI Sand from 402' to 412'		IX A Pass P
**Additional seals were installed to 402'	KEUE	IVE
Steel ring welded between the 16" and 10"		
Steel plate welded on bottom of 10"	CEP 2	2017
Manss 10J4 pitless adapter with 30" bury	JEI 4	2011
	Dept of	
	Central Reg	
Start Date _ 5/18/17 Completed Date _9	/13/17	L

WELL CONSTRUCTION CERTIFICATION: I constructed and/or accept responsibility for construction of this well, and its compliance with all Washington well construction standards. Materials used and the information reported above are true to my best knowledge and belief.

☐ Driller ☐ Engineer ☐ Traince Name Steve Schneider	Drilling Company Schneider Water Services
Driller/Engineer/Trainee Signature	Address 21881 River RD NE
Driller or trainee License No. 0649	City, State, Zip St. Paul, OR 97137
IF TRAINEE: Driller's License No:	Contractor's
Driller's Signature:	Registration No. SCHNEEI940R8 Date 9/15/17



Water Rights Records from Washington Department of Ecology Water Resources Explorer Accessed 18 December 2018

Record No.	Person or Organization		Record Status	Imaged	Metered	Low Flow Provision	Application No.	Permit No.	Certificate No.	Record Type
G4-32618	Lavine, Garyc	1/5/1998	Active	Y	N	N				New Application
G4-122044CL	Burlington Northern,	1/1/1926	Active	N	N	N				Claim
G4-122045CL	Burlington Northern,	1/1/1930	Active	N	N	N				Claim
G4-116815CL	Smith, Otis	1/1/1948	Active	N	N	N				Claim
S4-116816CL	Smith, Otis	01/01/1898	Active	N	N	N				Claim
S4-103473CL	Delaney, Ralph H	1/1/1900	Active	N	N	N				Claim
S4-096272CL	Kochel, Lawrence S	01/01/1881	Active	N	N	N				Claim
G4-038375CL	Lyon, Lewis	1/1/1900	Active	N	N	N				Claim
G4-*09278CWRIS	Coffield & Sons,	3/8/1968	Active	Υ	N	N	9278	8664	6528	Certificate
G4-*00904SWRIS	Sp & S Ry Co,	10/1/1927	Active	Υ	N	N	904		819	Certificate
G4-*00905SWRIS	Sp & S Ry Co,	8/16/1930	Active	Υ	N	N	905		820	Certificate
G4-30396	Klickitat Cnty Pud 1 *,	9/4/1990	Active	Υ	Υ	N		G4-30396		Permit
S4-301764CL	Kayser Nate,	01/01/1861	Active	N	N	N				Claim
S3-+00935CWRIS	Coffield & Sons,	9/17/1969	Active	Υ	N	N	21826		S3+00935 C	Certificate
CG4-GWC6528-A	Klickitat Cnty Pud 1- Doug Miller,	12/23/2004	Active	Υ	Υ	Υ	9278	8664	6528	Change- ROE
CS3-00935C	Klickitat Cnty Pud 1- Doug Miller,	12/23/2004	Active	Υ	Υ	Υ	21826	S3- 00935P	S3+00935 C	Change- ROE
CG4-GWC6528- A@1	Klickitat Cnty Pud 1 *,	2/6/2017	Active	Υ	Υ	N	9278	8664	6528	Change- ROE
CG4-30396P	Klickitat Cnty Pud 1 *,	4/13/2018	Active	Υ	Υ	N		G4-30396		Change- ROE



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Please take notice that state law states that all private citizen names and addresses may not be used for any solicitation/commercial purpose.

Well Log Data Export

Data Dictionary

The table below lists the data field names, descriptions, and examples of each data item that makes up the well log data extract file.

Column Name	Description	Example
well_log_id	WELL LOG ID. A sequential	100564
	number generated by the	
	system to track a well log	
	record.	
well_tag_nr	WELL TAG NUMBER. The	AAA-000
	number issued by the	
	Department of Ecology that is	
	stamped on a metal tag that is	
	attached to the actual well.	
project_tag_nr	PROJECT TAG NUMBER –	MW-001
	The number issued by the	
	property owner or consulting	
	firm to track the well. This	
	number is NOT affiliated with	
	Ecology's tag number in any	
	way.	
nit_id_nr	NOTICE OF INTENT ID	W072515
	NUMBER. A sequential	
	number issued by the	
	Department of Ecology to	
	track the Notice of Intent to	
	Construct or Decommission a	
11 1 1	Well.	5.5
well_depth_qt	WELL DEPTH. Depth of the	55
11 1:	well in feet.	
well_diameter_qt	WELL DIAMETER.	6
	Diameter of the casing of the	
11	well in inches.	T.1. C. '.1
well_owner_nm	WELL OWNER NAME. The	John Smith
	name of the original property	
	owner who had the well	
4	drilled.	05
township_nr	TOWNSHIP. The identifier	05
	describing which Township	
	the well falls within. Based	
	on the Washington State	
	Public Land Survey (PLS).	

range_nr	RANGE. The identifier describing the Range location of the well. (PLS)	15
range_dir_cd	RANGE DIRECTION. The direction code describing further which range the well falls within. Washington State is divided into two halves – 'West' and 'East'. (PLS)	Е
section_nr	SECTION. The identifier describing which Section the well falls within. (PLS)	06
qtr_section_cd	QUARTER SECTION (1/4). The identifier describing which Quarter section the well falls within. (PLS)	NW
qtr_qtr_section_cd	QUARTER-QUARTER SECTION (1/4-1/4). The identifier describing which Quarter-Quarter section the well falls within. (PLS)	SW
well_comp_dt	WELL COMPLETION DATE. Date the well was drilled.	1/1/1997
county_nm	COUNTY NAME. County name where the well is located.	King
well_type_cd	WELL TYPE. Code which indicates the well type. See appendix for code descriptions.	W
driller_nr	DRILLER LICENSE NUMBER. License number of the well driller.	2327
well_log_recv_dt	WELL LOG RECEIVAL DATE. Date the Department of Ecology received the well log form.	1/6/1997
tax_parcel_nr	TAX PERCEL IDENTIFIER. County Assessor code of the parcel where the well was drilled.	232019130050

st plane xcoord nr	STATE PLANE X-	2031126
st_plane_xcoola_in	COORDINATE. The	2031120
	horizontal geographic	
	coordinate value of the well	
	within the WA State Plane	
	Coordinate System (adjusted	
	to the quarter-quarter, quarter,	
	or whole section).	
st_plane_ycoord_nr	STATE PLANE Y-	780897
	COORDINATE. The vertical	
	geographic coordinate value	
	of the well within the WA	
	State Plane Coordinate System	
	(adjusted to the quarter-	
	quarter, quarter, or whole	
	section).	

Appendix

Well Type Codes:

W Water

R Resource Protection

A Abandonment

well_log_id well_tag_nr	nit_id_nr	well_depth_qt w	vell_diameter_qt	well_owner_nm	well_comp_dt	well_log_recv_dt
143847 AFL874	W025804	550	8	PUD/WISHRAM	10/25/1993	11/1/1993
144595		180	6	RICHARD TROUTMAN	3/2/1979	
144596		300	6	RICHARD TROUTMAN	6/2/1979	
				SPOKANE, PORTLAND		
296882		399	15	& SEATTLE RY CO	12/23/1926	10/1/1927
341489 AHK335	W160753	380	6	MICHAEL SUMMERS	7/10/2002	8/5/2002
367346 AHK330	W171119	602	6	JAMES DOUGAL	7/30/2003	8/11/2003
				GARY AND LYNDA		
417933 ALC273	W189156	675	8	LAVINE	8/11/2005	8/26/2005
1581936 BIN746	W357798	385	6	Mark Portukalian	7/18/2016	7/25/2016
				PUD No 1 Of Klickitat		
1642314 AAR991	WE27476	450	10	County	9/13/2017	9/21/2017

Appendix P

Terrestrial Ecological Evaluation



Simplified Terrestrial Ecological Evaluation-Exposure Analysis Procedure

Table 749-1

Estimate the area of contiguous (connected) <u>undeveloped land</u> on the site or within 500 area of the site to the nearest 1/2 acre (1/4 acre if the area is less than 0.5 acre).	feet of any
1) From the table below, find the number of points corresponding to the area and enter this number in the field to the right.	
Area (acres) Points 0.25 or less 4 0.5 5 1.0 6 1.5 7 2.0 8 2.5 acres 2.5 9 3.0 10 3.5 11 4.0 or more 12	9
2) Is this an <u>industrial</u> or <u>commercial</u> property? If yes, enter a score of 3. If no, enter a score of 1	3
3) ^a Enter a score in the box to the right for the habitat quality of the site, using the following rating system ^b . High=1, Intermediate=2, Low=3	3
4) Is the undeveloped land likely to attract wildlife? If yes, enter a score of 1 in the box to the right. If no, enter a score of 2. ^c	1
5) Are there any of the following soil contaminants present: Chlorinated dioxins/furans, PCB mixtures, DDT, DDE, DDD, aldrin, chlordane, dieldrin, endosulfan, endrin, heptachlor, benzene hexachloride, toxaphene, hexachlorobenzene, pentachlorophenol, pentachlorobenzene? If yes, enter a score of 1 in the box to the right. If no, enter a score of 4.	4
6) Add the numbers in the boxes on lines 2-5 and enter this number in the box to the right. If this number is larger than the number in the box on line 1, the simplified evaluation may be ended.	11

Notes for Table 749-1

Low: Early <u>successional</u> vegetative stands; vegetation predominantly noxious, nonnative, exotic plant species or weeds. Areas severely disturbed by human activity, including intensively cultivated croplands. Areas isolated from other habitat used by wildlife.

^a It is expected that this habitat evaluation will be undertaken by an experienced field biologist. If this is not the case, enter a conservative score of (1) for questions 3 and 4.

^b **Habitat rating system.** Rate the quality of the habitat as high, intermediate or low based on your professional judgment as a field biologist. The following are suggested factors to consider in making this evaluation:

High: Area is ecologically significant for one or more of the following reasons: Late-<u>successional</u> native plant communities present; relatively high species diversity; used by an uncommon or rare species; <u>priority habitat</u> (as defined by the Washington Department of fish and Wildlife); part of a larger area of habitat where size or fragmentation may be important for the retention of some species.

Intermediate: Area does not rate as either high or low.

[Area Calculation Aid] [Aerial Photo with Area Designations] [TEE Table 749-1] [Index of Tables]

[Exclusions Main] [TEE Definitions] [Simplified or Site-Specific?] [Simplified Ecological Evaluation] [Site-Specific Ecological Evaluation] [WAC 173-340-7493]

[TEE Home]

^c Indicate "yes" if the area attracts wildlife or is likely to do so. Examples: Birds frequently visit the area to feed; evidence of high use b mammals (tracks, scat, etc.); habitat "island" in an industrial area; unusual features of an area that make it important for feeding animals; heavy use during seasonal migrations.

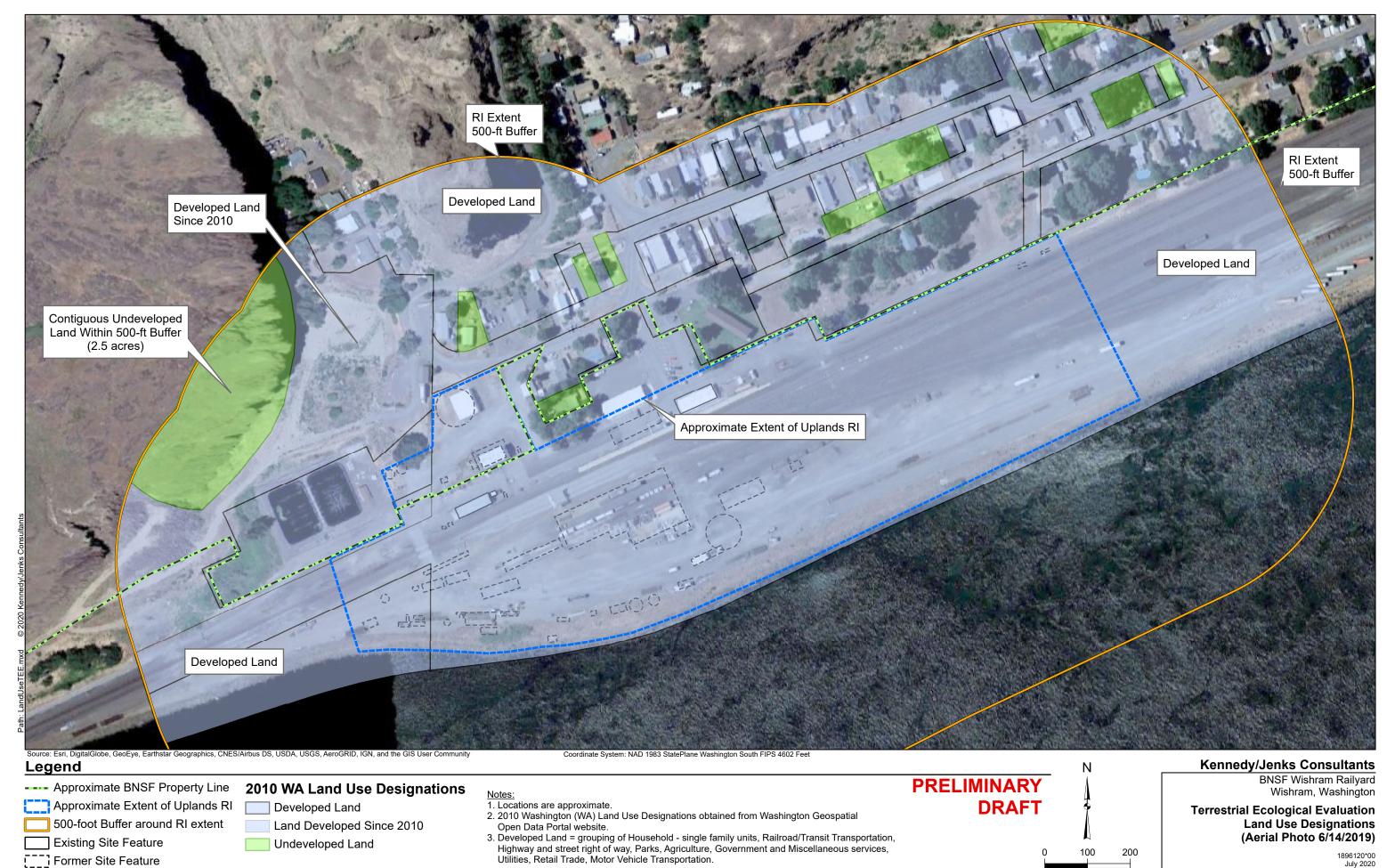


Figure P-1

Scale: Feet

Appendix Q

Petroleum Vapor Intrusion Evaluation

TABLE Q-1

SUMMARY OF SOIL ANALYTICAL RESULTS FOR VAPOR INTRUSION EVALUATION BNSF Wishram Railyard, Wishram, Washington

	1					Location ID	WSB-1	WSB-1	WSB-2	WSB-2	WSB-3	WSB-3	M-2-14	M-2-8	T-7	T-8	T-9	T-10	B-18-25	B-18-25	B-18-25
						Location ib	W3D-1	WOD-1	W3D-2	W3D-2	W3D-3	WSD-3	M-2-	M-2-	1-7	1-0	1-9	1-10	D-10-23	DUP-04-	B-18-25(9.5-
						Sample ID	WSB-1-10	WSB-1-15	WSB-2-8	WSB-2-14	WSB-3-10	WSB-3-16	14 20051108	8 20051108	T-7-12	T-8-11	T-9-14	T-10-11.5	B-18-25(2-2.5)		10)
						Parent Sample ID	W3D-1-10	W3D-1-13	W3D-2-0	W3D-Z-14	W3D-3-10	W3D-3-10	14_20031100	0_20031100	1-7-12	1-0-11	1-5-14	1-10-11.5	D-10-23(2-2.3)	B-18-25(2-2.5)	10)
						Sample Date	9/2/2003	9/2/2003	9/2/2003	9/2/2003	9/2/2003	9/2/2003	11/8/2005	11/8/2005	5/20/2010	5/20/2010	5/20/2010	5/20/2010	8/21/2018	8/21/2018	8/21/2018
						Sample Depth	10 ft	9/2/2003 15 ft	8 ft	9/2/2003 14 ft	10 ft	9/2/2003 16 ft	11/6/2003	8 ft	12 ft	11 ft	14 ft	11.5 ft	2-2.5 ft	2-2.5 ft	9.5-10 ft
						Water Table Note		BWT	AWT	AWT	AWT	BWT	BWT	AWT	BWT	BWT	BWT	BWT	AWT	AWT	AWT
						Water Table Note	AVVI	DWI	AVVI	AVVI	AVVI	DWI			DVVI	DVVI	DVVI	DVVI	AVVI	AVVI	AVVI
										PAHs SW8270			Excavation confirmation soil	Excavation confirmation soil							
						Notes				without SIM			sample.	sample.							
						1.0.00		1	1	marout onn		1			ı	1	1	ı	 		
		Criteria for PVI Soil Protective of Soil Protective of Pre-Bioventing System Operation										Bioventing System Operation (2012-2019)									
Chemical	Units	(Impl Memo #14) MTCA A then Lowest B GW (Vadose) GW (Saturated)												3.7							
NWTPH-Gx					•		•													-	-
Gasoline-Range Organics	mg/kg	250	30	Method A											< 5.9	< 5.4	< 6.3	< 6.1			
NWTPH-Dx - without silica gel cleanup				l	- I	1	ļ.					1		!					+		4
Diesel-Range Organics	mg/kg	250	2.000	Method A															< 88.9	< 46.7	< 4.85
Oil-Range Organics	mg/kg		2.000	Method A						-									276	< 117	< 12.1
TPH-Dx Sum (HalfDL WA)	mg/kg		2.000	Method A															320	< 23.4	< 2.43
TPH-Dx Sum (HitsOnly)	mg/kg		2.000	Method A															276	ND	ND
NWTPH-Dx - with silica gel cleanup			_,000			+			•				+							· · · · · ·	+
Diesel-Range Organics	mg/kg	250	2.000	Method A			47.6	< 0.0250	6,900	15,700	< 0.0250	< 0.0250	182	89.9	< 24.5	< 20.4	< 21.9	< 24.8			
Oil-Range Organics	mg/kg		2.000	Method A		1	359	< 0.0500	4.710	10,500	< 0.0500	< 0.0500	< 27.7	< 27.3	< 98.1	< 81.6	< 87.4	< 99.3			
TPH-Dx Sum (HalfDL WA)	mg/kg		2.000	Method A			407	< 0.0125	11,600	26,200	< 0.0125	< 0.0125	196	104	< 12.3	< 10.2	< 11.0	< 12.4			
TPH-Dx Sum (HitsOnly)	mg/kg		2.000	Method A			407	ND	11,600	26,200	ND	ND	182	89.9	ND ND	ND	ND	ND			
BTEX	mg/kg		2,000	ļ	-	!	401	110	11,000	20,200	ND	110	102	00.0	IND	110	110	IND	+		+
Benzene	mg/kg	100	0.03	Method A	0.027	0.0017	< 0.05	< 0.05	< 0.1	< 0.1	< 0.05	< 0.05			< 0.0235	< 0.0217	< 0.0253	< 0.0242	< 0.00113	< 0.00121	< 0.00121
Toluene	mg/kg	100	7	Method A	4.5	0.27	0.0147	< 0.05	< 0.1	< 0.1	< 0.05	< 0.05			< 0.0294	< 0.0271	< 0.0316	< 0.0303	0.0225	0.0134	< 0.00606
Ethylbenzene	mg/kg		6	Method A	5.9	0.34	< 0.05	< 0.05	0.178	0.687	< 0.05	< 0.05			< 0.0294	< 0.0271	< 0.0316	< 0.0303	< 0.00283	< 0.00303	< 0.00303
Xylene, m,p-	mg/kg			mounou, t	3.3	0.04		1 0.00	0.170	0.007					· 0.0234	1 0.0211	· 0.0510		0.0200	0.0141	< 0.00485
Xylene, o-	mg/kg		16.000	Method B Non cancer	14	0.84				-									0.0154	0.00850	< 0.00303
Total Xylenes (HalfDL WA)	mg/kg		9	Method A	14	0.83													0.0354	0.0226	< 0.00152
Xvlene, total	mg/kg		9	Method A	14	0.83	< 0.1	< 0.1	0.0817	0.739	< 0.1	< 0.1			< 0.0882	< 0.0814	< 0.0947	< 0.0909			
Polycyclic Aromatic Hydrocarbons using SIM				mounday.	17	0.00	١٠٥.١	٠٥.١	0.0017	0.755	٠٥.1	٧٥.١			₹ 0.0002	10.0014	· 0.0341	· 0.0303			
1-Methylnaphthalene	mg/kg		34	Method B Cancer								I							0.0412	0.0274	< 0.0242
2-Methylnaphthalene	mg/kg		320	Method B Non cancer						61.9									0.0412	0.0274	< 0.0242
Anthracene	mg/kg		24.000	Method B Non cancer	2300	110				< 16.5									0.0123	0.0310	< 0.0242
			24,000	Wethod B Non cancer	2300	110				< 16.5									0.0123	0.0139	< 0.00727
Benzo(a)anthracene	mg/kg	-	0.1	Method A	3.9	0.19				< 16.5					-				0.0304	0.0139	< 0.00727
Benzo(a)pyrene	mg/kg		U. I	INIGUIOU A	3.9	0.19															
Benzo(b)Fluoranthene	mg/kg	-			+	1				< 16.5		-			-				0.0610	0.0314	< 0.00727
Benzo(k)Fluoranthene	mg/kg				+					< 16.5		-							0.0213	0.00783	< 0.00727
Chrysene	mg/kg				+	1				< 16.5		-	-						0.0375	0.0173	< 0.00727
Dibenz(a,h)Anthracene	mg/kg			1	1	1		-		< 16.5					-				0.00933	< 0.00700	< 0.00727
Indeno(1,2,3-c,d)Pyrene	mg/kg			Mathad A	1.5					< 16.5									0.0318	0.0138	< 0.00727
Naphthalene	mg/kg		5	Method A	4.5	0.24		-		23.8		-			-	-	-		0.0380	0.0294	< 0.0242
Total Naphthalene (HalfDL_WA)	mg/kg		5	Method A	4.5	0.24				85.7					-				0.123	0.0878	< 0.0121
Total Naphthalene (HitsOnly)	mg/kg		5	Method A	4.5	0.24				85.7									0.123	0.0878	< 0.00
Total cPAH TEQ (HalfDL_WA)	mg/kg		0.1	Method A	3.9	0.19		-	-	< 8.25			-			-			0.0649	0.0274	< 0.00364
Total cPAH TEQ (HitsOnly)	mg/kg		0.1	Method A	3.9	0.19				< 0.00			-						0.0649	0.0271	< 0.00
Volatile Organic Compounds				In a state of the	1	T	1	T		1		1		ı	ı	1	1	ı	T		
1,2-Dibromoethane (EDB)	mg/kg		0.005	Method A						-									< 0.00283	< 0.00303	< 0.00303
1,2-Dichloroethane (EDC)	mg/kg		11	Method B Cancer	0.023	0.0016													< 0.00283	< 0.00303	< 0.00303
Naphthalene	mg/kg		5	Method A	4.5	0.24				-		-			-				0.0160	< 0.0152	< 0.0152
Metals																					
Arsenic	mg/kg		20	Method A	2.9	0.15			4.3	5.27									2.31	< 2.33	< 2.42
Barium	mg/kg		16,000	Method B Non cancer	1600	83			<u>4,680</u>	6,500			-						95.3	83.5	103
Lead	mg/kg		250	Method A	3000	150			387	37.1									19.4	20.0	4.61

 TABLE Q-1

SUMMARY OF SOIL ANALYTICAL RESULTS FOR VAPOR INTRUSION EVALUATION BNSF Wishram Railyard, Wishram, Washington

34300
< 0.18
1700

1700

Detected concentrations above the cleanup level are shaded blue and bolded.

Non-detect values above the cleanup level are shaded gray and italicized.

Detected concentrations at or above the method reporting limit are shown in bold.

Detected concentrations above the screening level for soil protective of groundwater in the vadose or saturated zone are underlined and bolded.

Abbreviations and Symbols

"AWT" denotes soil sample collected above the water table in the vadose zone. Results compared to MTCA CULs (see below) and soil protective of groundwater in the vadose zone screening levels.

"BWT" denotes soil sample collected below the water table in the saturated zone. Results compared to MTCA CULs (see below) and soil protective of groundwater in the saturated zone screening levels.

- " - " denotes not measured, not available, or not applicable.
- " < " denotes not detected at or above the indicated method reporting limit.

"ND" denotes that the result was not detected and the method reporting limit is unknown.

"B" denotes that the value has been qualified due to blank contamination by the laboratory.

"DUP" denotes a field duplicate sample. Primary sample ID is provided beneath the duplicate sample ID.

"E" indicates that the concentration exceeded the calibration curve and is an estimate.

"J" indicates an estimated concentration based on either the being less than the laboratory reporting limit or data validation findings.

"J+" indicates an estimated concentration likely biased high based on data validation findings or as reported by the laboratory.

"U" denotes that the value has been qualified as undetected (at the detected concentration if above the method reporting limit) due to blank contamination.

"Y" denotes that the chromatographic fingerprint of the sample resembles a petroleum product eluting in approximately the correct carbon range, but the elution pattern does not match the calibration standard.

ft = feet

mg/kg = milligrams per kilogram

μg/kg = milligrams per kilogram

Total TPH-Dx = Total TPH-Dx concentrations were calculated by summing diesel-range organics (DRO) and oil-range organics (ORO) concentrations. Non-detects were included as noted.

Total cPAHs = Possible Total Carcinogenic Polycyclic Aromatic hydrocarbons (cPAHs) are based on the relative toxicity of each cPAH to benzo(a)pyrene and were calculated by

multiplying the individual cPAH concentrations by a toxicity equivalency factor (TEF) and summing the adjusted concentrations. Non-detects were included as noted.

Total Naphthalenes = Total Naphthalenes concentrations were calculated by summing 1-Methylnaphthalene, 2-Methylnaphthalene, and Naphthalene concentrations. Non-detects were included as noted.

Total Xylenes = Total Xylenes concentrations were calculated by summing Xylene, m,p- and Xylene, o- concentrations. Non-detects were included as noted.

(HitsOnly) = If an individual chemical was not detected, it was not included in the calculation.

(HalfDL_WA) = If an individual chemical was not detected, a value of one half the method reporting limit was used as the concentration in the calculation, except when all chemicals used in the calculation were not detected then one half the lowest method reporting limit was used as the total concentration.

Cleanup Levels (CUL)

Cleanup level values based on Model Toxics Control Act (MTCA) Method A values for unrestricted land use (Method A) based on Washington State Administrative Code (WAC) 173-340-740 Table 740-1.

Where MTCA Method A values are not available, the lowest of MTCA Method B values (B Cancer or B Non Cancer) from Cleanup Levels and Risk Calculation (CLARC) tables have been used (Accessed January 2020).

Methods

Samples analyzed for gasoline-range organics (GRO) using Northwest Total Petroleum Hydrocarbon (NWTPH)-Gx and diesel- and oil-range organics (DRO and ORO) using NWTPH-Dx (with or without silica gel cleanup as noted). Samples analyzed for benzene, toluene, ethylbenzene, and xylenes (BTEX) and Volatile Organic Compounds using EPA Method 8021 or 8260.

Samples analyzed for metals using EPA Method 6010, 3060, or 7471.

Samples analyzed for Semivolatile Organic Compound using EPA Method 8270 with selective ion monitoring (SIM). In cases where SIM was not used, it is noted in the notes row.

