# Appendix C Vendor Packages

# **Kaiser Mead Water Treatment System Specifications**

# 03-25-2020

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# **Section 1. General Description**

# 1.0 Extraction Wells – Wetlands

Customer will install five extraction wells for water removal from the local aquifer. Water is pumped through the Water Treatment building for flow measurement and manual control. A flow-indicating transmitter mounted in a prefabricated pipe section will send 4-20mA signal to the United Rentals control PLC. Flow rate can be monitored on screen, as well as at the transmitter. The anticipated flow rate is entered by the operator at the HMI control panel. If flow falls below an adjustable rate (deviation value) indicating a pumping problem, the PLC will indicate an alarm condition.

Extraction well piping includes a pneumatically actuated fail close ball valve controlled by the United Rentals control PLC. The pneumatically actuated valve is closed when power is off, treatment system is off, estop is activated, or wetland lift station indicates a general alarm condition. Additionally, manual valves in the pipeline allow for maintenance services, sample collection and by-pass of the wetland system.

#### 1.1 Electrocoagulation Treatment

Water will enter United Rental's electrocoagulation system from a wetlands process for cyanide destruction. Water entering the equalization tank is monitored for conductivity. Water in the equalization tank will be monitored for pH and adjusted by United Rentals's pH system. Calcium chloride will be dosed into the equalization tank to assist in water treatment for the removal of fluoride. Conductivity is monitored in the equalization tank. Once water reaches desired state it will be pumped by United Rentals's equipment into and through the United Rentals Hi-Flo Electrocoagulation nominal 50 GPM treatment package with a maximum hydraulic flow rate of 75 gpm.

The electrocoagulation unit, controls, tanks, and additional equipment will be housed inside a building for climate control. The building shall maintain the temperature greater than 40 degrees and provide air exchanging (100 CFM) for exhausting hydrogen production during the EC process.

A polish step is included for final filtration. Water discharged from the clarifier will flow through multimedia filtration and bag filters, for polishing, before leaving the system.

#### 1.2 Water Delivery to United Rentals Treatment System

United Rentals system will control an equalization vessel. The EQ vessel must be agitated to prevent stratification either by density or by temperature. A pH controller will adjust pH in the equalization vessel if required. The maximum operating temperature for the building and liquids used in the treatment system is 104F. Note operating system at an abnormally high or abnormally low pH or temperature will cause damage to treatment system and cause undesired results. United Rentals will bring water to the reactor using appropriately sized pump(s) whose speed is controlled by the United Rentals system. The water in the equalization vessel will contain no free oil.

# 1.2.1 Entering United Rentals System

A flow-indicating transmitter mounted in a prefabricated pipe section ahead of the Hi-Flo unit will send 4-20mA signal to the United Rentals control PLC. Flow rate can be monitored on screen, as well as at the transmitter.

Flow is to be adjusted by the operator at the controls using a 4-20ma output and displayed in gpm. If flow falls below an adjustable rate indicating a pumping problem, the PLC will shut down the system and indicate the fault.

Normally, the pumped flow rate is not proportionally controlled by the EQ tank water level. The pumped flow rate is a constant flow rate set by the operator. A program modification will be implemented to allow the operator to input a minimum flow rate and maximum flow rate for the treatment system as well as the tank level associated with the minimum and maximum flow rate. For example, this modification will allow the system to automatically increase the flow rate for a short period following a media filter backwash event and thus remove the backwash water from the EQ tank. Treatment flow rate would return to the steady state condition once the additional water is removed from the EQ tank.

In a scenario where flow rate from the wetlands decreases and pumped flow rate from the EC system is not changed, the EQ tank level will drop and reach an EC stop level condition. The EC stop level condition will place the EC system in standby mode. Once the EQ tank level increases to an EC start level condition, the EC system will automatically resume treatment. Operator can input the EC start and EC stop levels through the HMI.

In a scenario when the flow rate from the wetlands increases and pumped flow rate from the EC system is not changed, the EQ tank level will rise and reach a High level condition. The High level condition will close the pneumatic valve on the feed line from the lift station; the EC system will continue to treat water. Once the EQ tank level decreases and returns to a normal operating level, the pneumatic valve will automatically open and continue to move water from the lift station to the EQ tank. Operator can input the EC start and EC stop levels through the HMI.

Flow rate is recorded through the HMI. Operator can view the graphical representation of the flow rates with time.

Reactor inlet flow control includes a pneumatically actuated butterfly valve controlled by the EC unit's PLC. Additionally, manual valves in the pipeline allow for maintenance services.

# **Section 2: System Scope of Supply**

The EC Treatment System to be furnished is specified to operate as a nominal 50 GPM system. Hydraulically, the system can operate in a 50-75 GPM flow range. All components required for the complete reaction shall be furnished. Replacement of sacrificial plates is the responsibility of the customer.

# 2.1 United Rentals Hi-Flo Electrocoagulation Treatment Package

The 50 GPM reactor cell will consist of the following, Tandem United Rentals Hi-Flo Reactor Package of this description:

#### 2.1.1 Hi-Flo Reactors

Wastewater delivered by the centrifugal pump will enter the United Rentals Hi-Flo Treatment Reactor, RX- 1, with a removable Reactor Treatment Cartridge.

The United Rentals Electrocoagulation Hi-Flo® Dual-Tandem Reactor Cell System by Kaselco employs electrolysis-based technology that does not require the use of chemical precipitants to remove suspended and dissolved solids from solution. The electrochemical process facilitates the settling of suspended particle and drives chemical reactions between constituents in the water.

The control system for the Electrocoagulation has the following features:

- Provide for automatic control of reactor cell electrode current in response to routine variations in waste stream characteristics.
- Provide the capability for on-site modification of electrode configuration when required to accommodate substantial and ongoing changes in waste stream characteristics.
- Provide the capability for the system operator to adjust power settings as necessary to optimize treatment efficiency.
- Provide for automatic control of reactor cell polarity to optimize the consumption rate of electrode plate material.
- Provide the capability to manually control surge current at operator discretion to allow periodic purging of accumulated surface impurities from electrode plates to optimize performance.
- Provide electrode cartridge configuration with segmented intermediate plates and designed to accommodate replacement of electrode plates on-site by facility personnel using locally sourced materials.
- Provide for manual cleaning of electrode plates without disassembly of the reactor cells when necessary to accommodate waste streams generating excessively high solids content.

Wastewater delivered by the pump will enter a Hi-Flo Treatment Reactor, RX-1, with a removable Reactor Treatment Cartridge. Wastewater enters the bottom of this vessel through an inlet and up through the vertically arranged steel plates in the first Reactor Cartridge. Treated water overflows the top of the cartridge and enters the second chamber of the Treatment Reactor Vessel through internal piping in the vessel. Treated water overflow from RX-2 then proceeds to the post EC tank. The reactors are open to the atmosphere.

Reactor vessels can be upgraded, with a change order, with plastic covers to contain off-gasses and removed using an air ventilation system.

To eliminate the possibility of reactor treatment plates shorting in the event of a large piece of rust or scale sloughing off of a reactor plate, each Reactor Treatment Vessel has a deep sump. This allows even the largest pieces of scale to fall to the bottom, below the treatment plate pack, eliminating the possibility of shorting out reactor sections.

The steel and aluminum plates are sacrificial. The iron from the steel plates and aluminum in the aluminum plates is slowly driven off and into the water. Under the influence of the electrical field, the iron an aluminum atoms engage in a series of electrochemical reactions, their final act being the reaction with pollutants such as dissolved metals and emulsions in the wastewater causing them to be insoluble so they can be settled out in a solids separation system.

To remove heavy particles of rust or scale that may slough off of the treatment plates and that are not entrained in the water stream, a sub-system called "Scale Purge" is occasionally energized to remove heavy solids from the bottom of the treatment reactor. The cycle time is adjustable and the PLC manages this cycle. The cycle time for scale purge is set by the operator based on needs for this specific installation. The scale system provided will include the two air-operated valves, the AODD pump, and the interconnecting plumbing. The scale purge system requires no chemicals.

The scale purge cycle can be manually engaged to remove water from the reactor vessel for maintenance and inspection activities.

#### 2.1.2 Treatment Power

Power is applied to select plates through a copper buss system. The copper buss bar is connected to power plates, and connects to the positive and negative posts on the rectifiers, which supply the treatment power.

Two rectifiers provide treatment power through the buss to the reactor. Typically, power supply to the rectifier is 480VAC, 60Hz, 3-phase power. The rectifier's continuous duty rated output is 2,000 Amps at 48VDC with reversing polarity. Polarity reversal time is adjusted in the PLC program by the operator. Amperage is the primary controlled treatment power parameter. The operator can adjust power within a range to ensure treatment, and to save electrical

energy cost and treatment plates if the water can be treated adequately with less power. Voltage automatically "floats" depending on the conductivity of the wastewater.

Reactor Power Monitor: If reactor treatment power supply voltage drops below an adjustable voltage, the PLC shuts down the reactor package and indicates treatment power failure on the control panel.

# 2.1.3 Solids Separation

Step 1: The normal flow will be a single pass through the EC reactor into an open top Post-EC Tank. Treated water is pumped using a Post-EC pump to the Defoam Tank or to the EQ Tank using the Post-EC Recycle valve. Operations and controls for the Post-EC Tank, Post-EC Pumps, and Post-EC Recycle valve.

# Post-EC Tank

- This system has a single open top Post EC tank.
- The tank is equipped with a LSH, LSL, and LIT.
- The HMI indicates an alarm and the HiFlo system enters standby mode if the level exceeds a high level setting or if the high level switch floats. This alarm remains enabled in all modes of the treatment system (i.e., standby, off, etc.).
- The system resumes treatment when high level clears.
- The level transmitter is used for starting, stopping and controlling the speed of the Post EC pumps, as described below.

#### Post-EC Pump and Valve (ACV-0409)

- Profinet communication between PLC and VFD drives
- Two pumps operate as a redundant pair
  - One pump runs at a time
  - Each time the system starts a pump, it chooses the one that was not used last if that pump is available.
  - The backup pump is started whenever the primary pump becomes unavailable (i.e., fails to run or is put in MANUAL/OFF).
  - The primary / backup pumps are swapped when the primary has run for a long time (the setting is configurable through the HMI).
- Pump starts when system is in service and Post-EC tank level is above a "start pump" setting.
- Pump stops when tank level is below a "stop pump" level. In Standby, the pump continues to run until the tank level is low.
- The pump speed is modulated in proportion to tank level. The HMI allows the operator to adjust
  - Pump minimum speed
  - Pump maximum speed

- Level corresponding to minimum speed (same as the level for starting the pump)
- Level corresponding to maximum speed (an alarm is posted if the tank reaches this HI LEVEL setting).
- Post-EC valve opens whenever Post-EC pump runs.
- Post-EC pump will not run in auto if the valve is not available.
- System will **not** run if the Post-EC pump or valve is not available.

#### Post-EC Recycle Valve (ACV-0414)

- When the associated discrete output is energized, the valve directs flow to the equalization tank (i.e., water is directed away from the solids treatment system).
- Valve solenoid is not energized when the system is treating, except for these cases:
  - o Solenoid is energized for a period of time following EC start-up.
  - Solenoid is energized for a period of time following polarity reversal
- The valve may be manually controlled via the HMI
- The EC system is allowed to treat when the valve is in manual, directing flow either way.

The de-foam tank drives the electrolysis bubbles from the solids, allowing them to settle. The tank will be equipped with an agitator and aeration. A downcomer in the de-foam tank will ensure that only the heavier, de-gassed solids exit. A mixer and aeration disc is provided in package costs for solids separation.

Sulfuric acid is dosed into the Defoam tank to control the pH range. The pH is monitored on the HMI. The PLC will control the chemical metering pump in an "On/Off" operation. The sulfuric acid dosing rate is manually set by the operator. Two pumps operate as a redundant pair; one pump runs at a time.

# <u>Defoam pH adjustment</u>

- A packaged system measures pH.
- The packaged system provides 4-20mA signals for pH. These will be recorded by the HMI.
- The HMI will provide alarms for high and low pH. All settings may be adjusted by the operator.
- The system provides the following alarm and process control transition points for pH, presented from high to low pH:
  - High-high pH alarm. Stop sending water to ECs if condition persists for set amount of time.
  - o High alarm: present alarm
  - Start acid pump
  - Stop acid pump
  - o Low pH alarm
  - Low-low pH alarm; stop sending water to ECs.

Step 2: The treated water will then flow into a flocculation tank. A polymer will be fed by chemical feed pump(s) to the entrance of the flocculation tank to aid floc formation and settling. The pump will draw from a supply vessel. This process will aid in the formation of larger solids for improved settling. Mixer is provided in package costs for solids separation.

Step 3: A slant-plate clarifier will remove the settleable solids. Standard flow rate of 0.125 gpm/square foot of projected surface area.

- Inclined plates set at 55-degree angle
- Maximum inclined plate length, direction of flow, is four feet (48 inches)
- Plate spacing at 1" between slanted plates
- Dual sludge discharge points at bottom of clarifier
- Flow through unit is by gravity only

Step 4: Sludge from the bottom of the slant plate clarifier will periodically be pumped into a cone bottom sludge thickening tank. Periodic sludge removal from the clarifier is conducted automatically. The frequency, time interval between sludge pumping events, and the duration, how long the sludge pumping event lasts, is set by the operator through the HMI.

# Clarifier Sludge

- Equipped with a high level switch.
- System presents an alarm and enters Standby Mode if the tank has a high level; system resumes treatment when high level clears.
- Equipped with two pneumatic actuated valves (SV-0526 and SV-0536) and a sludge pump for solids removal.
- After treating for a given time, the system opens the sludge removal valve for a preset period. Delay and duration are set through the HMI.
- Valve opens when sludge pump runs.
- System will <u>not</u> treat water if sludge pump is not in AUTO.
- System will **not** treat water if valve is not in AUTO.
- The sludge pump and valve will open if system enters Standby. Pump will run for a preset time that is adjusted by the operator through the HMI.

Overflow from the top of this tank will return to the inlet of the Defoam tank. This tank allows the clear water to rise to the top while the floc settles in the cone bottom. Sludge collected in the cone bottom tank will be pumped to a filter press for solids dewatering. The operator manually pumps sludge to the filter press using the HMI and the "remote start" signal to the filter press controls. Pumping sludge to the filter press is conducted daily. Draining the sludge thickener is implemented manually by the operator.

# 2.1.4 Solids Management

#### FILTER PRESS

The filter press provided with your system is designed and sized to handle the expected solids load. The base frame and plumbing were manufactured and assembled by United Rentals. The filter plates are supplied by Evoqua. The cloth is polypropylene. The hydraulic pump is operated as an air over hydraulic system. The chutes under the press facilitate collection of the solids falling from the plate into barrels facilitating transport to a disposal facility.

#### **CLOSE PRESS:**

- Verify the plates are clean of solid residue around the gaskets.
   Wipe any remaining material from the o-rings on the plates to allow a good water tight seal between the plates.
- View the plates from the side. Verify the plates have a one-dot and three-dot alignment along the length of the press. Plates must alternate between a one-dot and three-dot plate to have good water flow through the plates.
- Align the plates beginning with the intermediate plate adjacent to the tail plate and press them lightly against each other by sliding them along the frame rail. The side frame rails of the press serve as an alignment rail for the plates. Push the head plate into position last.
- The J-PRESS controller is used to operate the hydraulic cylinder of the filter press (Figure 2). The ON/OFF switch engages the air pressure to facilitate hydraulic operation. OPEN/CLOSE switch allows pressurizing the dual acting hydraulic cylinder for opening and closing the press.



Figure 1. Filter press control panel for hydraulic cylinder operation.

- Once the plates are aligned correctly, turn the switch to "ON" and the second switch to "CLOSE". The air over hydraulic system will close the press to engage the head plate.
- Once resistance is encountered and hydraulic pressure is sustained, operation will change to a pulsing operation. Continue in "CLOSE" mode until a pressure of greater than 5000 psi is developed. This pressure is maintained while the press is filled with sludge.

# **SET VALVES:**

The filter press has several valves controlling operation. The valves provide two
different functions: controlling water flow, and controlling air flow. The water control
valves are schedule 80 PVC manual ball valves. The air control valves are ½" PVC ball
valves.

#### Water control valves:

- The AODD pump inlet plumbing has a ball valve, open the ball valve connected to the bottom of the settling tanks. The filter press has an inlet ball valve (Valve E). Valve E should be open to fill filter press (Figure 3).
- Piping connected to the outlet of the filter press conveys liquid to the primary holding tank 1. All four outlet valves are open when filling the filter press (Valves A, B, C &D).
   Valves C & D can be closed during the first portion of the press cycle to fill all of the voids between the plates. The press is ready to operate once solids can enter and exit the press.

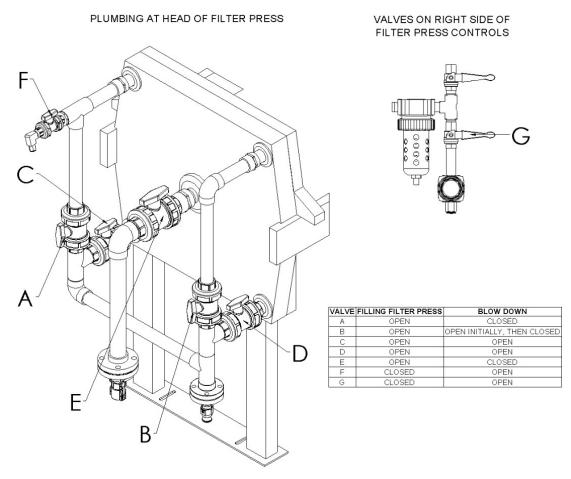


Figure 2. Filter press valve numbering and valve positions.

#### Air control valves:

- A main air control valve regulates air delivery to the filter press (Valve G).
- A secondary air control valve regulates air delivery to the filter press for conducting air blow down (Valve F). Valve F is opened to conduct an air blow down event, once the filter press is full of sludge.

#### FILLING THE PRESS:

 The filter press pump (sludge pump) is operated to fill the press by opening the manual ball valve at the inlet to the AODD filter press pump and the main air inlet valve. The air supply to the AODD pump is delivered through a three- stage air supply. The three-stage controller provides a method to slowly coat the plates while minimizing the solids pressed through the filter press cloth covering the plates.



Figure 3. Filter press controls panel.

• The three-stage press system is started by turning the selector knob on the filter press panel to the "ON" position (Figure 4). A green light should illuminate indicating the press system is activated. The first timer will start delivering

air to the first stage. The filter press pump will operate for a period of six to ten minutes at the first stage pressure of 20 psi. The second timer will then deliver sludge to the press using the second stage for a period of up to two hours at a pressure of 60 psi. The third stage will deliver sludge to the filter press at a pressure up to 100 psi. When the filter press pump stalls between strokes for 60 seconds or more at its full set pressure, the filter press is full and the panel is turned off. A red light will illuminate indicating the press is full.



Figure 4. AODD filter press pump.

• Make sure the press does not run out of sludge in the source tank. If the tank is emptied, stop the press by closing the ball valve in the airline at the pump.

# **BLOWDOWN:**

- When the press is full, it will still contain considerable water in the plate channels and the cake. A compressed air blowdown valve located off the upper left water removal line is used to blow this water from the press. The valves are set to the 'blowdown' position: A – closed, B – open initially then closed, C – open, D – open, E – closed, Fopen, and G-open (Figure 3).
- The air ball valve (F) is opened slowly allowing air to enter the sludge inlet line at the end of the press to activate press blowdown. Liquid will first be blown from the press, followed by an air-liquid mixture. Watch the end of the discharge line. Once water stops exiting the discharge line, the blowdown operation is complete. Close the ball valve in the air line to stop the blowdown process.
- **NOTE:** This press is equipped with two additional valves in the filter press discharge lines. These valves are located to stop discharge from the top two ports (A, B) of the blowdown manifold (the blowdown manifold originates at the four corners of the plates on the inlet/outlet end). Air will preferentially exhaust from the upper two ports and will

not blow down the cake in the lower part of the press when a filter press is not filled completely with sludge. Closing the two valves after several minutes during blowdown will ensure the lower portion of the cake will be properly blown down. Re-open the top two valves for several minutes near the end of the blowdown cycle.

• To use the valve B initiate blowdown normally. Close the valve in the blowdown manifold after several minutes. Open the valve for several minutes when blowdown is nearly complete.

#### **EMPTYING THE PRESS:**

- Make sure that blowdown is complete and the blowdown air valve and sludge inlet valves are closed.
- Open the Press by turning the OPEN/CLOSE valve to the OPEN position (Figure 2).
- Wait for the cylinder to reach its fully retracted position. Then, turn the ON/OFF knob to the OFF position.
- Grasp the handles on the plastic head plate and pull it all the way to the pressure plate.
   A section of the filter cake will be exposed.
- Using a **plastic spatula** (never metal), loosen the cake from the plate and let it fall into a roll off. Then move the second plate, etc. Try to pry, rather than scrape, the sludge cake from the plates. **BE CAREFUL TO NOT DAMAGE THE PLATE CLOTH.**
- When all the cake has been removed, clean the O-ring gasket areas thoroughly with a brush or paper towels and return the plates to the tail plate end, aligning them as you go.
- See CLOSE PRESS section, above for the next cycle.

#### **ROLL-OFF OVERVIEW:**

Sludge is processed from the treatment system using a 25 cubic foot filter press. The dried solids are removed from the treatment system using a roll-off for disposal. The roll-off box is transported to and from the site using a truck. An empty roll-off is placed at the building door area, approximately 1/3 to 1/2 of the roll-off is expected to be placed into the building by the truck driver.

A metal guide rail system is mounted on the floor inside the building. This allows the truck driver to have a guide for placing the roll-off. In addition, the guide rail will ensure the roll-off will move in a straight path and not into the metal structure and catwalk when the winch is in use.

A winch, located inside the building and manually operated, is used to pull the roll-off into the building. The roll-off will be filled with dried solids. As the roll-off is filled with dried solids the operator will use the winch to pull the roll-off further underneath the filter press to evenly fill the roll-off.

A full roll-off is removed from the building by using a truck. The truck will connect to the roll-off and pull the roll-off out of the building before loading the roll-off onto the truck for disposal. The guide rails will ensure the roll-off is pulled out of the building without damaging the metals structure or building.

#### SLUDGE MANAGEMENT:

- Dried sludge will leave filter press and drop into a section of a roll-off
- Filling the roll-off evenly requires the use of a winch, controlled by the operator
  - Winch is mounted inside the building on the concrete floor and filter press frame structure
- As roll-off is filled, the winch is activated by the operator and will pull the roll-off towards the filter press to evenly distribute dried sludge to fill the roll-off
- Estimated weight of roll-off when full is 25,000 pounds

#### **ROLL-OFF OPERATIONS:**

- A roll-off will be delivered to the site using a truck
- Truck will place the back third or half of the roll-off into the building
  - Concrete pad must be flat for roll-off to travel
- To accomplish this, an unobstructed area is required outside the building door
  - Approximate unobstructed area is 20' wide by 40' long
- Roll-off is then pulled into the building using the winch and a guiderail track
  - o Guiderail track installed on the floor to ensure roll-off is pulled straight
- A full roll-off is removed from the building using a roll-off truck by pulling the roll-off out
  of the building for transport and disposal

#### **REFRESHING THE CLOTHS:**

- After a period of time, the cloths will begin plugging with fine material and performance will deteriorate.
- Traditionally, the cloth would be cleaned by circulating hydrochloric acid through the press. Equivalent results can be obtained by drying the plates completely. With the press open and sludge removed, spread the plates out evenly so that air can circulate between them. A fan can help speed drying.
- Leave the plates open until dry, then the press is ready to close and use. A brush with soft plastic bristles can be used to wipe dried material from the press.

#### **RESTARTING:**

- If the press cycle has been interrupted for less than a day before the press was filled it can be restarted by checking valve positions, then resetting and re-starting the cycle.
- If it has been more than a day **OR** if the press has been blown down, re-start at the lower (20psi) pressure to re-coat the plates where cake shrinkage has exposed the cloth.

To remove heavy particles of rust or scale that may slough off of the treatment plates and that are not entrained in the water stream, a sub-system called "Scale Purge" is occasionally energized to remove heavy solids from the bottom of the treatment reactor. The time is adjustable and the PLC manages this cycle. The cycle time for scale purge is set by the operator based on needs for this specific installation. The scale system provided will include two basket strainers, two air-operated valves, the 1.5" AODD pump, and the interconnecting plumbing. The scale purge system requires no chemicals. The scale purge cycle can be manually engaged to remove water from the reactor vessel for maintenance and inspection activities.

#### 2.1.5 Treated Water

Treated water will flow by gravity from the clarifier to a post treatment tank. The water will be pumped from the post treatment tank to multi-media filters and bag filters for final clarification before being pumped to the infiltration basin.

# Multimedia (Sand/Anthracite) Filter System

- The multimedia filter system includes a packaged control system.
- Backwash is required when a pressure differential of 10 PSI is seen between the inlet and
  outlet pressure readings. This occurs when the media has been dirtied by solids in the
  process line. Backwashing lifts the media bed allowing solids to be washed from the
  media.
- The media filter controller sends one discrete signal to the PLC to indicate a backwash is required. The PLC returns a discrete signal to indicate the Media system may perform a backwash.
- Pressure differential transmitter provides 4-20mA signals for pressure drop across the media filters. Pressure drop will be recorded by the HMI.
- Backwash cycles through a single pod at a time. Water from the post treatment tank that has been through "non-backwashing" sand filters is used to backwash. Pneumatically actuated valves close the influent line into the pod being backwashed and allows water to flow backwards from the discharge piping of the other pods. When the signal is received to backwash, the skid will automatically cycle through all pods.
- When signaling to "backwash now", the PLC will hold the post treatment pump at a constant speed.
- Pump speed is held for a specified time to allow sand filter controller to complete a backwash cycle.

- Before, initiating a backwash:
  - The level in the Post Treatment Tank must be above a prescribed level. If level is below the prescribed level, the post treatment pump is stopped until the prescribed level is reached.
- Backwashed water is sent to the Equalization Tank.

# Post-Treatment Bag Filters

- One (1) micron bag filters
- Pressure differential transmitter provides 4-20mA signals for pressure drop across the bag filters. Pressure drop will be recorded by the HMI.
- Bag change is required when a pressure differential of 10 PSI is seen between the inlet and outlet pressure readings.
- System presents an alarm (and continues to treat) when pressure drop across bag filters exceeds preset limit.
- Manual switch from one bag filters to other bag filter.
- Bag filter units are plumbed in parallel allowing bag of one unit to be changed during system operation.

#### 2.2 Controls

An enclosure panel contains the control and electrical system. A Programmable Logic Controller (PLC) serves as the controller for the treatment package. A touch-screen OIT provides the operator with easy monitoring of operating conditions and control of the system. All components controlled can be run in either Automatic or Manual mode.

Remote access is being implemented through a cellular modem. This remote access feature allows customer connection to the treatment system remotely. The access allows control of all outputs and to remotely monitor system operating status. Valves do not have feedback switches.

The EC system can be set by the operator in either Manual, Off, or Automatic mode. When the operator enables automatic mode, the EC system will function on-off in response to the liquid level in the equalization vessel. A level indicating transmitter in the equalization vessel supplies a 4-20mA signal to the PLC representing the level in the equalization vessel. This signal will be calibrated to start and stop the treatment system at High and Low level set points and sound alarm at High-High and Low-Low conditions.

While operating, the PLC monitors these conditions and shuts the package down if parameters are outside of range:

• Treatment power delivered to the reactors: If the power decreases below a preset level, the PLC shuts down the system and indicates a treatment power fault.

- Wastewater flow into the reactor: If the flow decreases below a preset level, the system shuts down and a fault is indicated.
- Wellfield valve will be shut upon loss of power and after EQ Hi-Hi level has alarmed for a specified time.

All sub-systems (rectifier, control power...) are internally fused on all legs. Motors are protected by fuses and/or overload relays.

# 2.3 Structure

The United Rentals Hi-Flo Treatment Vessel and support stand is mounted in a heated and ventilated building. A structural steel platform is built around the reactor to allow personnel easy access and viewing of the treatment process. Guardrails are used where required.

The treatment power rectifier cabinets are mounted in the same building adjacent to the system.

# 2.4 Hoist

To facilitate changing of the reactor cartridges, a hoist trolley monorail system is suspended above the reactors on their centerline. A 3-ton electric hoist (4.9 hp motor) with tractor (1/8 hp motor) is used by an operator to lift the treatment cartridge from the reactor vessel, move it to the reactor rebuild area, and lower it onto a cartridge pan. The operator uses this same hoist to re-install a fresh cartridge into the reactor. Hoist system is a free standing monorail system over the treatment vessel support structure.

# **Section 3: Equipment Description and Specifications**

Unless otherwise stated:

- Valves are two-way schedule 80 PVC ball valves
- Plumbing is Schedule 80 PVC
- Valves are manual and pneumatic
- Flanged connections are 150# ANSI
- Electrical and control conduit is employed where necessary (PVC).
- Pneumatic systems are aluminum pipe and air pressure hose.

This is an overview of the equipment to be supplied by United Rentals.

# 3.0 Summary of Supplied Equipment

The table below provides a summary for the equipment provided as part of the water treatment system. Greater discussion regarding the components is provide in other sections of this specifications document.

System Component	Manufacturer	
PLC & Controls	Siemens	
Sensors	Endress + Hauser, George Fischer	
pH Controller	Endress + Hauser	
Tank Mixing	Baldor, Dodge Gear, United Rentals	
Rectifiers	Aldonex	
Air Compressor	Kaeser	
Chemical Metering Pumps	Pulsatron	
AODD Pumps	ARO	
Electric Pumps	Gorman-Rupp, Grundfos, Zoeller	
Plumbing	United Rentals	
Hoist	Bay Area General Crane Service Co.	
Electrocoagulation Reactors	United Rentals	
	LF Manufacturing, Regal Plastics, Snyder,	
Process Tanks	ChemTainer	
Clarifier	Pan American	
Solids Dewatering	Evoqua, Gilmore-Kramer, United Rentals	
Multi-Media Filters	Yardney	
Bag Filters	Rosedale	
Catwalk	United Rentals	

# 3.1 PLC and Controls

- PLC controller with digital and analog modules programmed to monitor and control the United Rentals Electrocoagulation wastewater treatment system. Controls include tank level sensing, pump control, rectifier control, reactor auto scale purge, solids management, filter press availability controls, air system controls, and alarms.
- Touchscreen operator interface panel for ease of operator control and maximum functionality mounted in a control cabinet.
- Controls for alarm/start-stop notification via cell phone, or web e-mail
- Main electrical control panel:
  - o 80 Amp/480 Volt/3 phase
- Free standing skid mounted enclosure
- Air Cooled
- PLC controls
- Touch Screen Panel (Operator Interface Terminal, OIT)
- Treatment Volt meter
- Treatment Ammeter
- Various parameter alarms
- Fused field control input device connections
- Fused field outputs (control and power)
- Motor starters with overload relays as needed
- Electrical/air solenoids to operate air-operated valves
- Data logging with graphical data display, temporary storage

# 3.2 Sensors

# 3.2.1 Level Switch High (LSH)

- Madison M8000 Miniature Plastic float switch
- Alarm PLC of Hi-Hi tank level
- Stem Material: Polypropylene
- Float Material: Polypropylene
- Max Temperature: 105° C
- Max Pressure: 100 PSIG
- Float SG: 0.80 SG
- Switch Rating: 30 Watt, 240V max (AC/DC), SPST

# 3.2.2 Level Switch Low (LSL)

- Model: P7300
- MFG: Advanced Control Technology
- 73 Series Plastic paddle switch to alarm PLC of Low tank level
- Switch differential: 90°

- Housing: Polypropylene
- PVC Jacketed Cable

# 3.2.3 Level Indicating Transmitter (LIT)

- MJK Expert™ 2100 Hydrostatic Level Transmitter (0-15 ft)
- Piezoresistive measuring device used to monitor tank levels
- Nominal measuring range (ftWG): 0-15 ft.
- Measuring Principle: Piezoresistive
- Min. programmable range: 0-6 ft.
- Max programmable range: 0-36 ft.
- Max overpressure: 50 psi
- Temperature range: 15-150 °F
- Measurement accuracy: Better than +/- 0.5% FS @ full temperature range
- Materials:
  - o Housing: PP
  - Diaphragm: Stainless steel (AISI 316L)
- Supply Voltage: 10-30 V DC (12-30 V DC for cable lengths above 315 ft)
- Output signal: 2-wire 4-20 mA (passive transmitter)

# 3.2.4 pH Probe

- CPF81D Orbipac pH probe by Endress + Hauser
- The membrane glass of the electrode supplies an electrochemical potential which is dependent upon the pH value of the medium. This potential is generated by the selective penetration of H+ ions through the outer layer of the membrane. An electrochemical boundary layer with an electric potential forms at this point. An integrated Ag/AgCl reference system serves as the required reference electrode. The transmitter converts the measured voltage into the corresponding pH value using the Nernst equation.
- pH is monitored and adjusted in the EQ Tank and Defoam Tank.
- Storage Temperature: 32-120 °F
- Process Temperature: LH 32-230 °F or NN 32-170 °F
- Process Pressure: 15-145 psia at 176 °F
- Glass Impedance: 150 MΩ at 77 °F
- Minimum Conductivity: 50 μS/cm
- Weight: 0.26-0.33 lbs
- Materials
  - Housing, electrode shaft: PPS
  - o Electrode: Lead-free membrane glass, suitable for process applications
- Process Connection: ¾" NPT

• Double chamber reference system: KNO<sub>3</sub> AND KCI/AgCl

#### 3.2.5 Conductivity Probe

- Condumax CLS21D Conductivity Probe by Endress + Hauser
- Conductivity of liquids is determined with a measuring arrangement where two
  electrodes are located in the medium. An alternating voltage that causes a current to
  flow through the medium is applied at these electrodes. The electrical resistance, or its
  reciprocal value conductance G is calculated based on Ohm's law. The specific
  conductance κ is determined from the conductance value using the cell constant k,
  which depends on the sensor geometry.

#### 3.2.6 Flow Meter

- George Fischer Signet 2551 Magmeter
- PN: 3-2551-P0-42
- Quantity: (3)
- Sends 4-20mA signal to PLC to measure flow in pipe
- Pipe size range: DN15 to DN 300 (0.5 in. to 12 in.)
- Flow Range
  - o Minimum: 0.05 m/s (0.15 ft/s)
  - Maximum: 10 m/s (33 ft/s)
- Linearity: ±1% reading plus 0.01m/s (0.033 ft/s)
- Repeatability: ±0.5% of reading @ 25°C (77°F)
- Minimum Conductivity: 20 μS/cm
- Power Requirements:
  - o 4 to 20 mA: 21.6 to 26.4 VDC, 22.1 mA max.
  - o Frequency: 5 to 26.4 VDC, 15 mA max.
  - Digital (S3L): 5 to 6.5 VDC, 15 mA max.
- Reverse polarity and short circuit protected

# 3.2.7 Pressure Differential Switch

- Series 629 Dwyer Pressure differential switch
- Sends signal to the PLC that the influent and effluent lines on the bag filters have a pressure differential of 10 PSI and require bags to be changed
- Working Pressure: 100 PSI
- Accuracy: ±0.5% FS
- Temperature Limits: 0 to 200°F
   Output Signal: 4 to 20 mA

# 3.3 pH Controller

• Liquiline CM444 by Endress + Hauser

- Multi parameter transmitter/controller for monitoring and controlling processes in industry and the environmental sector
- Supply Power: 100 to 230 V AC ± 15 %, 50/60 Hz

# 3.4 Tank Mixing

• Mechanical mixing will take place in the Equalization, defoam, and flocculation process tanks as well as the polymer tank. The mixers are used to help with pH adjustment and prevent stratification in the tanks.

# 3.4.1 Mixer motors

- Baldor motors used to drive prop
- 1.5 HP Equalization tank agitator motor:
  - o Model: CM 3554
  - o Power Supply: 208-230/460 3-ph
  - o Amps: 2.5 FLA
  - o RPM: 1800
- 1.5 HP Defoam tank agitator motor:
  - o Model: CM 3554
  - o Power Supply: 208-230/460V 3-ph
  - o Amps: 2.5 FLA
  - o RPM: 1800
- 1.0 HP flocculation tank agitator motor:
  - o Model: CM 3538
  - o Power Supply: 230/460V 3-ph
  - o Amps: 1 FLA
  - o RPM: 1800
- 0.25 HP Polymer Tank Agitator motor
  - o MFG: Leeson
  - Power Supply: 115/208-230 V
  - o Amps: 5.4/2.4-2.7 FLA
  - o RPM: 1725 RPM

# 3.4.2 Gear Boxes

- Defoam/EQ
  - Dodge Tigear-2 reducers Size 20
  - Part Number: 20Q05H56
  - o Ratio: 5
  - o Output RPM: 350
  - Mechanical Input HP: 3.47

Output Torque: 581 lb in.

Shaft Position: Hollow

#### Flocculation

Dodge Tigear-2 reducers – Size 17

o Part Number: 17Q05H56

o Ratio: 5

o Output RPM: 350

Mechanical Input HP: 2.59
 Output Torque: 430 lb in.
 Shaft Position: Hollow

# 3.4.3 Shaft and Propeller

Appropriate shaft lengths and propeller sizing to promote tank mixing

- EQ Tank:
  - o Propeller: One (1) 12" right handed (upward mixing) stainless steel propeller
  - Shaft: 1.25" diameter x 118" long stainless steel shaft
- Defoam Tank:
  - Propeller: One (1) 6" left handed (downward mixing), stainless steel propeller,
     one (1) 12" right handed (upward mixing), stainless steel propeller
  - Shaft: 1.25" diameter x 88" long stainless steel shaft
- Flocc Tank:
  - o Propeller: One (1) 7" right handed (upward mixing) stainless steel propeller
  - Shaft: 1.00" diameter x 72" long stainless steel shaft
- Polymer Tank:
  - o Propeller: One (1) 3" right handed (upward mixing) stainless steel propeller
  - o Shaft: 0.50" diameter x 48" long stainless steel shaft

#### 3.4.4 Aerators

- Model: FlexAir 12" High Capacity Aeration discs
- Utilized in the Equalization and Defoam tanks
- Peak Airflow: 18 SCFM
- Design Airflow: 2.0-13.0 SCFM
- Diffuser Diameter: 13.8"
- Active Surface Area: 0.73 FT<sup>2</sup>
- Coupler: ¾" MNPT
- Diffuser Membrane Material: EPDM

# 3.5 Rectifiers

- MFG: Aldonex
- Model No: T-448-20CR-CCV-APR-IOS
- A Silicon-Controlled Rectifier (SCR) serves to convert AC power to DC power for the reactor. The DC power operates at or below 48 volts, which allows the operator to be in direct contact with the electrical supply based on OSHA specifications (less than 50 VDC).
- Output Rating: 2000 Amps @ 48VDC Max Voltage output
- Rectifier Elements: Utilizes multi-cell semiconductor diode assemblies. Diode assemblies
  are oversized by approximately 45% or better in order to withstand any excessive surge
  in current.
- Power Transformer: Transformer core consists of steel laminations of grain oriented silicon steel. The Primary and Core are separated by a solid preformed silicon impregnated class H insulation coil form, to minimize the possibility of Primary to Core short circuits. The transformer has heavy duty solid copper buss bar secondary windings for greatest rigidity.
- Current in windings limited to a density of 600 circular mils per ampere.
- Complete transformer assembly is double dipped in the highest quality insulating varnish, resulting in quiet units which will withstand the typical plating shop environment and operate cool under a full load.
- Controls: Main Starter, Motor Starter, Control Step Down Transformer, SCR Gate Drive, and V/C Control Board are located behind an Easy-Access Panel. Control equipment is kept dust proof and entry of potentially corrosive moisture is minimized.
- Overload relay on main contactor
- Treatment Power Busses and wiring
- Independent Constant Current and Constant Voltage control with automatic crossover provide + 0.5% voltage and current regulation.
- Soft start allows the power delivered to the load to be brought up slowly when the unit is turned on. Prevents possible clearing of fuses when the unit is turned on due to high current surge.
- Current Trip (limit) Circuitry protects the Power Supply against direct short circuit of the
  output buss. When a continuous short-circuit occurs, the trip circuitry shuts down the
  SCR Firing Board, thus protecting the Diodes, SCR's, and Power Transformer from
  damage.
- Direct process control with 4-20MA signal input for automatic operation.
- Primary SCR Design, incorporates SCR's connected in inverse parallel, (back to back), configuration and placed between the AC Mains and Power Transformer.
- Secondary SCR Design, incorporates the SCR's as rectifying elements, changing secondary AC Voltage and Current to DC Voltage and Current.

- All ALDONEX, SCR POWER SUPPLY Components are designed to operate continuously at 50°C maximum. Operating below this will insure a Longer Life Cycle.
- All ALDONEX TAP SWITCH POWER SUPPLY Components are designed to Operate Continuously at 50°C Maximum. Operating below this will insure a Longer Life Cycle
- Reactor Power Monitor: If reactor treatment power supply voltage drops below an adjustable voltage set-point the PLC shuts down the reactor package and indicates treatment power failure on the control panel.

# 3.6 Air Compressor

- Kaeser Air compressor used to supply air for automated treatment system valves and for air operated dual diaphragm pumps
- Model: SK 20
- Dryer Model: Integral
- Capacity: 88cfm at 125 PSIG
- Drive Motor: 20 HP
- Controller: Sigma Control 2™
- Electrical: 480VAC, 60 Hz, 3-phase
- Cooling Method: Air-cooled
- Air Receiver Size: 92.5 GAL
- Sound level: 68 dB(A)

# 3.7 Chemical Metering Pumps

• Metering pumps are used to convey chemical to process tanks for treatment. Pumps are chemical and dose specific.

# 3.7.1 Calcium Chloride Pump

- LMI Excel XR 5.6 GPH electronic metering pump
- Max Flow: 5.6 GPH
- Lift: 13.1'
- Max Pressure: 175 PSIG
- Power Input: 120 VAC
- Average Current Draw: 0.42 A
- Head and Materials: PVDF
- Seats Materials: PTFE
- Diaphragm: PTFE/PVDF
- Ball Materials: Ceramic
- Connection Type: 3/8" PE Tube

# 3.7.2 Sulfuric Acid Pump

• LMI Excel XR 5.6 GPH electronic metering pump

• Max Flow: 5.6 GPH

• Lift: 13.1'

Max Pressure: 175 PSIGPower Input: 120 VAC

Average Current Draw: 0.42 AHead and Materials: PVDF

Seats Materials: PTFEDiaphragm: PTFE/PVDFBall Materials: Ceramic

• Connection type: ½" NPT/BSP

# 3.7.3 Polymer Pump

Pulsatron LPH6 PTC 120 GPD electronic metering pump

Max Flow: 120 GPDMax Pressure: 50 PSIG

Power Input: 115 VAC/50-60 HZ/1 ph
 Average Current Draw: 1.0 A @115 VAC
 Head and Fittings Materials: PVDF (Kynar)

Seats Materials: TFEBall Materials: Ceramic

# 3.8 AODD Pumps

MFG: ARO

Model: 06-PD15P-FPS-PTT

- ARO diaphragm pumps are pneumatically powered positive displacement pumps used in the solids removal and solids dewatering processes
- ARO 1.5" Air Operated Double Diaphragm Pump

• Air Inlet Pressure Range: 20-120 PSI

Maximum Flow Rate: 123.1 GPM

Displacement per Cycle @ 100 PSI: 0.617 GAL

Maximum Particle Size: ¼"

# 3.8.1 Scale Purge Pump

Quantity: (1)

• Removes the scale buildup from the bottom of the reactor vessel sumps. One scale purge pump is used for multiple sumps in a sequential operation. This pump is also

used to drain the Defoam, Flocculation, and Post Treatment tanks for periodic maintenance.

# 3.8.2 Filter Press Sludge Pump

- Quantity: (1)
- Removes the settled sludge from the bottom of the sludge thickener and delivers it to the filter press for dewatering.

# 3.8.3 Clarifier Sludge Pump

- Quantity: (1)
- Removes the sludge accumulation from the bottom of the clarifier and delivers it to the sludge thickener tank.

# 3.9 Electric Pumps

# 3.9.1 Electrocoagulation Feed Pump

- Model: Gorman-Rupp 490B-98 3 HP
- Quantity: (2)
- Gorman-Rupp duplex centrifugal pump system with variable frequency drive for feeding EC reactors from the EQ Tank.
- Power Supply: 230/460V 3-ph
- FLA: 8/4
- Housing Material: Cast Stainless Steel
- Seal Material: Viton
- Max Head: 149 FT. (65 PSI)
- Max Flow: 118 GPM

#### 3.9.2 Post Electrocoagulation Pump

- Model: Gorman-Rupp 490B-98 3 HP
- Quantity: (2)
- Gorman-Rupp duplex centrifugal pump system with variable frequency drive for pumping from Post EC tank to downstream processing
- Power Supply: 230/460V 3-ph
- FLA: 8/4
- Housing Material: Cast Stainless Steel
- Seal Material: Viton
- Max Head: 149 FT. (65 PSI)
- Max Flow: 118 GPM

# 3.9.3 Post Treatment Pump

- Model: Grundfos CRI 10-6
- Quantity: (2)
- Grundfos duplex Centrifugal pump system with variable frequency drive for feeding filtration components after processing through the Defoam, Flocculation, Clarifier, and Post treatment tanks
- Vertical, multistage centrifugal pump with inlet and outlet ports on same the level (inline). Pump materials in contact with the liquid are in stainless steel. A cartridge shaft seal ensures high reliability, safe handling, and easy access and service. Power transmission is via a rigid split coupling. Pipe connection is via combined DIN-ANSI-JIS flanges.
- The pump is fitted with a 3-phase, fan-cooled asynchronous motor

Motor Power: 5 HPSupply Power: 480VMax Flow: 69 GPM

Suction: 2" ANSI 300# FlangeDischarge: 2" ANSI 300# Flange

# 3.9.4 Water Safety/Wash Water Pump

• Quantity: (1)

- The Grundfos CMBE TWIN Booster is a compact two-booster system for water supply in
  domestic and commercial applications. The integrated speed controller allows the CMBE
  Booster to maintain constant pressure in the pipe system. The cascade control ensures that
  the performance of the CMBE Booster is automatically adapted to consumption by switching
  pumps on or off and by changing the speed of the pumps in operation.
- The CME Booster consists of 2 units of CMBE Booster which each include
  - 5-way valve
  - expansion tank
  - pressure gauge
  - Pressure sensor

Motor Power: 2 HP

• Supply Power: 1P 220V, 18.

Max Flow: GPM

Max Pressure: 145 PSI

# 3.9.5 Sump Pump

Zoeller sump pump for building containment sump

• Model: N140

Supply Power: 115V

Amps: 12 ATDH: 20 FT

Flowrate: 66 GPM

# 3.10 General Plumbing

# 3.10.1 Water and Sludge Lines

- Plumbing will be done by United Rentals employees. Plumbing will include pneumatic actuated and manually actuated valves for process control.
- SCH 80 PVC
- WeldOn 711 PVC Glue
- WeldOn P70 Primer
- EPDM/Viton seals in valve and union fittings

# 3.10.2 Chemical Plumbing/Tubing

Plastic tubing will be supplied for the polymer and calcium chloride metering pumps.
 This tubing is specific to the chemical and to the size of the pump. Chemical tubing connections are made using compression fittings of the appropriate material. The sulfuric acid will be hard plumbed using SCH 80 CPVC.

# 3.10.2a 98% Sulfuric Acid Plumbing

- Size: Double wall ½ " ID delivery pipe with 2" ID containment pipe; ½" ID in the chemical tank
- Material: CPVC
- Temperature Range: 32° 200° F
   Maximum Pressure: 850 psi @ 73° F
- Clarity: Opaque

# 3.10.2b 9901 NALCO Polymer Tubing

- Size: 3/8" ID x ½" OD
- Material: PP
- Temperature Range: 40° 200° F
  Maximum Pressure: 120 psi @ 72° F
- Clarity: Semi-Clear

# 3.10.2c Calcium Chloride Tubing

- Suction: PE ¼" x 0.38" tubing
- Discharge: Reinforced PVC ¼"x ½" tubing

# 3.10.3 Primary Air Lines

- Aluminum tubing ran from compressor branches to the filter press and runs on to the controls skid
- TransAir® Aluminum Pipe
- Size:
  - o From compressor up to filter press: 25 mm,
    - Kaeser Compressors Part No.: AN66022500
  - From filter press to controls skid: 17 mm
    - Kaeser Compressors Part No.: AN1004A1704
- Max Working Pressure: 232 PSI from -4°F to +115°F
- Working Temperature: -4° to +140° F

# 3.11 Influent Plumbing

- Plumbing allows for wetlands bypass into EC system. All water pumped from wells is run through flowmeter. Wetlands bypass and post treatment divert are automated.
- Plumbing into the EC building will be 3" pipe but will be reduced to 2"

# 3.11.1 Wellfield Water Transfer Piping

- One each Inlet flange 2" 150# ANSI flange customer connection from extraction wells
- System isolation valve, manual
- Flow Shut Off 2" fail close valve, air-operated
- Flow Monitoring Pipe Section: Sch. 80 PVC pipe, 2" flange, with fitting for FIT-1
- Saddle to connect flow monitor section with inlet flange
- Flow Indicating Transmitter, 4-20mA
- Sample port: ½"
- Piping to bypass the constructed wetlands to equalization tank
- Outlet flange 2" 150# ANSI flange customer connection

# 3.11.2 Inlet piping to EC Reactors

- System isolation valve, manual
- Flow Shut Off 2", air-operated
- Variable Frequency Drive output (4-20ma)
- Flow Monitoring Pipe Section: Sch. 80 PVC pipe, 2" flange, with fitting for flow meter (FIT-1)
- Saddle to connect flow monitor section with inlet flange
- Flow Indicating Transmitter, 4-20mA
- Sample port, ½"

# 3.12 Emergency Wash Station

# 3.12.1 EEmax Tankless Water Heater

- Model: AP063480 EFD N4
- "EFD": Intended for Emergency Eye, Face & Drench showers
- N4 Powdered coated steel enclosure
- GFCI
- Min. Operating Pressure: 35 PSI
- Max Operating Pressure: 150 PSI
- Optimum Operating Pressure: 60-90 PSI
- Max outlet temperature: 90 °F
- Power: 76 A/ph.
- Turn on GPM: 2.5 GPM
- Water Hammer arrestor in-line

#### 3.12.2 Guardian Safety Station

- Model: GFR3100
- Heat traced unit intended for cold weather use down to -40 °F
- Self-regulated heating cable with external termination guards.
- Thermostat activates below 75 °F
- Power: 120 VAC
- Single flow throw switch for remote sensing
- 1.25" FNPT top inlet

# 3.12.3 Heat Trace

- 2" PVC (Safety Shower/hose bib water)
  - Thermon BSX 8-1 Self Regulating Heating Cable
  - Watt Density: 8 W/FT @ 50°F
  - Supply voltage: 120 VAC
  - Indoor and outdoor circuits on individual thermostats
- 1/2" PVC (Calcium Chloride)
  - Thermon BSX 5-1 Self Regulating Heating Cable
  - Watt Density: 5 W/FT @ 50° F
  - Supply voltage: 120 VAC

# 3.13 Insulation

- Material: Fiberglass
- R-Value: 4.3
- Thickness: 1"

#### 3.14 Hoist

- Bay Area Crane Services' I beam supported mono-rail system for overhead cartridge change and removal. Multi speed lift and travel functions with wireless controller for user friendly operation
- Crane Type: Freestanding Monorail Crane System(CT)
- Runway Capacity: 6,000 lbs.
- Monorail Overall Length: 37'-6"(OAL)
- CL to CL Baseplates(Length): 19'-0"(CL to CL) & 16'-6"(CL to CL)
- Number of Support Columns: (6)
- Hoist: Electric Chain Hoist
- Hoist Mfg.: Gorbel
- Hoist Capacity: 6,000 LB
- Lifting Speed: Dual Speed(12/3 fpm)
- Trolley Speed: Dual Speed(78/19 fpm)
- Crane Wireless Controls: Included with Spare Transmitter
- Supply Voltage: 480V, 3-phase, 60hz

# 3.15 Electrocoagulation Reactors

- Electrical busses for single configuration on each cartridge to bolt to rectifier busses
- Scale removal system with (1) sump each plus 2" air-operated valves and 1.5" AODD pump

# 3.15.1 Cartridge

- Lifting frame for cartridge change
- Four cartridge pans
- Four reactor treatment cartridges (Two for each reactor unit, one spare unit per reactor unit)
- Four sets of steel and aluminum/Iron treatment plates
- The Treatment Reactor Cartridge is constructed of PVC or HDPE and is assembled with stainless steel bolts to allow repairs. Stainless steel straps around the cartridge allow for attachment of a lifting frame (included) so the whole cartridge can be removed and replaced easily and reliably. The treatment reactor plates in this reactor are in a parallel vertical arrangement in a cartridge that lifts in and out of the reactor vessel to facilitate plate replacement. A chain hoist is provided to facilitate the movement of and replacement of the treatment cartridges.

# 3.15.2 Vessels

- The Treatment Reactor Vessel is fiberglass and rests in a steel support structure.
- The reactor treatment vessels are molded from fiberglass along with the scale sumps to create one integrated unit.

- The purpose of the sumps is to catch the scale that sloughs off of the sacrificial plates and funnels it to a collection port so the scale can be removed during the descale cycle of the treatment system. Without the sumps to collect the scale, the plates can short together from the scale staying between the plates creating a zone in the reactor where there will be no treatment thus reducing the systems effectiveness.
- Periodically, pneumatic valves and an AODD pump are energized to remove residuals from the sumps. Electrochemical reactions are maintained through protection of the reactive plate surfaces.
- All plumbing connections are made with ANSI Class 150 flanges.
- 3" wide foam rubber gasket where the reactor cartridge will sit creating a seal that forces the untreated water to rise up through the reactor for treatment.

#### 3.15.3 Plate Pack

- The Reactor Treatment Plates are ¼" thick metal and are energized to serve as the electrodes in the reactor. For this application, the power plates are carbon steel and intermediate plates are two rows of carbon steel and the top row aluminum. The plates must be flat to maintain the separation distance between the electrodes in the reactor.
  - o 24" x 38" Steel power plates (16)
  - o 24" x 10.3" Steel intermediate plates (60)
  - o 24" x 10.3" Aluminum intermediate plates (30)

### 3.15.4 Reactor Leads

- Quantity: (4) per rectifier/reactor pair
- Reactor leads are cable that run from the rectifiers to power plates of EC reactors
- CCI Royal 4/0 Cable
- Stranding: 532/24
- Voltage Rating: 2000V rms Max
- Temperature Range: -40°C to 90°C
- Net Weight: 753 lb per 1000 feet

### 3.15.5 Hayward Strainer Baskets:

- Model: SB1300F
- Quantity: (2)
- Hayward Strainer Baskets are used to filter out solids pumped from reactor vessel sumps. The strainers have manual and pneumatic ball valves.
- Material: SCH 80 PVC
- Seal Material: FPM
- Size: 3"
- Pressure Rating: 150 PSI @ 70° F Non-Shock

#### 3.16 Process Tanks

### 3.16.1 Equalization (EQ) Tank

- Quantity: (1)
- Raw water flows into the EQ Tank from the KM Lift Station. The water will be dosed with calcium chloride and sulfuric acid. This tank serves as a mix tank and buffers the water before it enters the EC reactors. The EQ tank contains a mixer and aerator to ensure mixing of chemical and inhibit stratification.
- One hour holding capacity
- Volume: 6,463 GAL
- Vertical FRP tank for Above Ground service Open top, Flat bottom
- 10'-0" dia. X 11'-0" straight sidewall length
- Gray gel coat exterior
- Top 3" inside flange lip
- (2) 2" FRP threaded half couplings
- 4" FRP threaded half coupling
- Galvanized lifting lugs
- Hydro Test Chop Liner 1/8" VE liner
- Service acid water, waste water,
- Ambient temperature, atmospheric pressure
- With hold-down lugs, wind rated to 130 mph under all fill conditions.

### 3.16.2 Defoam Tank

- Quantity: (1)
- After undergoing the EC reactions, the Post-EC pumps send water into the Defoam Tank.
  The defoam tanks serve to remove gas from the solids generated in the EC reactions. A
  second pH adjustment will be performed in the Defoam Tank as needed. After passing
  through the defoam tank, the water gravity flows into the floc tank. This tank contains a
  mixer and aerator to prevent stratification.
- Volume: 6,463 GAL
- Vertical FRP tank for Above Ground service Open top, Flat bottom
- 10'-0" dia. X 11'-0" straight sidewall length
- Gray gel coat exterior
- Top 3" flange lip
- (2) 2" FRP threaded half couplings
- (1) 4" FRP threaded full couplings
- (1) 6" FRP threaded full couplings
- (2) Galvanized lifting lugs
- Hydro Test Chop Liner 1/16" ISO liner

- Service: Waste water
- Ambient temperature, Atmospheric pressure
- With hold-down lugs, wind rated to 130 mph under all fill conditions.

#### 3.16.3 Floc Tank

- Quantity: (1)
- After passing through the Defoam Tank, the water gravity flows into the Floc Tank. The
  water will be dosed and mixed with polymer to aid in floc formation with the goal of
  solids removal in the clarifier. After polymer treatment, the water will flow into the
  Clarifier. This tank will contain a mixer to assist in floc formation.
- Volume:3,760 GAL
- Vertical FRP tank for Above Ground service, Open top, Flat bottom
- 8'-0" dia. X 10'-0" straight sidewall length
- Gray gel coat exterior
- Top 3" flange lip
- (2) 2" FRP threaded half couplings
- (1) 4" FRP threaded full couplings
- (1) 6" FRP threaded full couplings
- (2) Galvanized lifting lugs
- Hydro Test Chop Liner 1/16" ISO liner
- Service: Waste water
- Ambient temperature, Atmospheric pressure
- With hold-down lugs, wind rated to 130 mph under all fill conditions.

#### 3.16.4 Post Treatment Tank

- Quantity: (1)
- Clarified water from the Clarifier will gravity flow into the Post-Treatment Tank prior to filtration. This tank serves as a buffer for automation of the post-treatment pumps.
- Volume: 1,057 GAL
- Vertical FRP tank for Above Ground service, Open top, Flat bottom
- 6'-0" dia. X 5'-0" straight sidewall length
- Gray gel coat exterior
- Top 3" flange lip
- (2) 2" FRP threaded half couplings
- (1) 4" FRP threaded half coupling
- Galvanized lifting lugs
- Hydro Test Chop Liner 1/16" ISO liner
- Service: Waste water

- Ambient temperature, Atmospheric pressure
- With hold-down lugs, wind rated to 130 mph under all fill conditions.

### 3.16.5 Sludge Thickener

- Manufacturer: Snyder Industries Inc.
- Tank Model: 5100Stand Model: 79400
- Quantity: (1)
- Sludge from the Clarifier will be pumped into this cone bottom tank. The sludge will be allowed to further settle in this tank and separate from the water. Water with the settled solids will be drawn from the bottom of the tank and sent to the Filter Press. Decanted water from the sludge thickener will gravity over-flow to the defoam tank.
- Capacity: 2600 GAL
- Bottom: 45° Cone Bottom
- Type II Resin: molded from linear polyethylene resin (not cross-linkable resin).

### 3.16.6 Polymer Tank

- Quantity: (1)
- 150-gallon chemical pretreatment tank (polymer)
- Manufacturer: Snyder Industries Inc.
- Dimensions: 30" D x 57" Height

#### 3.16.7 Water Safety/Wash Water Tank

- Quantity: (1)
- 1900 GAL Water holding tank
- Dimensions: 64" x 147.3"
- Specific gravity 1.9
- Rotational molded tank with closed top, High-density linear polyethylene (HDLPE) natural white color, 18" Polyethylene manway with 15" access at top of tank.
- Flush gallonage marks on side of tank.
- Bulkhead at base of tank for connection to water reuse pumps
- Bulkhead fittings for water entering and exiting the tank.

### 3.16.8 Calcium Chloride Tank (provided by others)

- Quantity: (1)
- Mini bulk tank

### 3.16.9 Acid Tank (provided by others)

- Quantity: (1)
- Mini bulk tank

### 3.17 Clarifier

- Pan American Slant Plate Clarifier for solids settling after primary water treatment processes. Dual sump bottom for solids removal.
- Model: SPC-42-P-600
- Manufacturer: Pan America
- Quantity: (1)
- Slant Plate clarifier equivalent footprint: 600 ft<sup>2</sup>
- Plate Loading: 0.3 GPM/FT<sup>2</sup> (at manufactures max flow); 0.125 GPM/FT<sup>2</sup> (expected at max flow of system)
- Tank and interior baffles: 3/16" ASTM A-36 Carbon Steel
- All Steel pipe: Black Schedule 40 ASTM-A53
- All Flanges flat face type and match 150# ANSO B16.5 Flange. Bolt holes to straddle main centerlines.
- Wetted hardware: 316 SS material
- Interior surfaces: Prepare to SSPC-SP10 near white metal blast, and coated with ameron high build coal tar epoxy Amercoat 78 HB, 16 mils dft minimum
- Exterior surfaces: Prepare to SSPC-SP6 commercial blast and coat with Ameron epoxy primer, Amerlock 2 5-8 mils DFT final coated to be Amershield aliphatic polyurethane enamel, 5 mils DFT

#### 3.18 Solids Dewatering

### 3.18.1 Filter Press

- Model: Evoqua 800G32-49-25SYLW
- Quantity: (1)
- The Filter Press will press entrained water out of the sludge from the clarifier. The Filter Press will run through a cycle until it fills up with solids or a predetermined time has passed. After a cycle ends, the Filter Press needs to be opened and cleaned, then reassembled for the next cycle. The Filter Press is mounted on a stand over a roll off box for easier collection of solids. The pressed water is sent back to the EQ Tank.
- The Filter Press Controls are mounted on a skid with the Filter Press Pump. This skid controls the pressure the Filter Press is operating under. The Filter Press Controls cycle the Filter Press Pump through a low, medium, and then high pressure. The pressure changes after a predetermined time has passed.
- Press Capacity: 25 FT<sup>3</sup>
- Design Operating Pressure: 100 PSI
- Plate Size: 800 mm x 800 mm
- Cake Thickness: 1.25"
- Dimensions:

- o Approx. Overall length: 210"
- o Approx. Overall width: 57"
- Approx. Overall height: 65"
- Approx. Overall equipment dry weight: 6,100 lbs
- Filter Plates: Standard recessed, center feed, alternating 4 corner discharge
- Material of construction: Polypropylene
- Maximum operating pressure 100 psi @ 120°F operating temperature
- Gasketed sealing area with EPDM elastomer O-ring type gaskets
- Filter Cloths:
  - Polypropylene filter cloths with sewn-in, high-density cord for caulked-in-place installation
- Filter Press Frame:
  - Sidebar style
- Material of construction: ASTM-A36 steel
- Design pressure: 100 psi
- Rugged solid steel components and sidebars
- Full width 304 stainless steel, sidebar caps
- Feed and Discharge Manifold
- Designed for air blow, even fill
- Materials of construction: ABS/PVC
- One (1) center feed valve on feed pipe assembly
- Four (4) discharge valves on discharge pipe assembly
- One (1) air blow valve on discharge pipe assembly
- Manual valve actuation

#### 3.18.2 Roll-Off Box (provided by others)

- Quantity: (1)
- Provided by Others for solids collection below the filter press
- Capacity: 20 YD<sup>3</sup>
- Height: 5'-6" (grade to top of tarp bow)
- Length: 21'-0"
- Width: 8'-4" (top cap, side to side), 9'4" (tarp roll on side of box to opposite side of top cap)
- Inside dimensions: 192" L x92" W x42" H
- Wheels: 8" wide x 9" diameter
- Hook-up: 1" thick open hook, bulkhead end
- Structural Design:
- Floor: ¼" thick steel plate

• Walls: 3/16" thick steel plate

• Door Sheet: 3" x 3" x 11 ga. Structural tubing

• Bulkhead: 3/16" thick steel plate

• Top cap: 4" x 3" x 11 ga. Structural tubing

Wetted Materials

Carbon steel: Shell and door sheet

Door gasket: EPDM

### 3.18.3 Roll-Off Winch and Rail

### 3.18.3a Winch

• Winch used to pull Roll-off under the filter press after unloading from truck

• Manufacturer: Allied Power Products Inc. Electric Winch

• Pulling capacity: 11,000 lbs

• 460 VAC, 3 phase, 3 HP, 1725 RPM motor

• Gear ratio: 261:1

• First layer speed: 8 fpm

• Cable: 3/8" wire rope

• Cable material: 7x19 Galvanized Aircraft Cable

Breaking strength: 14,400 lbs

### 3.18.3b Rail

• Rail frame built to guide the 20 YD<sup>3</sup> roll off box to/from under the filter press.

### 3.19 Multi-Media Filters

- Yardney Multi-media filter skid filled with different media to provide fine particulate filtration. The filter housing has a designated controller to provide automatic backwashing. System backwashing is implemented based upon a differential pressure reading across the media filter beds
- Yardney Model: MM-1860-4A

• Quantity: (1) – 4 pod skid

Standard Flow Range: 36-88 GPM

Total Filtration Surface Area: 7.08 FT<sup>2</sup>

Backwash Flowrate: 27 GPM

• Max Pressure: 100 PSI

• Number of tanks: 4

Diameter: 18"

• Media Requirements (per tank):

- o 1 FT<sup>3</sup> 1/2" 3/4" Gravel
- o 1 FT<sup>3</sup> 1.45 mm Garnet
- o 2.5 FT<sup>3</sup> 0.35 mm Garnet
- o 2.5 FT<sup>3</sup> 0.75 mm Anthracite
- Tank material: Carbon Steel
- Interior Coating: 3M ScotchKote 134 Fusion bonded epoxy
- Underdrain: 304 Stainless steel wedgewire lateral
- Inlet and Outlet Pipe Size: 3"
- Backwash Pipe Size: 2"

### 3.20 Bag Filters

- Rosedale bag filters
- Model: NC08-302P-\*-150-S-V-PB
- Quantity: (2)
- Filter housings will be plumbed in parallel with one bag filter sock per housing. Bag filters are used as a final or polishing solids removal.
- Housing Height: 30"
- Inlet/Outlet size/fitting: 2" NPT
- Pressure Rating: 150 psi
- Housing Material: 304 Stainless Steel
- Cover Seal: Flouroelastomer
- Basket Type: Filter bag basket

#### 3.21 Catwalk

Steel walk platform structure, sandblasted and painted, used to navigate system. Gives
operator ability to look into reactor vessels, handle filter press plates, and look into
process water tanks

# **Section 4: Component List – P&ID Identification**

# 4.1 Manual Valves:

BV-	DESCRIPTION	MANUFACTURER	PART NO.
0116	2" PVC BALL VALVE	SPEARS	2339-020
0117	1/2" PVC BALL VALVE	SPEARS	2339-005
0118	2" PVC BALL VALVE	SPEARS	2339-020
0119	2" PVC BALL VALVE	SPEARS	2339-020
0120	2" PVC BALL VALVE	SPEARS	2339-020
0121	2" PVC BALL VALVE	SPEARS	2339-020
0125	1/2" PVC BALL VALVE	SPEARS	2339-005
0201	2" PVC BALL VALVE	SPEARS	2339-020
0202	2" PVC BALL VALVE	SPEARS	2339-020
0203	4" PVC Ball Valve	SPEARS	3632-040
0205	2" PVC BALL VALVE	SPEARS	2339-020
0206	2" PVC BALL VALVE	SPEARS	2339-020
0207	2" PVC BALL VALVE	SPEARS	2339-020
0208	2" PVC BALL VALVE	SPEARS	2339-020
0220	2" PVC BALL VALVE	SPEARS	2339-020
0304	2" PVC BALL VALVE	SPEARS	2339-020
0305	1/2" BRASS BALL VALVE	MCMASTER	47865K23
0311	2" PVC BALL VALVE	SPEARS	2339-020
0312	2" PVC BALL VALVE	SPEARS	2339-020
0321	2" PVC BALL VALVE	SPEARS	2339-020
0350	2" PVC BALL VALVE	SPEARS	2339-020
0353	2" PVC BALL VALVE	SPEARS	2339-020
0409	3" PVC BALL VALVE	SPEARS	2332-030
0410	2" PVC BALL VALVE	SPEARS	2339-020
0411	2" PVC BALL VALVE	SPEARS	2339-020
0412	2" PVC BALL VALVE	SPEARS	2339-020
0413	2" PVC BALL VALVE	SPEARS	2339-020
0420	2" PVC BALL VALVE	SPEARS	2339-020
0511	2" PVC BALL VALVE	SPEARS	2339-020
0515	2" PVC BALL VALVE	SPEARS	2339-020
0525	2" PVC BALL VALVE	SPEARS	2339-020
0530	2" PVC BALL VALVE	SPEARS	2339-020
0535	2" PVC BALL VALVE	SPEARS	2339-020
0540	2" PVC BALL VALVE	SPEARS	2339-020
0541	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0550	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0551	1/2" PVC BALL VALVE	SPEARS	2339-005

0552	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0553	1/2" BRASS BALL VALVE	MCMASTER	47865K23
0621	1/2" BRASS BALL VALVE	MCMASTER	47865K23
0622	1/2" BRASS BALL VALVE	MCMASTER	47865K23
0630	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0632	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0633	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0634	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0635	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0636	1 1/2" PVC BALL VALVE	SPEARS	2339-015
0637	1/2" BRASS BALL VALVE	MCMASTER	47865K23
0640	1/2" BRASS BALL VALVE	MCMASTER	47865K23
0701	4" PVC BALL VALVE	SPEARS	2339-040
0702	2" PVC BALL VALVE	SPEARS	2339-020
0706	2" PVC BALL VALVE	SPEARS	2339-020
0707	2" PVC BALL VALVE	SPEARS	2339-020
0708	2" PVC BALL VALVE	SPEARS	2339-020
0709	2" PVC BALL VALVE	SPEARS	2339-020
0721	1/4" CHROME PLATED BALL VALVE	MCMASTER	4912K92
0722	1/4" CHROME PLATED BALL VALVE	MCMASTER	4912K92
0741	1/4" CHROME PLATED BALL VALVE	MCMASTER	4912K92
0742	2" PVC BALL VALVE	SPEARS	2339-020
0743	2" PVC BALL VALVE	SPEARS	2339-020
0744	2" PVC BALL VALVE	SPEARS	2339-020
0745	2" PVC BALL VALVE	SPEARS	2339-020
0747	1/4" CHROME PLATED BALL VALVE	MCMASTER	4912K92
0749	2" PVC BALL VALVE	SPEARS	2339-020
0750	2" PVC BALL VALVE	SPEARS	2339-020
0751	1/2" PVC BALL VALVE	SPEARS	2339-005
0752	2" PVC BALL VALVE	SPEARS	2339-020
0753	2" PVC BALL VALVE	SPEARS	2339-020
0754	2" PVC BALL VALVE	SPEARS	2339-020
0755	2" PVC BALL VALVE	SPEARS	2339-020
0756	2" PVC BALL VALVE	SPEARS	2339-020
0757	2" PVC BALL VALVE	SPEARS	2339-020
0761	2" PVC BALL VALVE	SPEARS	2339-020
0762	2" PVC BALL VALVE	SPEARS	2339-020
0775	1 ¼" PVC BALL VALVE	SPEARS	2339-012
0776	1 ¼" PVC BALL VALVE	SPEARS	2339-012
0777	½" PVC BALL VALVE	SPEARS	2339-005
0778	½" PVC BALL VALVE	SPEARS	2339-005
0810	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0812	1/2" PVC BALL VALVE	SPEARS	2339-005

0821	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0822	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0823	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0824	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0825	1/2" PVC BALL VALVE	SPEARS	2339-005
0826	1/2" PVC BALL VALVE	SPEARS	2339-005
0831	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0832	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0833	1/2" CPVC BALL VALVE	SPEARS	2339-005C
0834	1/2" CPVC BALL VALVE	SPEARS	2339-005C

<u>4.2</u> <u>Valves</u>

<u>Gate</u>

GV-	DESCRIPTION	MANUFACTURER	PART NO.
0520	1.25" GV	SPEARS	2022-012
0717	2" GV	SPEARS	2022-020
0770	HOSE BIB #1	EVERBILT	VHNSTDB4EB*
0771	HOSE BIB #2	EVERBILT	VHNSTDB4EB*
0772	HOSE BIB #3	EVERBILT	VHNSTDB4EB*
0773	HOSE BIB #4	EVERBILT	VHNSTDB4EB*

<sup>\*=</sup> or similar

# 4.3 Air Controlled Valves

ACV-	DESCRIPTION	MANUFACTURER	PART NO.
0115	2" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-078
0129	2" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-078
0204	4" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-081
0303	2" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-078
0311	2" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-078
0321	2" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-078
0409	3" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-080
0414	3" 3-WAY PNEUMATIC VALVE	GEORG FISHER	199-285-388
0526	2" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-078
0536	2" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-078
0705	4" PNEUMATIC BALL VALVE	GEORG FISHER	199-233-081
			2513-030 (VALVE BODY)
0708	3" 3-WAY PNEUMATIC VALVE	ASAHI/AMERICA	2302-030 (ACTUATOR)
			2513-030 (VALVE BODY)
0717	3" 3-WAY PNEUMATIC VALVE	ASAHI/AMERICA	2302-030 (ACTUATOR)

# 4.4 Solenoid Valves

SV-	DESCRIPTION	MANUFACTURER	PART NO.
0115	1/4" TUBING AIR SOLENOID	BURKERT	5470
0129	1/4" TUBING AIR SOLENOID	BURKERT	5470
0204	1/4" TUBING AIR SOLENOID	BURKERT	5470
0212	1/2" TUBING AIR SOLENOID	ASCO	8210G002
0302	1/2" TUBING AIR SOLENOID	ASCO	8210G002
0303	1/4" TUBING AIR SOLENOID	BURKERT	5470
0311	1/4" TUBING AIR SOLENOID	BURKERT	5470
0321	1/4" TUBING AIR SOLENOID	BURKERT	5470
0409	1/4" TUBING AIR SOLENOID	BURKERT	5470
0414	1/4" TUBING AIR SOLENOID	BURKERT	5470
0526	1/4" TUBING AIR SOLENOID	BURKERT	5470
0527	1/2" TUBING AIR SOLENOID	ASCO	8210G002
0536	1/4" TUBING AIR SOLENOID	BURKERT	5470
0553	1/2" TUBING AIR SOLENOID	ASCO	8210G002
0705	1/4" TUBING AIR SOLENOID	BURKERT	5470
0708	1/4" TUBING AIR SOLENOID	BURKERT	5470
0717	1/4" TUBING AIR SOLENOID	BURKERT	5470

# 4.5 Check Valves

CV-	DESCRIPTION	MANUFACTURER	PART NO.
0116	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0118	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0120	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0201	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0202	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0220	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0410	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0411	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0706	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0707	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0754	WATER SAEFTY/WASH WATER PUMP	GRUNDFOS	CMBE 10-54
0755	WATER SAEFTY/WASH WATER PUMP	GRUNDFOS	CMBE 10-54
0761	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0762	2" PVC SPRING CHECK VALVE	GEORG FISCHER	562
0775	1 ¼" CHECK VALVE	GEORG FISCHER	562

# 4.6 Flow Meters

FT-	DESCRIPTION	MANUFACTURER	PART NO.
0101	EXTRACTION WELL FLOW METER	GEORGE FISCHER	3-2551-P0-42
0305	EC FEED FLOW METER	GEORGE FISCHER	3-2551-P0-42
0770	DISCHARGE FLOW METER	GEORGE FISCHER	3-2551-P0-42

# 4.7 Rectifiers

RC-	DESCRIPTION	MANUFACTURER	PART NO.
0401	RECTIFIER	ALDONEX	T-448-20CR-CCV-APR-IOS
0402	RECTIFIER	ALDONEX	T-448-20CR-CCV-APR-IOS

# 4.8 Basket Strainers

STR-	DESCRIPTION	MANUFACTURER	PART NO.
0311	BASKET STRAINER	HAYWARD	SB1300F
0321	BASKET STRAINER	HAYWARD	SB1300F

### <u>4.9 Pumps</u>

PMP-	DESCRIPTION	MANUFACTURER	PART NO.
0201	EC FEED PUMP (DUPLEX)	GORMAN-RUPP	490B-98
0202	EC FEED PUMP (DUPLEX)	GORMAN-RUPP	490B-98
0220	SUMP PUMP	ZOELLER	N140
0302	SCALE PURGE PUMP	ARO	06-PD15P-FPS-PTT
0410	POST EC PUMP (DUPLEX)	GORMAN-RUPP	490B-98
0411	POST EC PUMP (DUPLEX)	GORMAN-RUPP	490B-98
0514	POLYMER PUMP	PULSATRON	LPH6-PTC
0518	POLYMER PUMP	PULSATRON	LPH6-PTC
0527	SLUDGE PUMP	ARO	06-PD15P-FPS-PTT
0631	SLUDGE PUMP	ARO	06-PD15P-FPS-PTT
0706	POST TREATMENT PUMP (DUPLEX)	GRUNDFOS	CRI 10-6
0707	POST TREATMENT PUMP (DUPLEX)	GRUNDFOS	CRI 10-6
0754,			
0755	WATER SAFETY/WASH WATER PUMP (DUPLEX)	GRUNDFOS	CMBE 10-54 TWIN
0831	ACID PUMP	LMI	XRD121A74TCA7PN
0832	ACID PUMP	LMI	XRD121A74TCA7PN
0833	ACID PUMP	LMI	XRD121A74TCA7PN
0834	ACID PUMP	LMI	XRD121A74TCA7PN
0835	CALCIUM CHLORIDE	LMI	XRD121A74TCA7T1
0836	CALCIUM CHLORIDE	LMI	XRD121A74TCA7T1

# 4.10 Filter Press Controls

	DESCRIPTION	MANUFACTURER	PART NO.
	FILTER PRESS 25 CU. FT	EVOQUA	800G32-49-25SYLW
PS-0611	PRESSURE SWITCH	UNITED ELECTRIC	H54-25
PR-0612	PRESSURE REGULATOR	WILKERSON	R18-04-F000
SV-0613	1/2" TUBING AIR SOLENOID	ASCO	8210G002
PR-0614	PRESSURE REGULATOR	WILKERSON	R18-04-F000
SV-0615	1/2" TUBING AIR SOLENOID	ASCO	8210G002
PR-0616	PRESSURE REGULATOR	WILKERSON	R18-04-F000
SV-0617	1/2" TUBING AIR SOLENOID	ASCO	8210G002
PR-0618	PRESSURE REGULATOR	WILKERSON	R18-04-F000
NV-0619	NEEDLE VALVE	ARO	104104-N04
NV-0620	NEEDLE VALVE	ARO	104104-N04
CV-0638	1/2" FILTER PRESS	MILWAUKEE VALVE	UP0967000012
CV-0639	1/2" FILTER PRESS	MILWAUKEE VALVE	UP0967000012
PR-0641	PRESSURE REGULATOR	WILKERSON	R18-04-F000

### 4.11 Pressure Gauges

	DESCRIPTION	MANUFACTURER	PART NO.
PG	BAG FILTER INLET LIQUID PRESSURE GAUGE	WEKSLER	BY12YPG4LW
PG	BAG FILTER OUTLET LIQUID PRESSURE GAUGE	WEKSLER	BY12YPG4LW
PG	BAG FILTER INLET LIQUID PRESSURE GAUGE	WEKSLER	BY12YPG4LW
PG	BAG FILTER OUTLET LIQUID PRESSURE GAUGE	WEKSLER	BY12YPG4LW

# 4.12 Safety Shower

PR	DESCRIPTION	MANUFACTURER	PART NO.
	WATER HEATER	EEMAX	AP063480 EFD N4
		GUARDIAN	
	SAFETY SHOWER	SAFETY STATION	GFR3100
PR-0775	WATER HEATER PRESSURE REGULATOR	WATTS	11/4 25AUB-GG-Z3
	WATER HAMMER ARRESTOR SAFETY		
HR-0776	SHOWER #1	ZURN LC	WH2950XL
	WATER HAMMER ARRESTOR SAFETY		
HR-0777	SHOWER #2	ZURN LC	WH2950XL
ST- 0775	WATER HEATER Y-STRAINER 40 MESH	HAYWARD	YS10125SU1/16

# 4.13 Tank Mixer

MXR-	DESCRIPTION	MANUFACTURER	PART NO.
0211	EQ TANK 1.5 HP	BALDOR	CM 3554
	GEAR BOX	DODGE TIGEAR	20Q05H56
0504	DEFOAM TANK 1.5 HP	BALDOR	CM 3554
	GEAR BOX	DODGE TIGEAR	20Q05H56
0516	FLOCCULATION TANK 1.0 HP	BALDOR	CM 3538
	GEAR BOX	DODGE TIGEAR	17Q05H56
0521	POLYMER TANK 0.25 HP	LEESON	C4C17FB21E

### 4.14 Pressure Switches

	DESCRIPTION	MANUFACTURER	PAT NO.
PSL-0305	PRESSURE SWITCH LOW	UNITED ELECTRIC	H54-25
PT-0723	MULTI MEDIA FILTER PRESSURE SWITCH	DWYER	SERIES 629
PT-0749	BAG FILTER PRESSURE SWITCH	DWYER	SERIES 629

# 4.15 Tanks

DESCRIPTION	MANUFACTURER	PART NO.
EQ TANK	LF MANUFACTURING	A-LP10104
POST EC TANK	REGAL PLASTICS	TA00230S19X36X80
DEFOAM TANK	LF MANUFACTURING	A-LP10105
FLOCCULATION TANK	LF MANUFACTURING	A-LP10106
CLARIFER	PAN AMERICAN	SPC-42-P-600
POLYMER TANK	SNYDER	57100VOT45S
SLUDGE THICKENER	SNYDER	TANK: 5100 STAND: 79400
POST TREATMENT TANK	LF MANUFACTURING	A-LP10107
MULTI MEDIA FILTER (FLTR-0709)	YARDNEY	MM-1860-4A
BAG FILTER (FLTR-0748-1)	ROSEDALE	NC08-302P-*-150-S-V-PB
BAG FILTER (FLTR-0748-1)	ROSEDALE	NC08-302P-*-150-S-V-PB
WATER SAFETY/WASH WATER TANK	SNYDER	830000N45
CALCIUM CHLORIDE MINI BULK TANK		
(BY OTHERS)	-	-
ACID MINI BULK TANK (BY OTHERS)	-	-

# 4.16 Tank Sensors

	DESCRIPTION	MANUFACTURER	PART NO.
LSH-0201	CONTAINMENT SUMP FULL	MADISON	M8000
LSL-0202	LEVEL SENSOR LOW SUMP	ADVANCED CONTROL TECHNOLOGY	P7300
			EXPERT
LT-0213	EQ TANK LEVEL TRANSMITTER	MJK	2100
LSH-0214	EQ REDUNDANT HIGH LEVEL	MADISON	M8000
LSL-0215	EQ TANK REDUNDANT LOW LEVEL	ADVANCED CONTROL TECHNOLOGY	P7300
AIC-0217	EQ FEED LINE CONDUCTIVITY PROBE	ENDRESS + HAUSER	CLS21D
AIC-0218	EQ TANK pH PROBE	ENDRESS + HAUSER	CPF81D
AIC-0219	EQ TANK CONDUCTIVITY PROBE	ENDRESS + HAUSER	CLS21D
LSH-0404	POST EC TANK REDUNDANT HIGH LEVEL	MADISON	M8000
LSL-0407	POST EC TANK REDUNDANT LOW LEVEL	ADVANCED CONTROL TECHNOLOGY	P7300
			EXPERT
LT-0408	POST EC TANK LEVEL TRANSMITTER	MJK	2100
AIC-0505	DEFOAM TANK pH PROBE	ENDRESS + HAUSER	CPF81D
LSH-0506	DEFOAM TANK HIGH LEVEL	MADISON	M8000
LSH-0517	FLOCCULATION TANK HIGH LEVEL	MADISON	M8000
LSL-0520	POLYMER TANK LOW LEVEL	ADVANCED CONTROL TECHNOLOGY	P7300
LSH-0523	CLARIFIER HIGH LEVEL	MADISON	M8000
	POST TREATMENT TANK LEVEL		EXPERT
LT-0702	TRANSMITTER	MJK	2100
	POST TREATMENT TANK REDUNDANT		
LSH-0703	HIGH LEVEL	MADISON	M8000
	POST TREATMENT TANK REDUNDANT		
LSL-0704	LOW LEVEL	ADVANCED CONTROL TECHNOLOGY	P7300
LSL-0751	WATER SAFETY/WASH WATER TANK LOW LEVEL	ADVANCED CONTROL TECHNOLOGY	P7300
LSL-0803	CALCIUM CHLORIDE TANK LOW LEVEL	ADVANCED CONTROL TECHNOLOGY	P7300

### **Section 5: Applicable Standards**

### 5.1 Fiberglass Tanks

Tanks shall be designed, fabricated, and inspected in accordance with the latest issue of the following standards:

ASTM D-3299, Filament-Wound Glass-Reinforced Chemical-Resistant Tanks, latest edition.

ASTM C-582, Contact-Molded Reinforced Thermosetting Plastic Laminates for Corrosion-Resistant Equipment.

ANSI B 16.5, Flange Dimensions.

ASTM D-2583, Test Method for Indentation Hardness of Rigid Plastics by Means of a Barcol Impression tester.

ASTM D-2584, Test Method for Ignition Loss of Cured Reinforced Resins.

National Bureau of Standards (NBS) Voluntary Product Standard PS 15-69, Custom Contact-Molded Reinforced-Polyester Chemical-Resistant Process Equipment.

ASTM D-2563, Classifying Visual Defects in Glass-Reinforced Plastic Laminate Parts.

ASTM D-4097, Contact Molded Glass – Fiber Reinforced Thermosetting Resin Chemical-Resistant Tanks.

FRP tanks shall be corrosion-resistant to the specified tank contents and shall be suitable for the intended service life.

Additional loads from pumps, or catwalks shall be supported externally from the tank.

Dimensional Requirements-Cylindrical Vessels and Tanks: Diameters shall be measured internally. Tolerance on nominal diameter including out-of-roundness shall be plus or minus 1 percent. Measurements shall be taken with the tank in the vertical position. Taper shall not exceed 0.25 percent per side. The minimum knuckle radius on formed heads shall be 1-1/2 inches unless noted otherwise on the attached data sheets.

The final locations of nozzles and accessories shall be subject to change until shop drawing approvals.

All FRP tanks shall be designed for outdoor service with direct sunlight exposure.

Tanks shall be designed to meet pressure, loading or seismic criteria using strengthening ribs, unless otherwise indicated on the data sheets. Where no strengthening ribs are specified, loads shall be distributed over a uniform side shell thickness.

#### 5.2 Plastic Tanks

All plastic tanks utilized will be of adequate specific gravity to meet the type of water being stored within. Water Safety/Wash Water tank fabricated to ASTM standards. Polymer and sludge thickener tanks are fabricated according to specific gravity rating.

### 5.3 ASTM (American Society for Testing and Materials) Standards

D618 Conditioning Plastics and Electrical Insulating Materials for Testing

**D638 Tensile Properties of Plastics** 

D790 Flexural Properties of Unreinforced and Reinforced Plastics and Electrical Insulating Materials

D883 Definitions of Terms Relating to Plastics

D1505 Density of Plastics by the Density-Gradient Technique

D1525 Test Method for Vicat Softening Temperature of Plastics

D1693 Test Method for Environmental Stress-Cracking of Ethylene Plastics

D1998 Standard Specification for Polyethylene Upright Storage Tanks

D2765 Degree of Crosslinking in Crosslinked Ethylene Plastics as Determined by Solvent Extraction

D2837 Method for Obtaining Hydrostatic Design Basis for Thermoplastic Pipe Materials

D3892 Practice for Packaging/Packing of Plastics

F412 Definitions of Terms Relating to Plastic Piping Systems

#### 5.4 ARM (Association of Rotational Molders) Standards

• Low Temperature Impact Resistance (Falling Dart Test Procedure)

### 5.5 ANSI Standards

• B-16.5 Pipe Flanges and Flanged Fittings

### 5.6 OSHA Standards

• 29 CFR 1910.106 Occupational Safety and Health Administration, Flammable and Combustible Liquids

### 5.7 UBC CODE

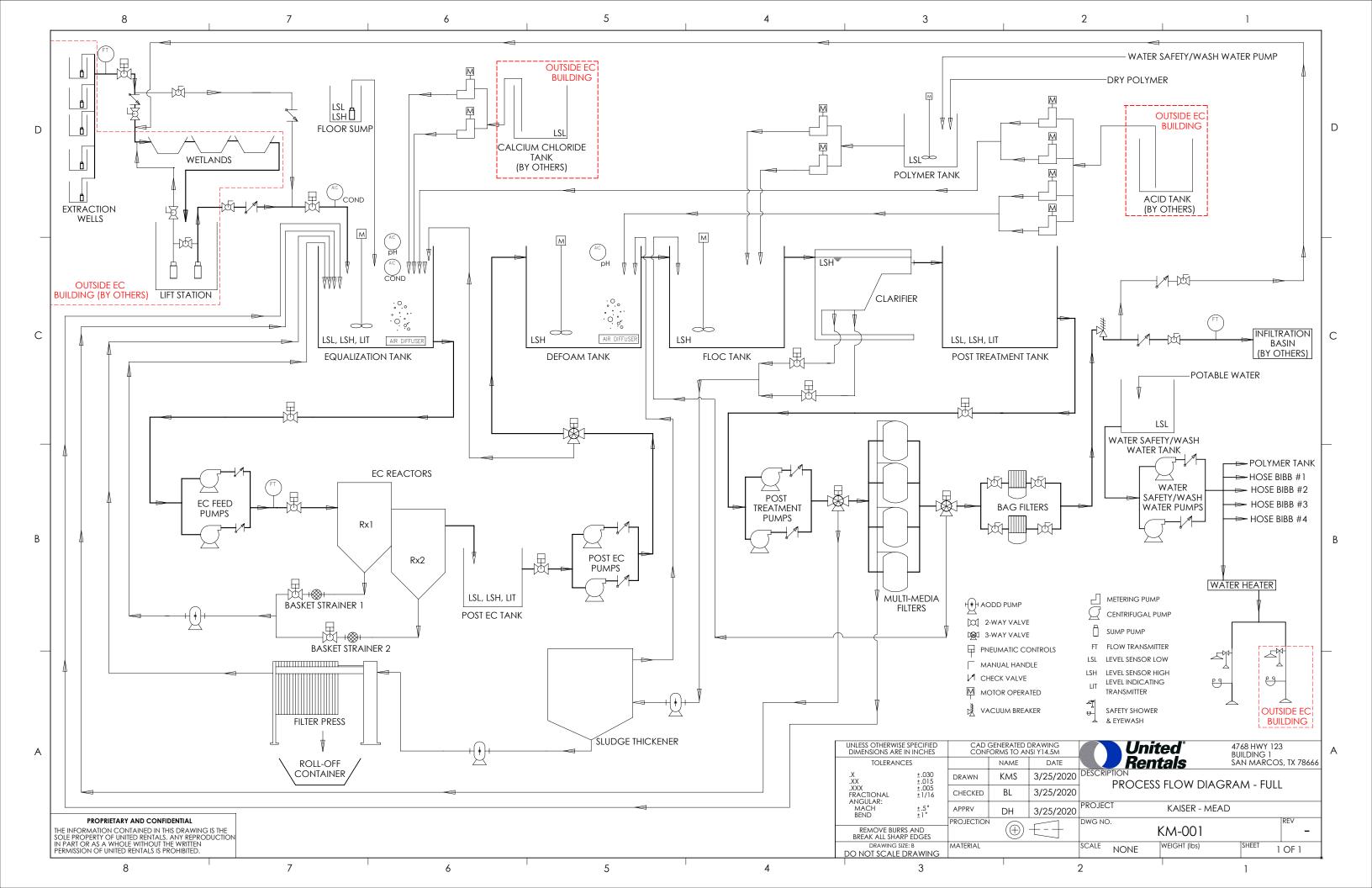
• Uniform Building Code 2006 Edition

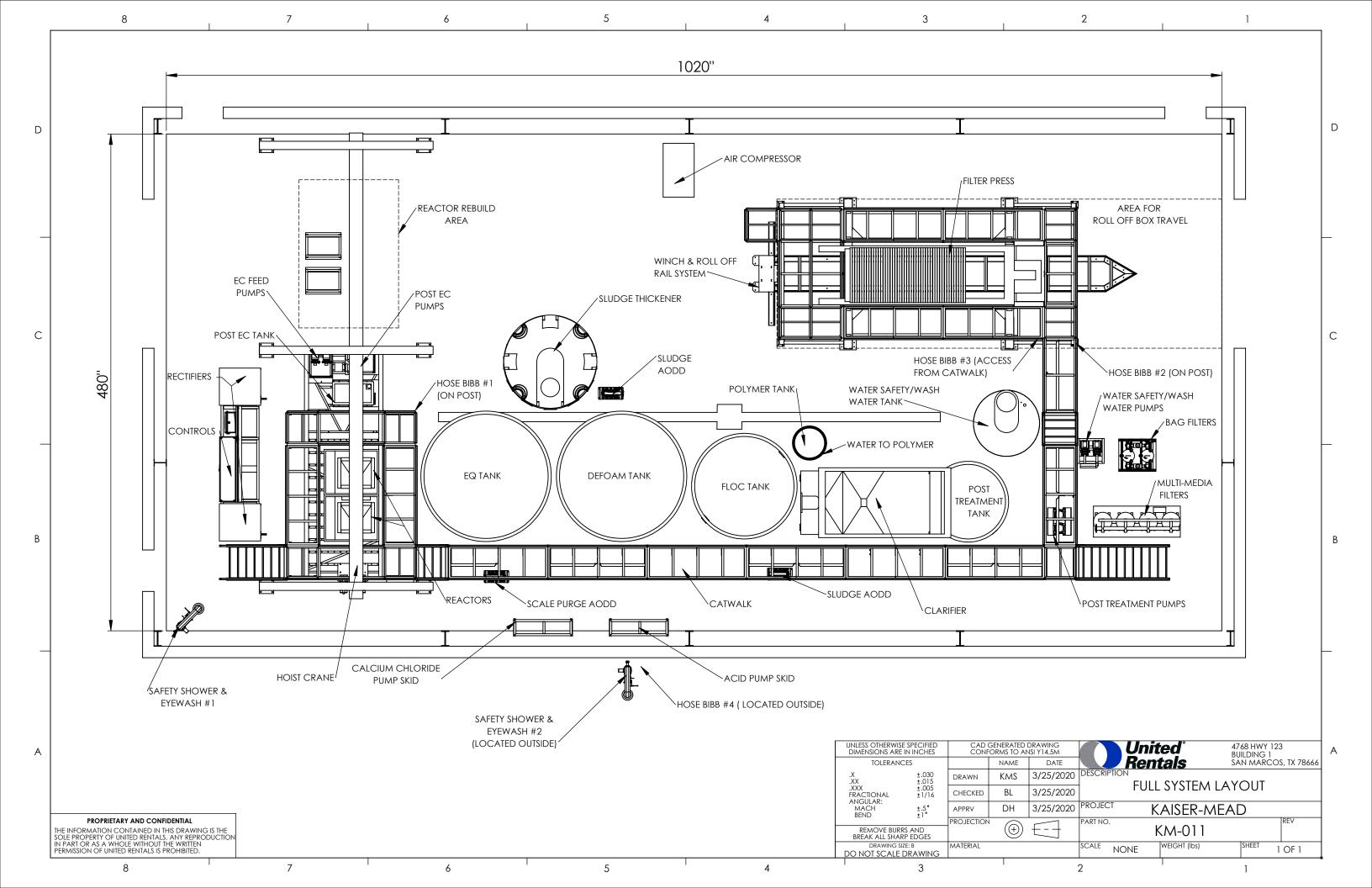
### 5.8 IBC CODE

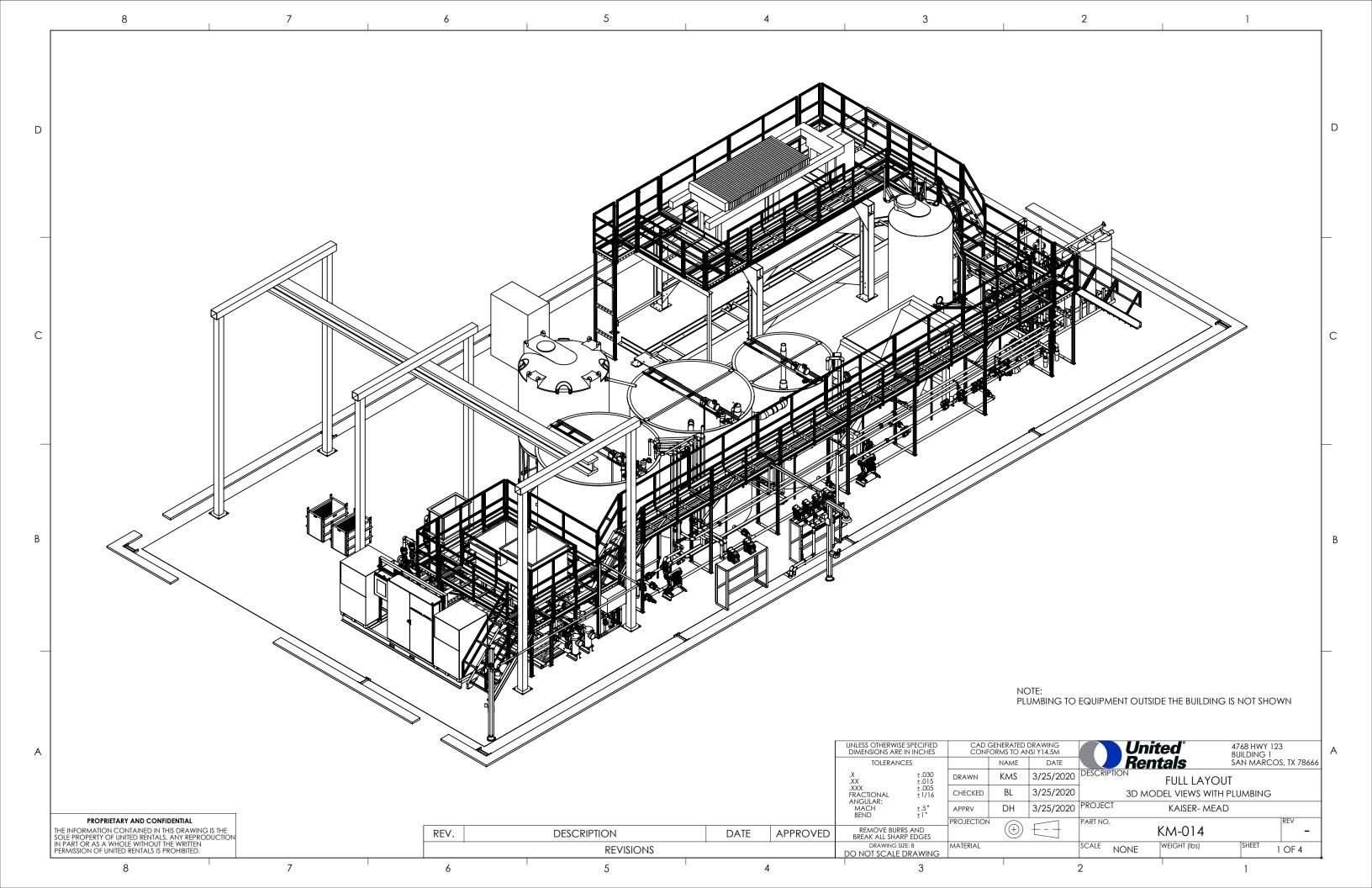
• International Building Code 2009 Edition

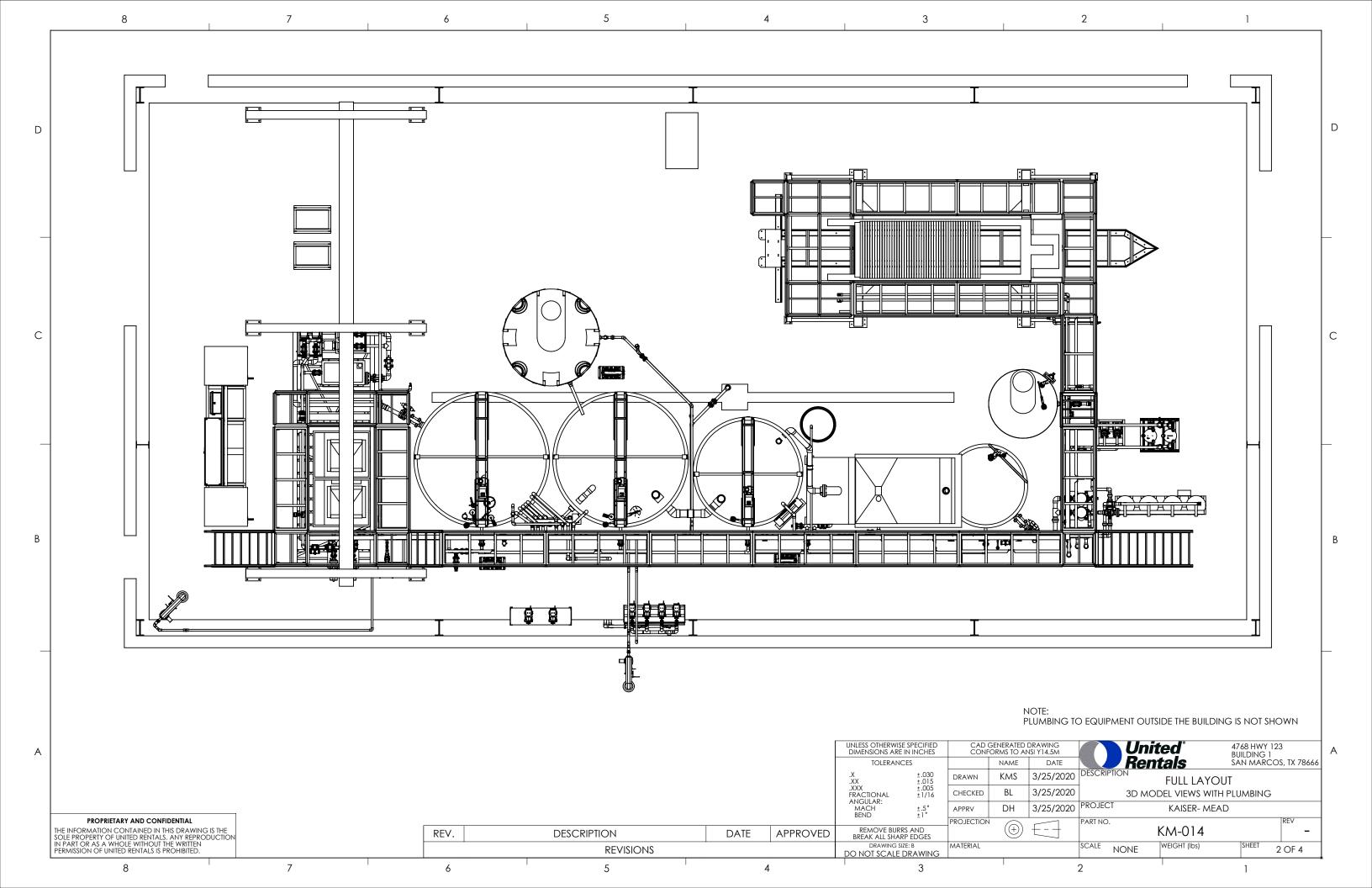
### **Section 6: Site Requirements**

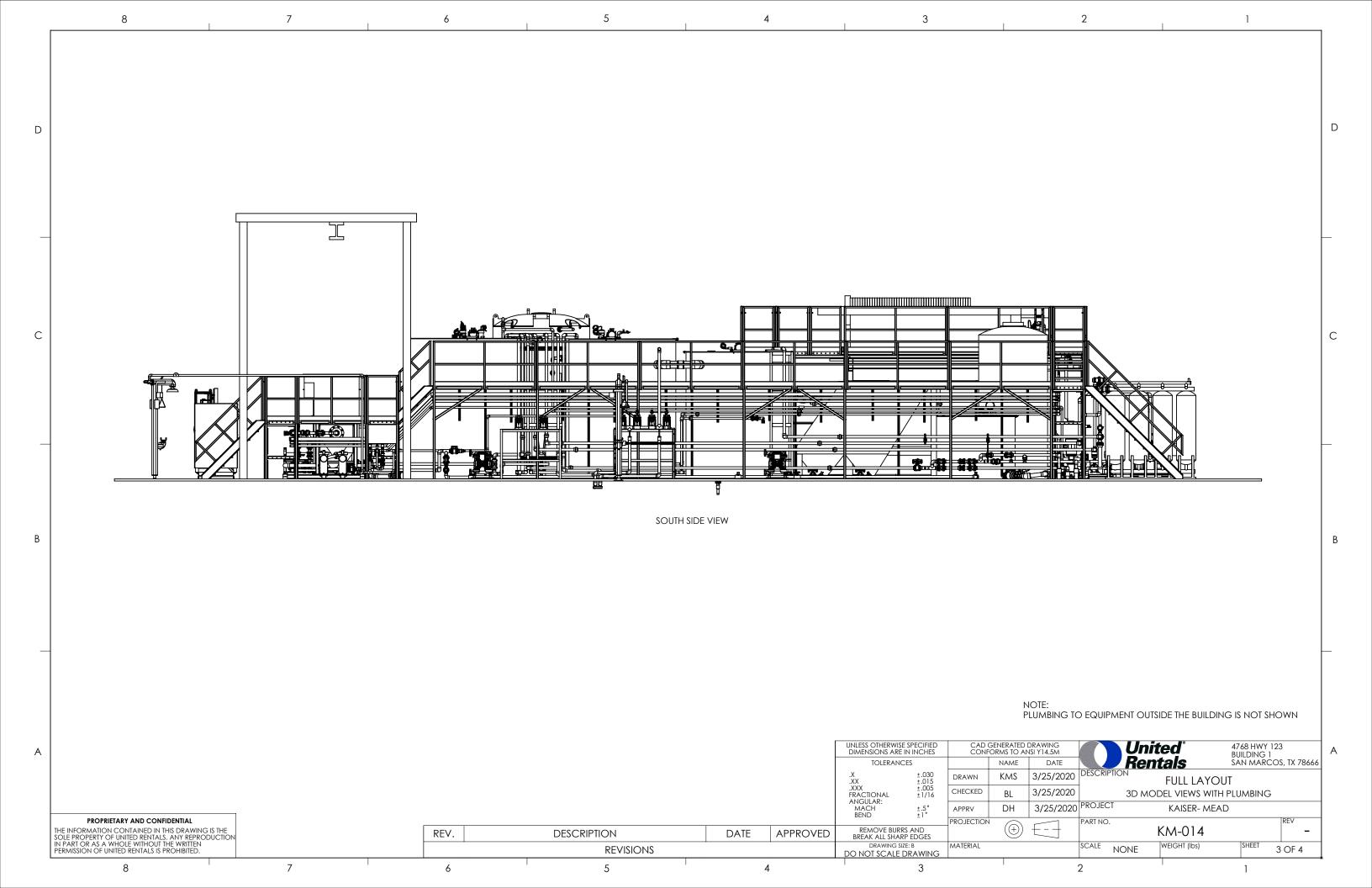
- All site work and concrete slab pouring are the responsibility of site General Contractor.
- A suitable structure to protect the treatment system components from rain or moisture and freezing conditions with a minimum interior width of 40 feet, minimum interior length of 84 feet and minimum clearance height of 21 feet. Assume temperature maintained at or above 40 degrees F during winter months.
- The floor of the structure should be level or graded to provide adequate drainage if desired. The floor should be formed to provide any required containment.
- A sulfuric acid storage/containment area should be constructed into the facility to store the 93% sulfuric acid being used in the treatment process.
- Storage area for process materials: calcium chloride and polymer
- Electrical service panel with 480VAC, 3-phase power with amperage load to be calculated based upon total building load.
- Electrical drops providing 120VAC, single phase power at specified locations.
- Electrical drop with two disconnects in a local panel for connecting water safety/wash water pumps. Each pump requires 240 VAC, 1 phase, 9.1 amps for 2 HP motor.
- Ethernet connection between VPN router and local network; an assigned IP address for the router in customer's local area network (must port forward 5900, 10443 and 1194 to the IP address assigned to the VPN router). A virtual network computing (VNC) client to customer's remote access device(s) to allow remote access to and control of the EC Treatment System HMI screens.
- Potable water supply for chemical make-up and wash water.
- Safety facilities and equipment as required by national, state, and local codes including any safety showers and personal protection equipment.
- Any equipment not supplied by United Rentals required for completing the installation and operation of the treatment system.

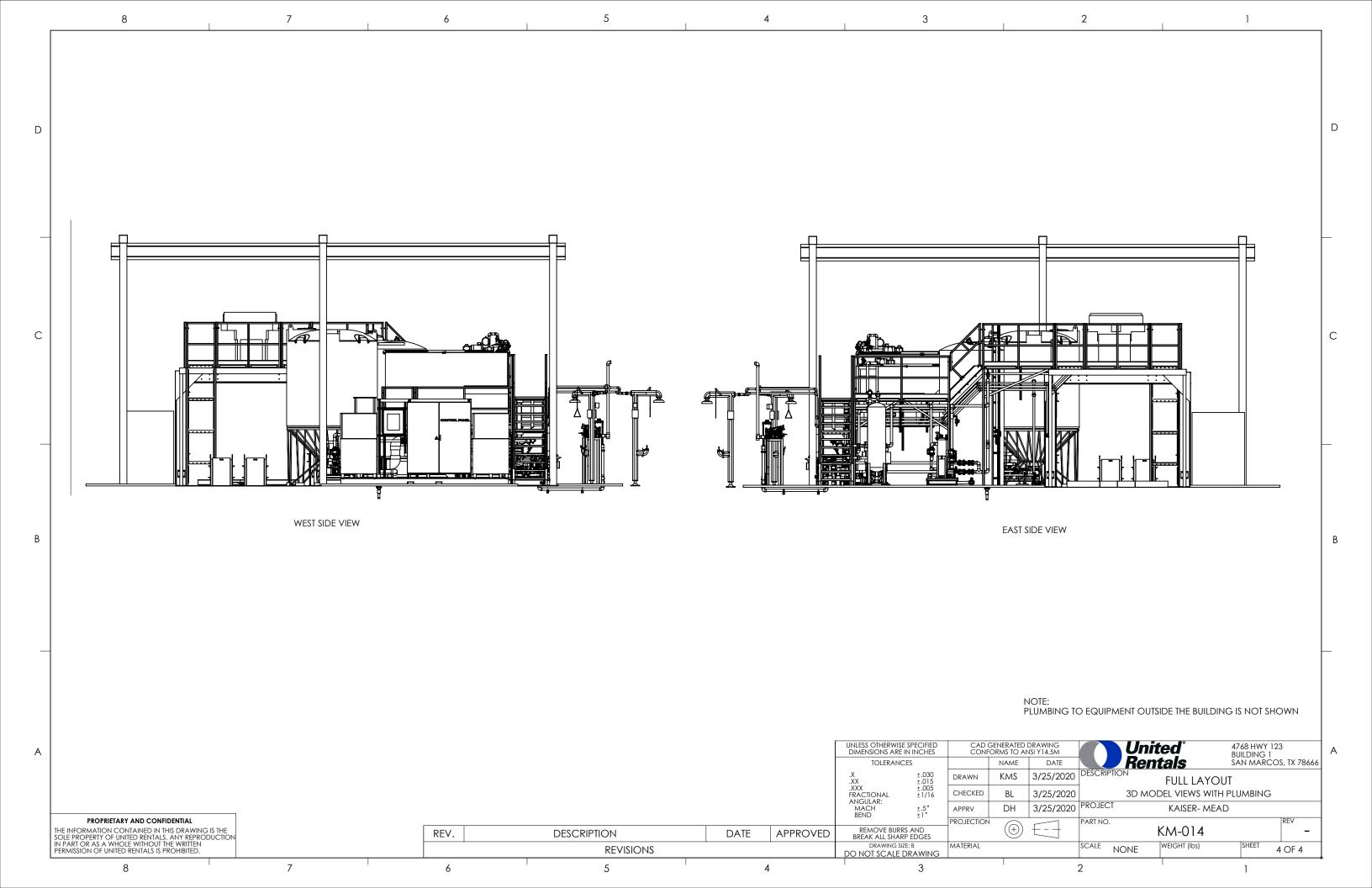


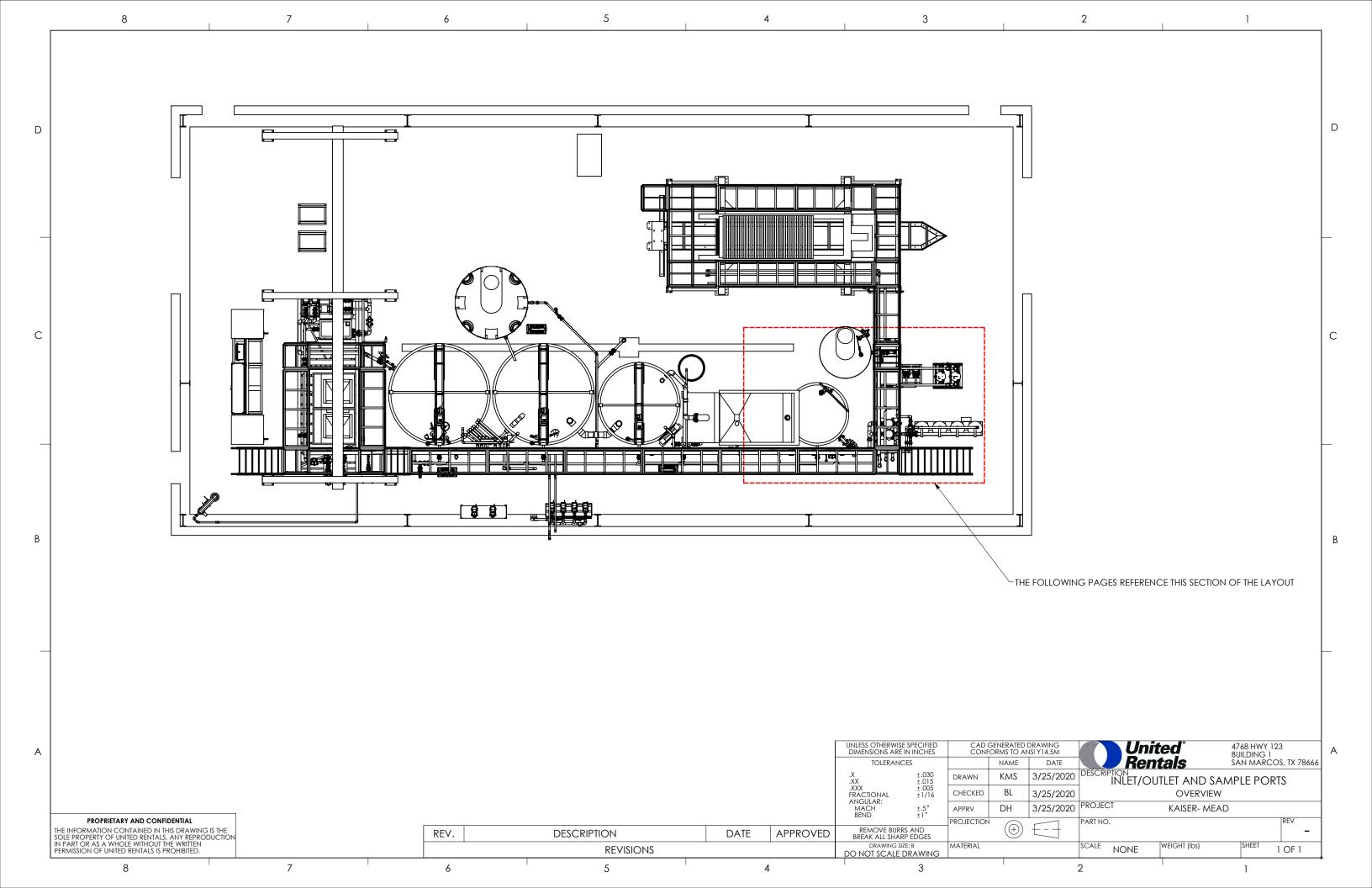


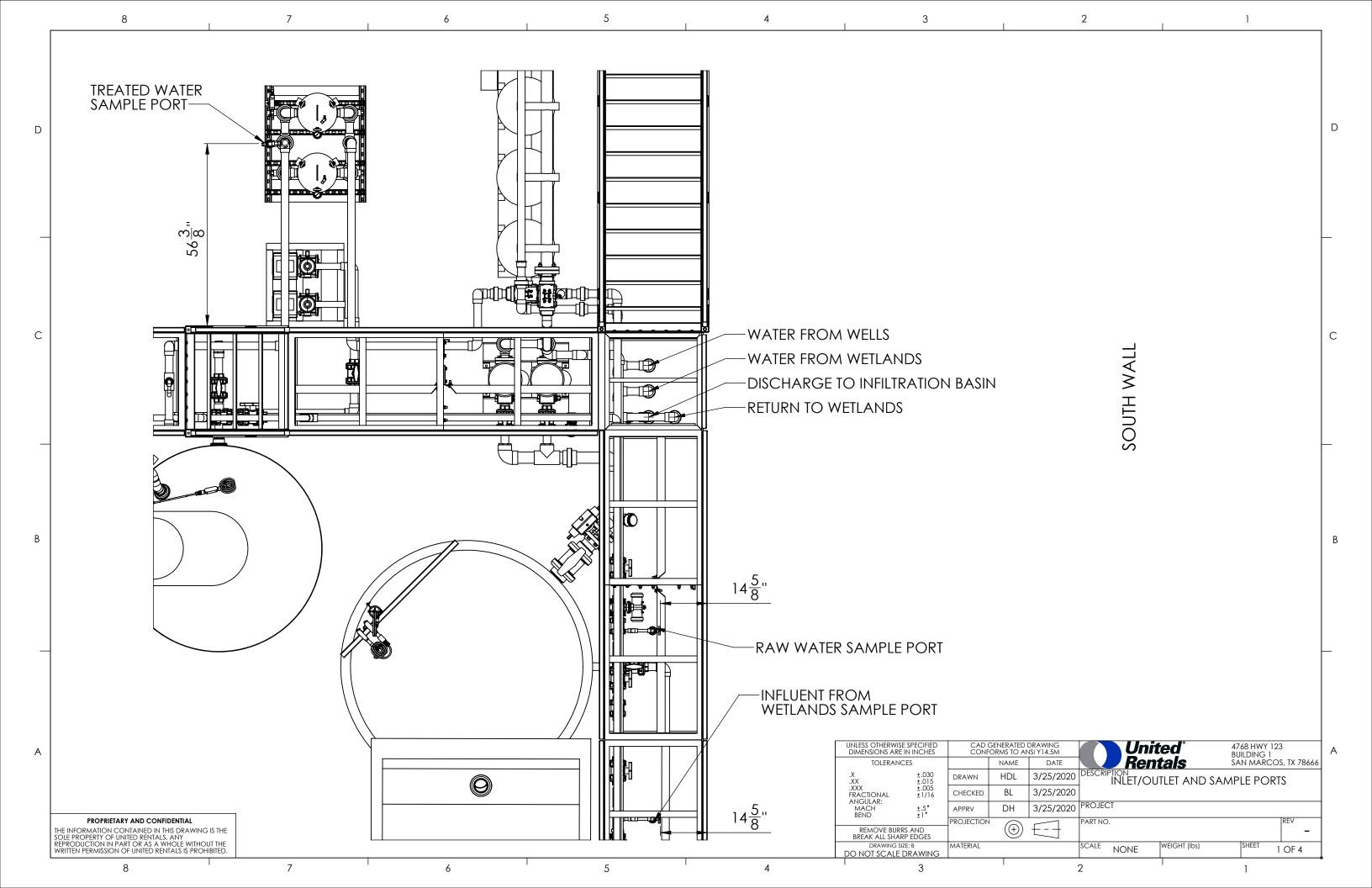


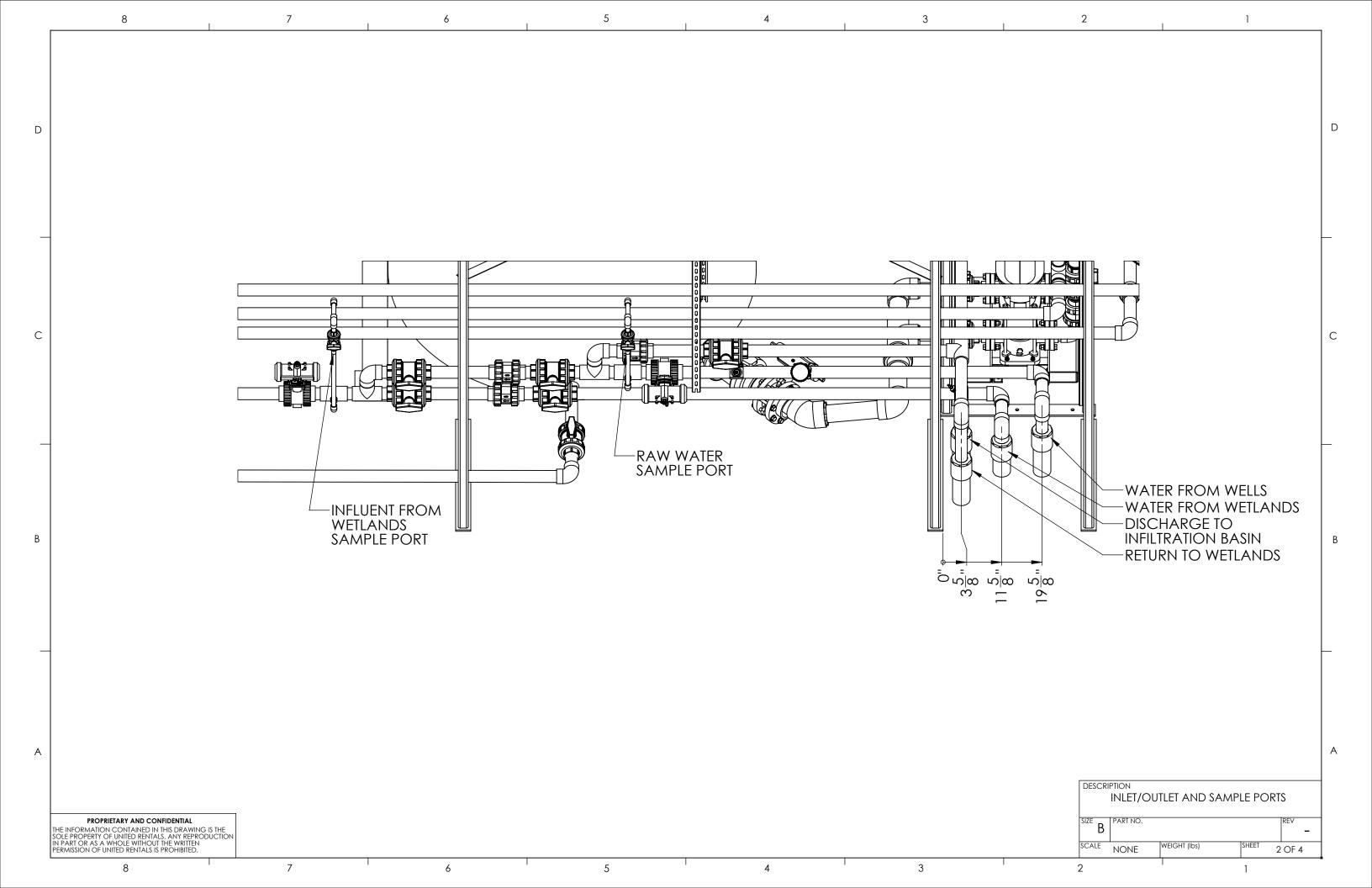


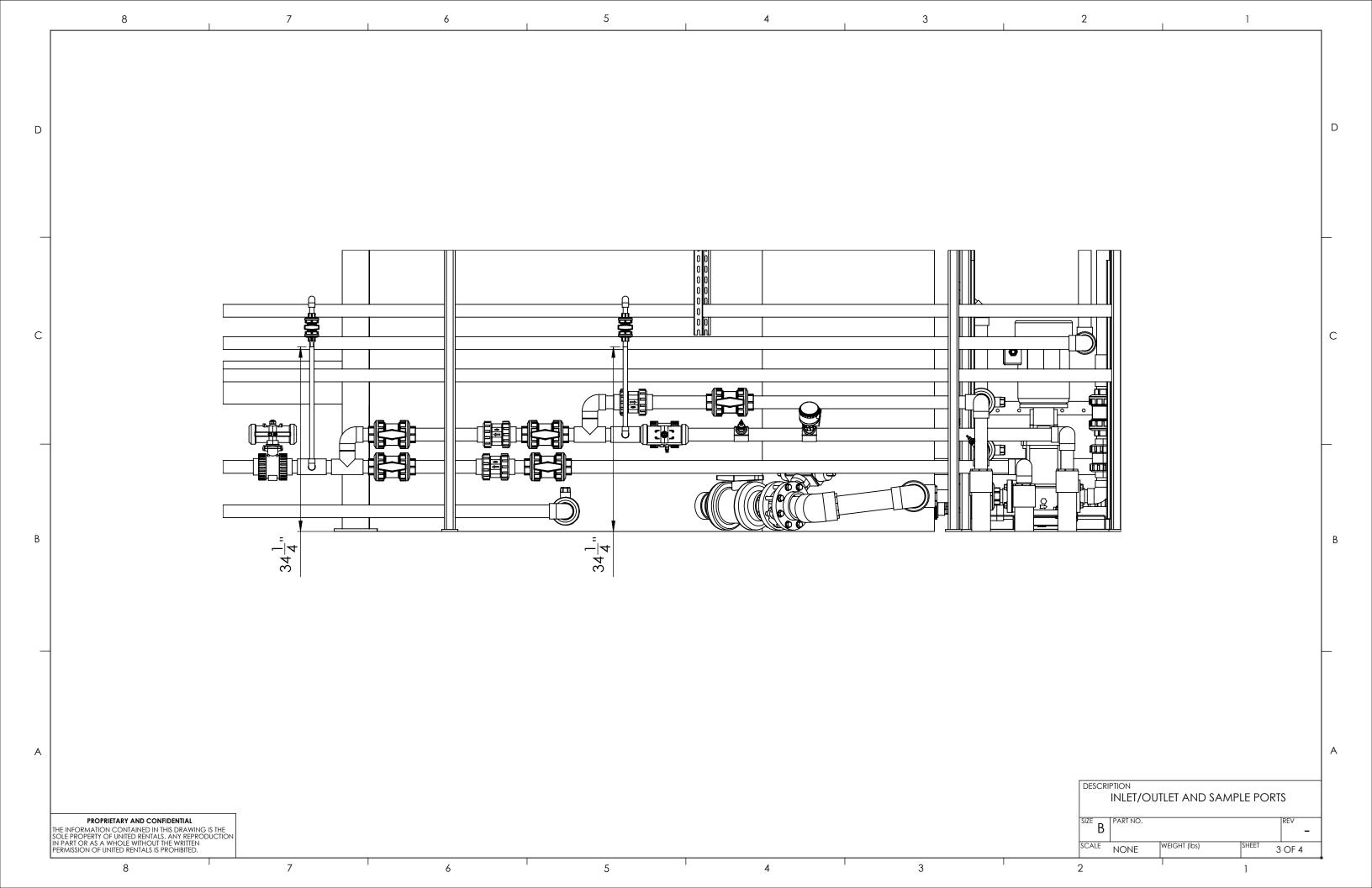


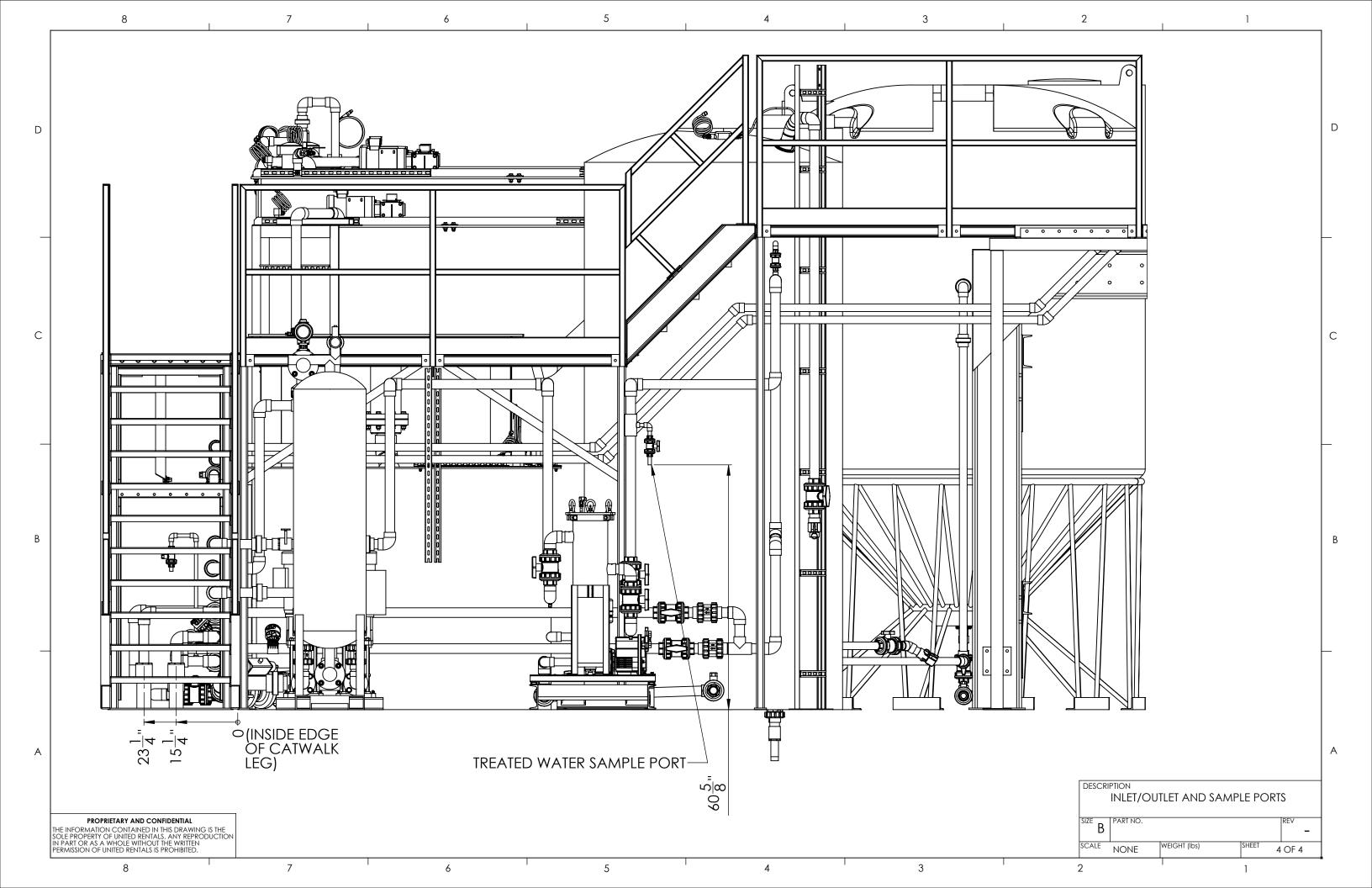


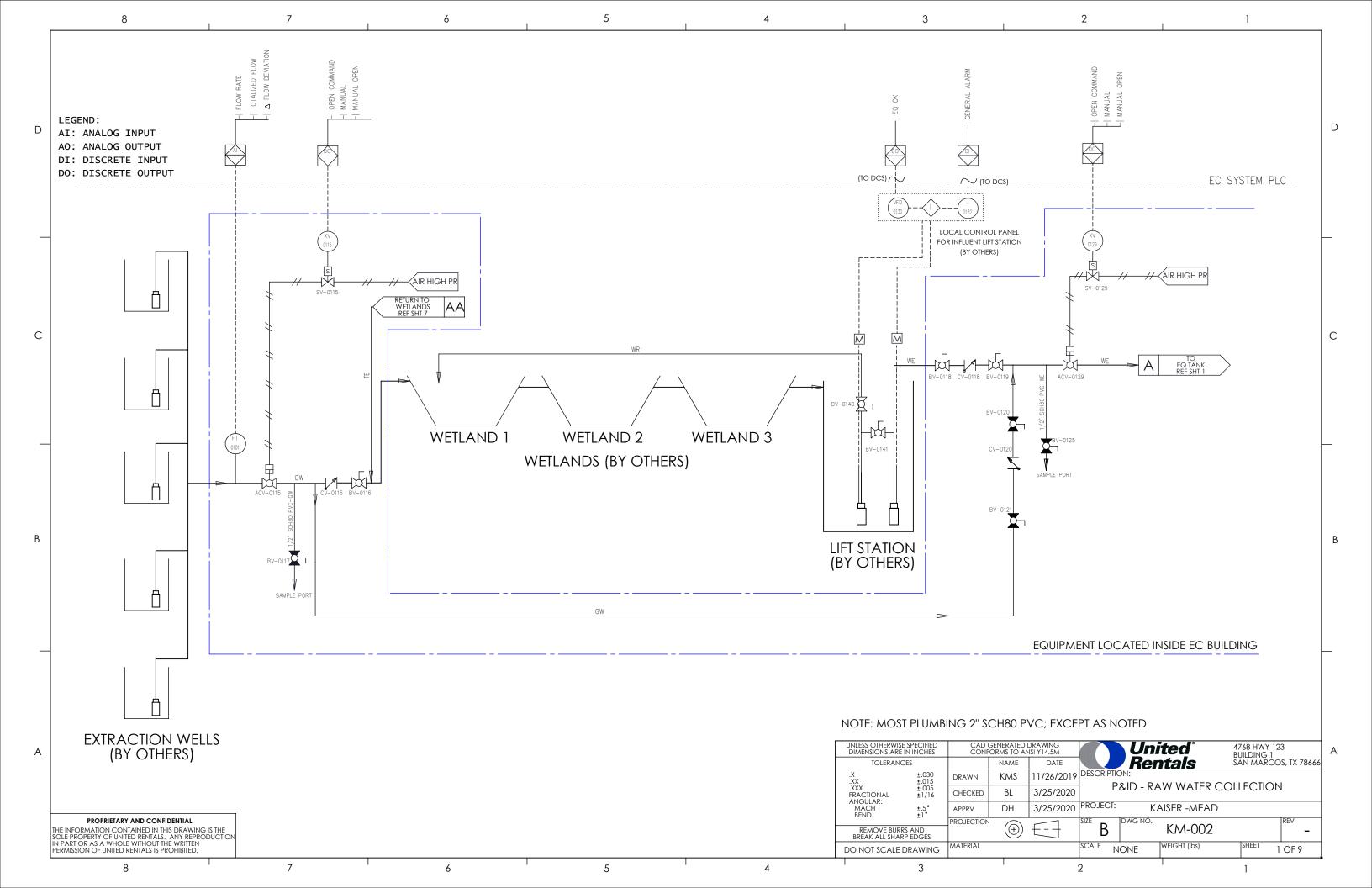


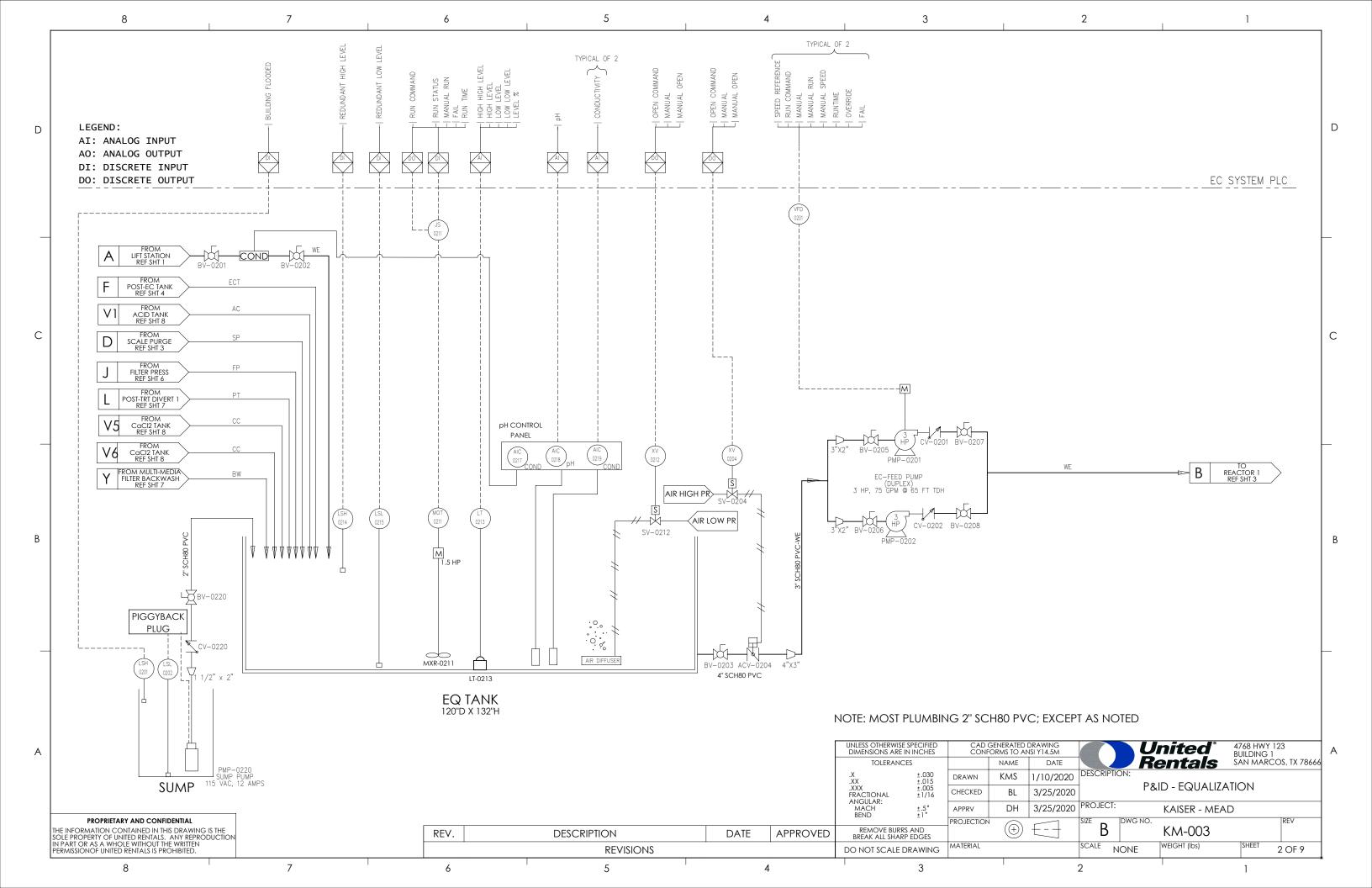


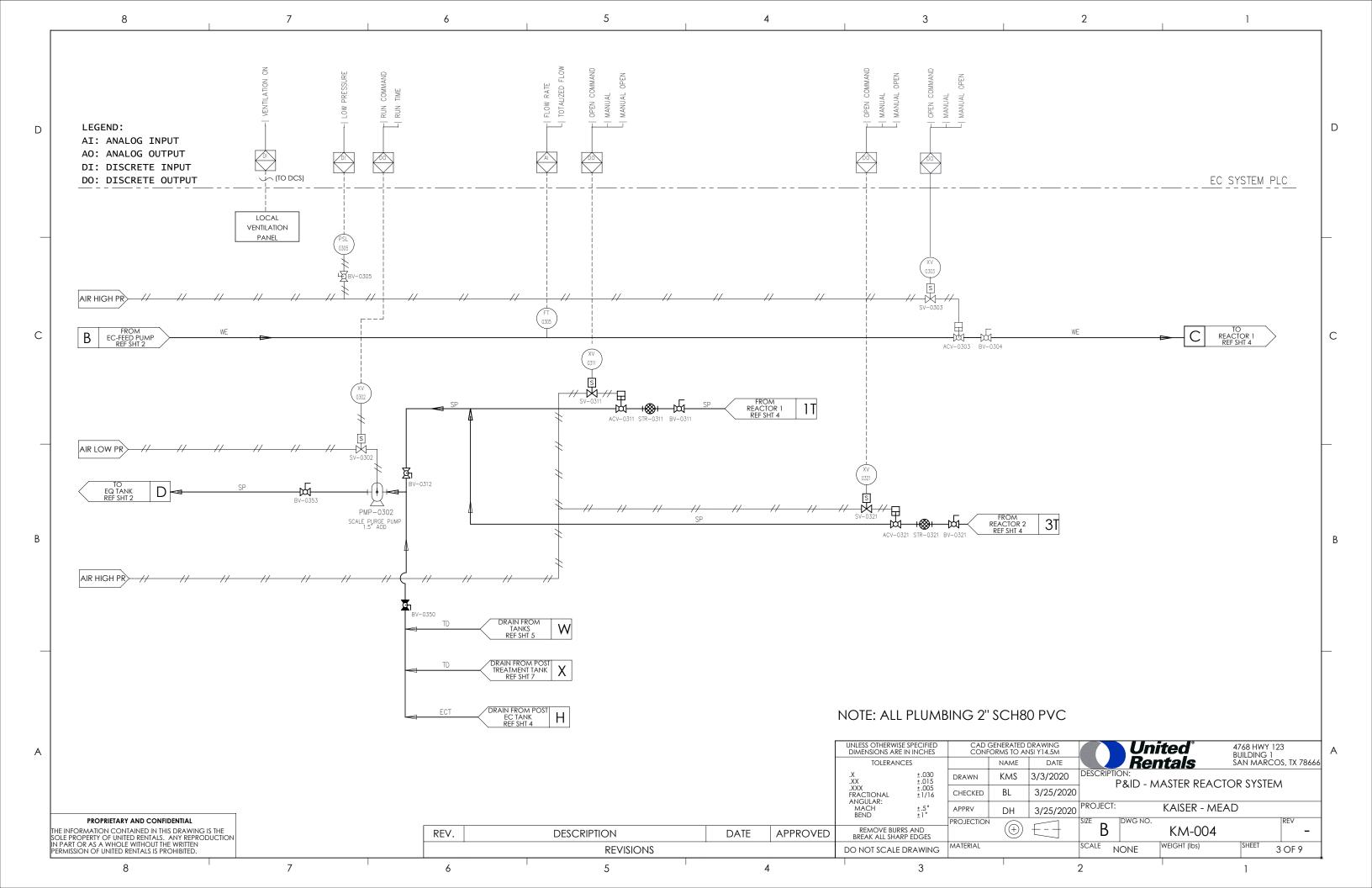


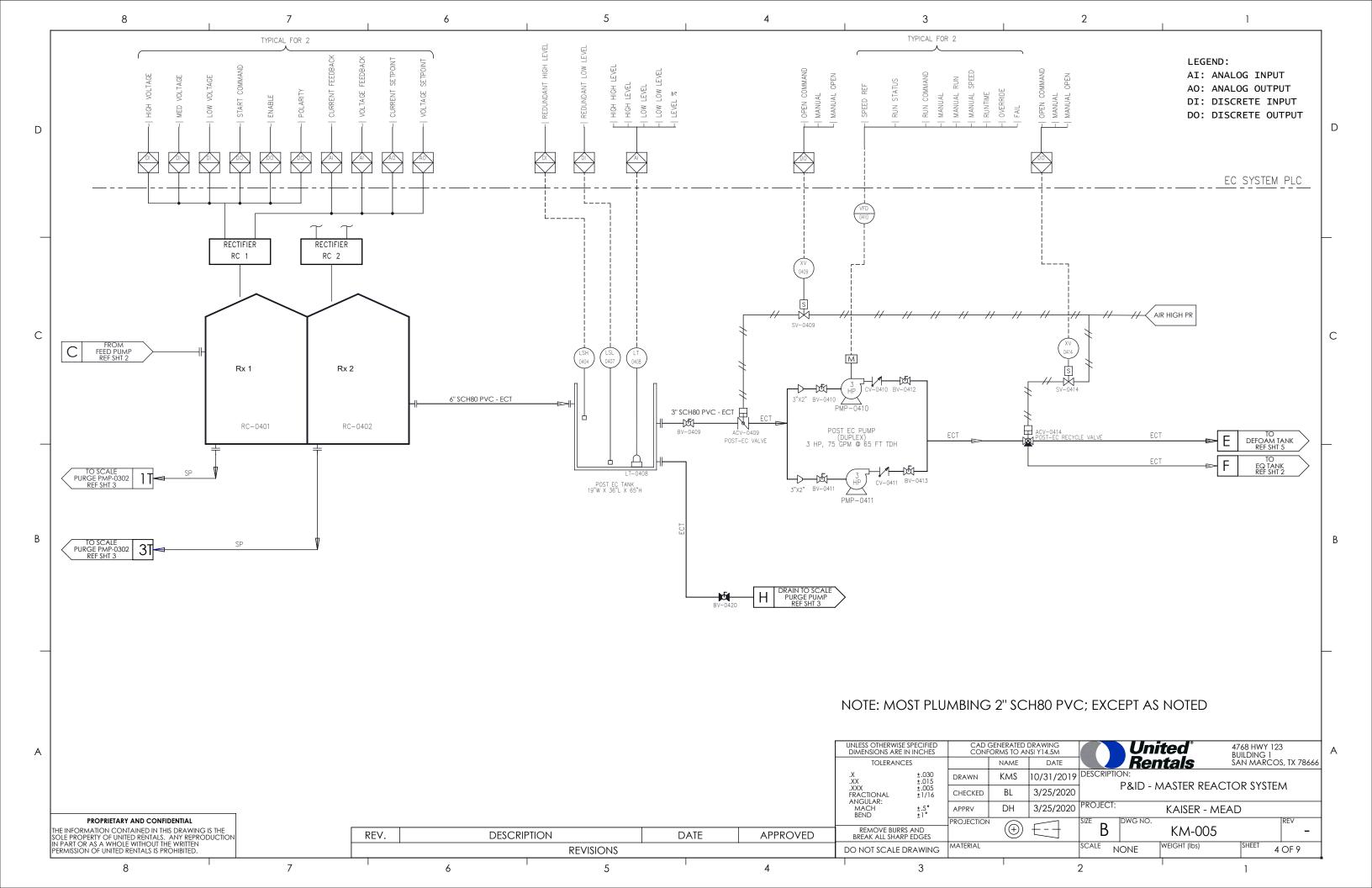


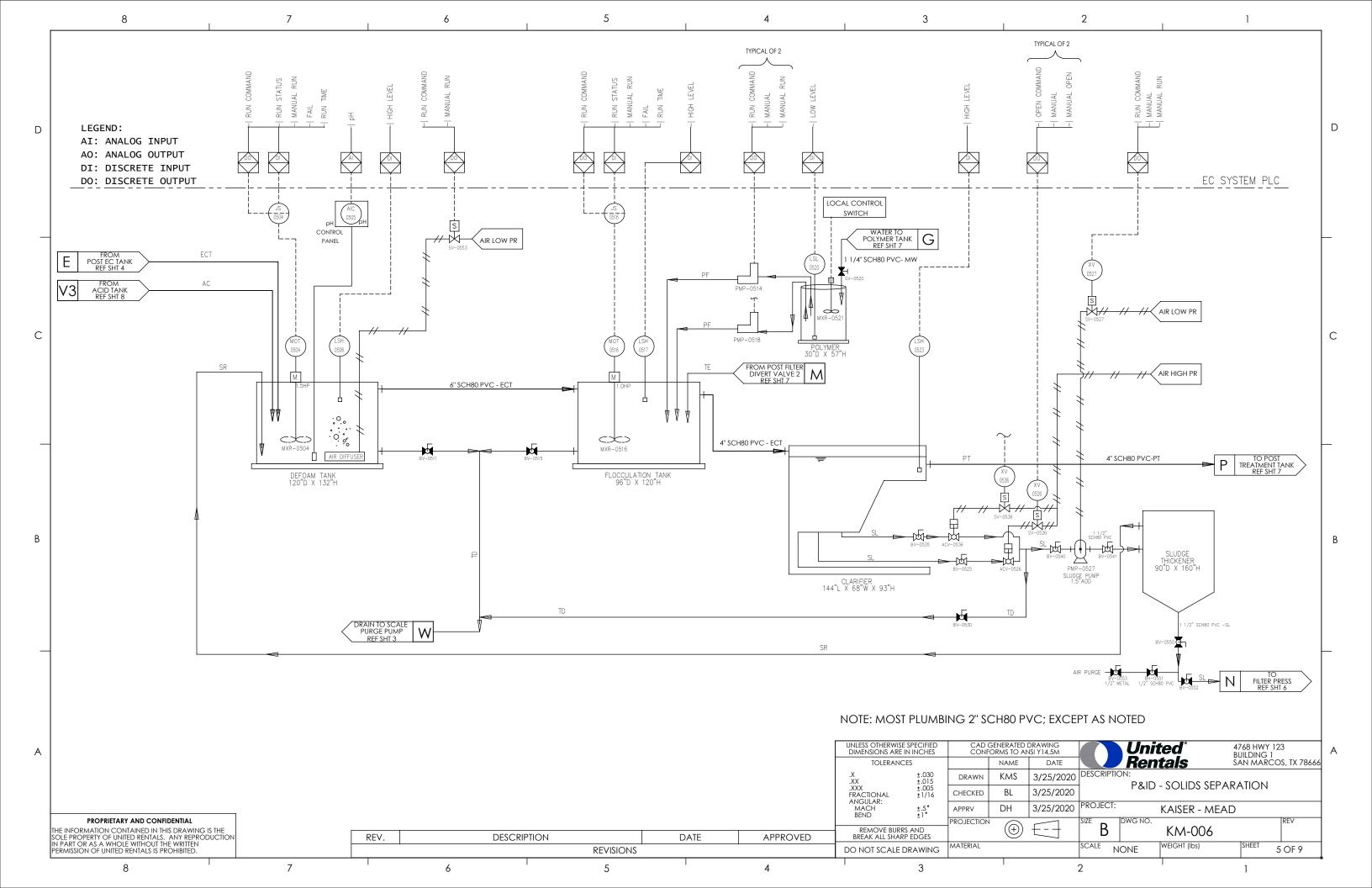


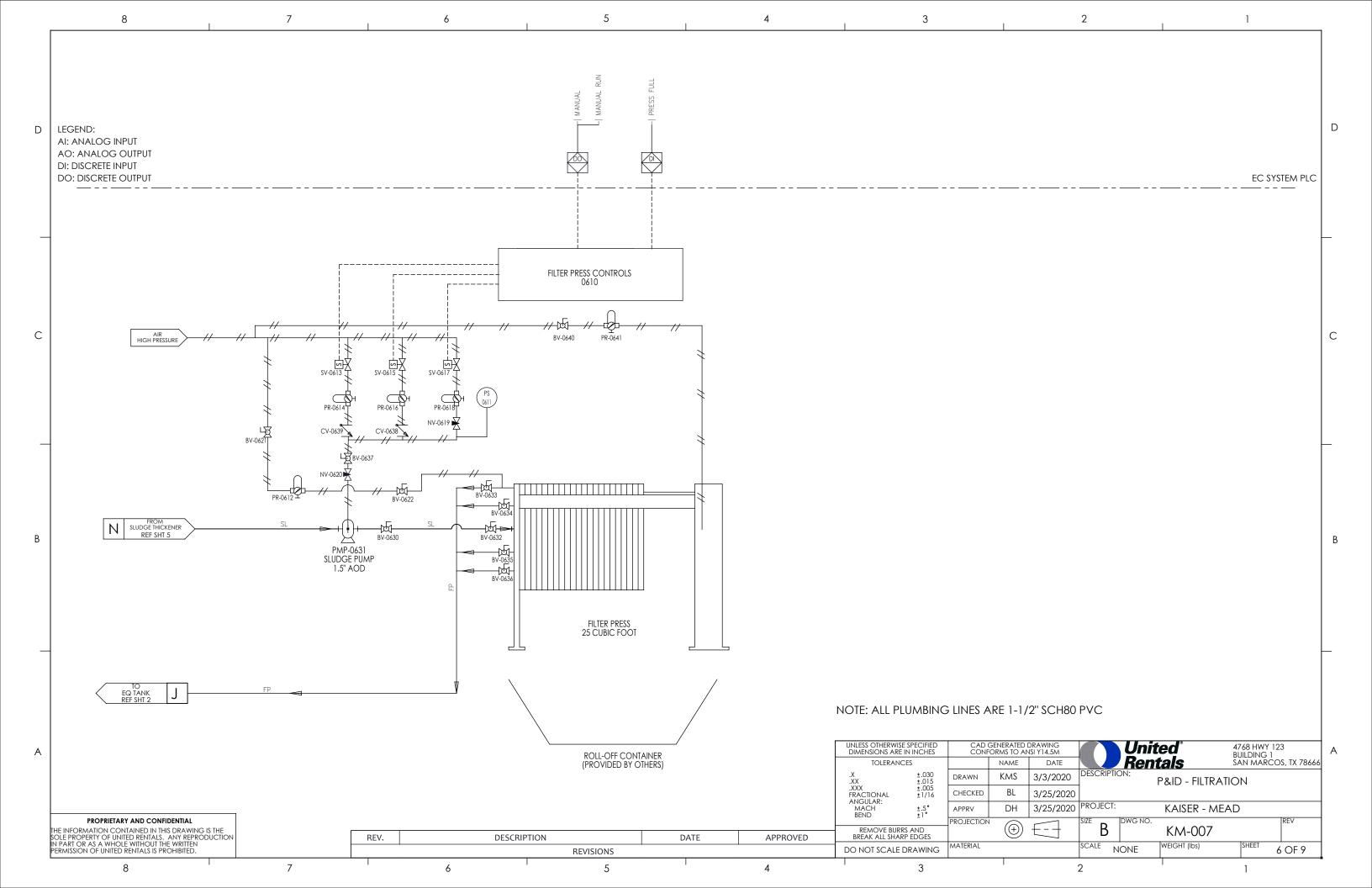


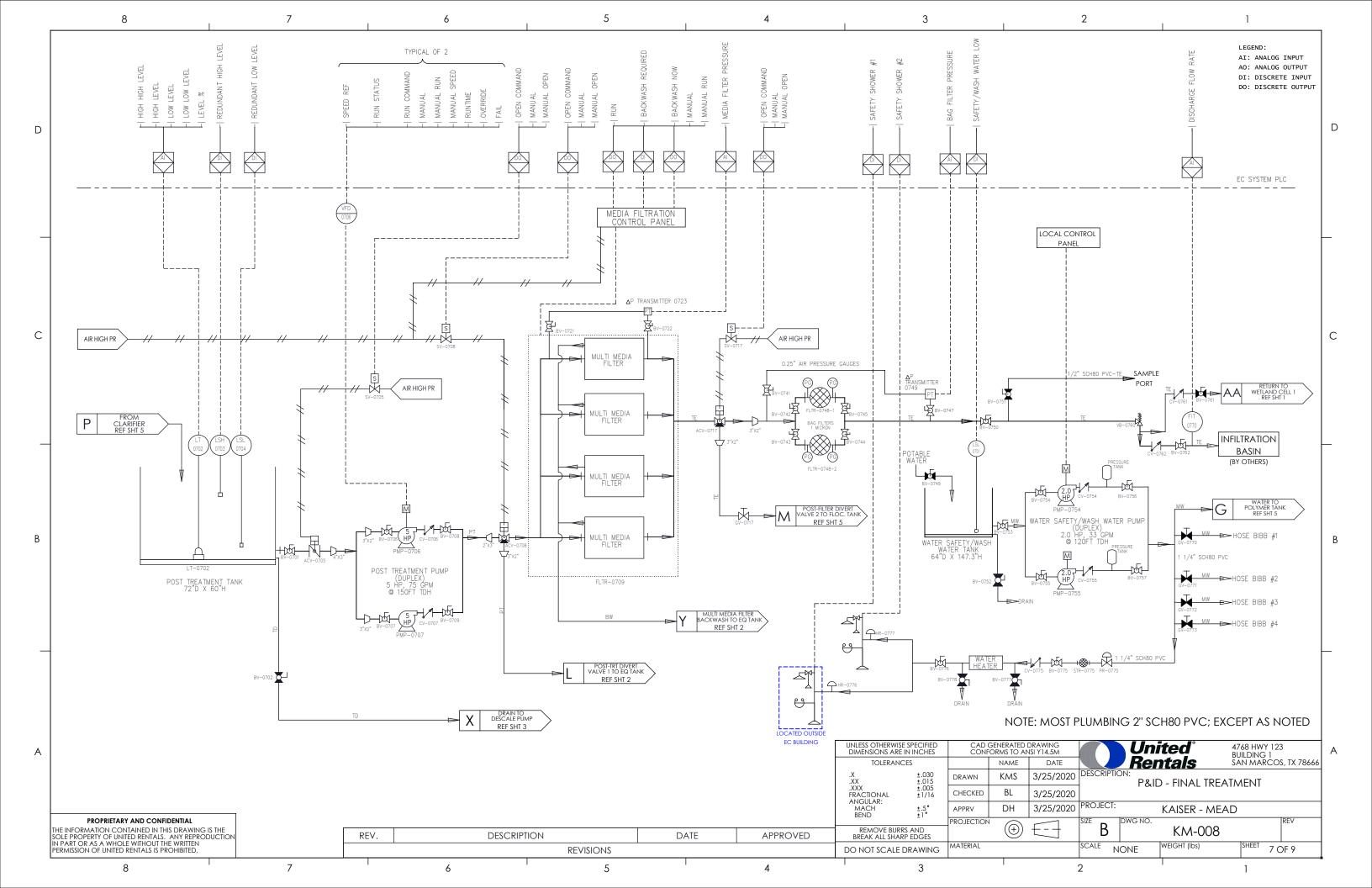


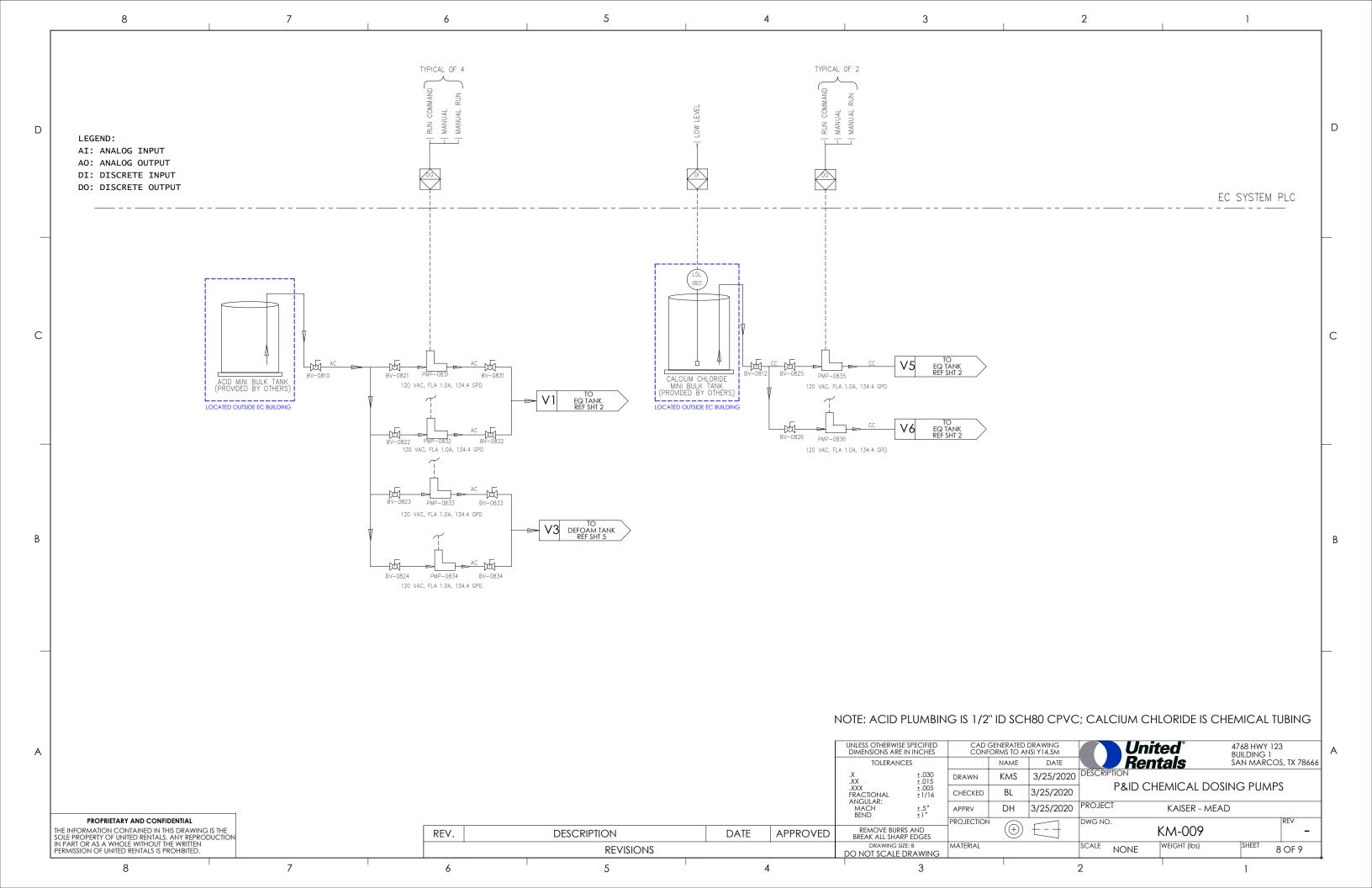


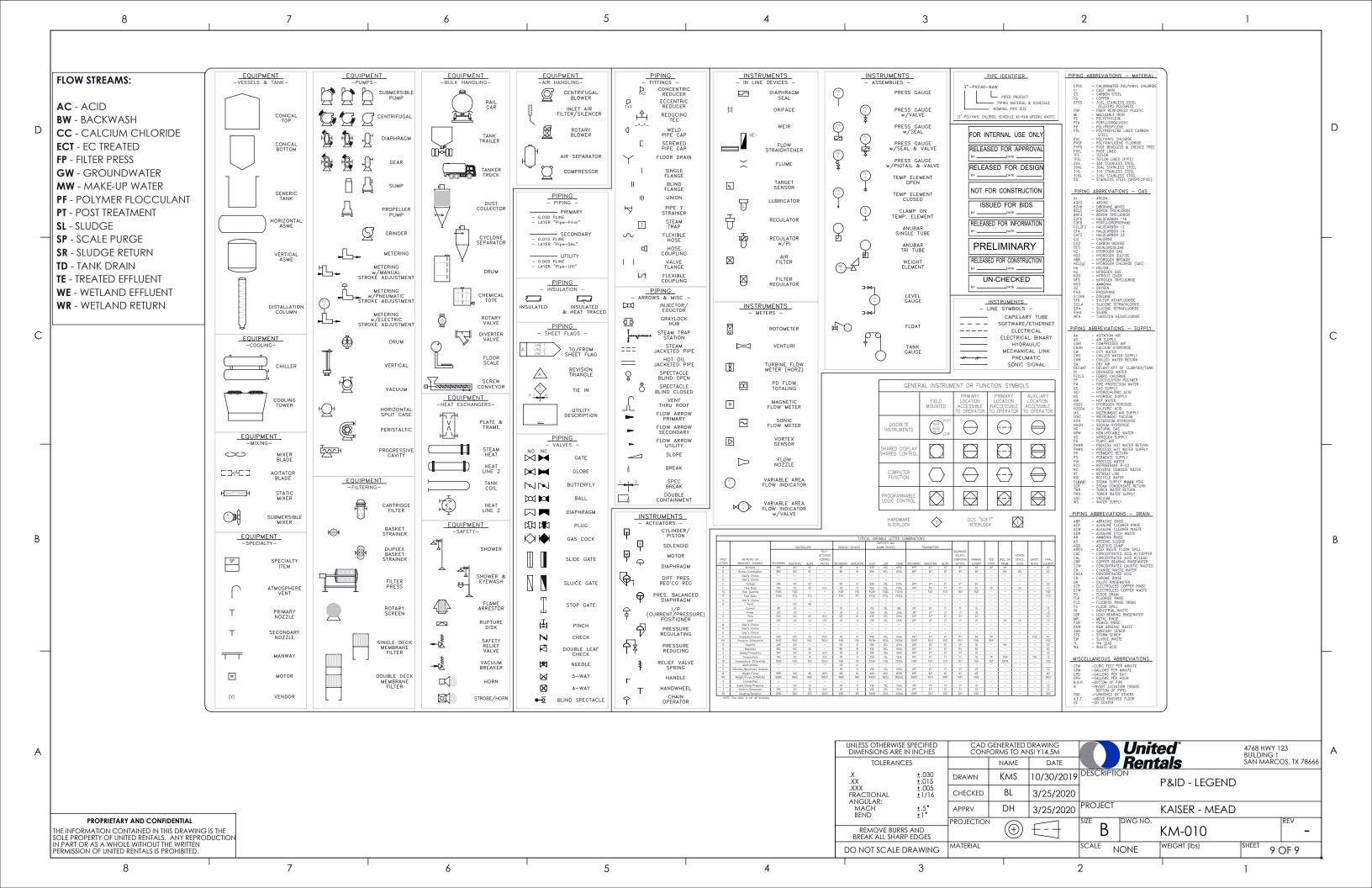


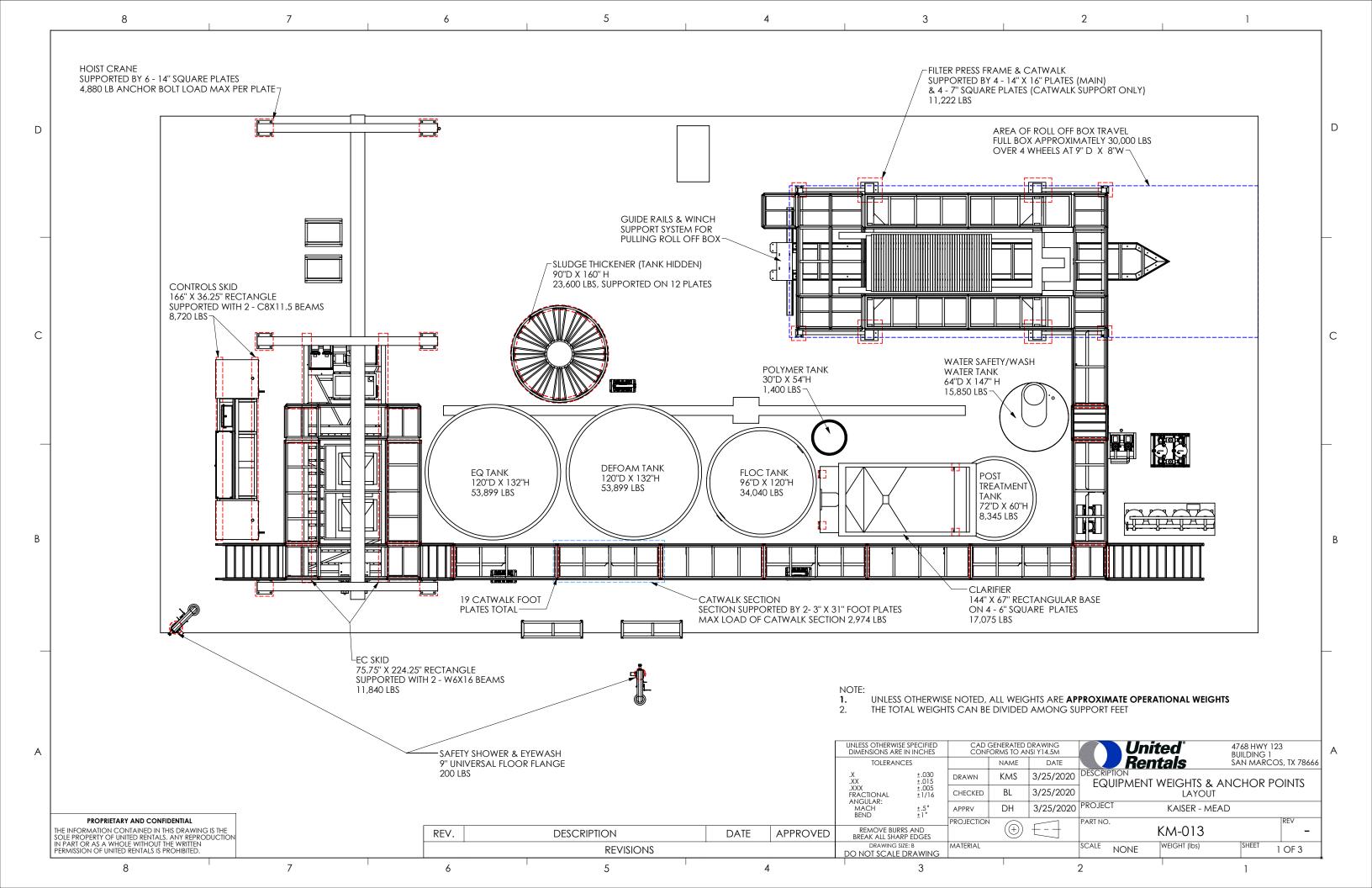


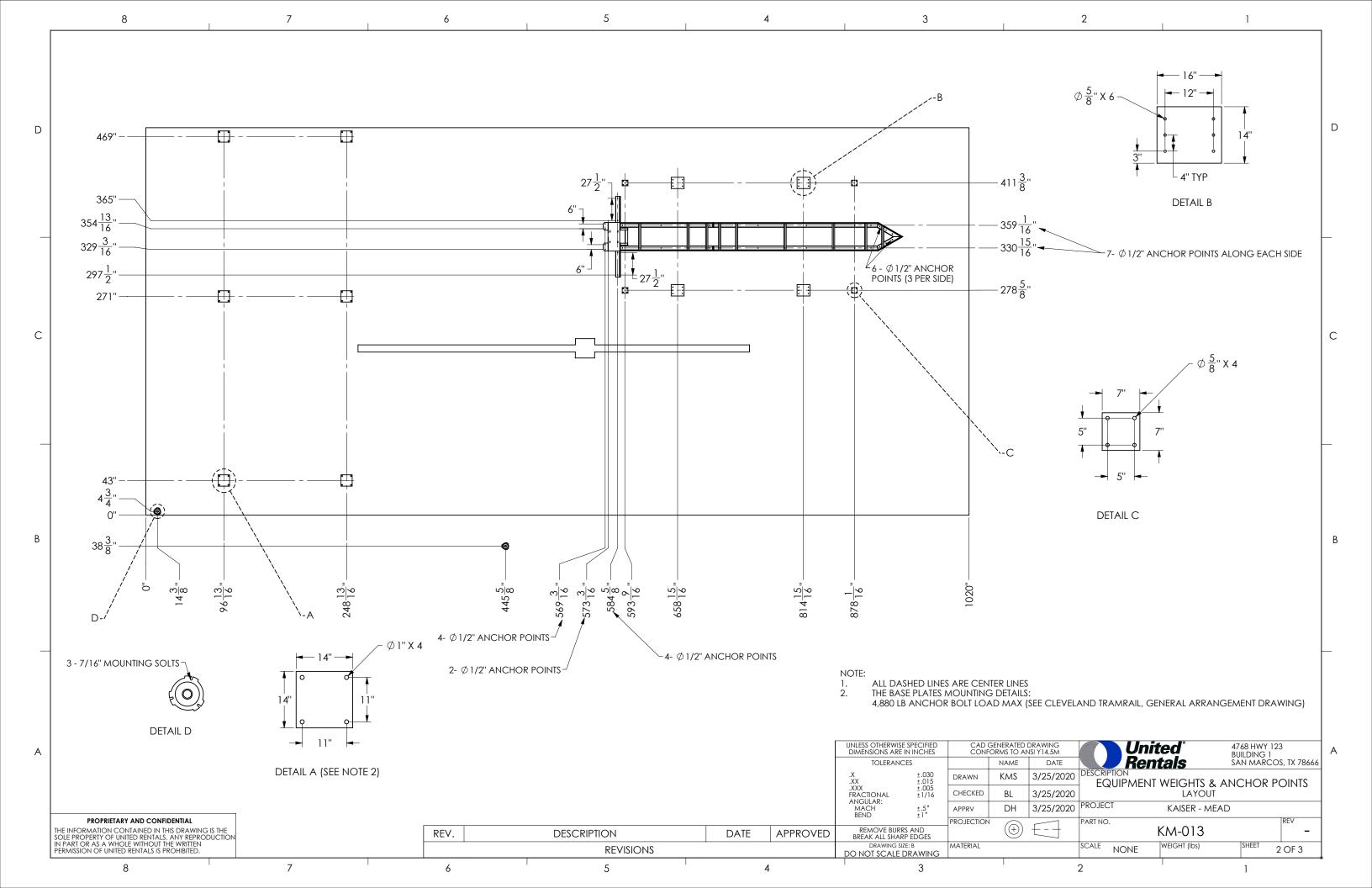


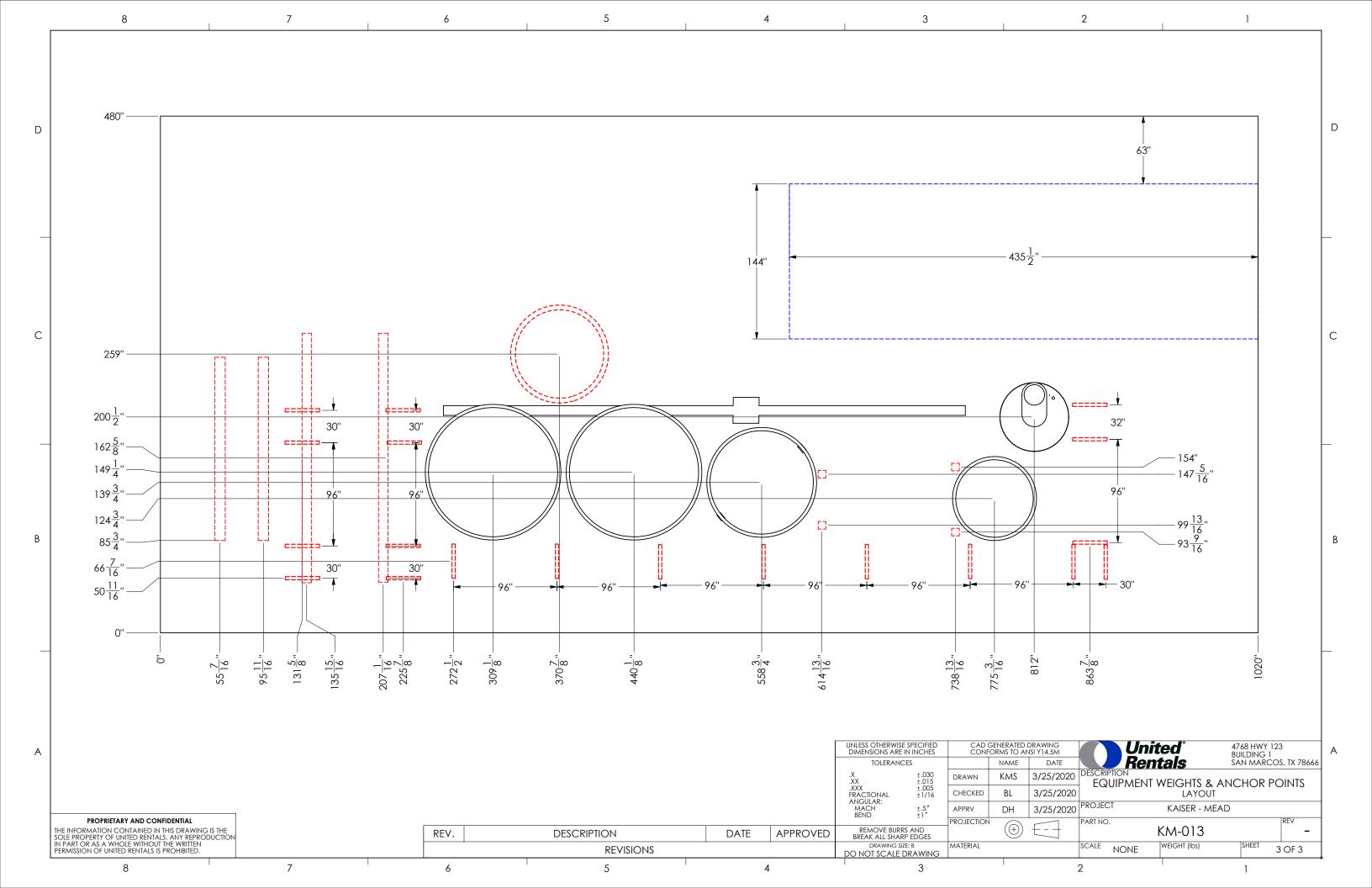


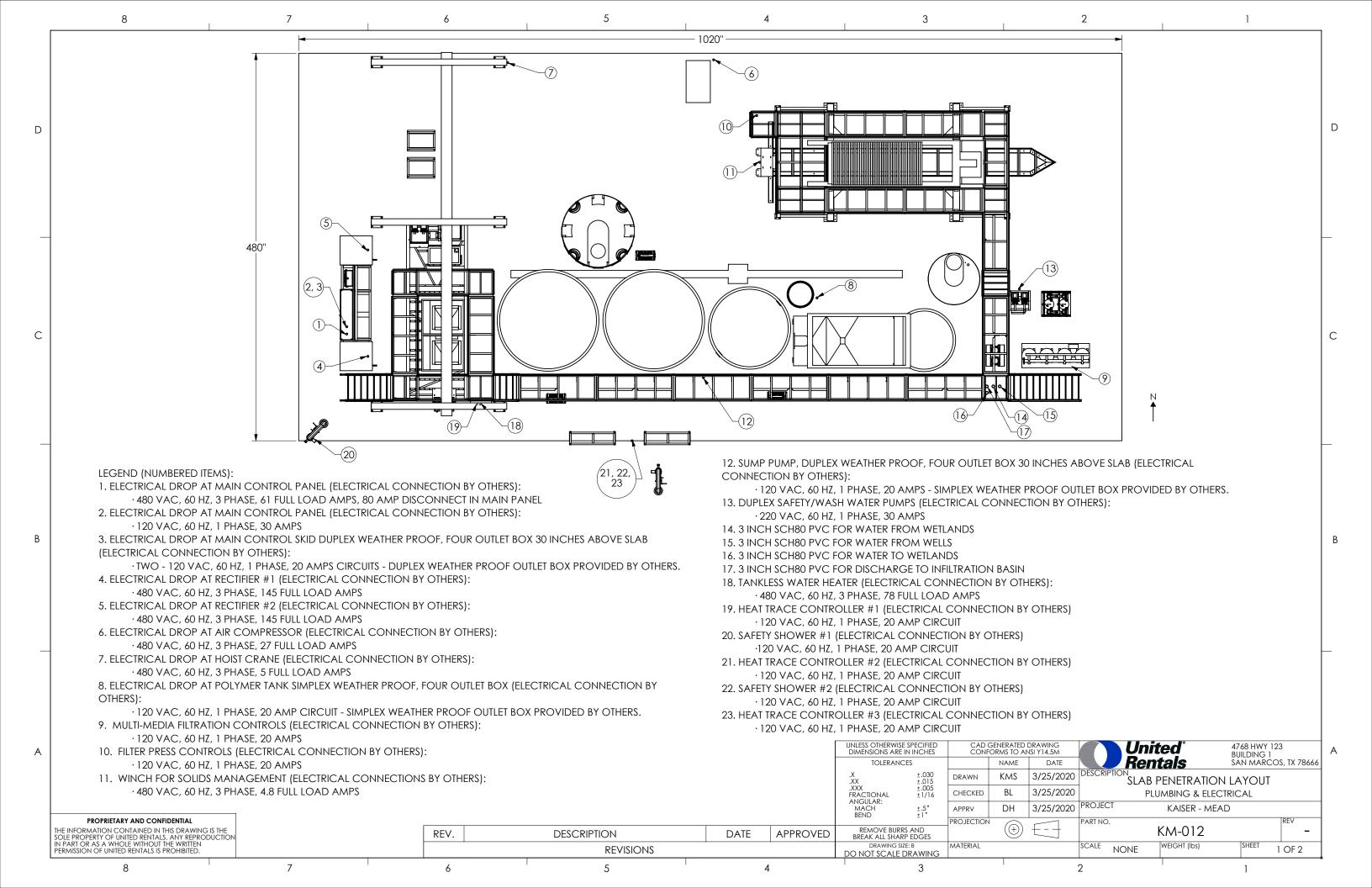


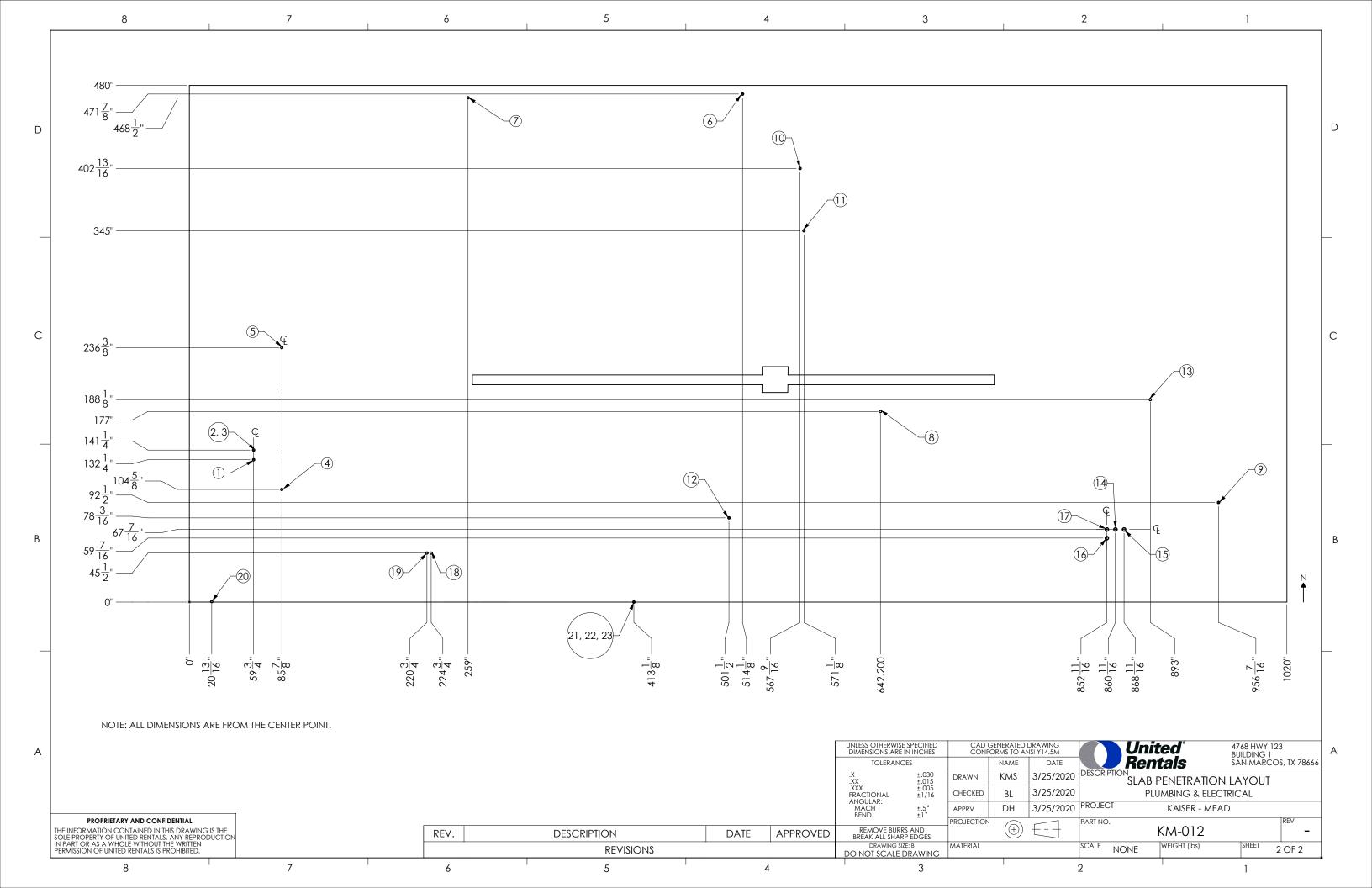












# **PART 1.0 GENERAL NOTES**

1.1 THIS DESIGN IS SITE SPECIFIC AND MAY NOT BE USED AT A DIFFERENT SITE WITHOUT THE ENGINEER'S WRITTEN PERMISSION.

1.2 ASE IS NOT RESPONSIBLE FOR ANY OF THE EXISTING BUILDING STRUCTURE IN WHICH THIS NEW FRAME SYSTEM WILL BE PLACED. SPECIFIC ELEMENTS OF THE NEW FRAME SYSTEM IS ALSO NOT INCLUDED IN OUR SCOPE OF WORK AS REQUESTED BY OUR CLIENT, INCLUDING BUT NOT LIMITED TO HANDRAILS, CATWALK ELEMENTS, HANDRAIL/CATWALK CONNECTIONS, AND SPECIFIC PRE-MANUFACTURED AND/OR PROPRIETARY ITEMS.

1.3 DO NOT SCALE THIS DRAWING. THIS IS A SCHEMATIC PLAN TO BE USED TO LOCATE AND IDENTIFY STRUCTURAL FRAMING ELEMENTS ONLY. DIMENSIONAL CONTROL IS THE RESPONSIBILITY OF THE BUILDER AND/OR CONTRACTORS TO FOLLOW THE ARCHITECTURAL PLANS, DESIGNER PLANS, OR EXISTING SITE CONDITIONS. USE THIS PLAN FOR PLACEMENT OF STRUCTURAL FRAMING ELEMENTS

1.4 THE CONTRACTORS SHALL VERIFY ALL DIMENSIONS, ELEVATIONS AND ALL OTHER NOTED ITEMS WITH ORIGINAL DESIGN PLANS PROVIDED BY UNITED RENTALS AND EXISTING SITE CONDITIONS PRIOR TO STARTING CONSTRUCTION. CONTRACTOR SHALL NOTIFY UNITED RENTALS AND ASE IN WRITING OF ANY DISCREPANCY AND FOR DIRECTIONS TO RESOLVE THE DISCREPANCY. THE ORIGINAL PLANS PROVIDED BY UNITED RENTALS TAKE PRECEDENCE OVER THIS DRAWING IF ANY NON-STRUCTURAL DIMENSIONAL DISCREPANCY EXISTS.

1.5 ASSUMPTIONS HAVE BEEN MADE BY THIS OFFICE REGARDING EXISTING CONDITIONS. ACTUAL CONDITIONS MAY VARY FROM THOSE ASSUMED. THE CONTRACTOR IS TO REPORT ANY SUCH DISCREPANCIES TO ASE FOR POSSIBLE MODIFICATIONS NEEDED TO THE CONTRACT DRAWINGS.

1.6 THE BUILDER SHALL COORDINATE THIS DRAWING WITH ALL STRUCTURAL, CIVIL, ELECTRICAL, AND MECHANICAL PLANS AND EXISTING SITE CONDITIONS AND SHALL NOTIFY THE DESIGNER AND ASE IN WRITING OF ANY DISCREPANCY AND FOR DIRECTIONS TO RESOLVE THE DISCREPANCY.

1.7 SEE ORIGINAL DESIGN DRAWINGS PROVIDED BY UNITED RENTALS FOR MISCELLANEOUS ITEMS NOT SHOWN HEREIN.

1.8 ALL EXISTING FOUNDATION, SLAB, AND FOOTING MEMBERS ARE THE DESIGN RESPONSIBILITY OF OTHERS.

# PART 2.0 STRUCTURAL STEEL (DESIGNED PER AISC ASD 14TH EDITION)

2.1 ALL STRUCTURAL STEEL SHALL BE SUPPLIED AS FOLLOWS:

CHANNELS & ANGLES ASTM A36

I BEAMS ASTM A992, GRADE 50 STEEL TUBE ASTM A500, GRADE B STEEL PIPE ASTM A53, GRADE B

HIGH-STRENGTH BOLTS ASTM A325 ANCHOR RODS ASTM F1554, GRADE 36

2.2 ALL STRUCTURAL STEEL PERMANENTLY EXPOSED TO WEATHER SHALL BE HOT-DIP GALVANIZED AFTER FABRICATION CONFORMING TO ASTM A-123.

2.3 STRUCTURAL STEEL SHALL BE ERECTED TRUE AND PLUMB W/ TEMPORARY SUPPORTS AND BRACING FOR LATERAL STABILITY UNTIL ALL FRAMING ELEMENTS ARE IN PLACE AND STEEL CONNECTIONS ARE COMPLETED. STEEL ERECTION SHALL COMPLY WITH ALL APPLICABLE OSHA REQUIREMENTS.

2.4 NO STRUCTURAL MEMBER SHALL BE CUT, NOTCHED OR OTHERWISE ALTERED UNLESS APPROVED IN WRITING BY ASE.

2.5 WELDED CONNECTIONS: WELDING ELECTRODES FOR A36, A572 GRADE 50 AND SCHEDULE NO. 40 STEEL SHALL BE E70XX. RETURN FILLET WELDS FOR FRAMED CONNECTIONS 1/2" AT EACH END. SHOP CONNECTIONS SHALL BE WELDED.

2.6 ALL CONTACT POINTS BETWEEN ANGLES, PLATES, BEAMS, ETC. SHALL BE WELDED USING E70XX ELECTRODES UNLESS NOTED OTHERWISE.

2.7 WELDING SHALL CONFORM TO AWS D1.1. ALL WELDERS SHALL BE CURRENTLY CERTIFIED WITH THE AMERICAN WELDING SOCIETY.

2.8 ALL BOLT HOLES SHALL BE MACHINE PUNCHED OR DRILLED, NOT FIELD BURNED. ALL BOLT HOLES SHALL BE 1/16" LARGER THAN BOLT DIAMETER.

# PART 3.0 SHOP DRAWINGS AND SUBMITTALS

3.1 SUBMIT SHOP DRAWINGS TO ASE FOR REVIEW PRIOR TO FABRICATION. DIMENSIONS WILL NOT BE CHECKED AND ANY ERRORS IN DIMENSIONS SHOWN ON SHOP DRAWINGS SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.

3.2 MATERIAL FABRICATORS SHALL PROVIDE COMPLETE DRAWINGS SHOWING LOCATION AND POSITION OF ALL STRUCTURAL ITEMS. ALL SUBMITTED SHOP DRAWINGS SHALL CONTAIN CLEAR IDENTIFICATION OF ALL DEVIATIONS FROM THE CONTRACT DOCUMENTS.

3.3 SHOP DRAWINGS SHALL NOT CONTAIN REPRODUCTIONS OF THE CONTRACT DOCUMENTS. SUBMITTALS SHALL CONFORM TO REQUIREMENTS OF CONTRACT DOCUMENTS, AND SHALL BE CHECKED AND MARKED "APPROVED" BY CONTRACTOR PRIOR TO SUBMITTAL. NON-CONFORMING SUBMITTALS WILL BE RETURNED WITHOUT REVIEW.

3.4 NO CHANGES ARE PERMITTED IN CONSTRUCTION FROM THAT SHOWN IN THE APPROVED SHOP DRAWINGS EXCEPT BY SPECIFIC WRITTEN APPROVAL OF ASE.

# PART 4.0 DESIGN DATA AND CRITERIA

**4.1** STRUCTURAL DESIGN LOADS:

LIVE LOADS: CATWALK LIVE LOAD - 40 PSF FILTER CHAMBER TANK LIVE LOAD - 10 KIPS (FULL) WENCH CAPACITY (APPLIED TO ROLL OFF BOX RAIL SYSTEM) - 11 KIPS

CATWALK DEAD LOADS - 10 PSF SELF-WEIGHT OF STEEL ELEMENTS - VARIES

ASSOCIATED STRUCTURAL ENGINEERS, INC.

FIRM NUMBER F-2820 2405 S. INTERSTATE 35

NEW BRAUNFELS, TX. 78130

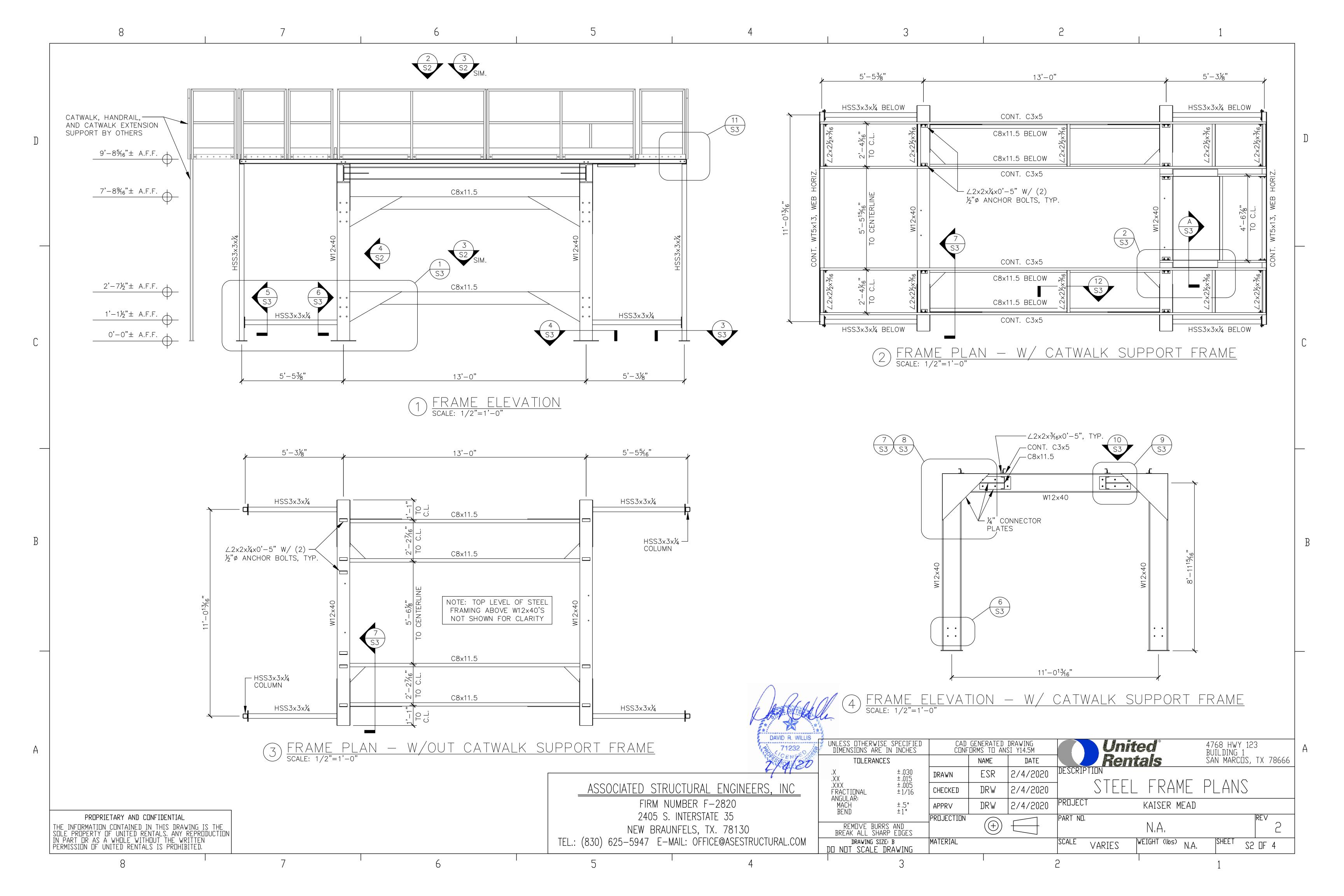
DAVID R. WILLIS

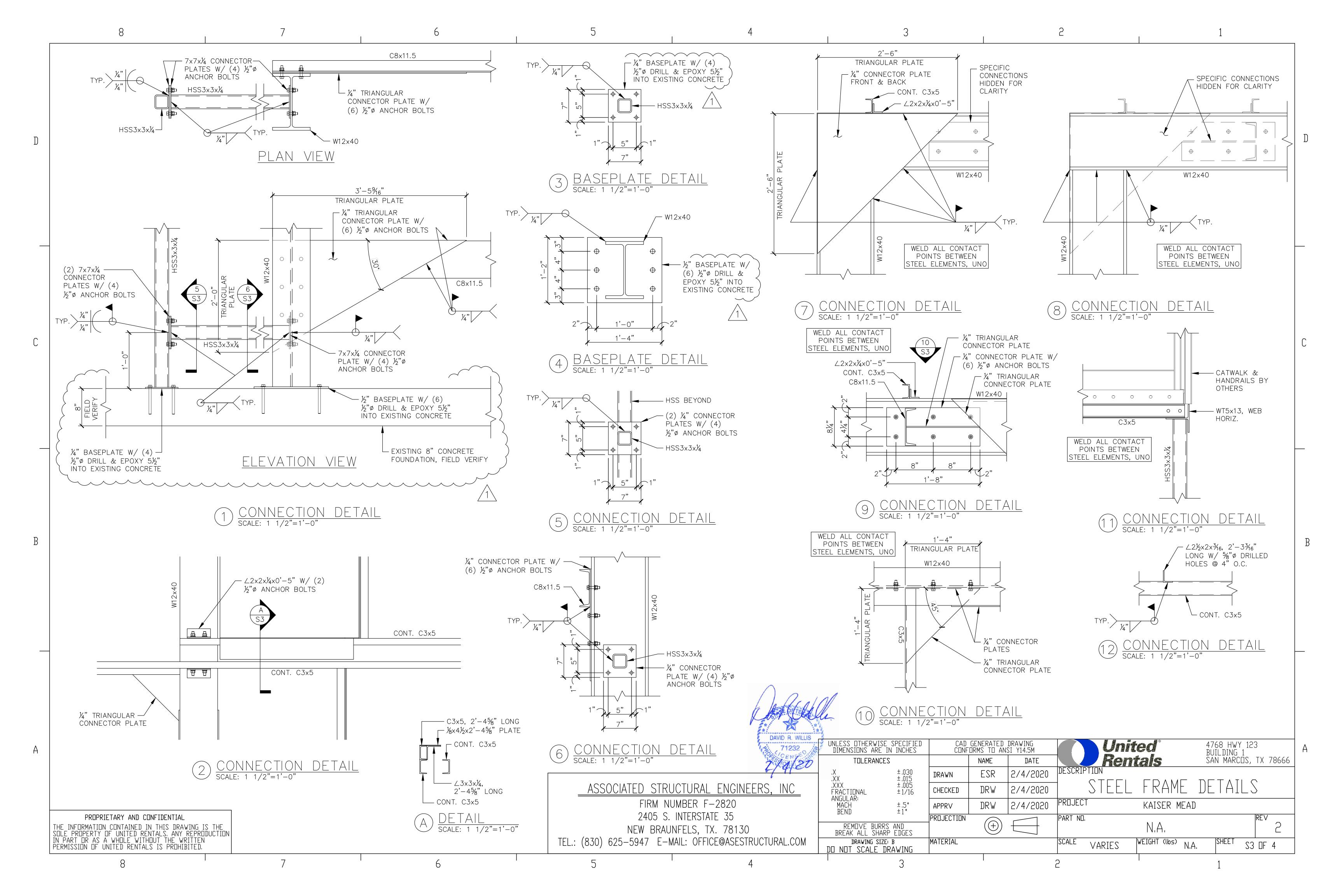
TEL.: (830) 625-5947 E-MAIL: OFFICE@ASESTRUCTURAL.COM

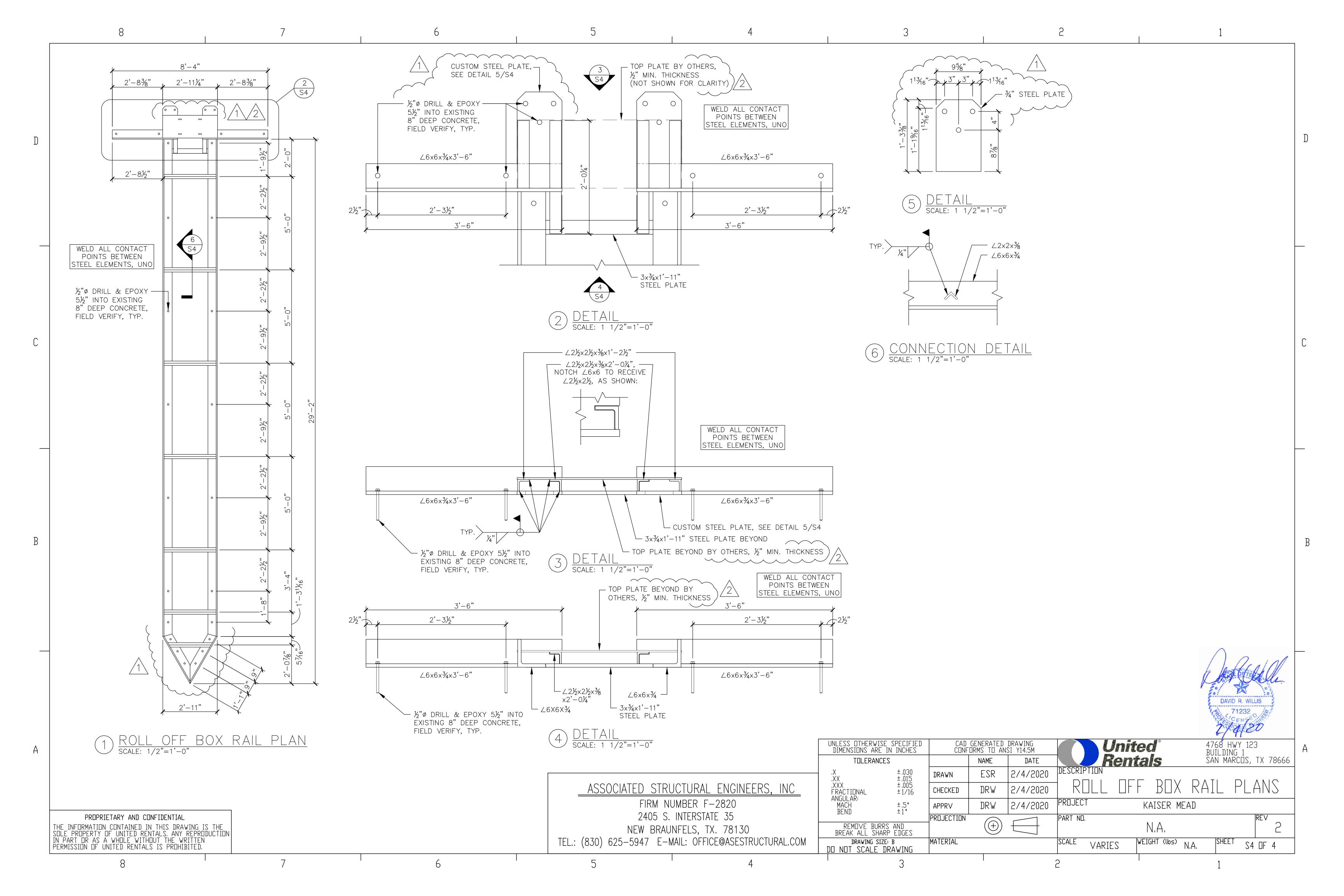
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES United CAD GENERATED DRAWING CONFORMS TO ANSI Y14.5M 4768 HWY 123 BUILDING 1 Rentals SAN MARCOS, TX 78666 TOLERANCES ± ,030 ± ,015 ± ,005 ± 1/16 2/4/2020 DRAWN ,XX GENERAL NOTES DRW 2/4/2020 CHECKED FRACTIONAL ANGULAR: PROJECT 2/4/2020 KAISER MEAD MACH BEND APPRV PROJECTION N.A. REMOVE BURRS AND BREAK ALL SHARP EDGES WEIGHT (lbs) N.A. DRAWING SIZE: B MATERIAL SHEET VARIES S1 DF 4 DO NOT SCALE DRAWING

PROPRIETARY AND CONFIDENTIAL THE INFORMATION CONTAINED IN THIS DRAWING IS THE

SOLE PROPERTY OF UNITED RENTALS, ANY REPRODUCTION IN PART OR AS A WHOLE WITHOUT THE WRITTEN PERMISSION OF UNITED RENTALS IS PROHIBITED.





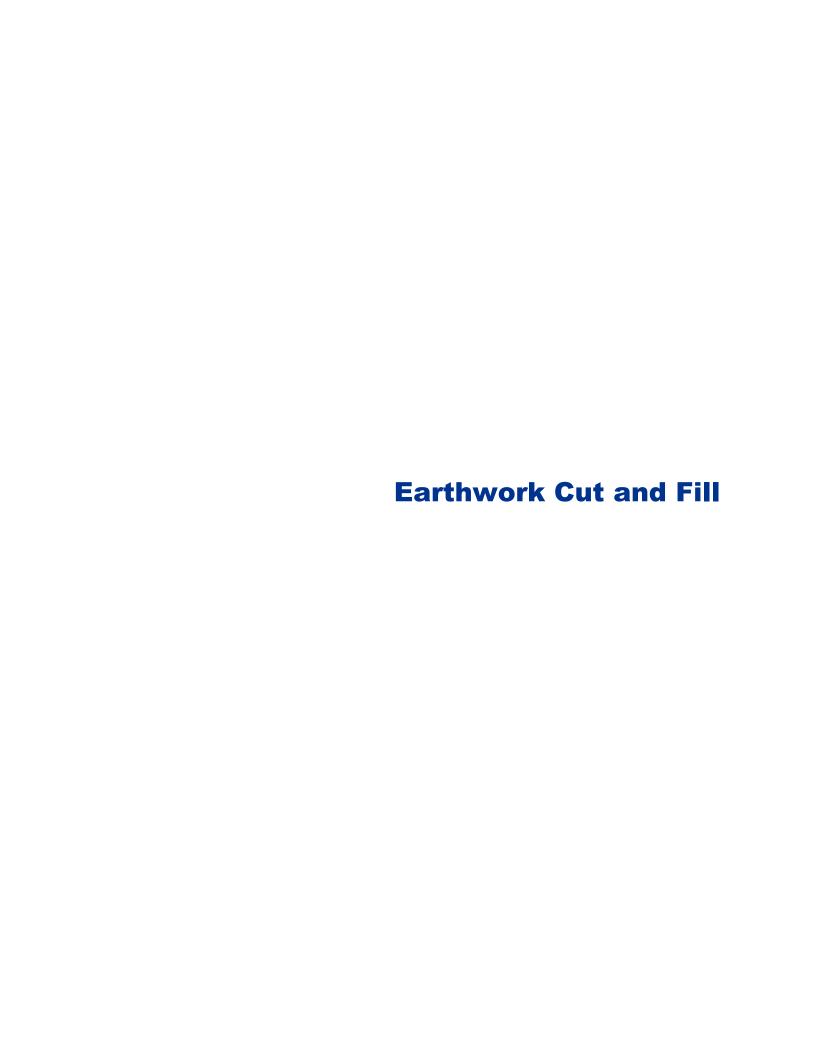


# **Appendix D Calculations**

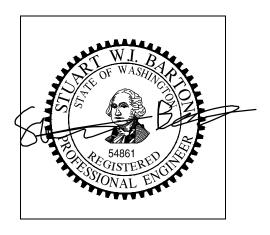
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# **Civil Calculations**



### EARTHWORK CUT AND FILL



Digitally Signed

on May 5, 2020

Stuart Barton

# **Cut/Fill Report**

2020-04-27 17:04:13 **Generated:** 

**BARTONS** By user:

C:\pw\_workdir\den003\jeg\_bartons\d0601468\C:\pw\_workdir\den003 **Drawing:** 

\jeg\_bartons\d0601468\Wetland\_Design.dwg

Volume Summary							
Name	Туре	Cut Factor	Fill Factor	2d Area (Sq. Ft.)	Cut (Cu. Yd.)	Fill (Cu. Yd.)	Net (Cu. Yd.)
Wetland Volume	full	1.00	1.00	106824.8	5081.95	3697.41	1384.54 <cut></cut>
Infilitration Basin Volume	full	1.00	1.00	25657.8	1846.49	1517.93	328.56 <cut></cut>
Fire Pond Volume	full	1.00	1.00	20064.6	1010.74	897.28	113.45 <cut></cut>

Totals				
	2d Area (Sq. Ft.)	Cut (Cu. Yd.)	Fill (Cu. Yd.)	Net (Cu. Yd.)
Total	152547.2	7939.18	6112.63	1826.55 <cut></cut>

<sup>\*</sup> Value adjusted by cut or fill factor other than 1.0

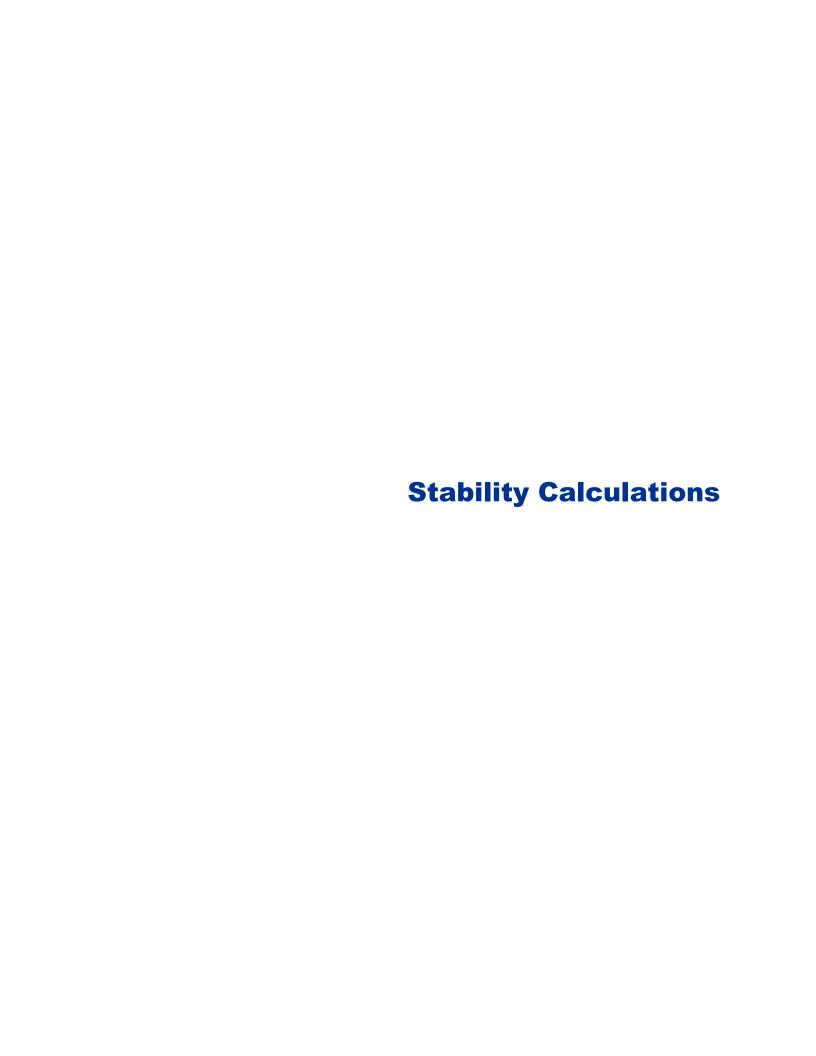
Source: AutoCAD Civil3D 2017 Stage Storage Report Generation Contours Drawn By Stu Barton

Cell 1

Contour	Contour	Depth	Incremental	Cumulative	
Elevation	Area		Volume	Volume	
(ft)	(sq. ft)	Avg. End	( ft)	(a ft)	
			(cu. ft)	(cu. ft)	
1,940.00	15,179.70	N/A	N/A	0	
1,941.00	16,849.10	1	16014.39	16014.39	
1,942.00	18,575.00	1	17712.02	33726.41	
1,943.00	20,357.30	1	19466.15	53192.56	
1,944.00	22,196.20	1	21276.8	74469.36	Hydraulic Profile elevation
1,945.00	24,091.70	1	23143.95	97613.31	
1,946.00	26,043.60	1	25067.62	122680.9	
Cell 2A					
Contour	Contour	Depth	Incremental	Cumulative	
Elevation	Area		Volume	Volume	
(ft)	(sq. ft)	Avg. End			
			(cu. ft)	(cu. ft)	
1,940.00	1,509.70	N/A	N/A	0	
1,941.00	2,145.50	1	1827.59	1827.59	
1,942.00	2,837.80	1	2491.63	4319.23	
1,943.00	3,586.60	1	3212.21	7531.44	
1,944.00	4,392.00	1	3989.33	11520.77	Hydraulic Profile elevation
1,945.00	5,253.90	1	4822.98	16343.75	,
1,946.00	6,172.40	1	5713.17	22056.91	
Cell 2B					
Contour	Contour	Depth	Incremental	Cumulative	
Contour Elevation	Contour Area	Depth	Incremental Volume	Cumulative Volume	
		Depth Avg. End			
Elevation	Area	•			
Elevation (ft)	Area (sq. ft)	Avg. End	Volume (cu. ft)	Volume (cu. ft)	
Elevation (ft) 1,938.00	Area (sq. ft) 9,796.70	Avg. End	Volume (cu. ft) N/A	Volume (cu. ft) 0	
Elevation (ft) 1,938.00 1,938.50	Area (sq. ft) 9,796.70 10,220.80	Avg. End N/A 0.5	Volume (cu. ft) N/A 5004.36	Volume (cu. ft) 0 5004.36	
1,938.00 1,938.50 1,939.00	Area (sq. ft) 9,796.70 10,220.80 10,651.90	Avg. End  N/A  0.5  0.5	Volume (cu. ft) N/A 5004.36 5218.17	Volume (cu. ft) 0 5004.36 10222.53	
1,938.00 1,938.50 1,939.00 1,939.50	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20	Avg. End  N/A  0.5  0.5  0.5	Volume (cu. ft) N/A 5004.36 5218.17 5435.54	Volume (cu. ft)  0 5004.36 10222.53 15658.07	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60	Avg. End  N/A  0.5  0.5  0.5  0.5	Volume (cu. ft)  N/A  5004.36  5218.17  5435.54  5656.46	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5	Volume (cu. ft)  N/A  5004.36  5218.17  5435.54  5656.46  5880.95	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50 1,941.00	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5	Volume (cu. ft)  N/A  5004.36  5218.17  5435.54  5656.46  5880.95	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50 1,941.00 1,941.50	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70	N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50 1,941.00 1,941.50	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70	N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50 1,941.00 1,941.50 1,942.00	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70	N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50 1,941.00 1,941.50 1,942.00	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80	N/A  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97	Hydraulic Profile elevation
Ilevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,941.00 1,942.00  Cell 3A  Contour	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80	N/A  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume  (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86	Volume  (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative	Hydraulic Profile elevation
1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,940.50 1,941.00 1,941.50 1,942.00 Cell 3A	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80 Contour	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  Depth	Volume  (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86	Volume  (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative	Hydraulic Profile elevation
Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,941.00 1,942.00  Cell 3A  Contour Elevation (ft)	Area (sq. ft) 9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80 Contour Area (sq. ft)	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  Depth  Avg. End	Volume  (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86  Incremental Volume  (cu. ft)	Volume  (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative Volume  (cu. ft)	Hydraulic Profile elevation
Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,941.00 1,942.00  Cell 3A  Contour Elevation (ft)	Area (sq. ft)  9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80  Contour Area (sq. ft)	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume  (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86  Incremental Volume  (cu. ft)  N/A	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative Volume (cu. ft)  0	Hydraulic Profile elevation
Ilevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,941.00 1,942.00  Cell 3A  Contour Elevation (ft)  1,938.00 1,938.50	Area (sq. ft)  9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80  Contour Area (sq. ft)  5,005.70 5,199.20	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume  (cu. ft)  N/A  5004.36 5218.17 5435.54  5656.46 5880.95 6109 6340.62 6379.86  Incremental Volume  (cu. ft)  N/A  2551.23	Volume  (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative Volume  (cu. ft)  0 2551.23	Hydraulic Profile elevation
Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,941.50 1,942.00  Cell 3A  Contour Elevation (ft)  1,938.00 1,938.50 1,939.00	Area (sq. ft)  9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80  Contour Area (sq. ft)  5,005.70 5,199.20 5,393.00	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86  Incremental Volume (cu. ft)  N/A  2551.23 2648.05	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative Volume (cu. ft)  0 2551.23 5199.28	Hydraulic Profile elevation
Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,942.00  Cell 3A  Contour Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50	Area (sq. ft)  9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80   Contour Area (sq. ft)  5,005.70 5,199.20 5,393.00 5,587.10	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume  (cu. ft)  N/A  5004.36 5218.17 5435.54  5656.46 5880.95 6109 6340.62 6379.86  Incremental Volume  (cu. ft)  N/A  2551.23	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative Volume (cu. ft)  0 2551.23 5199.28 7944.31	
Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,941.50 1,942.00  Cell 3A  Contour Elevation (ft)  1,938.00 1,938.50 1,939.00	Area (sq. ft)  9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80  Contour Area (sq. ft)  5,005.70 5,199.20 5,393.00	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86  Incremental Volume (cu. ft)  N/A  2551.23 2648.05 2745.03	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative Volume (cu. ft)  0 2551.23 5199.28	Hydraulic Profile elevation  Hydraulic Profile elevation
Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00 1,941.50 1,942.00  Cell 3A  Contour Elevation (ft)  1,938.00 1,938.50 1,939.00 1,939.50 1,940.00	Area (sq. ft)  9,796.70 10,220.80 10,651.90 11,090.20 11,535.60 11,988.20 12,447.80 12,914.70 12,604.80  Contour Area (sq. ft)  5,005.70 5,199.20 5,393.00 5,587.10 5,781.50	Avg. End  N/A  0.5  0.5  0.5  0.5  0.5  0.5  0.5  0.	Volume (cu. ft)  N/A  5004.36 5218.17 5435.54 5656.46 5880.95 6109 6340.62 6379.86  Incremental Volume (cu. ft)  N/A  2551.23 2648.05 2745.03 2842.14	Volume (cu. ft)  0 5004.36 10222.53 15658.07 21314.53 27195.48 33304.49 39645.11 46024.97  Cumulative Volume (cu. ft)  0 2551.23 5199.28 7944.31 10786.45	

Cell 3B

Contour Elevation	Contour Area	Depth	Incremental Volume	Cumulative Volume	
(ft)	(sq. ft)	Avg. End			
()	(-4)	6	(cu. ft)	(cu. ft)	
1,938.00	20,061.20	N/A	N/A	0	
1,938.50	20,606.60	0.5	10166.94	10166.94	
1,939.00	21,157.70	0.5	10441.08	20608.03	
1,939.50	21,714.60	0.5	10718.07	31326.1	
1,940.00	22,277.10	0.5	10997.9	42324	Hydraulic Profile elevation
1,940.50	22,845.30	0.5	11280.58	53604.58	•
1,941.00	23,418.90	0.5	11566.04	65170.62	
Infiltration Basin					
Contour	Contour	Depth	Incremental	Cumulative	
Elevation	Area		Volume	Volume	
(ft)	(sq. ft)	Avg. End			
			(cu. ft)	(cu. ft)	
1,919.00	6,659.00	N/A	N/A	0	
1,920.00	8,800.20	1	4400.22	4400.22	
1,921.00	10,997.70	1	9898.93	14299.15	Hydraulic Profile elevation
1,922.00	13,251.70	1	12124.73	26423.87	
Fire Pond					
Contour	Contour	Depth	Incremental	Cumulative	
Elevation	Area		Volume	Volume	
(ft)	(sq. ft)	Avg. End			
			(cu. ft)	(cu. ft)	
1,929.00	1,100.00	N/A	N/A	0	
1,930.00	1,578.30	1	1339.13	1339.13	
1,931.00	2,113.00	1	1845.65	3184.79	
1,932.00	2,704.40	1	2408.7	5593.49	Do not draw water down below 1,932
1,933.00	3,352.20	1	3028.27	8621.76	
1,934.00	4,056.50	1	3704.37	12326.13	
1,935.00	4,817.40	1	4436.99	16763.12	
1,936.00	5,634.80	1	5226.13	21989.25	
1,937.00	6,508.80	1	6071.8	28061.05	Water fill line designed as 1,937
1,938.00	7,439.20	1	6973.99	35035.04	
1,939.00	8,426.20	1	7932.7	42967.74	



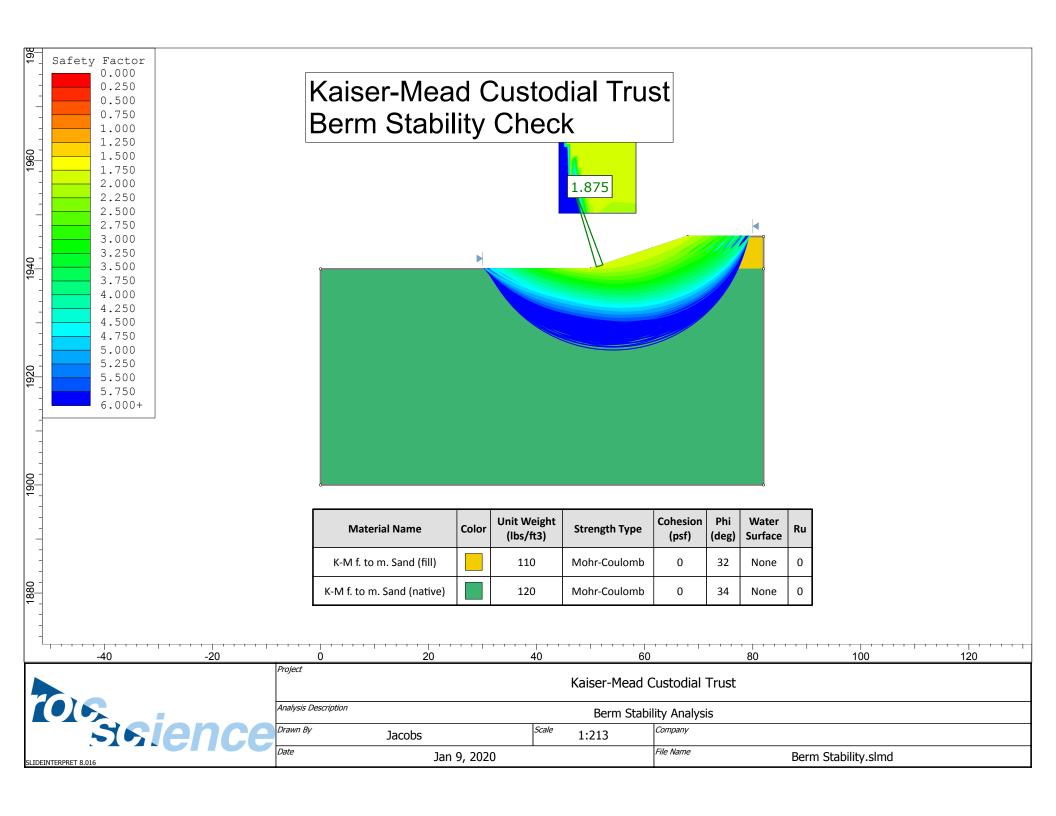
### STABILITY CALCULATIONS

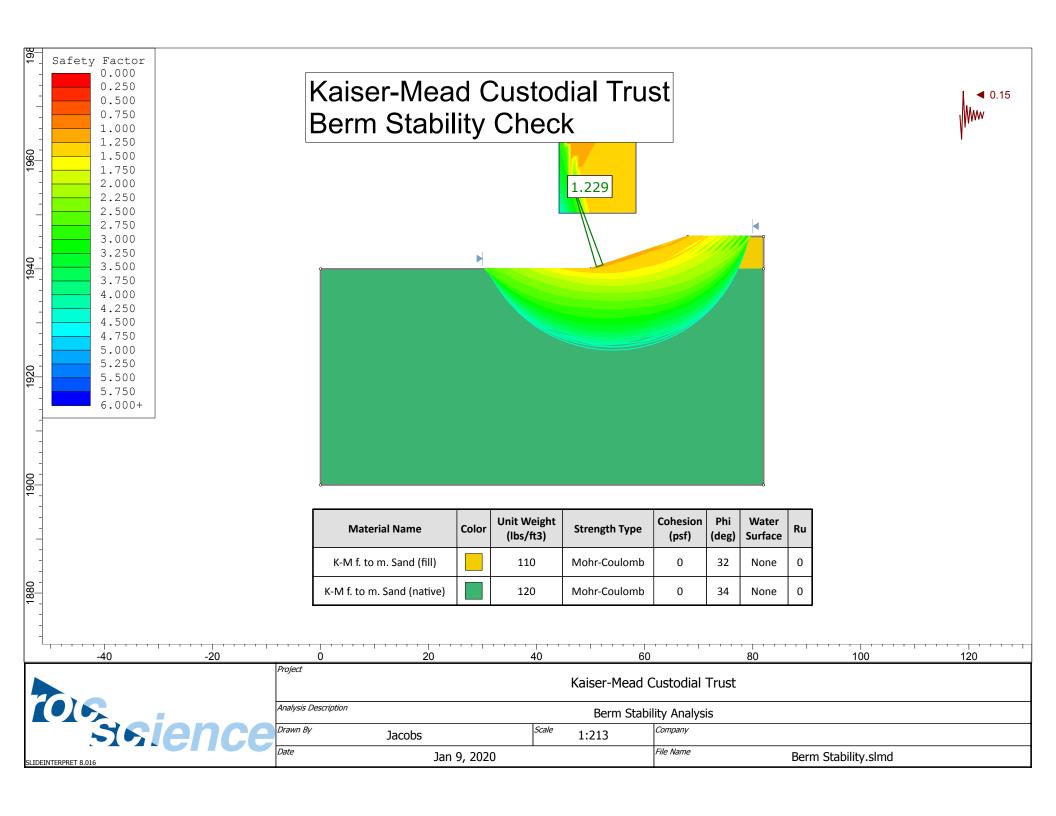


Digitally Signed on

April 3, 2020

Dave Paiko





Project: Kaiser-Mead Custodial Trust

Calculation: Slope Stability with Static and Pseudo-static analyses

Date: January 10, 2020

Material Properties – Design properties from Robert Martin/SPK 1/8/20 as follows:

Martin, Robert/SPK 2:39 PM:

I put on the design criteria sheet, 0 cohesion, 34 degrees friction angle, 120 pcf

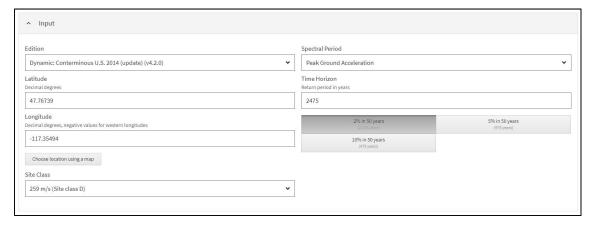
Static FS = 1.8 (Acceptable)

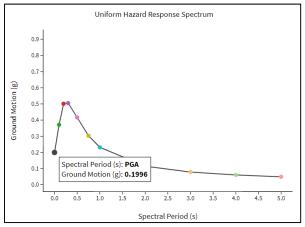
Psuedo-Static FS = 1.3 (Acceptable)

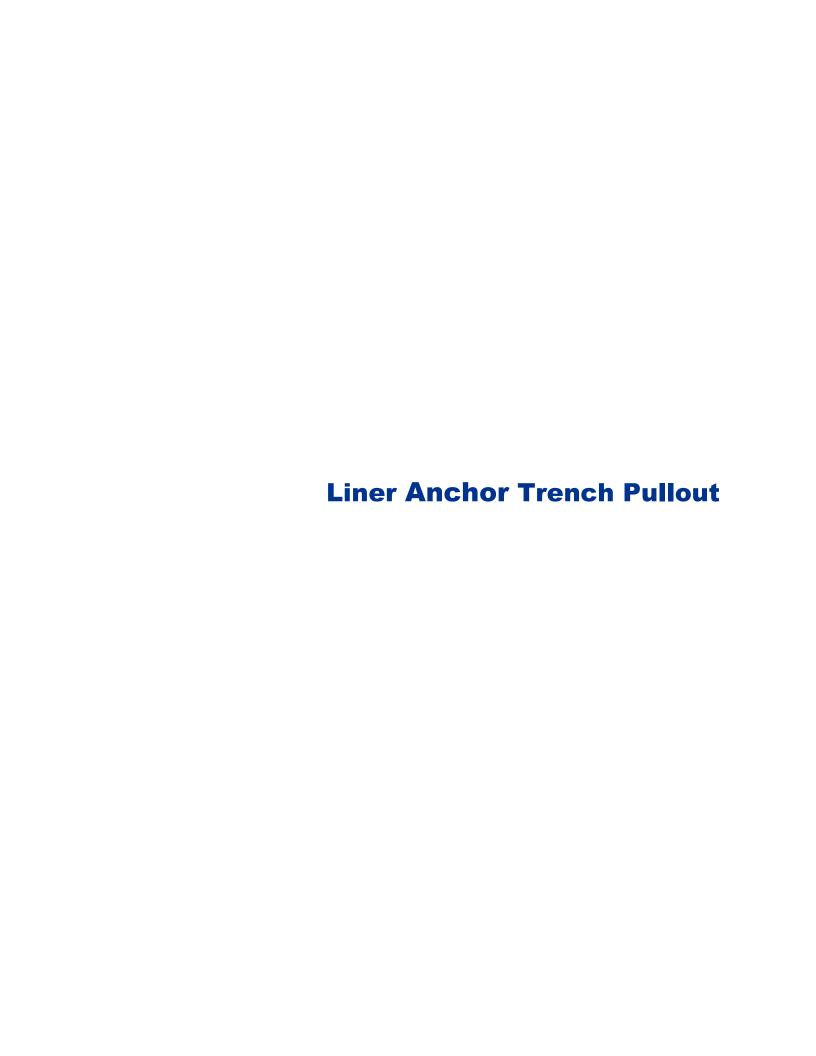
Max PGA for 2% in 50 years (2,475 years event) = 0.199

Typically use Kh = 0.5\*PGA = 0.10 - used 0.15 (assumed max PGA = 0.30) to be conservative

https://earthquake.usgs.gov/hazards/interactive/







The following Liner Anchor Trench Pullout calculation is for the geocomposite liner material GundSeal. The wetland liner system has since been revised to be constructed of separate geomembrane and geosynthetic clay composite lining materials. This revision does not substantively alter the properties of the geocomposite anchor trench relative to the conclusions of the calculation that the anchor forces do not exceed the geomembrane liner tensile strength. No revision of this calculation is necessary.



JUNE 2, 2020

LINER ANCHOR TRENCH PULLOUT



Digitally Signed on

April 3, 2020

Dave Paiko

**Method Reference:** Koerner, R.M. Xlibris Corporation, Bloomington, IN (2012). "Designing with Geosynthetics."

The purpose of this calculation is to verify the anchor trench design does not exceed the liner tensile strength.

#### **Project: Kaiser-Mead Custodial Trust**

Description: Project entails 3H:1V berm slopes constructed out of native or existing material. Liner subgrade consists of existing subgrade and fill material overlaine with 60-mil GSE Gundseal GCL. Liner trench will be backfilled and compacted using native fill material.

#### **Input Variables**

Backfill Soil	Trench Geometry

Unit weight of backfill soil:  $\gamma := 120 \cdot pcf$  Depth of cover soil:  $d_{cs} := 0 \cdot ft$ 

Friction angle of backfill soil:  $\phi := 34 \cdot deg$  Length of run out section:  $L_{ro} := 2 \cdot ft$ 

At rest earth pressure:  $k_0 := 1 - \sin(\phi)$  Depth of anchor trench:  $d_{at} := 2 \cdot ft$ 

Interface friction angle:  $\delta := 42 deg$  Length of anchor trench:  $L_{at} := 1 \cdot ft$ 

Cover Soil

Unit weight of cover soil:  $\gamma_{cs} := 120 \cdot pcf$ 

#### **Calculations**

Surcharge pressure:  $q := d_{cs} \cdot \gamma_{cs}$   $q = 0 \cdot psf$ 

Friction force below geomembrane:  $F_L := q \cdot tan(\delta) \cdot L_{ro}$   $F_L = 0 \cdot \frac{lbf}{ft}$ 

Friction force above geomembrane:  $F_{II} := 0$  assumed to be negligible

Friction force on anchor trench side:  $F_{at} := \left( d_{cs} + \frac{d_{at}}{2} \right) \cdot \gamma \cdot k_o \cdot \tan(\delta) \cdot d_{at} \qquad F_{at} = 95.3 \cdot \frac{lbf}{ft}$ 

Friction on anchor trench bottom  $F_{bot} := (d_{cs} + d_{at}) \cdot \gamma \cdot tan(\delta) \cdot L_{at}$   $F_{bot} = 216.1 \cdot \frac{lbf}{ft}$ 

#### Tension on Liner

$$T_A := F_L + F_U + 2 \cdot F_{at} + 2 \cdot F_{bot}$$
  $T_A = 623 \cdot \frac{lbf}{ft}$ 

 $L_{strength} \coloneqq 1080 \frac{lbf}{ft} \quad \textit{based on test data of 90 lb/in (allowable) for Gundseal GCL}$ 

#### Conclusion

Comparing anchor forces ( $T_A$ ) to liner properties strength, the anchor forces do not exceed liner tensile strength conservatively assuming interface friction of both sides of Gundseal is 42deg. Anchor Trench is acceptable.

# Shear strength assumptions based on GSE Environmental GundSeal GCL Design Manual

#### 3.2.1 Shear Strength Under Low-Normal Loads

3.2.1.1 <u>Dry Shear Strength Under Low-Normal Loads.</u> Figure 3.6 presents the recommended shear strength envelopes for dry GundSeal (bentonite moisture content, w < 30%) under low-normal loads [less than 2,000 psf (100 kPa)]. The shear strength envelopes for peak and residual [displacement of 2.25 in (57 mm)] conditions are approximated to be linear, with the following equations:

Chapter 3 - GundSeal Design For Slope Stability

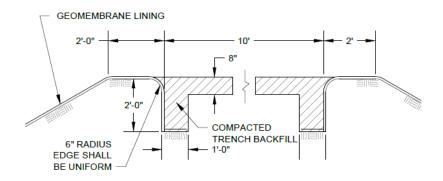
Page 3-19

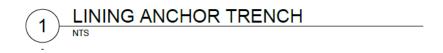
$$\tau_{(peak-day)} = \sigma \tan(48) \text{ [for } \sigma \leq 2,000 \text{ psf (96 kPa)]}$$
(3.17)

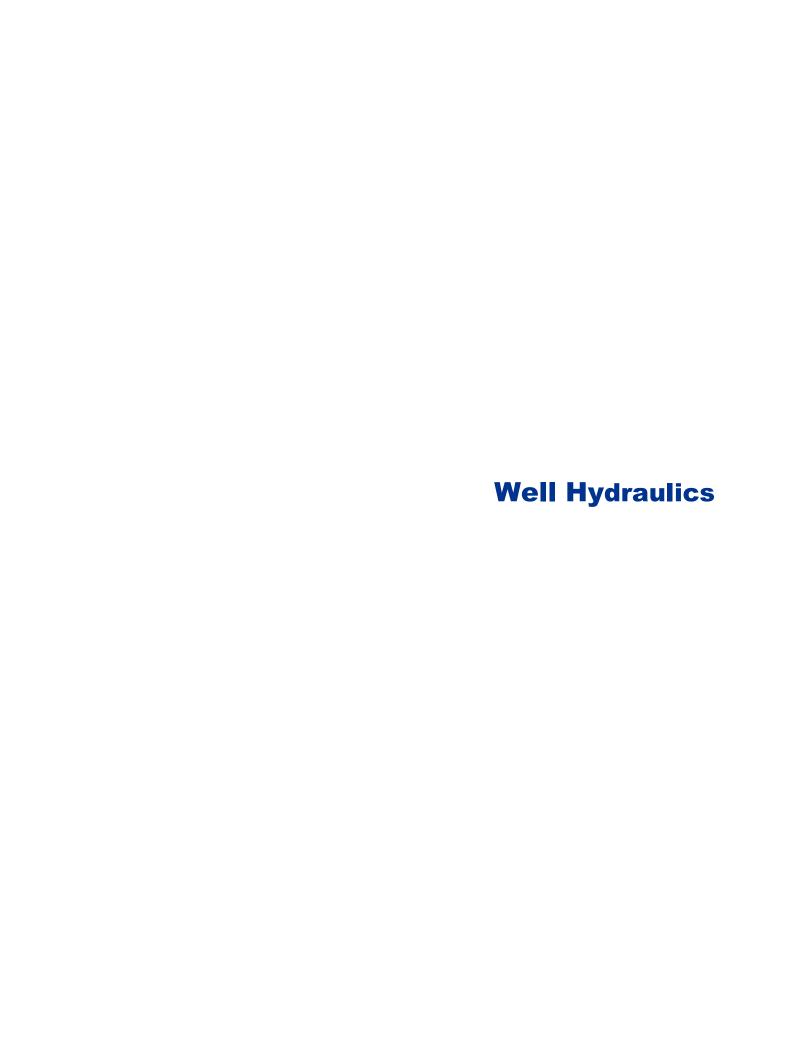
$$\tau_{(residual-dry)} = \sigma \tan(42) \quad \text{[for } \sigma \le 2,000 \text{ psf (96 kPa)]}$$
(3.18)

where,  $\tau$  = shear stress and  $\sigma$  = normal stress

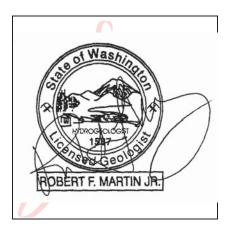
The shear strength envelopes were based on the most recent shear test data developed by the GeoSyntec Soil-Geosynthetic Interaction Testing Laboratory for this design manual. The laboratory data are presented in Appendix H. The envelopes were created by drawing a straight line from the origin through the shear strength data created at a 2,000 psf (100 kPa) normal load. These data are believed to be most representative of the dry shear strength of GundSeal using well-textured geomembranes.







### WELL HYDRAULICS



Digitally Signed on

April 3, 2020

Robert Martin



#### **CALCULATION COVER SHEET**

Project: Kaiser Mead Groundwater Remediation Issue Date: 01/15/2020

Interim Action

Client: Kaiser Mead Custodial Trust Project No. KMCT2019

Calculation Title: Groundwater and Well Hydraulics

Calculation Originator: Bob Martin
Calculation Checker: Mark Henry

Version	<b>Originator</b> Signature/Date	<b>Checker</b> Signature/Date
Pre-	Bob Martin	Mark Henry
Final	1/14/2020	1/15/2020

#### Comments:

Systematic approach is acceptable. Did not review explicit details of model input/calculations, but output seems reasonable given knowledge of aquifer properties. Reviewed provided tables for accuracy.

#### **Calculation Summary:**

Well Field Development drawdown, field parameters, and saturated zone profiling.

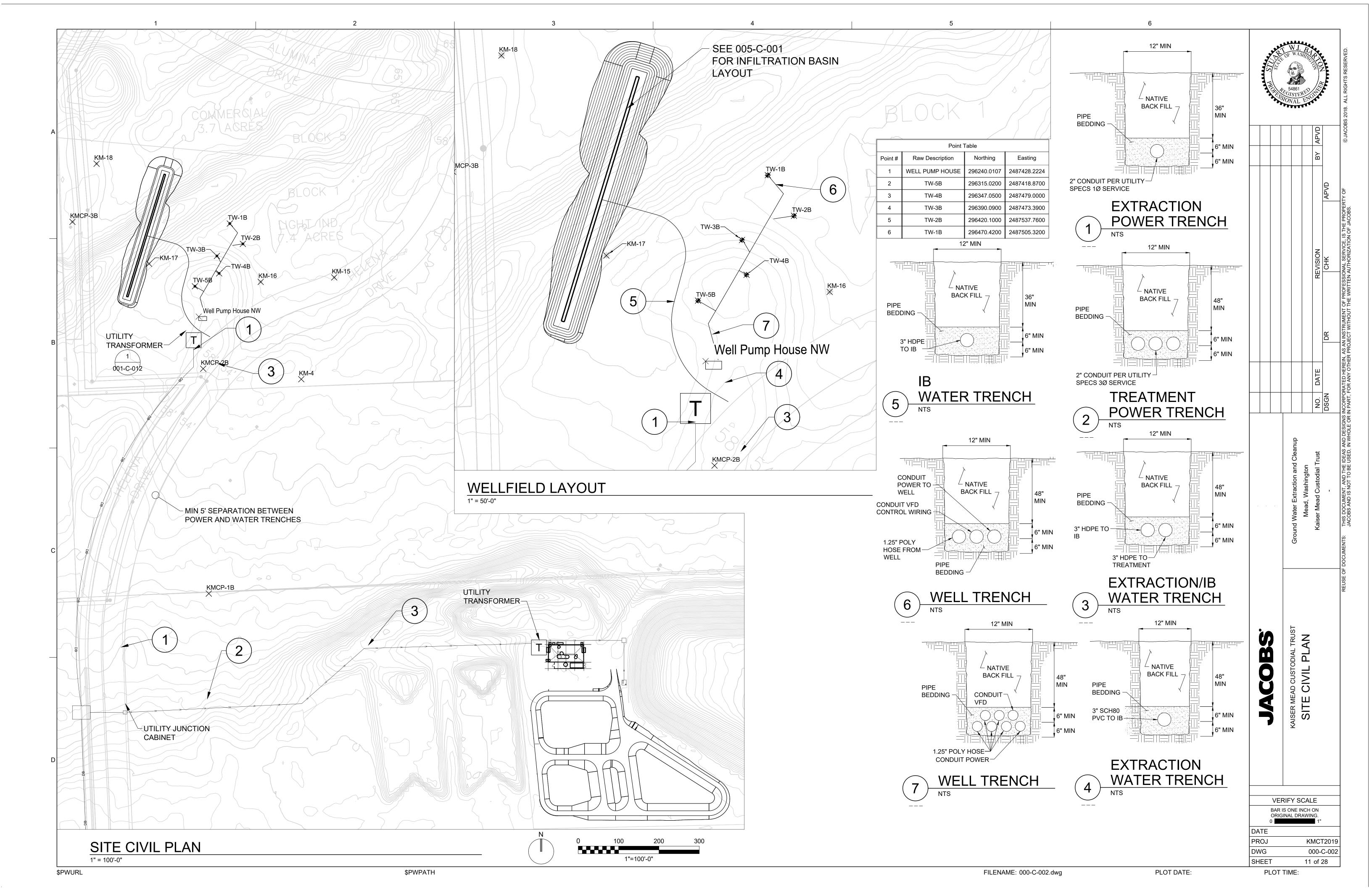
Analytic testing blending pumping rates for highest concentration blend

Correlation of TCN to EC for performance monitoring.

K value update based on development pumping and drawdown

Revised modeling for 3 Scenarios, includes actual well locations and updated K values

- 1 Planned pumping rate schedule with infiltration
- 2 Initial pumping rate schedule (10 gpm each well) with infiltration
- 3 Planned pumping rate schedule without infiltration (for simulated initial startup conditions and for comparison without IB)



## **Interim Action - Summary of Well Construction Details**

		•			
	TW-1B	TW-2B	TW-3B	TW-4B	TW-5B
GS Elevation <sup>1</sup>	1916.6	1916.0	1920.1	1922.3	1922.5
Total Depth Drilled (ft bgs)	167	160	169	167.5	175
Top of Aquitard (ft bgs)	163	160	167	167.5	170
Top of Aquitard Elev	1754	1756	1753	1755	1753
Well casing diameter (ft)	0.5	0.5	0.5	0.5	0.5
Sump length (feet)	0.5	1	4	1	1
Bottom Constructed sump (ft bgs)	163.4	160.5	168.7	167.3	168.5
Bottom screen (ft bgs)	163	159.5	164.7	166.3	167.5
Top of screen (ft bgs)	153	149.5	154.7	156.3	152.5
Screen length (ft)	10	10	10	10	15
Bottom screen elevation	1754	1757	1755	1756	1755
Top of screen elevation	1764	1767	1765	1766	1770
Packer assembly length (ft)	?	2	5	2	2
					25 slot (153-158)
	18 slot (153-158)	30 slot (150-155)	25 slot (155-160)	25 slot (156-161)	25 slot (158-163)
Screen size	20 slot (158-163)	30 slot (155-160)	18 slot (160-165)	20 slot (161-166)	20 slot (163-168)
Stickup (ft)	2.4	2.4	2.4	2.3	2.7
SWL (ft bgs) (Nov 2019)	148.3	147.4	151.7	153.8	154.1
SWL elevation (Nov 2019)	1768.3	1768.6	1768.4	1768.5	1768.4
1				L L	

<sup>&</sup>lt;sup>1</sup>Benthin & Associates survey

All elevations and as-built depths to be field verified post-drilling.

Existing

# Hydrometrics, Inc. Consulting Scientists and Engineers

Helena, Montana

Hole Name: TW-1B

Date Hole Started: 01/09/13 Date Hole Finished: 01/13/13

153 - 158; 158 - 163

Client: Mead Custodial Trust Project: Kaiser Mead NPL

County: Spokane State: Washington Property Owner: Kaiser Aluminum Investments Co

Legal Description: Tax ID: 36096.9060 Location Description: Approximately 300' east

of Compliance well KMCP-3

Recorded By: LMJ

Drilling Company: H2O Well Service

Driller: Mark

Drilling Method: Conventional Rotary Drilling Fluids Used: Air/Water Purpose of Hole: Aquifer Testing

Target Aquifer: Zone B Hole Diameter (in): 6-inch

Total Depth Drilled (ft): 167

WELL COMPLETION **DESCRIPTION** Y/N **INTERVAL** Well Installed? 6 inch Steel Casing +2 - 167

Surface Casing Used? Temporary 10" casing +2 - 18

Screen/Perforations? 0.018" slot; 0.020" slot stainless Sand Pack?

Annular Seal? Υ Bentonite Chips 0 - 18

Bentonite annular seal Surface Seal? Υ

DEVELOPMENT/SAMPLING

Well Developed? Air development Water Samples Taken? Y pumping test sample

Boring Samples Taken? Y Split Spoon Samples from 145-160 5' intervals

Easting: 296512 Northing: 2487494

Static Water Level Below MP: 147 Surface Casing Height (ft): +2

Date: 1/16/2013 Ground Surface Elevation (ft): 1916.60

MP Description: Top of Steel Casing MP Elevation (ft): 1919.04

MP Height Above or Below Ground (ft): 2'

Remarks: Field notes reference this well as TW-B, which was corrected to TW-1B in compiled Logs and field investigation report

#### WELL CONSTRUCTION GRAPHICS DEPTH GEOLOGICAL DESCRIPTION 6" steel casing 0.0 - 30.0' Coarse Sand with Gravel 5 0.0 Dark gray to brown, poorly sorted coarse sand with minor pebbles, set 10 10 inch casing to 18 feet, 20 foot plugging casing, injecting water. 15 \_ 20 25 30 30.0 - 51.0' Fine to Medium Grained Sand 35 40 Fine to medium grained sand with some silt. -45 50 55 51.0 - 52.0' Clay 60 Clay, less than one foot thick. 65 52.0 - 82.5' Sand with Gravel 70 Coarse sand with gravel, pebbles to 1/2", 60 feet, occasional pebble to 1 75 inch, 62 feet, decreasing pebbles, sand fining downward, 82 feet, 1/2 inch 80 -85 82.5 - 111.0' Fine Grained Sand with Silt \_ 90 Fine grained sand with minor silt 95 100 105 6/11/13 110 115 111.0 - 113.0' Clay GDT 120 Light gray to green gray plastic clay 125 113.0 - 131.0' Fine Grained Sand with Silt HYDHLN2. Fine grained sand plus or minus silt. Spoon sample at 115 - 116.5, very fine grained sand with silt - dry. 130 \_ 135 \_ 140 131.0 - 132.0' Clay 145 Light gray to green gray plastic clay. K:\GINT\PROJECTS\9088.GPJ 150 132.0 - 143.0' Sand K-packer at 147' 153.0 155 Fine grained sand, coarser grained at 134 feet. 0.018" slot stainless 158.0 160 143.0 - 145.0' Clay 163.0 0.020" slot stainless screen 165 Light gray to green gray plastic clay Bottom of Hole screen 167.0 170 145.0 - 163.0' Fine to Coarse Grained Sand 5" tail pipe \_ 175 Heaving sands, drill string gets sandpacked, have to inject water to free up drill rods. Let hole sit overnight and SWL = 147 feet, sample water with bailer, pH = 8.67, SC = 1249, about 1 foot of sand heave. Spoon samples 180 -185 at 155 feet and 160 feet, wet coarse sand, 162 feet making less than 5 190 -195 163.0 - 165.0' Clay with Silt 200 Green gray, firm, dense clay with silt, cuttings become dry. 205 TD at 165 feet. 210 215 220



PROJECT NUMBER

KMCT2019.3200

WELL NUMBER
TW - 2B

## WELL COMPLETION DIAGRAM

PROJECT: KMCT Interim Action Extraction Well Installation

LOCATION: Approx. 700 feet E-SE of Winchester Ave./Newport Highway intersection,

DRILLING CONTRACTOR: H2O Well Service Inc., Hayden ID Spokane, WA DRILLING METHOD AND EQUIPMENT USED: Air Rotary with Casing Hammer WATER LEVELS: During drilling, estimated at approx. 146 ft bgs. On 11/15/19, 150.01 ft btc (147.5 ft bgs) LOGGER: K Savage Unique Ecology Well ID Tag BKW-216 1- Top of casing elevation 1918.39 ft (NAVD88) 2- Ground elevation at well 1916.0 ft (NAVD88) 3- Wellhead riser and casing 6-inch ID steel casing with lockable aluminum lid. Key 2190 4- Surface seal 10-inch ID temporary casing to 18 feet bgs. At completion, 10-inch casing pulled and 18 annulus backfilled with bentonite chips 160.5 5- Well Casing 6-inch ID mild steel casing. Upon installation of the screen, the casing was pulled back to expose the telescoping screen 149.5 6- Packer assembly Figure K neoprene packer with 2 feet of 5 5-inch ID head pipe 7- Type/slot size of screen 6-inch stainless steel, continuous wire-wrapped telescoping screen (approx. 5-inch ID). 30 slot (0.030 inch) 149.5 to 159.5 ft. bgs 8- Sump 1-foot long steel sump, 5-inch ID 10 Comments: TD at top of clay aquitard Development: Pumped for 45 minutes at 9 gpm; drawdown of 0.47 ft Specific conductivity of 1,857 uS/cm and pH 9.05 at sample collection 6 inches



PROJECT NUMBER

KMCT2019.3200

WELL NUMBER

TW - 3B

Spokane, WA

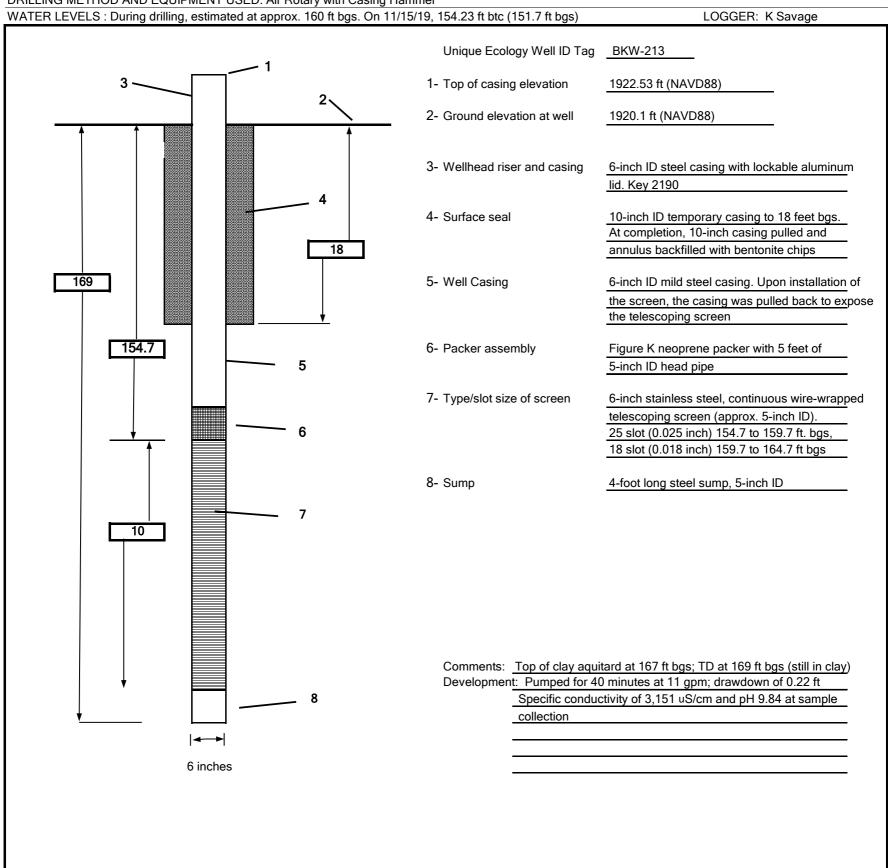
#### WELL COMPLETION DIAGRAM

PROJECT: KMCT Interim Action Extraction Well Installation

LOCATION: Approx. 700 feet E-SE of Winchester Ave./Newport Highway intersection,

DRILLING CONTRACTOR: H2O Well Service Inc., Hayden ID

DRILLING METHOD AND EQUIPMENT USED: Air Rotary with Casing Hammer





PROJECT NUMBER
KMCT2019.3200

WELL NUMBER
TW - 4B

## WELL COMPLETION DIAGRAM

PROJECT: KMCT Interim Action Extraction Well Installation

LOCATION : Approx. 700 feet E-SE of Winchester Ave./Newport Highway intersection,

DRILLING CONTRACTOR: H2O Well Service Inc., Hayden ID

Spokane, WA

R LEVELS : During drilling	g, estimated at approx. 160 ft bgs.	On 11/15/19, 156.27 ft btc (153.8 ft bgs)	LOGGER: K Savage
	<b>_1</b>	Unique Ecology Well ID Tag	BKW-215
3 —		1- Top of casing elevation	1924.60 ft (NAVD88)
-	2	2- Ground elevation at well	1922.3 ft (NAVD88)
	•	3- Wellhead riser and casing	6-inch ID steel casing with lockable aluminum lid. Key 2190
	4	4- Surface seal	10-inch ID temporary casing to 18 feet bgs. At completion, 10-inch casing pulled and
	18	5- Well Casing	annulus backfilled with bentonite chips  6-inch ID mild steel casing. Upon installation of
167.5		C Well edoling	the screen, the casing was pulled back to expose the telescoping screen
156.3	#####################################	6- Packer assembly	Figure K neoprene packer with 2 feet of 5-inch ID head pipe
	5	7- Type/slot size of screen	6-inch stainless steel, continuous wire-wrapped telescoping screen (approx. 5-inch ID).
	6		25 slot (0.025 inch) 156.3 to 161.3 ft. bgs, 20 slot (0.020 inch) 161.3 to 166.3 ft bgs
		8- Sump	1-foot long steel sump, 5-inch ID
10	7		
		Comments: Top of clay agui	tard at 167.5 ft bgs; TD at 167.5 ft bgs
		Development: Pumped for 45	5 minutes at 9.5 gpm; drawdown of 0.07 ft
	8		ctivity of 3,845 uS/cm and pH 10.05 at sample
<u> </u>		collection	
	17 7		
	6 inches	-	



PROJECT NUMBER

KMCT2019.3200

WELL NUMBER

**TW - 5B** 

#### WELL COMPLETION DIAGRAM

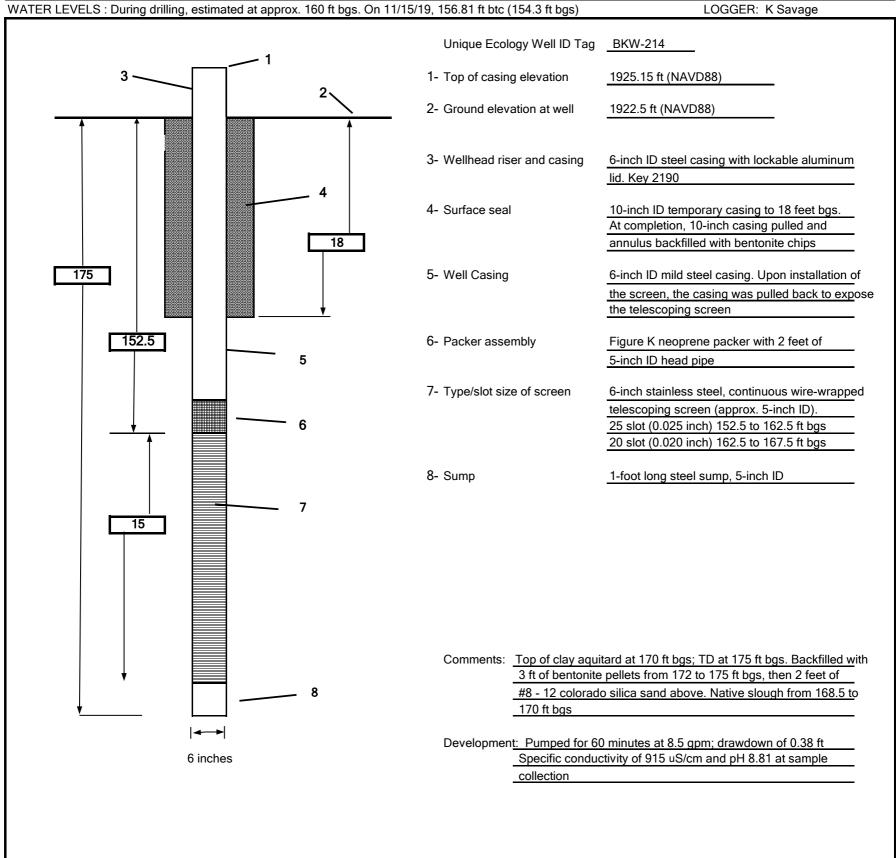
PROJECT: KMCT Interim Action Extraction Well Installation

LOCATION : Approx. 700 feet E-SE of Winchester Ave./Newport Highway intersection,

DRILLING CONTRACTOR: H2O Well Service Inc., Hayden ID

Spokane, WA DRILLING METHOD AND EQUIPMENT USED: Air Rotary with Casing Hammer

WATER LEVELS: During drilling, estimated at approx. 160 ft bgs. On 11/15/19, 156.81 ft btc (154.3 ft bgs)

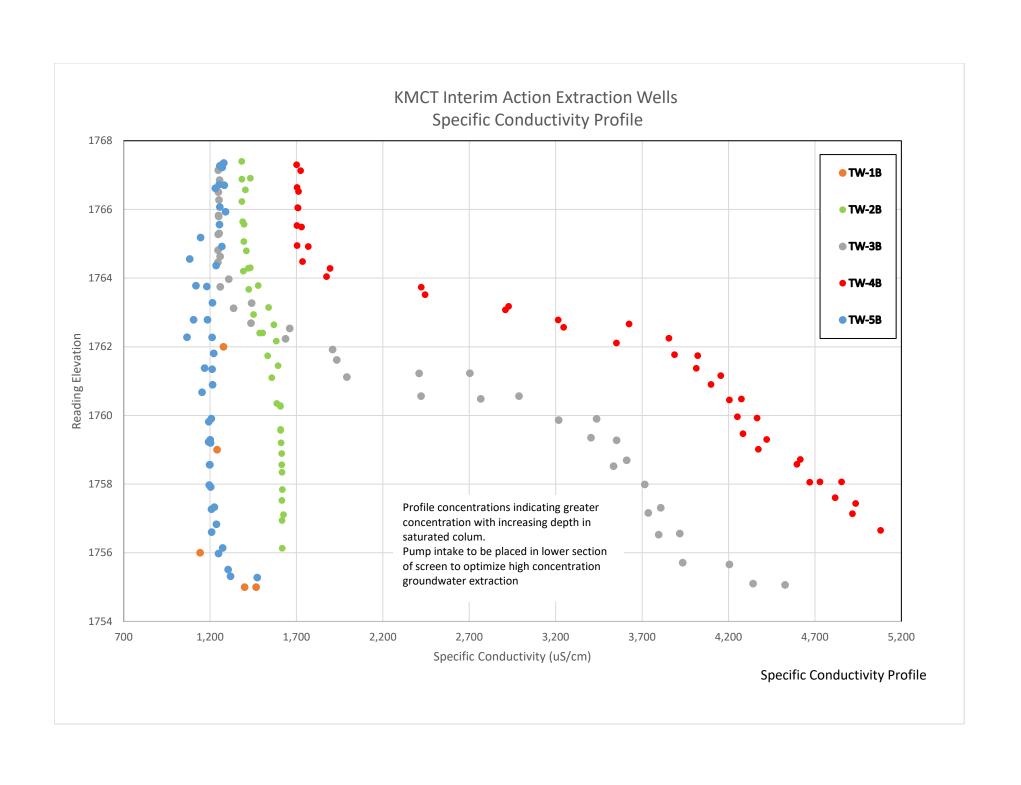


## **KMCT Interim Action Well Development Summary (November 2019)**

								Drawdo	wn in nearb	nearby wells during development (feet)		
Well	Pumping Time (minutes)	Total Volume Pumped (gallons)	Average Pumping Rate (gpm)	Drawdown in Pumping Well (feet)	Specific Capacity (gpm/ft) <sup>1</sup>	Specific Conductivity (uS/cm)	pH (SU)	TW-1B	TW-2B	TW-3B	TW-4B	TW-5B
TW-1B	26	320	12.3	0.33	37	1,467	8.8	XX	0.00	0.00	NM	NM
TW-2B	53	420	9.0	0.47	19	1,857	9.1	0.06	XX	0.00	0.00	NM
TW-3B	40	450	11.3	0.22	51	3,151	9.8	NM	0.00	XX	0.01	NM
TW-4B	45	430	9.6	0.07	137	3,845	10.0	NM	NM	0.03	XX	0.02
TW-5B	60	510	8.5	0.38	22	915	8.8	0.00	0.00	0.00	0.04	XX
NM - Not N	Neasured	_										

#### Notes

<sup>1 -</sup> Specific capacity based on short pumping duration conducted as part of well screen development. These values and aquifer parameters based on this data represent an overestimate for long term aquifer characteristics.



Comparison of Water Chemistry from Extraction Wells and Perimeter Well KMCP-3B

			Ex	traction Wells	а		Perimeter Well	
Parameter	Units	TW-1B	TW-2B	TW-3B	TW-4B	TW-5B	KMCP-3B <sup>b</sup>	
рН	s.u.	8.8	9.0	9.7	9.8	8.7	9.7	
Conductivity	uS/cm	1,222	1,726	2,860	3,070	868	3600	Assumed to be specific conductivity
Chloride	mg/L	20.0	24.0	35.0	37.0	19.0	17.0	based on field measurements
Fluoride	mg/L	12.0	16.0	26.0	30.0	3.60	15.0	
Sulfate	mg/L	120	190	210	210	76.0	130	
Total-P	mg/L as P						0.86 J	
Iron, dissolved	mg/L	5.80	8.60	13.0	13.0	1.90	8.50	
Nitrogen Forms								
NO2-N	mg/L as N	1.10	1.20	3.80	3.70	0.67	3.90	
NO3-N	mg/L as N	8.50	15.0	37.0	38.0	8.10	15.0	
NH3-N	mg/L as N							
TKN	mg/L as N							
Cyanide Forms								
Free Cyanide	mg/L	0.27	0.36	0.46	0.50	0.16	0.77	
WAD Cyanide	mg/L	0.03	0.39	0.58	0.56	0.0046 J	0.82	
Total Cyanide	mg/L	14.0 B	22.0 B	39.0 B	41.0 B	4.90 B	24.0 B	

 $<sup>^{\</sup>rm a}$  Samples received at the Corvallis, OR treatability lab on 11/18/2019

#### **Anticipated Blend Concentrations given Specific Extraction Rates**

Pumping Schedule for Highest TCN Concentration in Blended Extraction

Scenario 1

		TW-1B	TW-2B	TW-3B	TW-4B	TW-5B			
		10%	20%	30%	35%	5%	Percent	100%	contribution
		5	10	15	17.5	2.5	Flow rate	50	gpm
	,		•	Contribution				Blend conc	
рН	s.u.	0.9	1.8	2.9	3.4	0.4		9.5	
Conductivity	uS/cm	122	345	858	1075	43		2443	Assume EC and not SC
Chloride	mg/L	2.0	4.8	10.5	13.0	1.0		31	
Fluoride	mg/L	1.2	3.2	7.8	10.5	0.18		23	
Sulfate	mg/L	12	38	63	73.5	3.8		190	
Total-P	mg/L as P								
Iron, dissolved	mg/L	0.58	1.72	3.9	4.55	0.10		11	
NO2-N	mg/L as N	0.11	0.24	1.14	1.30	0.03		2.8	
NO3-N	mg/L as N	0.85	3.0	11.1	13.3	0.41		28.7	
NH3-N	mg/L as N								
TKN	mg/L as N								
Free Cyanide	mg/L	0.03	0.07	0.14	0.18	0.01		0.42	
WAD Cyanide	mg/L	0.00	0.08	0.17	0.20	0.00		0.45	
Total Cyanide	mg/L	1.4	4.4	11.7	14.4	0.25		32.1	

Scenario 2								•	
		TW-1B	TW-2B	TW-3B	TW-4B	TW-5B		•	
		5%	15%	35%	40%	5%	Percent	100%	contribution
		2.5	7.5	17.5	20	2.5	Flow rate	50	gpm
				Contribution			_	Blend conc	
рН	s.u.	0.4	1.4	3.4	3.9	0.4		9.5	
Conductivity	uS/cm	61	259	1001	1228	43		2592	Assume EC and not SC
Chloride	mg/L	1.0	3.6	12.25	14.8	1.0		33	
Fluoride	mg/L	0.6	2.4	9.1	12	0.18		24	
Sulfate	mg/L	6	28.5	73.5	84	3.8		196	
Total-P	mg/L as P								
Iron, dissolved	mg/L	0.29	1.29	4.55	5.2	0.10		11	
NO2-N	mg/L as N	0.055	0.18	1.33	1.48	0.03		3.1	
NO3-N	mg/L as N	0.425	2.3	12.95	15.2	0.41		31.2	
NH3-N	mg/L as N								
TKN	mg/L as N								
Free Cyanide	mg/L	0.01	0.05	0.16	0.20	0.01		0.44	
WAD Cyanide	mg/L	0.00	0.06	0.20	0.22	0.00		0.49	
Total Cyanide	mg/L	0.7	3.3	13.65	16.4	0.25		34.3	

B = Compound was found in the blank and sample

J = Estimated value below reporting limit.

#### **Selected** Well Field Pumpi TW-5B Scenario 3 TW-1B TW-2B TW-3B TW-4B **5**% 10% 40% 40% **5**% Percent 100% contribution 2.5 5 20 20 2.5 Flow rate 50 gpm Contribution **Blend conc** 0.4 9.6 рΗ 0.9 3.9 3.9 0.4 s.u. 2649 uS/cm 1144 1228 43 Assume EC and not SC Conductivity 61 173 mg/L 33 Chloride 1.0 2.4 14 14.8 1.0 mg/L 25 0.6 1.6 12 Fluoride 10.4 0.18 mg/L 197 6 84 84 Sulfate 19 3.8 mg/L as P Total-P 12 Iron, dissolved mg/L 0.29 0.86 5.2 5.2 0.10 3.2 NO2-N mg/L as N 0.055 0.12 1.52 1.48 0.03 32.3 NO3-N mg/L as N 0.425 1.5 14.8 15.2 0.41 mg/L as N NH3-N mg/L as N TKN 0.44 Free Cyanide mg/L 0.01 0.04 0.18 0.20 0.01 0.50 WAD Cyanide mg/L 0.00 0.22 0.04 0.23

16.4

0.25

mg/L

0.7

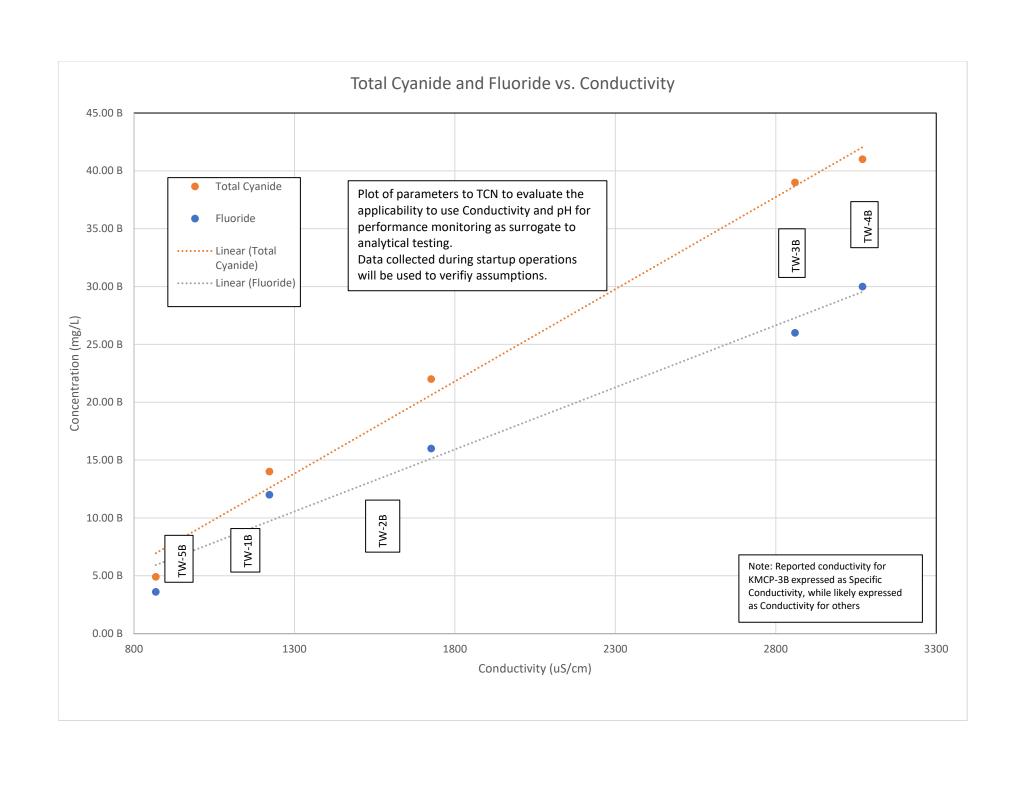
2.2

15.6

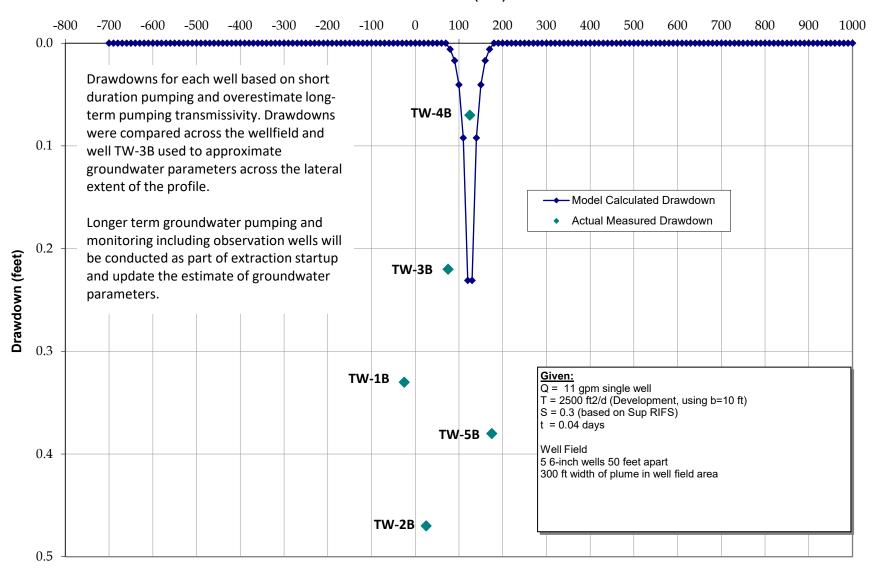
Total Cyanide

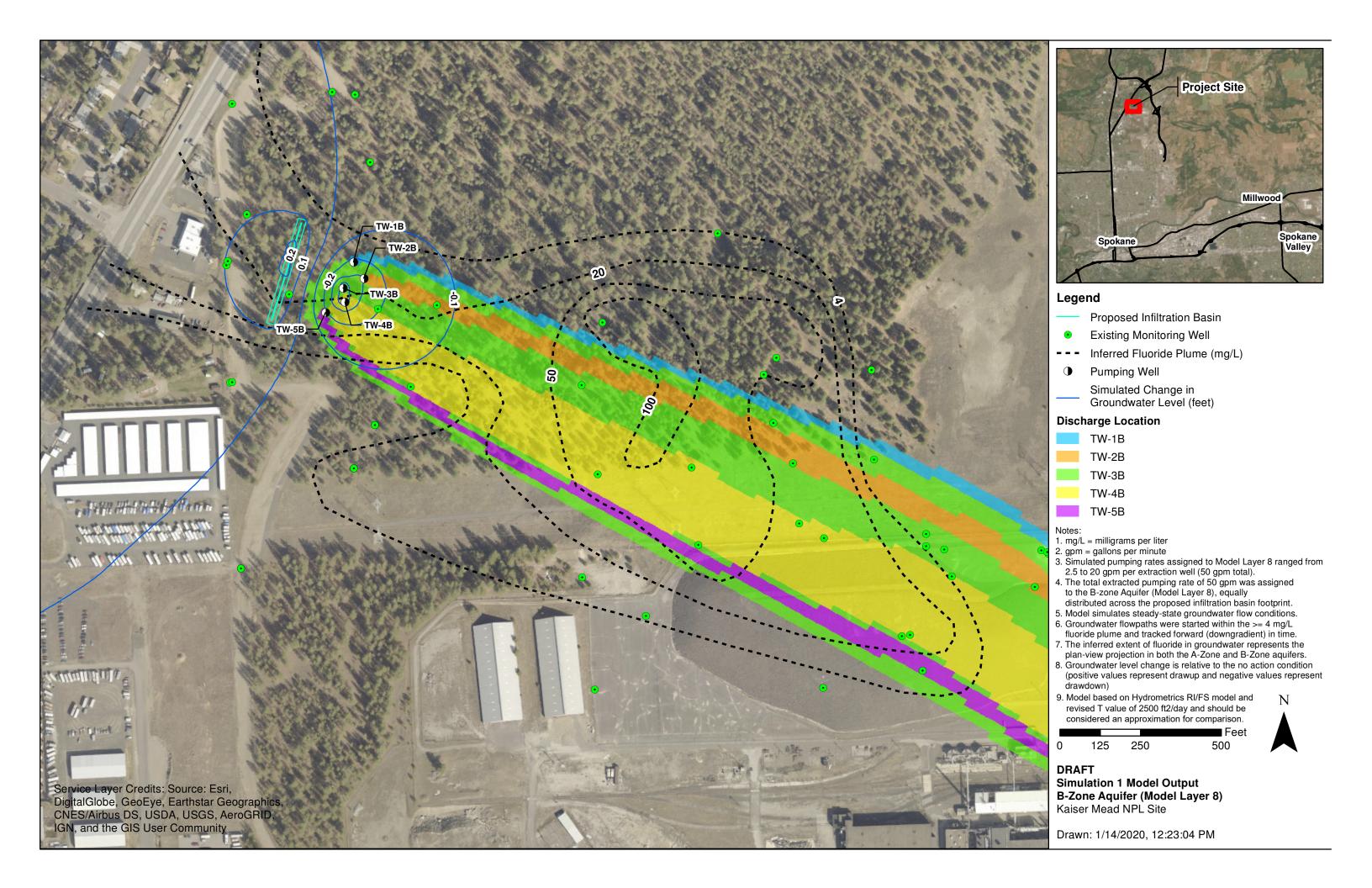
Scenario 4		TW-1B	TW-2B	TW-3B	TW-4B	TW-5B		ī	
Scenario 4		15%	20%	30%	30%	5%	Percent	100%	contribution
		7.5	10	15	15	2.5	Flow rate	50	
		7.5	10	Contribution	<u> </u>	2.5	Flow rate	Blend conc	gpm 1
			1		I	1	1		4
рН	s.u.	1.3	1.8	2.9	2.9	0.4		9.4	
Conductivity	uS/cm	183	345	858	921	43		2351	Assume EC and not SC
Chloride	mg/L	3.0	4.8	10.5	11.1	1.0		30	
Fluoride	mg/L	1.8	3.2	7.8	9	0.18		22	
Sulfate	mg/L	18	38	63	63	3.8		186	
Total-P	mg/L as P						]		
Iron, dissolved	mg/L	0.87	1.72	3.9	3.9	0.10		10	
NO2-N	mg/L as N	0.165	0.24	1.14	1.11	0.03		2.7	
NO3-N	mg/L as N	1.275	3.0	11.1	11.4	0.41		27.2	
NH3-N	mg/L as N								
TKN	mg/L as N								
Free Cyanide	mg/L	0.04	0.07	0.14	0.15	0.01	]	0.41	
WAD Cyanide	mg/L	0.00	0.08	0.17	0.17	0.00		0.42	
Total Cyanide	mg/L	2.1	4.4	11.7	12.3	0.25	]	30.7	

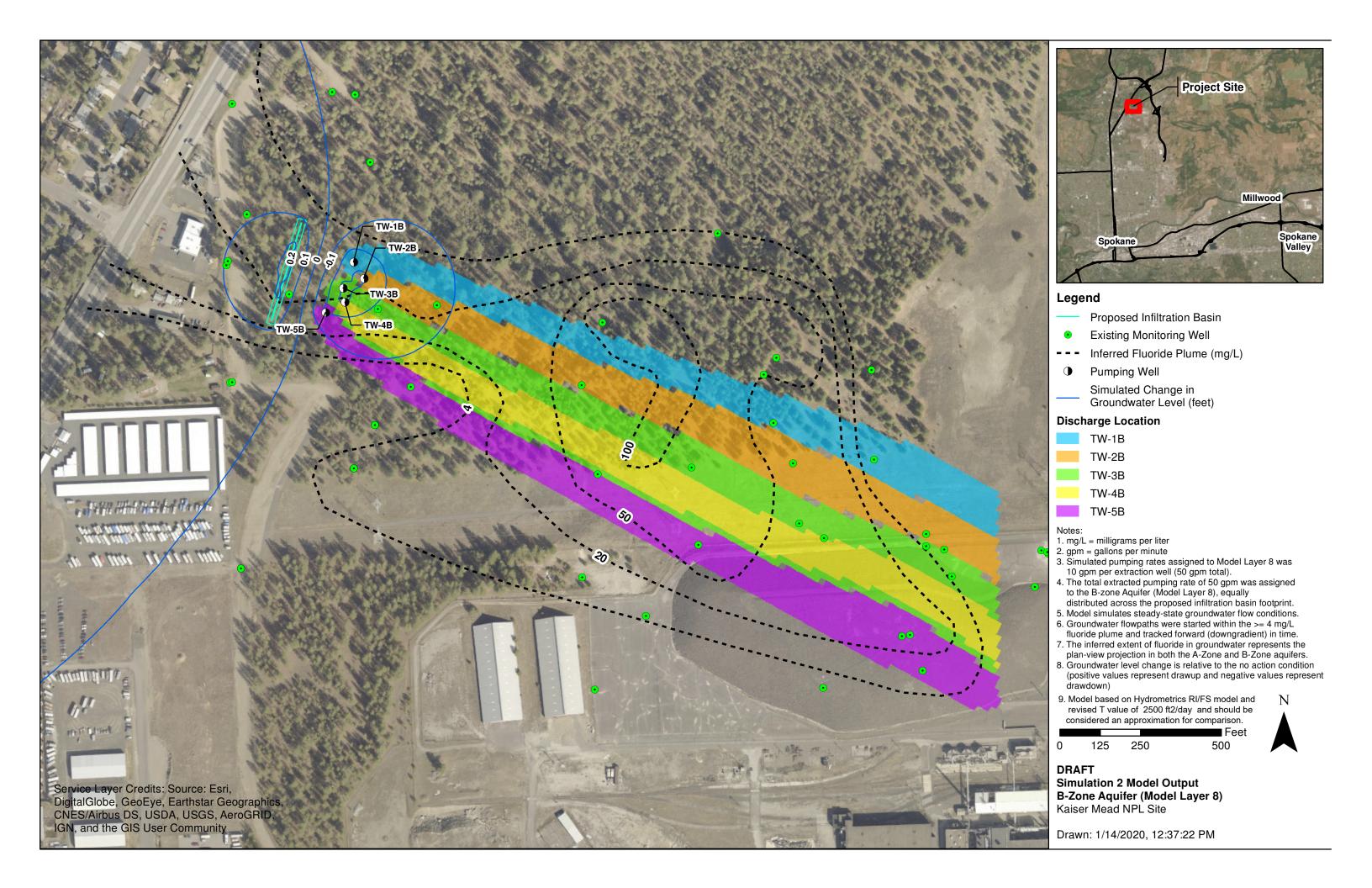
35.1

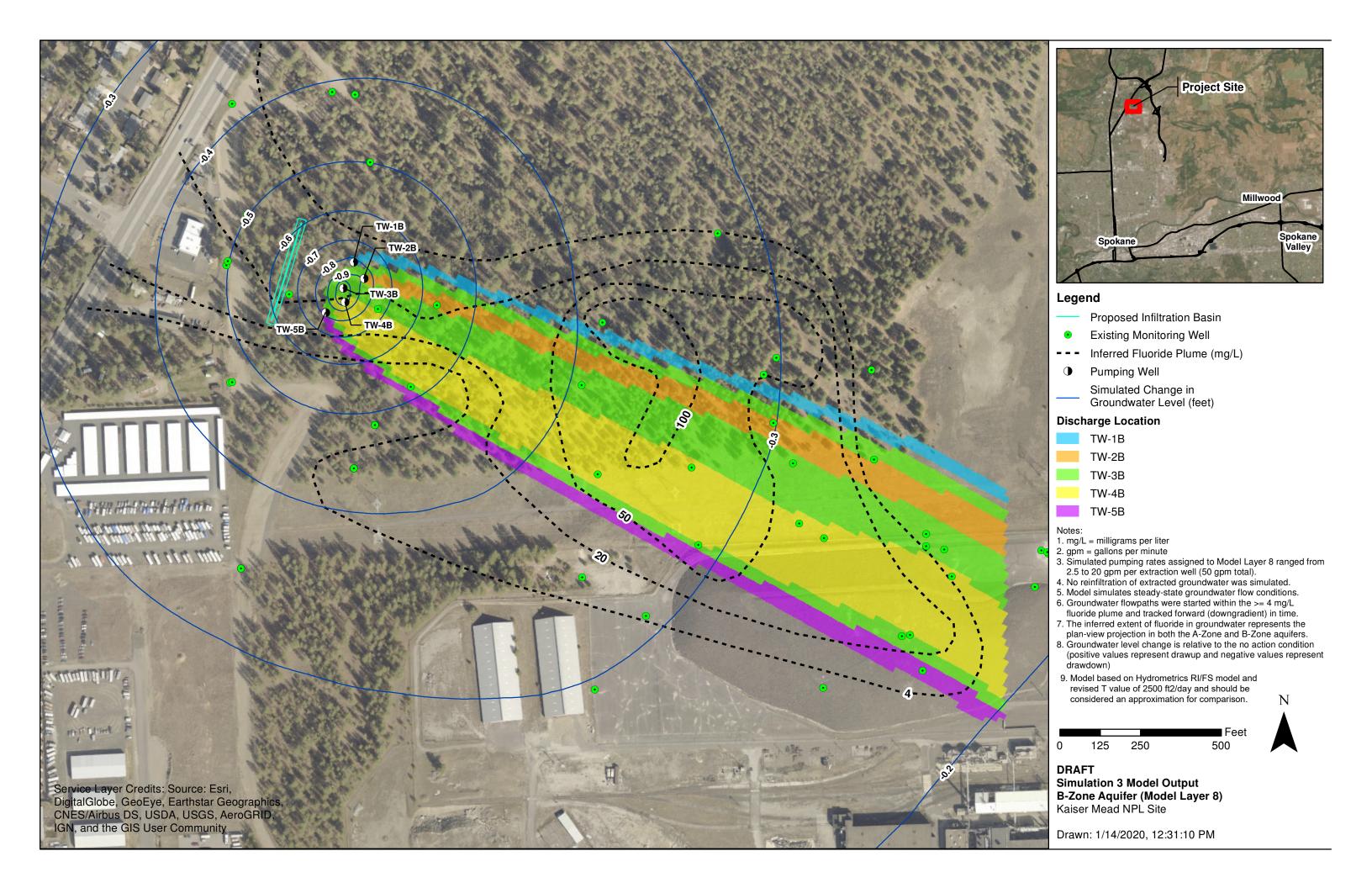


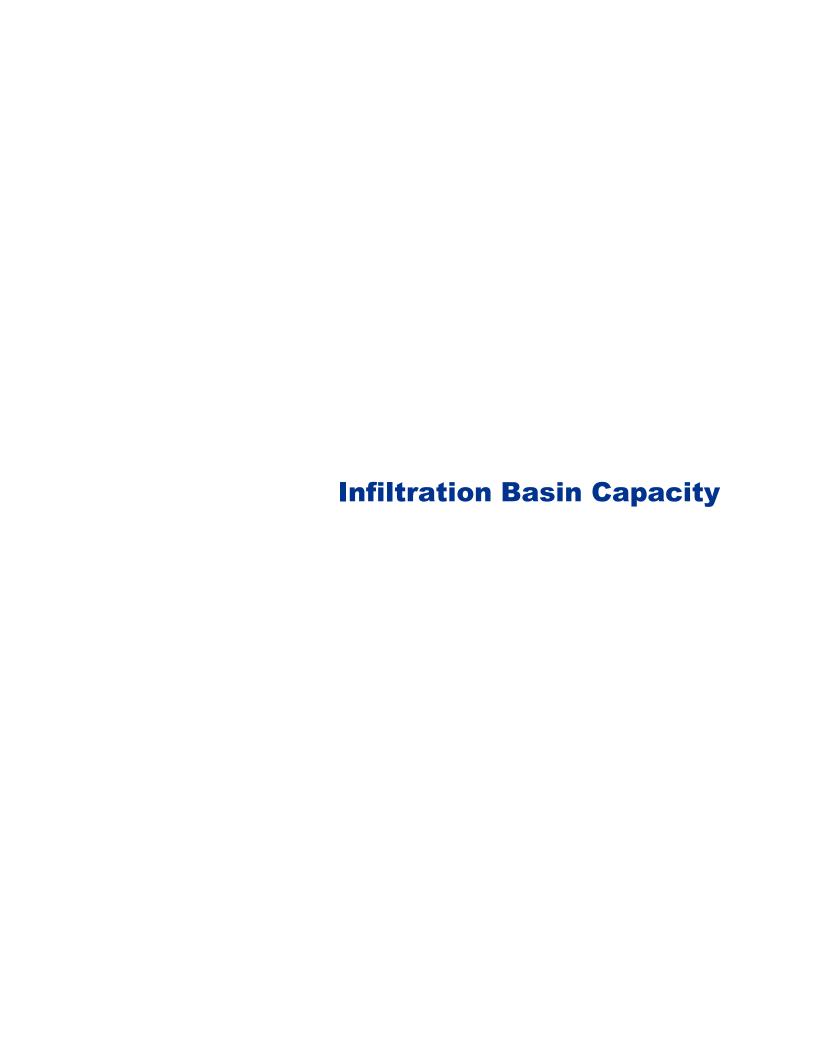
#### Distance (feet)





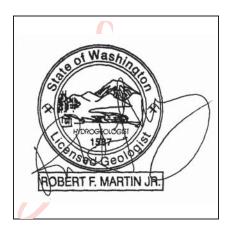






#### **CALCULATIONS**

#### INFILTRATION BASIN CAPACITY



Digitally Signed on

April 3, 2020

Robert Martin

## **Infiltration Basin Capacity Calculations**

**Project** KMCT Groundwater Remediation Interim Action

Calculation by: Robert Martin

Date: 12/13/2019 Checked by: Mark Henry Date: 1/2/2020

Length

Calculating a range of percolation rates based on maximum and minimum soil type percolation rates, and for the gravel channel and larger infiltration

basin bottom.

<u>Assumptions</u>			
Percolation Rate	0.50 ft/hr	Percolation Rate	0.50 ft/hr
Width	4 ft	Width	20 ft
Length	300 ft	Length	300 ft
Percolation	595 ft3/hr	Percolation	2975 ft3/hr
	4451 gal/hr		22253 gal/hr
	74 gpm		371 gpm
Percolation Rate	1.665 ft/hr	Percolation Rate	1.665 ft/hr
Width	4 ft	Width	20 ft
Length	300 ft	Length	300 ft
Percolation	1998 ft3/hr	Percolation	9990 ft3/hr
	14945 gal/hr		74725 gal/hr
	249 gpm		1245 gpm

Web Soil Survey

**Percolation Calculations** 

Width

8 4 8

National Cooperative Soil Survey

Natural Resources Conservation Service

https://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx

Spokane County, Washington

3120 Marble loamy sand, 0 - 8 percent slopes

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)

Oi - 0 to 1 inches: slightly decomposed plant material

A - 1 to 4 inches: loamy sand

E - 4 to 8 inches: loamy sand

E and Bt1 - 8 to 27 inches: sand

E and Bt2 - 27 to 53 inches: sand

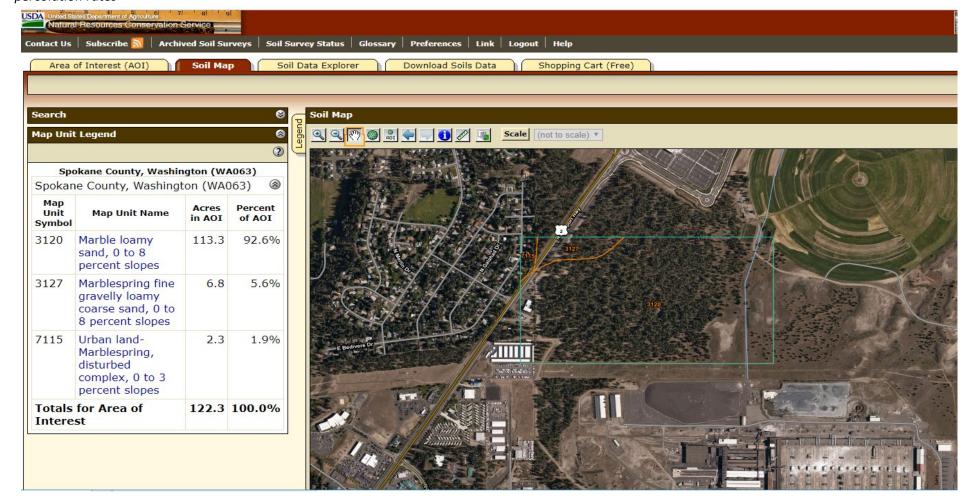
C - 53 to 60 inches: sand

J	Calculating estimated distance for flow within the gravel channel based on distance between risers. Used for approximating riser spacing						
4 ft	Width (W)	4 ft					
2 ft	Depth (b)	2 ft					
2 cm/s	Hydraulic Cond (K)	2 cm/s					
42400 gallons/day/ft2	Hydraulic Cond (K)	42400 gallons/day/ft2					
0.02 ft/ft for 50 ft	Gradient (i)	0.003333 ft/ft for 300 ft					
6784 gallons/day	Flow (Q)	1130.667 gallons/day					
4.7 gallons/min	Flow (Q)	0.79 gallons/min					
	distance between r  4 ft 2 ft 2 cm/s 42400 gallons/day/ft2  0.02 ft/ft for 50 ft 6784 gallons/day	distance between risers. Used for approxim  4 ft Width (W) 2 ft Depth (b) 2 cm/s Hydraulic Cond (K) 42400 gallons/day/ft2 Hydraulic Cond (K)  0.02 ft/ft for 50 ft Gradient (i)  6784 gallons/day Flow (Q)					

#### Number of Discharge points

75 gpm Flow Flow at each point 9 gpm Number of points

USDA Natural Resources Conservation Service, reference for soil type and percolation rates



#### Fencing

WSDOT reference for infiltration basins

## 560.02(4) Special Sites

Fencing may be needed at special sites such as pit sites, stockpiles, borrow areas, and stormwater detention facilities.

Fencing is not normally installed around stormwater detention ponds. Evaluate the need to provide fencing around stormwater detention facilities when pedestrians or bicyclists are frequently present. Document your decision in the Design Documentation Package.

The following conditions suggest a need to evaluate fencing:

- Children or persons with mobility impairments are frequently present in significant numbers in locations adjacent to the facility, such as routes identified in school walk route plans or nearby residential areas or parks.
- · Water depth reaches or exceeds 12 inches for several days.
- Sideslopes into the facility are steeper than 3H:1V.

Fencing proposed at sites that will be outside WSDOT right of way requires that local ordinances be followed if they are more stringent than WSDOT's.

Wetland mitigation sites are not normally fenced. When evaluating fencing for wetland mitigation sites, balance the need to restrict human access for safety considerations (such as the presence of children) with the need to provide animal habitat.

Other special sites where fencing may be required are addressed in the following chapters:

- Chapter 720, Bridges (refers to protective screening)
- Chapter 1510, Pedestrian Design Considerations

Page 560-2

WSDOT Design Manual M 22-01.14

July 2017

## **Wetlands Process Calculations**

# **Enhanced Wetland Treatment System Hydraulics**

#### **CALCULATIONS**

#### WETLAND PROCESS



Digitally Signed on

May 5, 2020

Mark Madison

J	AC	OB	BS <sup>™</sup>		T: ead Groundwater ion Interim Action	LOCATION: Mead Washir	ngton				
	LCULATIO			CLIENT: I Custodial	Kaiser Mead Trust	JOB No. KMCT2019					
TITLE: Final Design	Report for Extracti	on, Treatment, an	d Discharge Systen	ns Reference							
Enhanced W	Enhanced Wetland Treatment System Calculations 002-C-006										
OBJECTIVE: Document Design Criteria to obtain modeled treatment performance calibrated with pilot test data											
INPUTS: Treatment performance targets, Hydraulic Retention Time, Hydraulic Loading Rate, Media Specs, Aerobic/Anaerobic Cycling Regime											
	ASSUMPTIONS: Flow rates can be varied from 50 gpm to 100 gpm by adjusting the rate of recycled flow.										
	NS REQUIRING ( formance data can		ull scale with similar	results							
	BASIS OF CALCULATION, METHOD, OR SOFTWARE TO BE USED: Excel Spreadsheet										
CONCLUSION: The design provides operational flexibility to achieve performance targets.											
Revision	0	1	2	3	4	5	6				
Prepared Date	5/6/2020 Mark Madison										
Checker Date	Jim Bays										



## CALCULATION TABLE OF

PROJECT: Kaiser Mead Groundwater Remediation Interim Action J.O. NUMBER: KMCT2019

CALCULATION NUMBER: Final

PAGE: 2 OF 10

CONTENTS	7
TITLE Final Design Report for Extraction, Treatment, and Discharge Systems	PAGE
Enhanced Wetland Treatment System Calculations	
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TABLE 2 PIPELINE HYDRAULICS	4
4 cycles 50gpm	5
5 cycles 100gpm	6
6 cycles 50 gpm	7
6 cycles 100 gpm	8
8 cycles 50 gpm	9
8 cycles 100 gpm	10
Note: The worksheet titles refer to the number of cycles per day that occur between Cell 2A and Cell 2B plus the flow rate. These calculations bracket a range of cycles and flows that represent the adjustments that can be used to tune performance.	

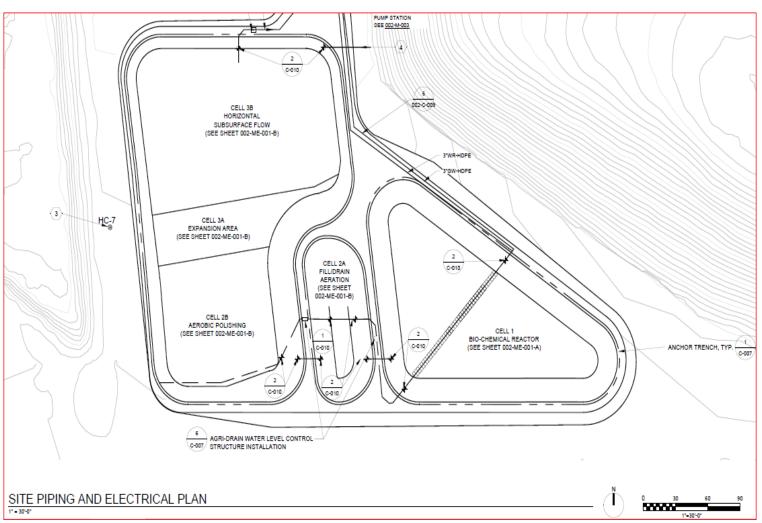
<b>JACOBS</b>	PROJECT: Kaiser Mead Custodial Trust	LOCATION: Mead Washington
CALCULATION SHEET	CLIENT:: Kaiser Mead Groundwater Remediation Interim Action	JOB No. KMCT2019
TITLE: Preimnary (90%) Design Report for Extraction, Treatment, and Discharge Systems Enhanced Wetland Treatment System Calculations	EQUIP /DWG. NO.: Reference Drawings - 11-4-2019_RMCT- 2019_80% pdf	CALCULATION NUMBER: Preliminary (90%)

Enhanced Wetland Treatment System Calculations											
Enhanced viveland Treatment System Calculations											
		9	73								
BLE 1 HYDRAULIC CALCULATIONS FOR NATURAL TREATM	L HYDRAULIC CALCULATIONS FOR NATURAL TREATMENT SYSTEM Page 3 of 10										
de/Revised by; Mark Madison/PDX		Date: 1/13/2020									
cked by, Jim Bays/TPA											
roved											

#### TABLE 1 HYDRAULIC CALCULATIONS FOR NATURAL TREATMENT SYSTEM

		Flow			Elevation		Vo	lume	А	rea	Hydi	aulic	Range of A	djustment	
		,				_		Water in pore	at Normal						
0	from wells	from	Total	Cell Bottom	Normal Water	Bypass Spillway		spaces at Normal	Water Surface	at Top of Berm	Residence Time	Loading Rate	Residence Time		
Operational Scenario	(gpm)	(gpm)	(gpm)		water (ft)	Spiliway (ft)	Spillway Elev. (gallons)	(gallons)	Surrace (ft2)	Berm (ft2)	(hrs)	(cm/day)		Loading Rate (cm/day)	
	(gpiii)	(gpiii)	(gpiii)	(11)	(11)	(11)	(gallolis)	(galloris)	(112)	(112)	(1113)	(cili/uay)	(1113)	(ciii/uay)	
50 Gallons per Minute from Wells no															
Recycle with 4 Cycles per day in Cell 2A	50	)	0	50											
Cell 1 Bio-Chemical Reactor	•			194	0 194	4 1945	584,118	445625	22196	26044	149	13.2	2 74.3	26	one side of membrane isolated
Cell 2A Tidal Flow Aeration				194	0 1942.	1945	104976	21192	3431	6172	2.8	85.5	5		
Cell 2B Aerobic Polishing with Plants				193			253005						5		
Cell 3 Horizontal Subsurface Flow with Plants				193	7 1939	9 1940	345126						3		
Total							1287225	599983	58718	72097					
											8.3	days			
50 Gallons per Minute from Wells plus 50															
gpm from Recycle with 5 Cycles per day in Cell 2A	50		0 1	00											
Cell 1 Bio-Chemical Reactor	50	, 5	10 I	194	0 194	4 1945	584,118	445625	22196	26044	74	26.4	4 37.1	E 2	one side of membrane isolated
Cell 2A Tidal Flow Aeration				194			104976							33	one side of membrane isolated
Cell 2B Aerobic Polishing with Plants				193			253005				6.9				
Cell 3 Horizontal Subsurface Flow with Plants				193			345126								
Total							1287225				101				
												days			
50 gpm from wells and no recycle for 6 tidal															
cycles per day in Cell 2A	50	)	0	50											
Cell 1 Bio-Chemical Reactor				194	0 194	4 1945	584,118	445625	22196	26044	149	13.2	2 74.3	26	one side of membrane isolated
Cell 2A Tidal Flow Aeration				194			104976		2896	6172	1.8	101.3	3		
Cell 2B Aerobic Polishing with Plants				193			253005				12.1				
Cell 3 Horizontal Subsurface Flow with Plants				193	7 1939	9 1940	345126						3		
Total							1287225	593983	58183	72097	198				
											8.2	days			
50 gpm from wells and 50 gpm from recycle															
for 6 tidal cycles per day in Cell 2A	50	1 5	0 1	00											
Cell 1 Bio-Chemical Reactor	,	, ,	.0 1	194	0 194	4 1945	584,118	445625	22196	26044	74	26.4	4 37.1	53	one side of membrane isolated
Cell 2A Tidal Flow Aeration				194			104976							33	one side of membrane isolated
Cell 2B Aerobic Polishing with Plants				193			253005								
Cell 3 Horizontal Subsurface Flow with Plants				193	7 1939	9 1940	345126		22029	25534			5		
Total							1287225	641568	60453	72097	101				
											4.2	days			
50 gpm from wells and no recycle for 8 tidal															
cycles per day in Cell 2A	50	)	0	50											
Cell 1 Bio-Chemical Reactor				194			584,118							26	one side of membrane isolated
Cell 2A Tidal Flow Aeration				194			104976								
Cell 2B Aerobic Polishing with Plants Cell 3 Horizontal Subsurface Flow with Plants				193 193			253005 345126								
Total				193	/ 193	9 1940	345126 1287225				35.0 197		3		
iotai							128/225	590983	3/8/6	72097		days			
											0.2	Lays			
50 gpm from wells and 50 gpm from recycle															
for 8 tidal cycles per day in Cell 2A	50	) 5	0 1	00											
Cell 1 Bio-Chemical Reactor		-	_	194	0 194	4 1945	584,118	445625	22196	26044	74	26.4	37.1	53	one side of membrane isolated
Cell 2A Tidal Flow Aeration				194			104976								
Cell 2B Aerobic Polishing with Plants				193	8 1939.	1941	253005	26483	11256	14347	6.9	52.:	1		
Cell 3 Horizontal Subsurface Flow with Plants				193	7 1939	9 1940	345126	106684	22029	25534	17.8	26.6	5		
Total							1287225	641568	60453	72097	100				
											4.2	days			

Notes: 1.)Porosity of 1.5", 1", and 3/4" rock is 35%, Porosity of Mix 2 organic media and wood chip insulation layer is 80%,
2.)The wetlands design is capable of a range of aeration pulses and flow rates from 4 cycles per day in Cell 2A at 50 gpm up to 8 cycles per day at 100 gpm. Any number of cycles between 5 and 8 will work with any flow rate into Cell 1 of between 50 and 100 gpm. To have as few as 4 cycles per day only works with 50 gpm at the cell sizes as designed.



<b>JACOBS</b>	PROJECT: Kaiser Mead Groundwater Remediation Interim Action	LOCATION: Mead Washington
CALCULATION SHEET	CLIENT: Kaiser Mead Custodial Trust	JOB No. KMCT2019
TITLE: Final Design Report for Extraction, Treatment, and Discharge Systems	EQUIP./DWG. NO.: Reference Drawings - 002-C-006	CALCULATION NUMBER: Final
Enhanced Wetland Treatment System Calculations		

TABLE 2 PIPELINE HYDRAULICS Page 4 of 10

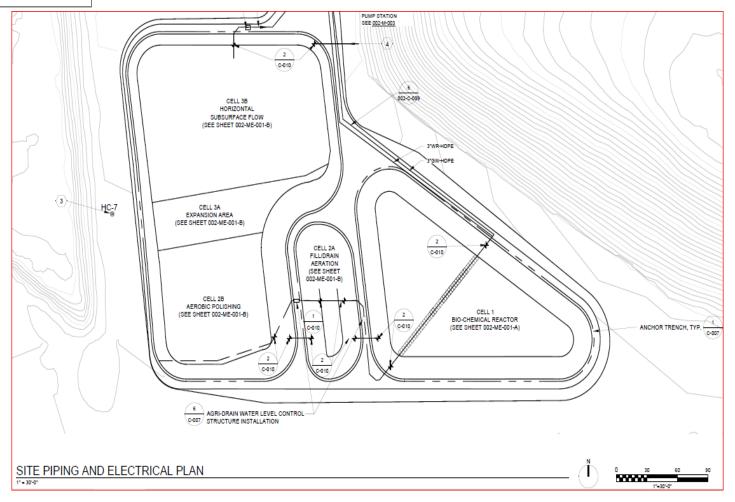
TABLE 2 TH CLINE THE DIVIOLICS	1 466 1 01 10				
Made/Revised by; Mark Madison/PDX	Date: 5/6/2020				
Checked by; Jim Bays/TPA					
Approved					

FLOW RATE in gpm

#### TABLE 2 PIPELINE HYDRAULICS

	25	50	100	150	600	900	1000
			VELOCITY O	F FLOW in f	t/sec		
12" bypass spillway pipes	0.07	0.14	0.28	0.43			
12" Cell 1 outlet		0.14	0.28	0.43	1.70	2.55	
12" Cell 2A outlet					1.70	2.55	2.84
10" Agri-Drain inlet and outlet		0.20	0.41	0.61			
6" drain line header to fill Cell 1	0.28	0.57	1.13				
3" pumped from wells and recycle		2.27	4.54				
3" drain lines average (flow split 10 ways)		0.23	0.45				
3" drain lines average (flow split 5 ways with 1/2 of Cell 1	Isolated)	0.45	0.91				
8" tall x 24" wide standard Infiltrators		0.08	0.16	0.24	0.96	1.44	1.60

Notes: 1.) all gravity pipelines have less than 1 ft of total head loss 2.) spillway pipes flow as partially full culverts with drop inlets





4 Cycles at 50 GPM Page 5 of 10 Made/Revised by; Mark Madison/PDX Date: 5/6/2020 Checked by: Jim Bays/TPA

50 gpm from wells and no recycle for 4 tidal cycles per day in Cell 2A 72000 gallons per day total flow

FINAL Design Specs

Project: Kaiser Mead Natural Treatment System Basin Description: Bio-Chemical Reactor

	Fr	om CAD Earthwork Mo	del		
Contour	Contour	Depth	Incremental	Cumulative	Cumulative
Elevation	Area		Volume	Volume	Volume
		Avg. End	(cu. ft)	(cu. ft)	of Water
(ft)	(sq. ft)	(ft)			at
					Porosity
1940	15,180	N/A	N/A	0	(gallons)
1941	16,849	1	16,014	16,014	41,926
1942	18,575	1	17,712	33,726	145,057
1943	20,357	1	19,466	53,193	318,304
1944	22,196	1	21,277	74,469	445,625
1944.25	23,144	0.25	5,786	80,255	480,248
1945	24,092	1	23,144	97,613	584,118
1946	26 044	1	25.068	122 681	825 888

Cell Profile For all cells wood chip layer has 80% porosity 12" of Drain Rock + 6" of 3/4" Rock 35% porosity 2.75' of Organic Media 80% porosity Normal Water Level

Maximum Water Level with 1 ft of Freeboard Top of Berm

Top of Berm

Hydraulic Surface Area 21,500,730 cm2 1 ft2 = 929 cm2 12.7 cm/day Hydraulic Loading Rate (cm/day) HRT at 50 gpm forward flow rate = 160 hours 6.7 days Time from normal water level to maximum water level at 50 gpm in and 0 gpm out = (assumes no recycle and well pumping and plugged outlet) at maximum water level the emergency bypass begins to flow to Cell 2A During Cell 2A fill cycle Cell 1 receives 50 gpm for 120 minutes or 6000 gallons in and 9000 gallons out 0.080785477 inches Maximum water level drop is 0.007 ft below normal water level During Cell 2A drain cycle Cell 1 stops discharging for 1 hour but receives 50 gpm for 3000 gallons accumulation 0.007 ft above normal water level Maximum Volume that could discharge if the outlet control slide gate fails open when Cell 1 is at normal water elevation Maximum Drain Down 1944.25-1942

272520000 cm3

Hydrualic Loading (cm3/day)

335191 gallons

Cell 2A Final Design Specs Kaiser Mead Tidal Flow Agration

Basın Description:	Tidal Flow Aeratio	on			
	Fr	om CAD Earthwork Mo	del		
Contour	Contour	Depth	Incremental	Cumulative	Cumulative
Elevation	Area		Volume	Volume	Volume
		Avg. End	(cu. ft)	(cu. ft)	of Water
(ft)	(sq. ft)	(ft)			at
					Porosity
1939	931	N/A	N/A	0	(gallons)
1940	1508	1	1219	1219	3192
1941	2142	1	1825	3044	7969
1942	2833	1	2487	5531	14480
1943	3582	1	3207	8738	22877
1944	4388	1	3985	12723	33309
1,944.25	4,820	0.25	1,205	13,928	36464
1945	5251	1	4820	17543	104976
1946	6172	1	5712	23255	156551

Cell Profile 1941.8 1 at max plus 3 at min 36000 +3\*12000 1942.8 1 at max plus 2 at min 36000 + 2\* 18000 36000 gal 1944.25 2 equal at max elev 72000 gal avail. 50 gpm = 4 equal at max elev 91509 gal demand 1944.25 4 equal at avaiablel elev 18000 gal Bottom 12" of Drain Rock 35% porosity 4.25' of 3/4" Angular Basalt Media 35% porosity Normal Water = 1944.25 for 4 equal cycles Hydraulic Profile elevation Maximum Water Level with 1 ft of Freeboard

# of cycles/day 272520000 cm3 1 gal = 3785 cm3 Hydrualic Loading (cm3/day) Hydraulic Surface Area 2,238,704 cm2 1 ft2 = 929 cm2 empty 50% of time 121.7 cm/day Hydraulic Loading Rate (cm/day) HRT = 3.81 hours average 0.16 days empty 50% of time Normal low water is 1940 (BOTTOM 1 FT DOESN'T DRAIN) 4 cycles per day uses 30 minutes to drain, 30 minutes to remain empty, and 30 minutes to refill cycling every 6 hours. 360 minutes per cycle Rate of Drainage for 30 minute draining time = 600 gpm (30 minutes empty with no flow) Rate of Filling for 30 minute filling time = 600 gpm 4 cycles/day Volume of forward flow into and out of Cell 1 in 360 minutes at 50 gpm = 18000 gallons time to reach spillway from normal high water with 50 gpm inflow and no discharge

1 gal = 3785 cm3

Cell 2h Final Desian Specs 0.5 ft contours Project: Kaiser Mead

Basin Description:	Aerobic Polishing	with Plants			
	Fr	om CAD Earthwork Mo	del		
Contour	Contour	Depth	Incremental	Cumulative	Cumulative
Elevation	Area		Volume	Volume	Volume
(ft)	(sq. ft)	Avg. End			of Water
			(cu. ft)	(cu. ft)	at
					Porosity
1,938.00	9,797	N/A	N/A	0.0	(gallons)
1,938.50	10,221	0.5	5004.36	5004.4	13101
1,939.00	10,652	0.5	5218.17	10222.5	26763
1,939.50	11,090	0.5	5435.54	15658.1	40993
1,940.00	11,536	0.5	5656.46	21314.5	55801
1,940.50	11,988	0.5	5880.95	27195.5	162738
1,941.00	12,448	0.5	6109	33304.5	249118
1,941.50	12,915	0.5	6340.62	39645.1	296545
1,942.00	12,605	0.5	6379.86	46025.0	344267

Cell Profile Bottom 1.5' of Drain Rock 35% porosity Normal water level is 1940 with breif drain down to 1939.5 0.5" of 3/4" Angular Basalt Media 35% porosity Maximum Water Level 1940 with 1 ft of Freeboard with 6" wood chips Top of Berm at Cell 3B outlet Top of Berm at Cell 2B

272520000 cm3 1 gal = 3785 cm3 Hydrualic Loading (cm3/day) 10,302,796 cm2 Hydraulic Surface Area 1 ft2 = 929 cm2 26.5 cm/day Hydraulic Loading Rate (cm/day) HRT = 13.7 hours average Normal Low Water Level = 1939.5 near Cell 3 or just before a fill surge Normal High Water Level = 1940 near fill point just after a fill surge flow through rock and plant roots dampens level changes caused by siphon discharge Maximum Drain Down 1940 to 1939.5 14809 gallons Assume discharge to cell 3 at 500 gpm during fill cycle 18000 gallons enters from Cell 2A in 30 minutes while discharge to Cell 3 is 50 gpm or 1500 gallons flow accumulated is 16500 gallons which causes a rise of 0.62 ft average over the total cell for 30 minutes actual rise is expected to be 1 ft at the input location and insignificant at the outlet weir. Root density will dampen rise with growth. Time to reach spillway from normal low water with no discharge and full inflow

Cell 3A Final Design Specs

Kaiser Mead Project: Horizontal Subsurface Flow with Plants Basin Description:

	Fr	om CAD Earthwork Mo	odel	
Contour	Contour	Depth	Incremental	Cumulative
Elevation	Area		Volume	Volume
	Avg. End	Avg. End	(cu. ft)	(cu. ft)
(ft)	(sq. ft)	(ft)		
1,938.00	5,006	N/A	N/A	0
1,938.50	5,199	0.5	2551.23	2551.23
1,939.00	5,393	0.5	2648.05	5199.28
1,939.50	5,587	0.5	2745.03	7944.31
1,940.00	5,782	0.5	2842.14	10786.45

2939.39

3036.79

13725.84

16762.63

102,669

125,384

Top of Berm

272520000 cm3 Hydrualic Loading (cm3/day) Hydraulic Surface Area 5,190,416 cm2

52.5 cm/day Hydraulic Loading Rate (cm/day)

HRT = 6.9 hours average

35% porosity

80% porosity

35% porosity

80% porosity

time to reach maximum water level from normal water level with 50 gpm in and 0 out (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

149 minutes or

2 hours

Cell 3B Final Design Specs Project: Kaiser Mead

5,976

6,171

0.5

0.5

1,940.50

1,941.00

Basin Description

Horizontal Subsurface Flow with Plants From CAD Earthwork Model Cell Profile Contour Contour Depth Incremental Cumulative Cumulative Elevation Area Volume Volume Volume Avg. End Avg. End (cu. ft) (cu. ft) of Water (ft) (sq. ft) (ft) Porosity 1,938.00 20,061 N/A N/A (gallons) Bottom 1,938.50 20,607 0.5 10166.94 10166.94 26,617 2' drain gravel 1.939.00 10441.08 20608.03 21.158 0.5 53.952 1.939.50 10718 07 31326.1 21 715 0.5 82 012 maximum water level 1.940.00 22,277 0.5 10997.9 42324 284.925 Woodchips 1.940.50 22,845 0.5 11280.58 53604 58 400.962 1,941.00 23,419 0.5 11566.04 65170.62 487,476 Top of Berm

Hydrualic Loading (cm3/day) 272520000 cm3 Hydraulic Surface Area 20,172,863 cm2

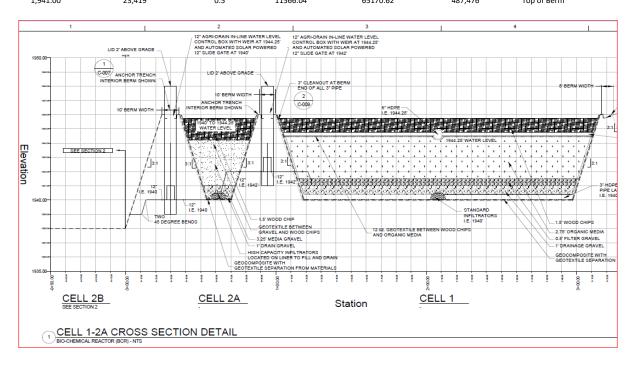
Hydraulic Loading Rate (cm/day) 13.5 cm/day

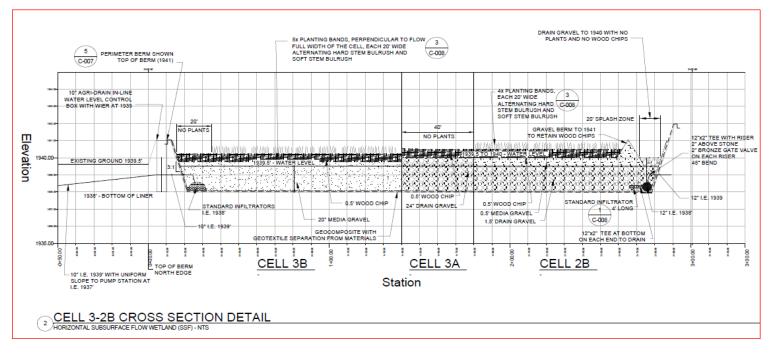
HRT = 27.3 hours average

time to reach maximum water level from normal water level with 50 gpm in and 0 out (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

4058 minutes or

68 hours





PROJECT: Kaiser Mead Custodial Trust LOCATION: Mead Washington **JACOBS** CLIENT::
Kaiser Mead Groundwater
Remediation Interim Action
EQUIP/DW G, NO.:
Reference Drawlings 002-C-006 **CALCULATION SHEET** TITLE:
Final Design Report for Extraction, Treatment, and Discharge
Systems CALCULATION NUMBER: Final Enhanced Wetland Treatment System Calculations

5 Cycles at 100 GPM

Made/Revised by; Mark Madison/PDX

Checked by; Jim Bays/TPA

Approved Page 6 of 10

Date: 5/6/2020

s/TPA				Date: 0/0/2020			
FA						_	
from Ma	lle plue EO apm from	Recycle with 5 Cycles	oor day in Coll 2A		144000 gallons nor day tota	nl flow	
HOIH WE	iis bigs 50 8biii it 0tti	Recycle with 5 cycles	Der day III Cell ZA		144000 gallons per day tota	ii jiuw	
Final De	sign Specs						
	lead Natural Treatm	ent System					
Description:	Bio-Chemical Red	•					
•	Fre	om CAD Earthwork Mo	del				
ur	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile	
tion	Area		Volume	Volume	Volume		
		Avg. End	(cu. ft)	(cu. ft)	of Water		
	(sq. ft)	(ft)			at	For all cells wood chip la	yer has 80% porosity
					Porosity		
940	15,180	N/A	N/A	0	(gallons)	Bottom	Hydrualic Loading ( cm3/day) 545040000 cm3 1 gal = 3785 cm3
941	16,849	1	16,014	16,014	41,926	12" of Drain Rock + 6" of 3/4" Rock 35% porosity	Hydraulic Surface Area 21,500,730 cm2 1 ft 2 = 929 cm2
942	18,575	1	17,712	33,726	145,057	2.75' of Organic Media 80% porosity	Hydraulic Loading Rate (cm/day) 25.3 cm/day
943	20,357	1	19,466	53,193	318,304	Maximum Drain Down 1944.25-1942 335191 gallons	only possible if Cell 2B slide gate also failed open. Cell 2B can hold
944	22,196	1	21,277	74,469	445,625		HRT at 100 gpm forward flow rate = 80 hours 3.3 days
.25	23,144	0.25	5,786	80,255	480,248	Normal Water Level	
945	24,092	1	23,144	97,613	584,118	Maximum Water Level with 1 ft of Freeboard	Time from normal water level to maximum water level at 100 gpm in and 0 gpm out = 17 hours (assumes maximum recycle and
6	26,044	1	25,068	122,681	825,888	Top of Berm	at maximum water level the en
							During Cell 2A fill cycle Cell 1 a receives 100 gpm for 120 minutes or 12000 gallons in and 18000 gallons out
							Maximum water level drop is 0.012 ft below normal water level 0.149923 inches
							During Cell 2A drain cycle Cell 1 stops discharging for 1 hour but receives 100 gpm for 6000 gallons accumulation
Final De	sign Specs						Maximum water level rise is 0.012 ft above normal water level 0.149923 inches
int:	Kaiser Mead Tidal Flow Aerati						Mayimum Valuma that could discharge if the outlet control slide gets fell access when Cell 5 is at accordance already
scription:		on om CAD Earthwork Mo	dal				Maximum Volume that could discharge if the outlet control slide gate fails open when Cell 1 is at normal water elevation 335,191 gallo
	Contour	Depth Depth	Incremental	Cumulative	Cumulative	Cell Profile	
n	Area	рерш	Volume	Volume	Volume	Cell i Totile	4 CYCLES DOESN'T QUITE WORK - USE 5 OR 4+ PER DAY
•	AI Ca	Avg. End	(cu. ft)	(cu. ft)	of Water		5 cycles per day uses 30 minutes to drain, 30 minutes to remain empty, and 3.8 hours to refill.
	(sq. ft)	(ft)	(cu. it)	(cu. it)	at		Hydrualic Loading ( cm3/day) 545040000 cm3
	(34.10)	(10)			Porosity		Hydraulic Surface Area 3,981,718 cm2
39	931	N/A	N/A	0	(gallons)	Bottom	Hydraulic Loading Rate (cm/day) 136.9 cm/day 28800 gallons per cycle
40	1508	1	1219	1219	3192	9" of Drain Rock 35% porosity	
941	2142	1	1825	3044	7969	4.25' of 3/4" Angular Basalt Media 35% porosity	HRT = 2.78 hours average empty 50% of time
942	2833	1	2487	5531	14480	Maximum Drain Down 1944.25-1940 21983 gallons	Rate of Drainage for 30 minute draining time = 733 gpm (30 minutes empty with no flow)
943	3582	1	3207	8738	22877		Rate of Filling for 228 minute filling time = 96 gpm
944	4388	1	3985	12723	33309	Normal High Water Level = 1944	Volume of forward flow into and out of Cell 1 in 288 minutes at 100 gpm 28800 gallons
25	4,820	0.25	1,205	13,928	36464	Hydraulic Profile elevation	
45	5251	1	4820	17543	104976	Maximum Water Level with 1 ft of Freeboard	time to reach spillway with full inflow and no discharge 12 hours
46	6172	1	5712	23255	156551	Top of Berm	Normal low water is 1940 (BOTTOM 1 FT DOESN'T DRAIN)
							Normal high water level is contour that holds 31992 gallons = 1943.874 FT
							1043.21 gal/tenth
							Normal water area 4286 9115 delta
Final De	sign Specs						0.87 additional tenths of ft to add above 1943
	Kaiser Mead						
scription:	Aerobic Polishing						
	Fr	om CAD Earthwork Mo	del				

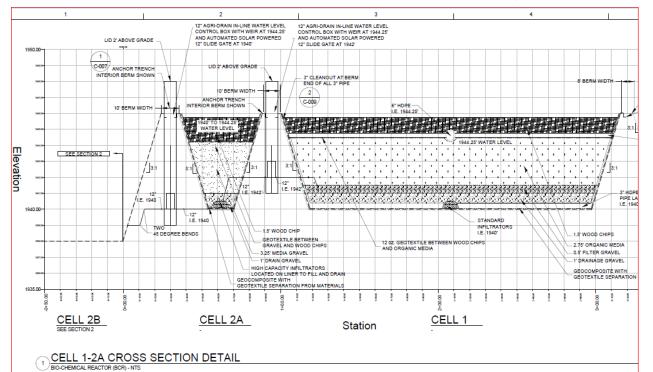
								1043.21 galytentn
								Normal water area 4286 9115 delta
	sign Specs							0.87 additional tenths of ft to add above 1943
Project:	Kaiser Mead							
Basin Description:	Aerobic Polishing	g with Plants						
	Fr	om CAD Earthwork Mod	del					
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile		
Elevation	Area		Volume	Volume	Volume			Hydrualic Loading ( cm3/day) 545040000 cm3
		Avg. End	(cu. ft)	(cu. ft)	of Water			Hydraulic Surface Area 10,302,796 cm2
(ft)	(sq. ft)	(ft)			at			Hydraulic Loading Rate (cm/day) 52.9 cm/day
					Porosity			
1,938.0	9,797	N/A	N/A	0.0	(gallons)	Bottom		HRT = 6.8 hours average
1,938.5	10,221	0.5	5004.36	5004.4	13101	1.5' of Drain Rock	35% porosity	Normal Low Water Level = 1939 near outlet weir
1,939.0	10,652	0.5	5218.17	10222.5	26763	0.5" of 3/4" Angular Basalt Media	35% porosity	Normal High Water Level = 1940 near fill point
1,939.5	11,090	0.5	5435.54	15658.1	40993			flow through rock and plant roots dampens level changes caused by siphon discharge
1,940.0	11,536	0.5	5656.46	21314.5	55801	Maximum Water Level with 1 ft of Freeboar	d	Maximum Drain Down 1940 to 1939.5 14809
1,940.5	11,988	0.5	5880.95	27195.5	203422			Assume discharge to cell 3 at 100 gpm during fill cycle 28800 gallons enters from Cell 2A in 30 minutes while discharge to Cell 3 is 100 gpm or 3000 gallo
1,941.0	12,448	0.5	6109	33304.5	199294	Top of Berm		flow accumulated is 25800 gallons which causes a rise of 0.96 ft.
1,941.5	12,915	0.5	6340.62	39645.1	237236			actual rise is expected to be 1 ft at the input location and insignificant at the outlet weir. Root density will dampen rise with growth.
1,942.0	12,605	0.5	6379.86	46025.0	275413			time to reach spillway with full inflow and no discharge 5 hrs

Cell 3A Final Design Specs Project: Kaiser Mead

Basin Description:	Horizontal Subsur	face Flow with Plants				
	Fro	m CAD Earthwork Mod	el			
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile
Elevation	Area		Volume	Volume	Volume	
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
1,938.00	5,005.70	N/A	N/A	0	(gallons)	Bottom
1,938.50	5,199.20	0.5	2551.23	2551.23	6,679	2' of drain gravel
1,939.00	5,393.00	0.5	2648.05	5199.28	13,612	
1,939.50	5,587.10	0.5	2745.03	7944.31	20,798	normal water level
1,940.00	5,781.50	0.5	2842.14	10786.45	28,239	maximum water level with 1 ft of freeboard
1,940.50	5,976.10	0.5	2939.39	13725.84	102,669	
1,941.00	6,171.00	0.5	3036.79	16762.63	125,384	Top of Berm

Cell 3B Final Design Specs Project: Kaiser Mead the description of the plants

Basin Description:	Horizontal Subsur	face Flow with Plants				
	Fro	m CAD Earthwork Mod	el			
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile
Elevation	Area		Volume	Volume	Volume	
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
1,938.00	20,061.20	N/A	N/A	0	(gallons)	Bottom
1,938.50	20,606.60	0.5	10166.94	10166.94	26,617	20"' of 3/4" Angular Basalt Media
1,939.00	21,157.70	0.5	10441.08	20608.03	53,952	
1,939.50	21,714.60	0.5	10718.07	31326.1	82,012	normal water level
1,940.00	22,277.10	0.5	10997.9	42324	229,523	maximum water level with 1 ft of freeboar
1,940.50	22,845.30	0.5	11280.58	53604.58	400,962	
1,941.00	23,418.90	0.5	11566.04	65170.62	487,476	Top of Berm



Hydrualic Loading (cm3/day) 545040000 cm3 Hydraulic Surface Area 5,190,416 cm2

Hydraulic Loading Rate (cm/day)

35% porosity

35% porosity

80% porosity

HRT = 3.5 hours average time to reach maximum water level from normal water level with 100 gpm in and 0 out

74 minutes

water level rise if Cell 1 slide gate fails open and all flow passes through other cells

0.00 ft rise in Cell 3 (1939.79 ft.)

(slide gate invert is at elevation 142)

TOTAL NTS SYSTEM HRT =

3.5 hours average

105.0 cm/day

27.0 cm/day

0.1 DAYS

Hydrualic Loading (cm3/day) Hydraulic Surface Area

545040000 cm3

Hydraulic Loading Rate (cm/day)

20,172,863 cm2

HRT = 13.7 hours average

time to reach maximum water level from normal water level with 100 gpm in and 0 out

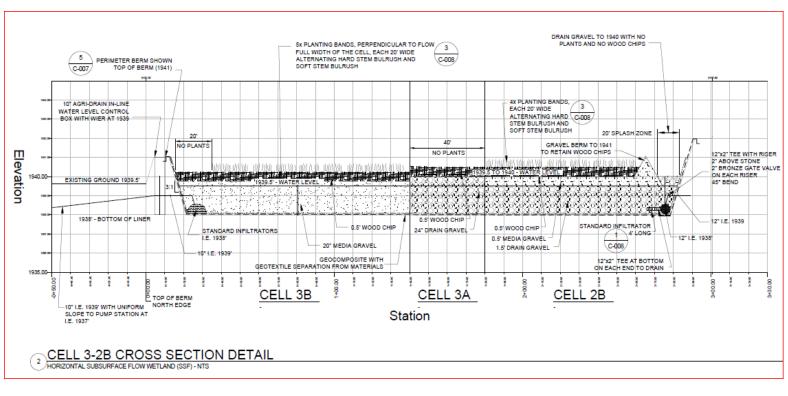
281 minutes or

5 hours

water level rise if Cell 1 slide gate fails open and all flow passes through other cells

(slide gate invert is at elevation 142)

4.09 ft rise in Cell 3 (1939.79 ft.)



<b>JACOBS</b>	PROJECT: Kaiser Mead Custodial Trust	LOCATION: Mead Washington
CALCULATION SHEET	CLIENT:: Kaiser Mead Groundwater Remediation Interim Action	JOB No. KMCT2019
TITLE: Final Design Report for Extraction, Treatment, and Discharge Systems Enhanced Wetland Treatment System Calculations	EQUIP./DWG. NO.: Reference Drawings - 002-C-006	CALCULATION NUMBER: Final

6 Cycles at 50 GPM Page 7 of 10 Made/Revised by; Mark Madison/PDX Date: 5/6/2020 Checked by; Jim Bays/TPA

50 gpm from wells and no recycle for 6 tidal cycles per day in Cell 2A

72000 gallons per day total flow

Cell 1 Final Design Specs

1,940.00

1,940.50

1,941.00

1,941.50

11,536

11,988

12,448

12,915

0.5

0.5

0.5

0.5

5656.46

5880.95

6109

6340.62

Project: Kaiser Mead Natural Treatment System

Basin Description: Bio-Chemical Reactor

	Fr	om CAD Earthwork Mo	del		
Contour	Contour	Depth	Incremental	Cumulative	Cumulative
Elevation	Area		Volume	Volume	Volume
		Avg. End	(cu. ft)	(cu. ft)	of Water
(ft)	(sq. ft)	(ft)			at
					Porosity
1940	15,180	N/A	N/A	0	(gallons)
1941	16,849	1	16,014	16,014	41,926
1942	18,575	1	17,712	33,726	145,057
1943	20,357	1	19,466	53,193	318,304
1944	22,196	1	21,277	74,469	445,625
1944.25	23,144	0.25	5,786	80,255	480,248
1945	24,092	1	23,144	97,613	584,118
1946	26,044	1	25,068	122,681	825,888

For all cells wood chip layer has 80% porosity

35% porosity 35% porosity

35% porosity 35% porosity

Bottom	
12" of Drain Rock + 6" of 3/4" Rock	35% porosity
2.75' of Organic Media	80% porosity
Maximum Drain Down 1944-1942	335191 gallons
Normal Water Level	

Cell Profile

Hydrualic Loading (cm3/day) 272520000 cm3 1 gal = 3785 cm3 Hydraulic Surface Area 1 ft2 = 929 cm2 Hydraulic Loading Rate (cm/day) 12.7 cm/day

HRT at 100 gpm forward flow rate =	160 hours	6.7 days								
Fime from normal water level to maximum water level at 100 gpm in and 0 gpm out =										

17 hours (assumes maximum recycle and well pumping and plugged outlet) at maximum water level the emergency bypass begins to flow to Cell 2A

335191

During Cell 2A fill cycle Cell 1 a receives 100 gpm for 180 minutes or 18000 gallons in and 24000 gallons out Maximum water level drop is 0.012 ft below normal water level 0.149923 inches

During Cell 2A drain cycle Cell 1 stops discharging for 1 hour but receives 100 gpm for 6000 gallons accumulation Maximum water level rise is 0.012 ft above normal water level 0.149923 inches

Maximum Volume that could discharge if the outlet control slide gate fails open when Cell 1 is at normal water elevation

272520000 cm3 1 gal = 3785 cm3

Hydrualic Loading (cm3/day) Hydraulic Surface Area 1 ft2 = 929 cm2 2,690,724 cm2 101.3 cm/day Hydraulic Loading Rate (cm/day)

HRT = 2.4 hours average per cycle empty 50% of the time Normal low water is 1940 (BOTTOM 1 FT DOESN'T DRAIN)

Rate of Drainage for 30 minute draining time = 400 gpm (30 minutes empty with no flow) Rate of Filling for 180 minute filling time = 67 gpm 6 cycles/da Volume of forward flow into and out of Cell 1 in 240 minutes at 100 gpm 12000 gallons

Maximum Drain Down 1942.08-1940 12000 gallons

15192 gallons = 1942.085 FT Normal high water level is contour that holds 839.67 gal/tenth Normal water area 2896.4 712 delta

0.08 additional tenths of ft to add

Hydrualic Loading (cm3/day) 272520000 cm3 1 gal = 3785 cm3 Hydraulic Surface Area 10,302,796 cm2 1 ft2 = 929 cm2

Hydraulic Loading Rate (cm/day) 26.5 cm/day

HRT = 13.7 hours average Normal Low Water Level = 1939 near outlet weir

Normal High Water Level = 1940 near fill point

flow through rock and plant roots dampens level changes caused by siphon discharge  $\,$ Maximum Drain Down 1940 to 1939 13661 gallons

Assume discharge to cell 3 at 100 gpm during fill cycle 12000 gallons enters from Cell 2A in 30 minutes while discharge to Cell 3 is 100 gpm or 3000 gallons flow accumulated is 9000 gallons which causes a rise of =9000 0.34 ft average over the total cell

actual rise is expected to be 1 ft at the input location and insignificant at the outlet weir. Root density will dampen rise with growth.

1943	20,357	1	19,466	53,193	318,304	Maximum Drain Down 1944-1942
1944	22,196	1	21,277	74,469	445,625	Normal Water Level
1944.25	23,144	0.25	5,786	80,255	480,248	
1945	24,092	1	23,144	97,613	584,118	Maximum Water Level with 1 ft of Freeboard
1946	26,044	1	25,068	122,681	825,888	Top of Berm
	sign Specs					
Project:	Kaiser Mead					
Basin Description:	Tidal Flow Aera					
		om CAD Earthwork Mo		0 1 11	0 1 11	0.11.0.171
Contour Elevation	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile
EIEVALION	Area	Ava End	Volume (cu. ft)	Volume (cu. ft)	Volume of Water	
(ft)	(sq. ft)	Avg. End (ft)	(cu. it)	(cu. it)	at at	
(it)	(34.11)	(11)			Porosity	
1939	931	N/A	N/A	0	(gallons)	Bottom
1940	1508	1	1219	1219	3192	9" of Drain Rock
1941	2142	1	1825	3044	7969	4.25' of 3/4" Angular Basalt Media
1942	2833	1	2487	5531	14480	Normal High Water Level = 1942.08
1943	3582	1	3207	8738	22877	
1944	4388	1	3985	12723	33309	
1945	5251	1	4820	17543	104976	Maximum Water Level with 1 ft of Freeboard
1946	6172	1	5712	23255	156551	Top of Berm
Cell 2b Final De: Project:	sign Specs Kaiser Mead					
Basin Description:	Aerobic Polishin	a with Plants				
		om CAD Earthwork Mo	del			
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile
Elevation	Area	-1	Volume	Volume	Volume	
		Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)	• •	• •	at	
		• •			Porosity	
1,938.00	9,797	N/A	N/A	0.0	(gallons)	Bottom
1,938.50	10,221	0.5	5004.36	5004.4	13101	1.5' of Drain Rock
1,939.00	10,652	0.5	5218.17	10222.5	26763	0.5" of 3/4" Angular Basalt Media
1,939.50	11,090	0.5	5435.54	15658.1	40993	
4 0 4 0 0 0	44.500		5050.40	242445	55004	

21314.5

27195.5

33304.5

39645.1

55801

203422

199294

237236

Maximum Water Level with 1 ft of Freeboard

Top of Berm

1,942.00 12,605 6379.86 46025.0 0.5 275413

Horizontal Subsurface Flow with Plants

Cell 3A Final Design Specs

Basin Description:

Project: Kaiser Mead

busin bescription.	monizontal Subsul	juce i low with i lants					
	Fro	m CAD Earthwork Mode					
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile	
Elevation	Area		Volume	Volume	Volume		
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water		
(ft)	(sq. ft)	(ft)			at		
					Porosity		
1,938.00	5,006	N/A	N/A	0	(gallons)	Bottom	
1,938.50	5,199	0.5	2551.23	2551.23	6,679	2' drain gravel	35% porosity
1,939.00	5,393	0.5	2648.05	5199.28	13,612		
1,939.50	5,587	0.5	2745.03	7944.31	20,798	normal water level near cell 3B	
1,940.00	5,782	0.5	2842.14	10786.45	28,239	maximum water level near cell 2B	
1,940.50	5,976	0.5	2939.39	13725.84	102,669		
1,941.00	6,171	0.5	3036.79	16762.63	125,384	Top of Berm	

Call Profile

Hydrualic Loading (cm3/day) 272520000 cm3 1 gal = 3785 cm3 Hydraulic Surface Area 1 ft2 = 929 cm2 5,190,416 cm2 Hydraulic Loading Rate (cm/day) 52.5 cm/day

HRT = 6.9 hours average

time to reach maximum water level from normal water level with 50 gpm in and 0 out  $\,$ 144 minutes or 2 hours (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

water level rise if Cell 1 slide gate fails open and all flow passes through other cells 16.12 ft rise in Cell 3 (1939.79 ft.) (slide gate invert is at elevation 142)

Cell 3B Final Design Specs Proiect: Kaiser Mead

Horizontal Subsurface Flow with Plants Basin Description: From CAD Earthwork Model

Contour	Contour	рерии	IIICI EIIIEIILAI	Cullidiative	Cullidiative	Celi Fiolile
Elevation	Area		Volume	Volume	Volume	
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
1,938.00	20,061	N/A	N/A	0	(gallons)	Bottom
1,938.50	20,607	0.5	10166.94	10166.94	26,617	20" media gravel
1,939.00	21,158	0.5	10441.08	20608.03	53,952	
1,939.50	21,715	0.5	10718.07	31326.1	82,012	maximum water level
1,940.00	22,277	0.5	10997.9	42324	253,267	Woodchips
1,940.50	22,845	0.5	11280.58	53604.58	400,962	
1,941.00	23,419	0.5	11566.04	65170.62	487,476	Top of Berm

Hydrualic Loading (cm3/day) 272520000 cm3 1 gal = 3785 cm3 20,172,863 cm2 Hydraulic Surface Area 1 ft2 = 929 cm2 Hydraulic Loading Rate (cm/day) 13.5 cm/day

HRT = 27.3 hours average

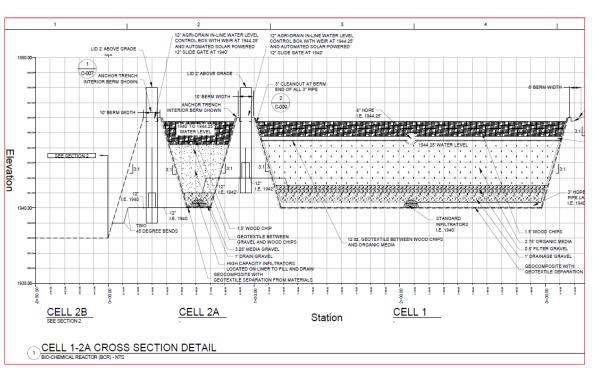
time to reach maximum water level from normal water level with 50 gpm in and 0 out  $\,$ 561 minutes or (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

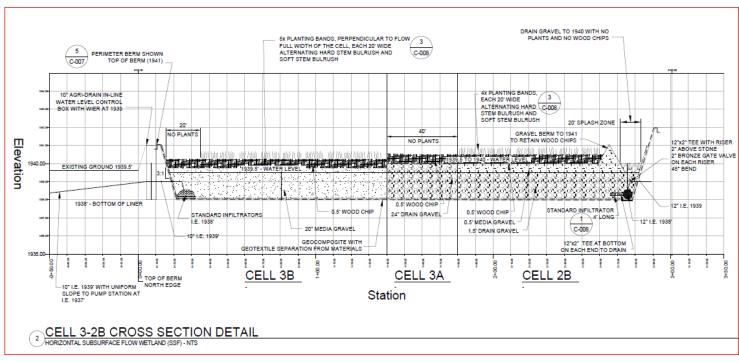
water level rise if Cell 1 slide gate fails open and all flow passes through other cells 0.00 ft

(slide gate invert is at elevation 142)

rise in Cell 3 (1939.79 ft.)

9 hours





<b>JACOBS</b>	PROJECT: Kaiser Mead Custodial Trust	LOCATION: Mead Washington
CALCULATION SHEET	CLIENT:: Kaiser Mead Groundwater Remediation Interim Action	JOB No. KMCT2019
TITLE: Final Design Report for Extraction, Treatment, and Discharge Systems	EQUIP/DWG. NO.: Reference Drawings - 002-C-006	CALCULATION NUMBER: Final
Enhanced Wetland Treatment System Calculations		

6 Cycles at 100 GPM Page 8 of 10 Made/Revised by; Mark Madison/PDX Date: 5/6/2020 Checked by; Jim Bays/TPA

50 gpm from wells and 50 gpm from recycle for 6 tidal cycles per day in Cell 2A

144000 gallons per day total flow

Cumanilation

825,888

104976

156551

Call Duafile

Top of Berm

Top of Berm

Cell Profile

Bottom 1.5' of Drain Rock

Top of Berm

0.5" of 3/4" Angular Basalt Media

Maximum Water Level with 1 ft of Freeboard

Maximum Water Level with 1 ft of Freeboard

Cell 1 Final Design Specs

Project: Kaiser Mead Natural Treatment System

26,044

5251

6172

**Aerobic Polishing with Plants** 

Basin Description: Bio-Chemical Reactor From CAD Earthwork Model

Contour	Contour	Depth	incrementai	Cumulative	Cumulative	Celi Profile
Elevation	Area		Volume	Volume	Volume	
		Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
194	15,180	N/A	N/A	0	(gallons)	Bottom
194	1 16,849	1	16,014	16,014	41,926	12" of Drain Rock + 6" of 3/4" Rock
194	2 18,575	1	17,712	33,726	145,057	2.75' of Organic Media
194	3 20,357	1	19,466	53,193	318,304	Maximum Drain Down 1944-1942
194	22,196	1	21,277	74,469	445,625	Normal Water Level
1944.2	23,144	0.25	5,786	80,255	480,248	Normal Water Level
194	5 24,092	1	23,144	97,613	584,118	Maximum Water Level with 1 ft of Freeboard

122,681

25,068

4820

5712

Cell 2A Final Design Specs Project: Kaiser Mead Tidal Flow Aeration

1946

Basin Description:	Haai Flow A	ration					
		From CAD Earthwork Model					
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile	
Elevation	Area		Volume	Volume	Volume		
		Avg. End	(cu. ft)	(cu. ft)	of Water		
(ft)	(sq. ft)	(ft)			at		
					Porosity		
1939	931	N/A	N/A	0	(gallons)	Bottom	
1940	1508	1	1219	1219	3192	9" of Drain Rock	35% porosity
1941	2142	1	1825	3044	7969	4.25' of 3/4" Angular Basalt Media	35% porosity
1942	2833	1	2487	5531	14480	Maximum Drain Down 1943.41-1940	24000 gallons
1943	3582	1	3207	8738	22877		
1944	4388	1	3985	12723	33309	Normal High Water Level = 1943.82	

17543

23255

Cell 2b Final Design Specs Kaiser Mead Proiect:

1945

1946

**Basin Description:** 

	Fr	om CAD Earthwork Mo	del		
Contour	Contour	Depth	Incremental	Cumulative	Cumulative
Elevation	Area		Volume	Volume	Volume
		Avg. End	(cu. ft)	(cu. ft)	of Water
(ft)	(sq. ft)	(ft)			at
					Porosity
1,938.0	9,797	N/A	N/A	0.0	(gallons)
1,938.5	10,221	0.5	5004.36	5004.4	13101
1,939.0	10,652	0.5	5218.17	10222.5	26763
1,939.5	11,090	0.5	5435.54	15658.1	40993
1,940.0	11,536	0.5	5656.46	21314.5	55801
1,940.5	11,988	0.5	5880.95	27195.5	203422
1,941.0	12,448	0.5	6109	33304.5	199294
1,941.5	12,915	0.5	6340.62	39645.1	237236

For all cells wood chip layer has 80% porosity

35% porosity

35% porosity

545040000 cm3 Hydrualic Loading (cm3/day) 1 gal = 3785 cm3 35% porosity Hydraulic Surface Area 21,500,730 cm2 1 ft2 = 929 cm2 80% porosity Hydraulic Loading Rate (cm/day) 25.3 cm/day 335191 gallons

> HRT at 100 gpm forward flow rate = 80 hours 3.3 days Time from normal water level to maximum water level at 100 gpm in and 0 gpm out =

17 hours (assumes maximum recycle and well pumping and plugged outlet) at maximum water level the emergency bypass begins to flow to Cell 2A

335191

During Cell 2A fill cycle Cell 1 a receives 100 gpm for 180 minutes or 18000 gallons in and 24000 gallons out Maximum water level drop is 0.012 ft below normal water level 0.149923 inches

During Cell 2A drain cycle Cell 1 stops discharging for 1 hour but receives 100 gpm for 6000 gallons accumulation Maximum water level rise is 0.012 ft above normal water level 0.149923 inches

Maximum Volume that could discharge if the outlet control slide gate fails open when Cell 1 is at normal water elevation

0.41 additional tenths of ft to add

545040000 cm3 Hydrualic Loading (cm3/day) Hydraulic Surface Area 3,637,151 cm2 149.9 cm/day Hydraulic Loading Rate (cm/day)

2.3 hours average per cycle empty 50% of the time Normal low water is 1940 (BOTTOM 1 FT DOESN'T DRAIN)

Rate of Drainage for 30 minute draining time = 800 gpm (30 minutes empty with no flow) Rate of Filling for 180 minute filling time = 133 gpm 24000 gallons

6 cycles/day Volume of forward flow into and out of Cell 1 in 240 minutes at 100 gpm

Normal high water level is contour that holds 27192 gallons = 1943.41 FT 1043.21 gal/tenth 4315 delta

Normal water area

Hydrualic Loading (cm3/day) 545040000 cm3 Hydraulic Surface Area 10,302,796 cm2 Hydraulic Loading Rate (cm/day) 52.9 cm/day

6.8 hours average Normal Low Water Level = 1939 near outlet weir Normal High Water Level = 1940 near fill point

flow through rock and plant roots dampens level changes caused by siphon discharge Maximum Drain Down 1940 to 1939 13661 gallons

during fill cycle 24000 gallons enters from Cell 2A in 30 minutes while discharge to Cell 3 is 100 gpm or 3000 gallons flow accumulated is 21000 gallons which causes a rise of 0.78 ft average over the total cell

actual rise is expected to be 1 ft at the input location and insignificant at the outlet weir. Root density will dampen rise with growth.

1,942.0 12,605 6379.86 46025.0 275413 0.5

Cell 3A Final Design Specs

Project: Kaiser Mead Horizontal Subsurface Flow with Plants

busin bescription.	Horizontal Subsul	juce i low with riunts					
	Fro	m CAD Earthwork Model					
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile	
Elevation	Area		Volume	Volume	Volume		
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water		
(ft)	(sq. ft)	(ft)			at		
					Porosity		
1,938.00	5,005.70	N/A	N/A	0	(gallons)	Bottom	
1,938.50	5,199.20	0.5	2551.23	2551.23	6,679	2' of drain gravel	
1,939.00	5,393.00	0.5	2648.05	5199.28	13,612		35% porosity
1,939.50	5,587.10	0.5	2745.03	7944.31	20,798	normal water level	
1,940.00	5,781.50	0.5	2842.14	10786.45	28,239	maximum water level with 1 ft of freeboard	
1,940.50	5,976.10	0.5	2939.39	13725.84	102,669		
1,941.00	6,171.00	0.5	3036.79	16762.63	125,384	Top of Berm	

Cell 3B Final Design Specs Project: Kaiser Mead 

23,418.90

1,941.00

Basin Description:	Horizontal Subsu	rface Flow with Plant:	S			
	Fro	m CAD Earthwork Mo	del			
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile
Elevation	Area		Volume	Volume	Volume	
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
1,938.00	20,061.20	N/A	N/A	0	(gallons)	Bottom
1,938.50	20,606.60	0.5	10166.94	10166.94	26,617	20"' of 3/4" Angular Basalt Media
1,939.00	21,157.70	0.5	10441.08	20608.03	53,952	
1,939.50	21,714.60	0.5	10718.07	31326.1	82,012	normal water level
1,940.00	22,277.10	0.5	10997.9	42324	229,523	maximum water level with 1 ft of freebo
1,940.50	22,845.30	0.5	11280.58	53604.58	400,962	

65170.62

487,476

Top of Berm

11566.04

0.5

Hydrualic Loading (cm3/day) 545040000 cm3 5,190,416 cm2 Hydraulic Surface Area Hydraulic Loading Rate (cm/day) 105.0 cm/day

3.5 hours average

time to reach maximum water level from normal water level with 50 gpm in and 0 out 149 minutes or (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

rise in Cell 3 (1939.79 ft.)

2 hours

water level rise if Cell 1 slide gate fails open and all flow passes through other cells

(slide gate invert is at elevation 142)

TOTAL NTS SYSTEM 92.6 hours average 3.9 DAYS HRT =

545040000 cm3 Hydrualic Loading (cm3/day) 20,172,863 cm2 Hydraulic Surface Area Hydraulic Loading Rate (cm/day) 27.0 cm/day

13.7 hours average time to reach maximum water level from normal water level with 50 gpm in and 0 out

2950 minutes or (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

49 hours

water level rise if Cell 1 slide gate fails open and all flow passes through other cells

0.00 ft

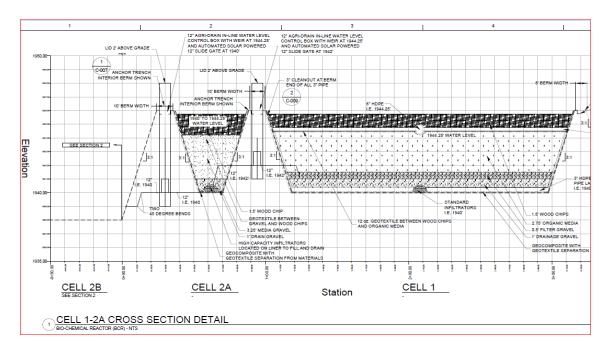
11.87 ft

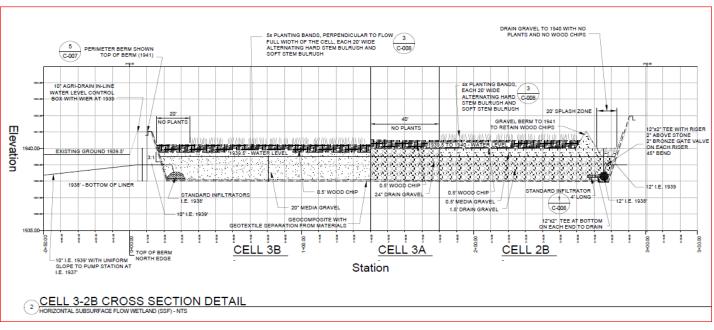
rise in Cell 3 (1939.79 ft.)

(slide gate invert is at elevation 142)

TOTAL NTS SYSTEM HRT =







<b>JACOBS</b>	PROJECT: Kaiser Mead Custodial Trust	LOCATION: Mead Washington
CALCULATION SHEET	CLIENT:: Kaiser Mead Groundwater Remediation Interim Action	JOB No. KMCT2019
TITLE: Final Design Report for Extraction, Treatment, and Discharge Systems	EQUIP./DWG. NO.: Reference Drawings - 002-C-006	CALCULATION NUMBER: Final
Enhanced Wetland Treatment System Calculations		

8 Cycles at 50 GPM Page 9 of 10

Made/Revised by; Mark Madison/PDX Date: 5/6/2020 Checked by; Jim Bays/TPA

50 gpm from wells and no recycle for 8 tidal cycles per day in Cell 2A

72000 gallons per day total flow

Final Design Specs Cell 1

Cell 2A Final Design Specs

Kaiser Mead

Contour

Area

(sa. ft)

Tidal Flow Aeration

931

1508

2142

2833

3582

4388

5251

6172

From CAD Earthwork Model

Depth

Avg. End

(ft)

Proiect:

Contour

Elevation

(ft)

Basin Description

1939

1940

1941

1942

1943

1944

1945

1946

Project: Kaiser Mead Natural Treatment System

Dusin Description.	Dio Chemical Ite	uctor			
	Fr	om CAD Earthwork Mo	del		
Contour	Contour	Depth	Incremental	Cumulative	Cumulative
Elevation	Area		Volume	Volume	Volume
		Avg. End	(cu. ft)	(cu. ft)	of Water
(ft)	(sq. ft)	(ft)			at
					Porosity
1940	15,180	N/A	N/A	0	(gallons)
1941	16,849	1	16,014	16,014	41,926
1942	18,575	1	17,712	33,726	145,057
1943	20,357	1	19,466	53,193	318,304
1944	22,196	1	21,277	74,469	445,625
1944.25	23,144	0.25	5,786	80,255	480,248
1945	24,092	1	23,144	97,613	584,118
1946	26.044	1	25.068	122.681	825.888

Incremental

1219

1825

2487

3207

3985

4820

5712

Volume

(cu. ft)

N/A

Cumulative

1219

3044

5531

8738

12723

17543

23255

Volume

(cu. ft)

For all cells wood chip layer has 80% porosity

35% porosity

35% porosity

12" of Drain Rock + 6" of 3/4" Rock 35% porosity 2.75' of Organic Media 80% porosity Maximum Drain Down 1944-1942 335191 gallons Normal Water Level Normal Water Level

Maximum Water Level with 1 ft of Freeboard

HRT at 50 gpm forward flow rate = 160 hours

Hydrualic Loading (cm3/day)

Maximum water level drop is

Hydraulic Loading Rate (cm/day)

Hydraulic Surface Area

35 hours (assumes maximum recycle and well pumping and plugged outlet) Time from normal water level to maximum water level at 50 gpm in and 0 gpm out = During Cell 2A fill cycle Cell 1 a receives 50 gpm for 120 minutes or 6000 gallons in and 9000 gallons out

272520000 cm3

21,500,730 cm2

During Cell 2A drain cycle Cell 1 stops discharging for 1 hour but receives 50 gpm for 3000 gallons accumulation Maximum water level rise is 0.006 ft above normal water level 0.075 inches

Maximum Volume that could discharge if the outlet control slide gate fails open when Cell 1 is at normal water elevation

0.006 ft below normal water level

12.7 cm/day

1 gal = 3785 cm3

1 ft2 = 929 cm2

0.075 inches

at maximum water level the emergency bypass begins to flow to Cell 2A

335,191 gallons

6.7 days

Hydrualic Loading (cm3/day) 272520000 cm3 Hydraulic Surface Area 2,406,074 cm2

Hydraulic Loading Rate (cm/day) 113.3 cm/day

HRT = 2.0 hours average (1/2 of fill time plus 1/2 of drain time) Normal low water is 1940 (BOTTOM 1 FT DOESN'T DRAIN)

180 minutes per cycle 8 cycles per day uses 30 minutes to drain, 30 minutes to remain empty, and 2 hours to refill. Rate of Drainage for 30 minute draining time = 300 gpm (30 minutes empty with no flow) 9000 gallons

Rate of Filling for 120 minute filling time = 75 gpm Volume of forward flow into and out of Cell 1 in 180 minutes at 50 gpm  $\,$ 9000 gallons

12192 gallons = 1941.649 FT Normal high water level is contour that holds 651.16 gal/tenth 4223 delta

0.65 additional tenths of ft to add

Normal water area

Cell 2b Final Design Specs Proiect: Kaiser Mead Rasin Description Aerohic Polishing with Plants

Basin Description:	Aerobic Polishing with Plants						
	Fr	om CAD Earthwork Mo	del				
Contour	Contour	Depth	Incremental	Cumulative	Cumulative		
Elevation	Area		Volume	Volume	Volume		
		Avg. End	(cu. ft)	(cu. ft)	of Water		
(ft)	(sq. ft)	(ft)			at		
					Porosity		
1,938.00	9,797	N/A	N/A	0.0	(gallons)		
1,938.50	10,221	0.5	5004.36	5004.4	13101		
1,939.00	10,652	0.5	5218.17	10222.5	26763		
1,939.50	11,090	0.5	5435.54	15658.1	40993		
1,940.00	11,536	0.5	5656.46	21314.5	55801		
1,940.50	11,988	0.5	5880.95	27195.5	203422		
1,941.00	12,448	0.5	6109	33304.5	199294		
1,941.50	12,915	0.5	6340.62	39645.1	237236		

Cell Profile

Top of Berm

Cell Profile

Top of Berm

Cell Profile

9" of Drain Rock

Top of Berm

4.25' of 3/4" Angular Basalt Media

Maximum Drain Down 1941.53-1940

Normal High Water Level = 1941.53

Maximum Water Level with 1 ft of Freeboard

Cumulative

Volume

of Water

Porosity

(gallons)

3192

7969

14480

22877

33309

104976

156551

Bottom 1.5' of Drain Rock 35% porosity 0.5" of 3/4" Angular Basalt Media 35% porosity Maximum Water Level with 1 ft of Freeboard

Hydrualic Loading (cm3/day) 272520000 cm3 Hydraulic Surface Area 10,302,796 cm2 Hydraulic Loading Rate (cm/day) 26.5 cm/day

HRT = 13.7 hours average Normal Low Water Level = 1939 near outlet weir Normal High Water Level = 1940 near fill point

flow through rock and plant roots dampens level changes caused by siphon discharge Maximum Drain Down 1940 to 1939 13661 gallons

during fill cycle 9000 gallons enters from Cell 2A in 30 minutes while discharge to Cell 3 is 50 gpm or 1500 gallons flow accumulated is 7500 gallons which causes a rise of 0.28 ft average over the total cell for 30 minutes

actual rise is expected to be <1 ft at the input location and insignificant at the outlet weir. Root density will dampen rise with growth.

1,942.00 12,605 6379.86 46025.0 275413 0.5

Horizontal Subsurface Flow with Plants

Cell 3A Final Design Specs

Basin Description:

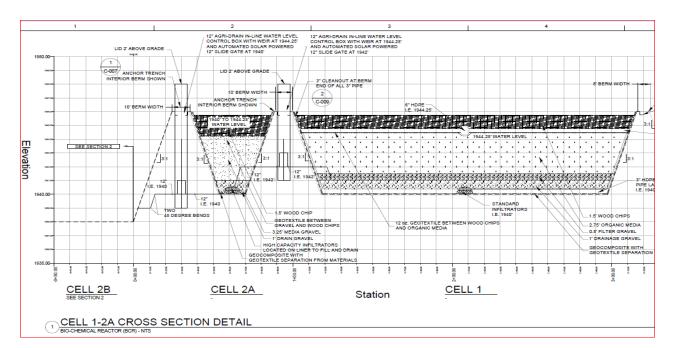
Project: Kaiser Mead

	Fro	m CAD Earthwork Mo	del			
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile
Elevation	Area		Volume	Volume	Volume	
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
1,938.00	5,006	N/A	N/A	0	(gallons)	bottom
1,938.50	5,199	0.5	2551.23	2551.23	6,679	2' Drain Gravel
1,939.00	5,393	0.5	2648.05	5199.28	13,612	
1,939.50	5,587	0.5	2745.03	7944.31	20,798	normal water level
1,940.00	5,782	0.5	2842.14	10786.45	28,239	maximum water level with 1 ft of freeboar
1,940.50	5,976	0.5	2939.39	13725.84	102,669	
1,941.00	6,171	0.5	3036.79	16762.63	125,384	Top of Berm

Cell 3B Final Design Specs

,	
Basin Description:	Horizontal Subsurface Flow with Plants
	From CAD Farthwork Modo

		,			
	Fro	m CAD Earthwork Mode	I		
Contour	Contour	Depth	Incremental	Cumulative	Cumulative
Elevation	Area		Volume	Volume	Volume
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water
(ft)	(sq. ft)	(ft)			at
					Porosity
1,938.00	20,061	N/A	N/A	0	(gallons)
1,938.50	20,607	0.5	10166.94	10166.94	26,617
1,939.00	21,158	0.5	10441.08	20608.03	53,952
1,939.50	21,715	0.5	10718.07	31326.1	82,012
1,940.00	22,277	0.5	10997.9	42324	253,267
1,940.50	22,845	0.5	11280.58	53604.58	400,962
1,941.00	23,419	0.5	11566.04	65170.62	487,476



0.35 Hydrualic Loading (cm3/day) 272520000 cm3 Hydraulic Surface Area 5,190,416 cm2 woodchip porosity 0.8 Hydraulic Loading Rate (cm/day) 52.5 cm/day HRT = 6.9 hours average time to reach maximum water level from normal water level with 50 gpm in and 0 out 144 minutes or 2 hours (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells) 16.12 ft rise in Cell 3 (1939.79 ft.) water level rise if Cell 1 slide gate fails open and all flow passes through other cells (slide gate invert is at elevation 142) TOTAL NTS SYSTEM HRT = 182.7 hours average 7.6 DAYS

> Hydrualic Loading (cm3/day) 272520000 cm3 20,172,863 cm2 Hydraulic Surface Area 13.5 cm/day Hydraulic Loading Rate (cm/day) HRT = 27.3 hours average

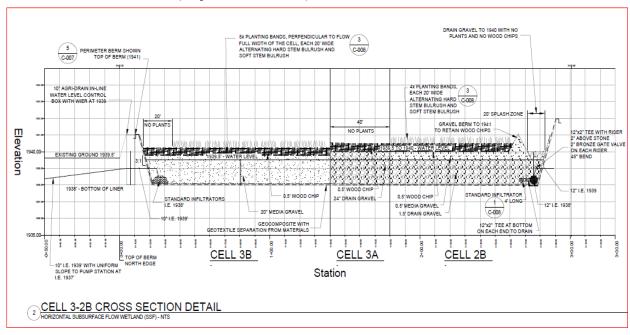
media porosity

35% porosity

time to reach maximum water level from normal water level with 50 gpm in and 0 out 561 minutes or (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

9 hours

water level rise if Cell 1 slide gate fails open and all flow passes through other cells 0.00 ft rise in Cell 3 (1939.79 ft.) (slide gate invert is at elevation 142)



<b>JACOBS</b>	PROJECT: Kaiser Mead Custodial Trust	LOCATION: Mead Washington
CALCULATION SHEET	CLIENT:: Kaiser Mead Groundwater Remediation Interim Action	JOB No. KMCT2019
TITLE: Final Design Report for Extraction, Treatment, and Discharge Systems	EQUIP./DWG. NO.: Reference Drawings - 002-C-006	CALCULATION NUMBER: Final
Enhanced Wetland Treatment System Calculations		

8 Cycles at 100 GPM Page 10 of 10

From CAD Earthwork Model

Made/Revised by; Mark Madison/PDX Date: 5/6/2019

50 gpm from wells and 50 gpm from recycle for 8 tidal cycles per day in Cell 2A

26,044

144000 gallons per day total flow

825,888

156551

Top of Berm

Top of Berm

Final Design Specs Cell 1

Project: Kaiser Mead Natural Treatment System

	Basin Desc	ription:	Bio-Chemical Reactor
--	------------	----------	----------------------

Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile
Elevation	Area		Volume	Volume	Volume	
		Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
1940	15,180	N/A	N/A	0	(gallons)	Bottom
1941	16,849	1	16,014	16,014	41,926	12" of Drain Rock + 6" of 3/4" Rock
1942	18,575	1	17,712	33,726	145,057	2.75' of Organic Media
1943	20,357	1	19,466	53,193	318,304	Maximum Drain Down 1944-1942
1944	22,196	1	21,277	74,469	445,625	Normal Water Level
1944.25	23,144	0.25	5,786	80,255	480,248	Normal Water Level
1945	24,092	1	23,144	97,613	584,118	Maximum Water Level with 1 ft of Freeboard

122,681

25,068

5712

Cell 2A Final Design Specs Proiect: Kaiser Mead Tidal Flow Aeration **Basin Description:** 

1946

	Fr	rom CAD Earthwork Model					
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile	
Elevation	Area		Volume	Volume	Volume		
		Avg. End	(cu. ft)	(cu. ft)	of Water		
(ft)	(sq. ft)	(ft)			at		
					Porosity		
1939	931	N/A	N/A	0	(gallons)	Bottom	
1940	1508	1	1219	1219	3192	9" of Drain Rock	35% porosity
1941	2142	1	1825	3044	7969	4.25' of 3/4" Angular Basalt Media	35% porosity
1942	2833	1	2487	5531	14480	Maximum Drain Down 1942.8-1940	18000 gallons
1943	3582	1	3207	8738	22877		
1944	4388	1	3985	12723	33309	Normal High Water Level = 1942.8	
1945	5251	1	4820	17543	104976	Maximum Water Level with 1 ft of Freeboard	

23255

Cell 2b Final Design Specs

1946

Kaiser Mead Proiect: Aerohic Polishing with Plants

6172

Basın Description:	Aerobic Polishing	with Plants					
	Fro	om CAD Earthwork Mode	·I				
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	Cell Profile	
Elevation	Area		Volume	Volume	Volume		
		Avg. End	(cu. ft)	(cu. ft)	of Water		
(ft)	(sq. ft)	(ft)			at		
					Porosity		
1,938.0	9,797	N/A	N/A	0.0	(gallons)	Bottom	
1,938.5	10,221	0.5	5004.36	5004.4	13101	1.5' of Drain Rock	35% porosity
1,939.0	10,652	0.5	5218.17	10222.5	26763	0.5" of 3/4" Angular Basalt Media	35% porosity
1,939.5	11,090	0.5	5435.54	15658.1	40993		
1,940.0	11,536	0.5	5656.46	21314.5	55801	Maximum Water Level with 1 ft of Freeboa	rd
1,940.5	11,988	0.5	5880.95	27195.5	162738		
1,941.0	12,448	0.5	6109	33304.5	199294	Top of Berm	
1,941.5	12,915	0.5	6340.62	39645.1	237236		

For all cells wood chip layer has 80% porosity

35% porosity 80% porosity 335191 gallons

Hydrualic Loading ( cm3/day)	545040000 cm3	1 gal = 3785 cm3
Hydraulic Surface Area	21,500,730 cm2	1 ft2 = 929 cm2
Hydraulic Loading Rate (cm/day)	25.3 cm/day	

HRT at 100 gpm forward flow rate = 80 hours 3.3 days Time from normal water level to maximum water level at 100 gpm in and 0 gpm out =

17 hours (assumes maximum recycle and well pumping and plugged outlet)

During Cell 2A fill cycle Cell 1 a receives 100 gpm for 120 minutes or 12000 gallons in and 18000 gallons out Maximum water level drop is 0.012 ft below normal water level 0.149923 inches

During Cell 2A drain cycle Cell 1 stops discharging for 1 hour but receives 100 gpm for 6000 gallons accumulation Maximum water level rise is 0.012 ft above normal water level 0.149923 inches

Maximum Volume that could discharge if the outlet control slide gate fails open when Cell 1 is at normal water elevation 335,191 gallons

at maximum water level the emergency bypass begins to flow to Cell 2A

545040000 cm3 Hydrualic Loading (cm3/day) Hydraulic Surface Area 3,187,803 cm2 Hydraulic Loading Rate (cm/day) 171.0 cm/day

HRT = 1.8 hours average (1/2 of fill time plus 1/2 of drain time) Normal low water is 1942.8 (BOTTOM 1 FT DOESN'T DRAIN)

8 cycles per day uses 30 minutes to drain, 30 minutes to remain empty, and 2 hours to refill.

180 minutes per cycle Rate of Drainage for 30 minute draining time = 600 gpm (30 minutes empty with no flow) Rate of Filling for 120 minute filling time = 150 gpm

Volume of forward flow into and out of Cell 1 in 180 minutes at 100 gpm 18000 gallons

21192 gallons = 1942.8 FT Normal high water level is contour that holds

839.7 gal/tenth 6712 delta

0.80 additional tenths of ft to add Normal water area 3431

Hydrualic Loading (cm3/day) 545040000 cm3 Hydraulic Surface Area 10,302,796 cm2 Hydraulic Loading Rate (cm/day) 52.9 cm/day

HRT = 6.8 hours average Normal Low Water Level = 1939 near outlet weir

Normal High Water Level = 1940 near fill point

flow through rock and plant roots dampens level changes caused by siphon discharge  $\,$ Maximum Drain Down 1940 to 1939 13661 gallons

during fill cycle 18000 gallons enters from Cell 2A in 30 minutes while discharge to Cell 3 is 100 gpm or 3000 gallons flow accumulated is 15000 gallons which causes a rise of 0.56 ft average over the total cell for 30 minutes

actual rise is expected to be 1 ft at the input location and insignificant at the outlet weir. Root density will dampen rise with growth.

6379.86 1,942.0 12,605 0.5 46025.0 275413

Cell 3A Final Design Specs

Kaiser Mead Project: Basin Description: Horizontal Subsurface Flow with Plants

6,171.00

22.845.30

23,418.90

	Fro	m CAD Earthwork Mod	lel			
Contour	Contour	Depth	Incremental	Cumulative	Cumulative	
Elevation	Area		Volume	Volume	Volume	Cell Profile
	Avg. End	Avg. End	(cu. ft)	(cu. ft)	of Water	
(ft)	(sq. ft)	(ft)			at	
					Porosity	
1,938.00	5,005.70	N/A	N/A	0	(gallons)	
1,938.50	5,199.20	0.5	2551.23	2551.23	6,679	bottom
1,939.00	5,393.00	0.5	2648.05	5199.28	13,612	2' and 2" of 3/4" Angular Basalt Media
1,939.50	5,587.10	0.5	2745.03	7944.31	20,798	normal water level
1,940.00	5,781.50	0.5	2842.14	10786.45	28,239	maximum water level with 1 ft of freeboa
1,940.50	5,976.10	0.5	2939.39	13725.84	102,669	Top of Berm

16762.63

53604.58

65170.62

125,384

400.962

487,476

3036.79

11280.58

11566.04

Cell 3B Final Design Specs Project: Kaiser Mead

1,941.00

1.940.50

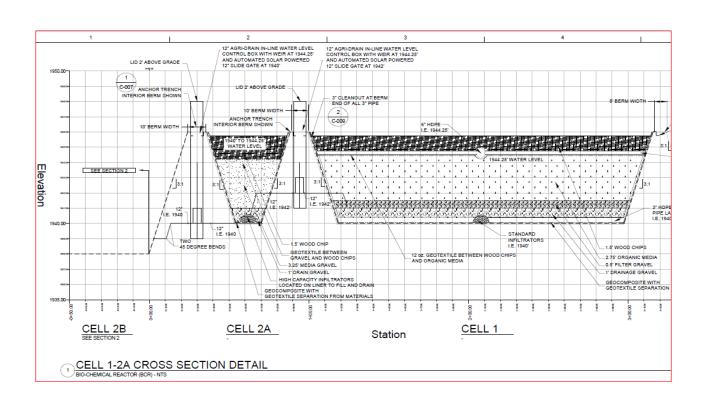
1,941.00

Basin Description Horizontal Subsurface Flow with Plants From CAD Earthwork Model Contour Contour Depth Incremental Cumulative Cumulative Elevation Area Volume Volume Volume (cu. ft) (cu. ft) of Water Avg. End Avg. End (ft) (sq. ft) (ft) Porosity 1,938.00 20,061.20 N/A (gallons) 1,938.50 20,606.60 0.5 10166.94 10166.94 26,617 1.939.00 21.157.70 0.5 10441.08 20608.03 53,952 1,939.50 21,714.60 0.5 10718.07 31326.1 82,012 1,940.00 22,277.10 42324 229,523 0.5 10997.9

0.5

0.5

0.5



media porosity woodchip porosity

35% porosity

0.8

0.35

Hydrualic Loading (cm3/day) Hydraulic Surface Area Hydraulic Loading Rate (cm/day)

545040000 cm3 5,190,416 cm2 105.0 cm/day

3.5 hours average

time to reach maximum water level from normal water level with 50 gpm in and 0 out (assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

2 hours

49 hours

water level rise if Cell 1 slide gate fails open and all flow passes through other cells

11.87 ft

rise in Cell 3 (1939.79 ft.)

TOTAL NTS SYSTEM HRT =

92.1 hours average

3.8 DAYS

545040000 cm3 Hydrualic Loading (cm3/day) Hydraulic Surface Area 20,172,863 cm2 Hydraulic Loading Rate (cm/day) 27.0 cm/day

HRT = 13.7 hours average

time to reach maximum water level from normal water level with 50 gpm in and 0 out

(assumes failed recycle and EC pumps and no discharge with 50 gpm from wells causing forward flow through all cells)

water level rise if Cell 1 slide gate fails open and all flow passes through other cells

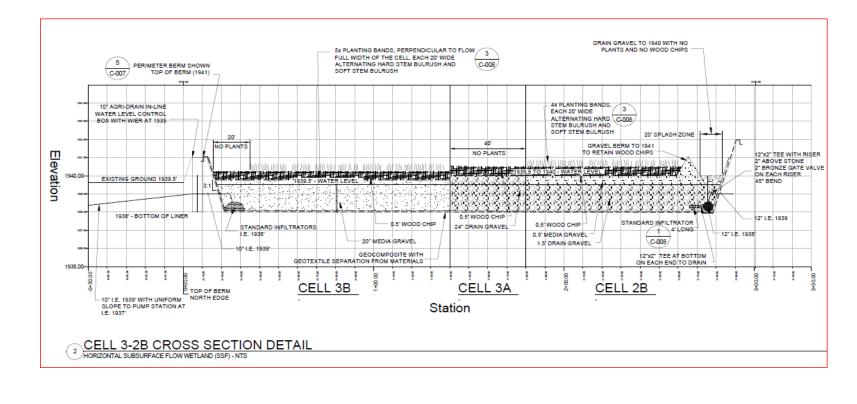
rise in Cell 3 (1939.79 ft.)

(slide gate invert is at elevation 142)

TOTAL NTS SYSTEM HRT =

17.1 hours average

0.7 DAYS



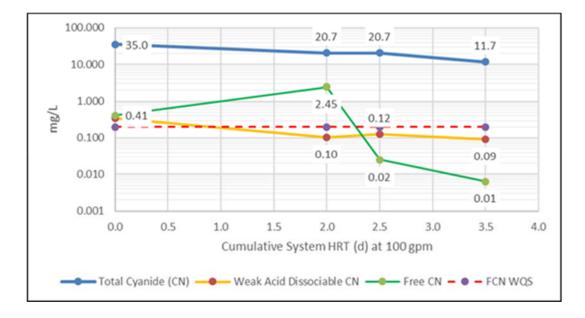
**Enhanced Wetland Treatment System Process** 

The expected performance results provided in the Pre-Final Design Report have been revised and are presented in Table 1.

**Table 1. Treatment Profile Summary** 

	Nominal HRT	Cumulative HRT	Total Cyanide (CN)	Weak Acid Dissociable CN	Free CN	FCN WQS
Station	d	d	mg/L	mg/L	mg/L	mg/L
Inlet	0.0	0.0	35.0	0.35	0.41	0.2
Cell 1	2.0	2.0	20.7	0.10	2.45	0.2
Cell 2	0.5	2.5	20.7	0.12	0.02	0.2
Cell 3	1.0	3.5	11.7	0.09	0.01	0.2
Concentration Reduction			66%	74%	98%	

Input values for total cyanide (TCN), weak acid dissociable cyanide (WAD CN) and free cyanide were selected from the average inflow values measured during the pilot system operation. First-order model removal rate constants calibrated from the final four data pairs of pilot data from each treatment cell were utilized to project performance under the design assumptions. Figure 2 presents the expected performance along the treatment profile based on cumulative hydraulic residence time. A total flow rate of 100 gpm (50 gpm forward flow, 50 gpm recirculation flow) was assumed. Total cyanide is projected to be discharged from the Enhanced Treatment Wetland at approximately 12 mg/L.



Kaiser Mead Enhanced Treatment Wetland Pre-Design Water Quality Performance Estimates p-k-C\* Model (Kadlec and Wallace 2009) Calibrated to Continuous Flow Pilot Study (Jacobs 2020) Prepared by Jim Bays/Jacobs Engineering Group Revised March 31 2020

Model assumptions, parameter values and performance results are summarized in Table 2. The model hydraulic characterization (P) reflects the typical number of tanks in series for each type of system (i.e., Biochemical Reactor, Aerobic Polishing Cell, Horizontal Subsurface Flow).

Table 2. Model Assumptions, Parameter Values, and Performance for 100 gpm Flow.

			Cell 1			Cell 2			Cell 3	
Parameter	Unit	TCN	WAD	FCN	TCN	WAD	FCN	TCN	WAD	FCN
Ci	mg/L	35	0.35	0.41	20.7	0.10	2.45	20.7	0.12	0.02
Co	mg/L	20.73	0.10	2.45	20.7	0.12	0.02	11.7	0.09	0.01
C*	mg/L	1.5	0	0	1.5	0	0	1.5	0	0
kv	1/d	0.31	0.76	-0.67	0.00	-0.37	31.7	0.66	0.33	1.5
T	d	2	2	2	0.5	0.5	0.5	1	1	1
Р	TIS	3	3	3	2	2	2	6	6	6
C-C*	mg/L	19.2	0.10	2.45	19.2	0.12	0.02	10.2	0.09	0.01
Ci-C*	mg/L	33.5	0.35	0.41	19.2	0.10	2.45	19.2	0.12	0.02
LH	unitless	0.57	0.29	5.96	1	1.21	0.01	0.533	0.73	0.26
RH	unitless	0.57	0.29	5.96	1.00	1.21	0.01	0.53	0.73	0.26

Note: Model formulation "C" selected for calibration and analysis from Equation 15.7 (Kadlec and Wallace 2009).

Model Source: Kadlec, R.H. and S. Wallace. 2009. Treatment Wetlands 2nd Ed. CRC

Press, Boca Raton FL.

Kaiser Mead Enhanced Treatment Wetland
Pre-Design Water Quality Performance Estimates
p-k-C\* Model (Kadlec and Wallace 2009) Calibrated to Continuous Flow Pilot Study (Jacobs 2020)
Prepared by Jim Bays/Jacobs Engineering Group

Horizontal Subsurface	Flow Wetland Si	mple PkC	Design M	lodel (Wast					
Project Name	KAISER MEA	D DESIGN 10	00 GPM CEL	L 1 N SERIES		ndicated by wi		S.	
Project Number				KMCT.2200			<b>3</b>		
	Gen	eral Inflow	Data						
Parameter		Value	Units						
Annual Average Daily Flow		100	gpm	▼					
Converted Flow		545	m <sup>3</sup> /d						
Wastewater Temperature		5	°C						
	Water O	rality Char	towinting						
Parameter	water Q	uality Char BOD5	TSS	Organic N	NH4-N	NO2/3-N	TN	TP	FC
Influent Concentration, mg/L	C <sub>i</sub> =	5050	1.00	13.0	3.0	34.4	50		
Average Target Effluent Conc., mg/L	C <sub>e</sub> =						0		
Desired Confidence Percentile	Ü	0.5		0.5	0.5	0.5	0.5	0.5	0.5
Max Month/Annual Factor		1.7	1.9	1	1	1	1.6	1.8	2.6
Design Target Conc., mg/L	C <sub>d</sub> =								
Wetland Background Limit, mg/L	C* =	1	3.03	1.5	0	0	1.5	0.02	0
Reduction fraction to target	$F_{e} = 1 - C_{e}/C_{i} =$	No Value	No Value	1.000	1.000	1.000	1.000	No Value	No Value
Reduction fraction to background	$F_b = 1 - C^*/C_i =$			0.885	1.000	1.000	0.970		
Areal Rate Constant, 20°C, m/y	k <sub>20</sub> =	86	1000	34.6	208	8458	18	12	103
Temperature Factor	θ =	1.00	1.065	1.01	1.01	1.09	1.01	1.00	1.00
P-Factor	P =	3	3	3	3	3	6	3	3
Areal Rate Constant, m/y	k <sub>T</sub> =	86 C*>Cd	1000 C*>Cd	30.2	168.6	2322.1	16.7	12	103
Area required for each parameter, ac  Use Aeration Design	Required T			C*>Cd rea	-0.6	0.0	C*>Cd	C*>Cd	C*>Cd
Required Treatment Wetland Area	A <sub>max</sub> =	0.000034	acres	Displays minir	mum wetland	area to treat	all pollutant	s down to d	esired
		0.000014	ha	targets	nam wouldne	aroa to troat	an ponatant	0 40111110 4	oonoa
User Defined Area	A <sub>user</sub> =	0.509555	acres						
Soci Bolliloa 7 liba	- user			User specified for effluent ca			t if you wish	to use A <sub>max</sub>	(above)
Fin	al Effluent Conce	0.206297	ha and Perce			•			
Area (ha) used for Calculations =		BOD5	TSS				TN	TP	FC
	0.2			Organic N	NH4-N	NO2/3-N	IIN		
Design Target Conc., mg/L	C <sub>d</sub> =			Organic N	NH4-N	NO2/3-N	0.0		
Influent concentrations, mg/L				Organic N	NH4-N 3.000	NO2/3-N 34.400			
	C <sub>d</sub> =			_			0.0		0.0
Influent concentrations, mg/L	C <sub>d</sub> =			13.0	3.000	34.400	0.0 50.4		0.0
Influent concentrations, mg/L	C <sub>d</sub> =			13.0	3.000	34.400	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration)	C <sub>d</sub> =			13.0 10.0	3.000 1.988	34.400 0.193	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration) Mass Loading (lb/day)	C <sub>d</sub> =			13.0 10.0 23% 16	3.000 1.988 34% 4	34.400 0.193 99% 41	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration)	C <sub>d</sub> =			13.0 10.0	3.000 1.988	34.400 0.193	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d)	C <sub>d</sub> =			13.0 10.0 23% 16 34.3 12 26.5	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)	$C_d = C_i =$		on Area	13.0 10.0 23% 16 34.3 12 26.5 23%	3.000 1.988 34% 4 7.9 2	34.400 0.193 99% 41 90.9 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)	C <sub>d</sub> =	ties Basec		13.0 10.0 23% 16 34.3 12 26.5 23% and Flow	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)	$C_d = C_i =$			13.0 10.0 23% 16 34.3 12 26.5 23% and Flow	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99%	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm)	C <sub>d</sub> = C <sub>i</sub> =	ties Basec Approx Aspe		13.0 10.0 23% 16 34.3 12 26.5 23% and Flow	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99%	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper	ties Basec Approx Aspe Length (m)	ect Ratio (L:V	13.0 10.0 23% 16 34.3 12 26.5 23% and Flow	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99%	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969	ties Basec Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C	ect Ratio (L:W e (m/m) onstraints	13.0 10.0 23% 16 34.3 12 26.5 23% and Flow	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969 10500	ties Basec Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil	ect Ratio (L:W e (m/m) onstraints lity	13.0 10.0 10.0 23% 16 34.3 12 26.5 23% and Flow V) = (1:1)	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969	ties Basec Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil	ect Ratio (L:W e (m/m) onstraints	13.0 10.0 10.0 23% 16 34.3 12 26.5 23% and Flow V) = (1:1)	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d) Design Outlet Water Depth h <sub>0</sub> (m)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969 10500 0.99	ties Based Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil G <sub>3</sub> , Distance	ect Ratio (L:V e (m/m) onstraints lity Thickening/	13.0 10.0 10.0 23% 16 34.3 12 26.5 23% and Flow V) = (1:1)	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969 10500 0.99 HLR =	ties Basec Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil	ect Ratio (L:W e (m/m) onstraints lity	13.0 10.0 10.0 23% 16 34.3 12 26.5 23% and Flow V) = (1:1)	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d) Design Outlet Water Depth h <sub>0</sub> (m)  Hydraulic Loading Rate, q (cm/d)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969 10500 0.99 HLR =	ties Based Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil G <sub>3</sub> , Distance	ect Ratio (L:V e (m/m) onstraints lity Thickening/	13.0 10.0 10.0 23% 16 34.3 12 26.5 23% and Flow V) = (1:1)	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d) Design Outlet Water Depth h <sub>0</sub> (m)  Hydraulic Loading Rate, q (cm/d)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969 10500 0.99 HLR = HRT =	ties Based Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil G <sub>3</sub> , Distance	e (m/m) onstraints lity Thickening/ cm/d days	13.0 10.0 10.0 23% 16 34.3 12 26.5 23% and Flow V) = (1:1)	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45 0	0.0 50.4		0.0
Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d) Design Outlet Water Depth h <sub>0</sub> (m)  Hydraulic Loading Rate, q (cm/d)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 1.1 75% 1477 1969 10500 0.99 HLR = HRT =	ties Based Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil G <sub>3</sub> , Distance	e (m/m) onstraints lity Thickening/ cm/d days	13.0 10.0 10.0 23% 16 34.3 12 26.5 23% and Flow V) = (1:1)	3.000 1.988 34% 4 7.9 2 5.3	34.400 0.193 99% 41 90.9 0 0.5 99% 1 45 45 0	0.0 50.4		0.0

#VALUE!

10.5

AOR = Actual Oxygen Transfer Requirement, kg/hr

Kaiser Mead Enhanced Treatment Wetland Pre-Design Water Quality Performance Estimates

p-k-C\* Model (Kadlec and Wallace 2009) Calibrated to Continuous Flow Pilot Study (Jacobs 2020)

Prepared by Jim Bays/Jacobs Engineering Group

February 11 2020

SOTR = Standardized Oxygen Transfer Reg, kg O2/hr

SOTR, lb O2/hr

SOTE = Standard Oxygen Transfer Efficiency, %

eair, lb/ft3

Air Flow, SCFM

Mass Air Flow, lb/s Blower Efficiency, %

Working Pressure, psig

PD Power Requirement, HP

Air Flow, SCFM

PD Power Requirement, HP

#VALUE!
#VALUE!
0.6%

0.07

**#VALUE! #VALUE!** 67.9%

6

#VALUE!

48.9 9.6% 0.07 527 0.676 67.9% 6

23.4

22.2

#VALUE! #VALUE!

#### Nitrogen Species Calculations

Nitrogen Models

per K&K Eqns 13-28. 13-29, 13-39:

Adapted for TIS model

Organic Nitrogen (ON)

$$C_{ON_{OUT}} = C_{ON}^* + (C_{ON_{IN}} - C_{ON}^*) \left[ 1 + \frac{k_{ON}A}{NQ} \right]^{-N}$$

DO NOT CHANGE						
(1+k <sub>ON</sub> /Nq)^-N	(1+k <sub>AN</sub> /Nq)^-N	(1+k <sub>NN</sub> /Nq)^-N				
0.742	0.001					
$k_{ON}/(k_{NH3}-k_{ON})$	kAN/(kNN-kAN)	kA/(kN-kO)				
0.2	0.078	0.074				

Ammonia Nitrogen (AN)

$$C_{AN_{OUT}} = C_{AN}^* + (C_{AN_{IN}} - C_{AN}^*) \left[ 1 + \frac{k_{AN}A}{NQ} \right]^{-N} + \left( \frac{k_{ON}}{k_{AN} - k_{ON}} \right) (C_{ON_{IN}} - C_{ON}^*) \left( 1 + \frac{k_{ON}A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{AN}A}{NQ} \right]^{-N}$$

Nitrate Nitrogen (NN)

$$C_{NN_{OUT}} = C_{NN_{N}} \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} + \Psi \left[ \left( \frac{k_{AN}}{k_{NN} - k_{AN}} \right) C_{AN_{N}} \left( \left[ 1 + \frac{k_{AN} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) + \left( \frac{k_{ON}}{k_{AN} - k_{ON}} \right) \left( \frac{k_{AN}}{k_{NN} - k_{ON}} \right) \left( C_{ON_{N}} - C_{ON}^{*} \right) \left( \left[ 1 + \frac{k_{ON} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) \left( \frac{k_{AN}}{k_{AN} - k_{ON}} \right) \left( C_{ON_{N}} - C_{ON}^{*} \right) \left( \left[ 1 + \frac{k_{AN} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) \right)$$

where  $\Psi$  = fraction of ammonium nitrified, assumed to be 100%

Kaiser Mead Enhanced Treatment Wetland
Pre-Design Water Quality Performance Estimates
p-k-C\* Model (Kadlec and Wallace 2009) Calibrated to Continuous Flow Pilot Study (Jacobs 2020)
Prepared by Jim Bays/Jacobs Engineering Group

Horizontal Subsurfac	e Flow Wetland S	imple PkC	Design N	lodel (Wast					
Project Name	User inputs indicated by white boxes.  KAISER MEAD DESIGN 100 GPM CELL 2 N SERIES Pop-up notes indicated by red triangles.								
Project Number	TO TO TO THE PART OF THE PART	D DEGIGIN 10	O OI W CLL	KMCT.2200	rop-up notes	illuicated by	reu triangles	·.	
•									
	Ger	eral Inflow							
Parameter		Value	Units						
Annual Average Daily Flow		100	gpm						
Converted Flow		545	m <sup>3</sup> /d						
Wastewater Temperature		5	°C						
	Water Q	uality Char	acteristics						
Parameter		BOD5	TSS	Organic N	NH4-N	NO2/3-N	TN	TP	FC
Influent Concentration, mg/L	$C_i =$			10.0	2.0	0.2	12		
Average Target Effluent Conc., mg/L	C <sub>e</sub> =						0		
Desired Confidence Percentile		0.5		0.5	0.5	0.5	0.5	0.5	0.5
Max Month/Annual Factor		1.7	1.9	1	1	1	1.6	1.8	2.6
Design Target Conc., mg/L	C <sub>d</sub> =								
Wetland Background Limit, mg/L	C* =	1	3.03	1.5	0	0	1.5	0.02	0
Reduction fraction to target	$F_e = 1 - C_e/C_i =$	No Value	No Value	1.000	1.000	1.000	1.000	No Value	No Value
Reduction fraction to background	$F_b = 1 - C^*/C_i =$			0.851	1.000	1.000	0.877		
Areal Rate Constant, 20°C, m/y	k <sub>20</sub> =	86	1000	4	193	4036	18	12	103
Temperature Factor	θ =	1.00	1.065	1.01	1.01	1.09	1.01	1.00	1.00
P-Factor	P =	3	3	2	2	2	6	3	3
Areal Rate Constant, m/y	k <sub>T</sub> =	86	1000	3.9	156.7	1108.1	16.7	12	103
Area required for each parameter, ac  Use Aeration Design	Required T	C*>Cd reatment V	C*>Cd Vetland A	C*>Cd	-0.6	0.0	C*>Cd	C*>Cd	C*>Cd
Required Treatment Wetland Area	A <sub>max</sub> =	0.000132	acres	Displays minir	num wotland	area to treat	all pollutant	e down to d	ocirod
'	max	0.000053	ha	targets	num wenanu	alea lo lieal	ali poliularii	s down to d	esileu
User Defined Area	A <sub>user</sub> =	0.372640		-					
Oser Defined Area	Auser -		acres	User specified for effluent cal			t if you wish	to use A <sub>max</sub>	(above)
Fir	nal Effluent Conc	0.150866	ha Porce			OW.			
	iai Lilluelli Colic	BOD5	TSS			NO2/2 N	TN		FC
Area (ha) used for Calculations =	= 0.2			Organic N	NH4-N	NO2/3-N		TP	
Area (ha) used for Calculations = Design Target Conc., mg/L	= <b>0.2</b> C <sub>d</sub> =			Organic N	NH4-N	NO2/3-N		TP	
` '				Organic N	1.988	0.193	12.2	TP	
Design Target Conc., mg/L	C <sub>d</sub> =							TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L	C <sub>d</sub> =			10.0	1.988	0.193	12.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L	C <sub>d</sub> =			10.0	1.988	0.193	12.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L	C <sub>d</sub> =			10.0	1.988 0.907	0.193 0.140	12.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L	C <sub>d</sub> =			10.0	1.988	0.193	12.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d)	C <sub>d</sub> =			10.0 9.8 2% 12 36.3	1.988 0.907 54% 2 7.2	0.193 0.140 28% 0 0.7	12.2 10.8 11% 15 44.1	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day)	C <sub>d</sub> =			10.0 9.8 2% 12 36.3 12	1.988 0.907 54% 2 7.2	0.193 0.140 28% 0 0.7 0	12.2 10.8 11% 15 44.1 13	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d)	$C_d = C_i =$			10.0 9.8 2% 12 36.3 12 35.4 2%	1.988 0.907 54% 2 7.2	0.193 0.140 28% 0 0.7	12.2 10.8 11% 15 44.1	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)	C <sub>d</sub> =	ties Basec		10.0 9.8 2% 12 36.3 12 35.4 2% and Flow	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28%	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Prope	rties Basec Approx Aspe		10.0 9.8 2% 12 36.3 12 35.4 2% and Flow	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28%	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper	rties Basec Approx Aspe Length (m)		10.0 9.8 2% 12 36.3 12 35.4 2% and Flow	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28%	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 0.6 40%	rties Basec Approx Aspe Length (m) Width (m)	ect Ratio (L:V	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3)	C <sub>d</sub> =   C <sub>i</sub> =	rties Basec Approx Aspe Length (m) Width (m) Bottom Slop	ect Ratio (L:V e (m/m)	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28%	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 0.6 40%	rties Basec Approx Aspe Length (m) Width (m)	ect Ratio (L:V e (m/m) onstraints	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3)	C <sub>d</sub> = C <sub>i</sub> = Hydraulic Proper 0.6 40% 589 1472	Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C	ect Ratio (L:V e (m/m) onstraints lity	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow V) = (1:1)	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d)	C <sub>d</sub> = C <sub>i</sub> =   Hydraulic Proper  0.6 40% 589 1472 10500	Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil	ect Ratio (L:V e (m/m) onstraints lity	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow V) = (1:1)	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39 0	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d)	C <sub>d</sub> = C <sub>i</sub> =   Hydraulic Proper  0.6 40% 589 1472 10500 0.54  HLR =	Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil	ect Ratio (L:V e (m/m) onstraints lity	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow V) = (1:1)	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39 0	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d) Design Outlet Water Depth h <sub>0</sub> (m)	C <sub>d</sub> = C <sub>i</sub> =   Hydraulic Proper  0.6 40% 589 1472 10500 0.54  HLR =	Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil G <sub>3</sub> , Distance	ect Ratio (L:V e (m/m) onstraints lity Thickening/	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow V) = (1:1)	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39 0	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d) Design Outlet Water Depth h <sub>0</sub> (m)  Hydraulic Loading Rate, q (cm/d)	C <sub>d</sub> = C <sub>i</sub> =   Hydraulic Proper  0.6 40% 589 1472 10500 0.54  HLR = HRT =	Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil G <sub>3</sub> , Distance	e (m/m) onstraints lity Thickening/ cm/d days	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow V) = (1:1)	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39 0	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0
Design Target Conc., mg/L Influent concentrations, mg/L Effluent concentrations, mg/L  Percent Reduction (by concentration) Mass Loading (lb/day) Mass Loading (kg/ha/d) Mass Out (lb/day) Mass Out (lb/day) Mass Out (kg/ha/d) Percent Reduction (by mass)  Gravel Diameter (cm) Bed Depth (m) Porosity e (%) Volume Water (m3) Volume Media (m3) Bed Conductivity k (m/d) Design Outlet Water Depth h <sub>0</sub> (m)  Hydraulic Loading Rate, q (cm/d)	C <sub>d</sub> = C <sub>i</sub> =   Hydraulic Proper  0.6 40% 589 1472 10500 0.54  HLR = HRT =	Approx Aspe Length (m) Width (m) Bottom Slop Hydraulic C G <sub>1</sub> , Drainabil G <sub>3</sub> , Distance	e (m/m) onstraints lity Thickening/ cm/d days	10.0 9.8 2% 12 36.3 12 35.4 2% and Flow V) = (1:1)	1.988 0.907 54% 2 7.2 1 3.3	0.193 0.140 28% 0 0.7 0 0.5 28% 1 39 39 0	12.2 10.8 111% 15 44.1 13 39.2	TP	0.0

AOR = Actual Oxygen Transfer Requirement, kg/hr #VALUE! 10.5

Kaiser Mead Enhanced Treatment Wetland Pre-Design Water Quality Performance Estimates

p-k-C\* Model (Kadlec and Wallace 2009) Calibrated to Continuous Flow Pilot Study (Jacobs 2020)

Prepared by Jim Bays/Jacobs Engineering Group

February 11 2020

SOTR = Standardized Oxygen Transfer Reg, kg O2/hr

SOTR, lb O2/hr

SOTE = Standard Oxygen Transfer Efficiency, %

eair, lb/ft3

Air Flow, SCFM

Mass Air Flow, lb/s

Blower Efficiency, %

Working Pressure, psig

PD Power Requirement, HP

Air Flow, SCFM

PD Power Requirement, HP

#VALUE!
#VALUE!
0.69/

9.6% 0.07

**#VALUE! #VALUE!** 67.9%

6

#VALUE!

48.9 9.6% 0.07 527 0.676 67.9% 6

23.4

22.2

#VALUE! #VALUE!

#### Nitrogen Species Calculations

Nitrogen Models

per K&K Eqns 13-28. 13-29, 13-39:

Adapted for TIS model

Organic Nitrogen (ON)

$$C_{ON_{OUT}} = C_{ON}^* + (C_{ON_{IN}} - C_{ON}^*) \left[ 1 + \frac{k_{ON}A}{NQ} \right]^{-N}$$

DO NOT CHANGE						
(1+k <sub>ON</sub> /Nq)^-N	(1+k <sub>AN</sub> /Nq)^-N	(1+k <sub>NN</sub> /Nq)^-N				
0.971	0.394	0.037				
$k_{ON}/(k_{NH3}-k_{ON})$	kAN/(kNN-kAN)	kA/(kN-kO)				
0.0	0.165	0.142				

Ammonia Nitrogen (AN)

$$C_{AN_{OUT}} = C_{AN}^* + (C_{AN_{IN}} - C_{AN}^*) \left[ 1 + \frac{k_{AN}A}{NQ} \right]^{-N} + \left( \frac{k_{ON}}{k_{AN} - k_{ON}} \right) (C_{ON_{IN}} - C_{ON}^*) \left( 1 + \frac{k_{ON}A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{AN}A}{NQ} \right]^{-N}$$

Nitrate Nitrogen (NN)

$$C_{NN_{OUT}} = C_{NN_{N}} \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} + \Psi \left[ \left( \frac{k_{AN}}{k_{NN} - k_{AN}} \right) C_{AN_{N}} \left( \left[ 1 + \frac{k_{AN} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) + \left( \frac{k_{ON}}{k_{AN} - k_{ON}} \right) \left( \frac{k_{AN}}{k_{NN} - k_{ON}} \right) \left( C_{ON_{N}} - C_{ON}^{*} \right) \left( \left[ 1 + \frac{k_{ON} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) \left( \frac{k_{AN}}{k_{AN} - k_{ON}} \right) \left( C_{ON_{N}} - C_{ON}^{*} \right) \left( \left[ 1 + \frac{k_{AN} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) \right)$$

where  $\Psi$  = fraction of ammonium nitrified, assumed to be 100%

Kaiser Mead Enhanced Treatment Wetland
Pre-Design Water Quality Performance Estimates
p-k-C\* Model (Kadlec and Wallace 2009) Calibrated to Continuous Flow Pilot Study (Jacobs 2020)
Prepared by Jim Bays/Jacobs Engineering Group

February 11 2020	,								
Horizontal Subsurface	Flow Wetland Si	imple PkC*	* Design N	lodel (Wast	ewater Pai	rameters)			
User inputs indicated by white boxes.  Project Name KAISER MEAD DESIGN 100 GPM CELL 3 N SERIES Pop-up notes indicated by red triangles.									
Project Name Project Number	KAISEK WEA	D DESIGN TO	JO GEWI CEL	KMCT.2200	Pop-up notes	indicated by	red triangles	5.	
General Inflow Data									
Parameter Annual Average Daily Flow		Value 100	Units gpm	-					
			2.0						
Converted Flow		545	m³/d						
Wastewater Temperature		5	°C						
	Water Qu	uality Char	acteristics	S					
Parameter		BOD5	TSS	Organic N	NH4-N	NO2/3-N	TN	TP	FC
Influent Concentration, mg/L	C <sub>i</sub> =			9.8	0.9	0.1	11		
Average Target Effluent Conc., mg/L	C <sub>e</sub> =						0.0		
Desired Confidence Percentile		0.5		0.5	0.5	0.5	0.5	0.5	0.5
Max Month/Annual Factor		1.7	1.9	1	1	1	1.6	1.8	2.6
Design Target Conc., mg/L	C <sub>d</sub> =								
Wetland Background Limit, mg/L	C* =	1	3.03	1.5	0	0	1.5	0.02	0
Reduction fraction to target	$F_{e} = 1 - C_{e}/C_{i} =$	No Value	No Value	1.000	1.000	1.000	1.000	No Value	No Value
Reduction fraction to background	$F_b = 1 - C^*/C_i =$			0.847	1.000	1.000	0.862		
Areal Rate Constant, 20°C, m/y	k <sub>20</sub> =	86	1000	20	11	42	18	12	103
Temperature Factor	θ = P =	1.00	1.065	1.01	1.01	1.09	1.01	1.00	1.00
P-Factor	k <sub>T</sub> =	3	3	6	6	6	6	3 12	3
Areal Rate Constant, m/y  Area required for each parameter, ac	KŢ -	86 C*>Cd	1000 C*>Cd	17.5 C*>Cd	8.9 C*>Cd	11.5 C*>Cd	16.7 C*>Cd	C*>Cd	103 C*>Cd
Use Aeration Design	Required T				0 >0u	0 >0u	C >Cu	O >Ou	O >Ou
Required Treatment Wetland Area	A <sub>max</sub> =	0.000000	acres	Displays minir	mum wetland	area to treat	all		
		0.000000	ha	pollutants dow			<b></b>		
User Defined Area	A <sub>user</sub> =	0.505714	acres	User specified	l wetland are:	a. leave blank	r if you wish		
000. 2004 / 1104	- user			to use A <sub>max</sub> (al			•		
Fin	al Effluent Conce	0.204742	ha and Perce	nt Removal					
Area (ha) used for Calculations =		BOD5	TSS	Organic N	NH4-N	NO2/3-N	TN	TP	FC
Design Target Conc., mg/L	C <sub>d</sub> =								
Influent concentrations, mg/L	C <sub>i</sub> =			9.8	0.907	0.140	10.8		
Effluent concentrations, mg/L				8.4	2.104	0.266	10.8		0.0
System Concentration Reduction , %				35%	30%	99%	79%		
Develop t Deduction (by consentration)			1	14%	-132%	-90%	00/	1	
Percent Reduction (by concentration) Mass Loading (lb/day)				12	1	0	0% 13		
Mass Loading (kg/ha/d)				26.1	2.4	0.4	28.9		
Mass Out (lb/day) Mass Out (kg/ha/d)				10 22.5	3 5.6	0.7	13 28.8		
Percent Reduction (by mass)				14%	-132%	-90%	0%		
	Hydraulic Proper	ties Based	on Area	and Flow					
Gravel Diameter (cm)		Approx Aspe	ect Ratio (L:V	V) = (2:1)		2			
Bed Depth (m)	0.6	Length (m)				64			
Porosity e (%)	40%	Width (m)				32			
Volume Water (m3)	779	Bottom Slope				0			
Volume Media (m3) Bed Conductivity k (m/d)	1948 10500	Hydraulic C G <sub>1</sub> , Drainabil				0.00	]		
Design Outlet Water Depth h <sub>0</sub> (m)	0.54	G <sub>3</sub> , Distance	•	Thinning		3.56			
5 · · · · · · · · · · · · · · · · · · ·	5.51	. 0,		3		3.03			
Hydraulic Loading Rate, q (cm/d)	HLR =	26.6	cm/d						
Nominal Hydraulic Residence Time (d)	HRT =	1.4	days						
	Aerat	ion Requir	ements						
		Zone 1		Zone 2					

#VALUE!

AOR = Actual Oxygen Transfer Requirement, kg/hr

10.5

Kaiser Mead Enhanced Treatment Wetland Pre-Design Water Quality Performance Estimates

p-k-C\* Model (Kadlec and Wallace 2009) Calibrated to Continuous Flow Pilot Study (Jacobs 2020)

Prepared by Jim Bays/Jacobs Engineering Group

February 11 2020

SOTR = Standardized Oxygen Transfer Req, kg O2/hr

SOTR, lb O2/hr

SOTE = Standard Oxygen Transfer Efficiency, %

eair, lb/ft3

Air Flow, SCFM Mass Air Flow, lb/s

Blower Efficiency, %

Working Pressure, psig

vvolking i ressure, psig

PD Power Requirement, HP

Air Flow, SCFM

PD Power Requirement, HP

#VALUE!
#VALUE!
9.6%

9.6% 0.07 #VALUE!

#VALUE! #VALUE! 67.9% 22.2 48.9 9.6% 0.07 527 0.676 67.9%

6

23.4

#VALUE!

#VALUE!

#### Nitrogen Species Calculations

Nitrogen Models

per K&K Eqns 13-28. 13-29, 13-39:

Adapted for TIS model

Organic Nitrogen (ON)

$$C_{ON_{OUT}} = C_{ON}^* + (C_{ON_{IN}} - C_{ON}^*) \left[ 1 + \frac{k_{ON}A}{NQ} \right]^{-N}$$

DO NOT CHANGE					
(1+k <sub>ON</sub> /Nq)^-N	(1+k <sub>NN</sub> /Nq)^-N				
0.838	0.889				
$k_{ON}/(k_{NH3}-k_{ON})$	kAN/(kNN-kAN)	kA/(kN-kO)			
-2.0	3.433	-1.500			

Ammonia Nitrogen (AN)

$$C_{AN_{OUT}} = C_{AN}^* + (C_{AN_{IN}} - C_{AN}^*) \left[ 1 + \frac{k_{AN}A}{NQ} \right]^{-N} + \left( \frac{k_{ON}}{k_{AN} - k_{ON}} \right) (C_{ON_{IN}} - C_{ON}^*) \left( 1 + \frac{k_{ON}A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{AN}A}{NQ} \right]^{-N}$$

Nitrate Nitrogen (NN)

$$C_{NN_{OUT}} = C_{NN_{N}} \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} + \Psi \left[ \left( \frac{k_{AN}}{k_{NN} - k_{AN}} \right) C_{AN_{N}} \left( \left[ 1 + \frac{k_{AN} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) + \left( \frac{k_{ON}}{k_{AN} - k_{ON}} \right) \left( \frac{k_{AN}}{k_{NN} - k_{ON}} \right) \left( C_{ON_{N}} - C_{ON}^{*} \right) \left( \left[ 1 + \frac{k_{ON} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) \left( \frac{k_{AN}}{k_{AN} - k_{ON}} \right) \left( C_{ON_{N}} - C_{ON}^{*} \right) \left( \left[ 1 + \frac{k_{AN} A}{NQ} \right]^{-N} - \left[ 1 + \frac{k_{NN} A}{NQ} \right]^{-N} \right) \right)$$

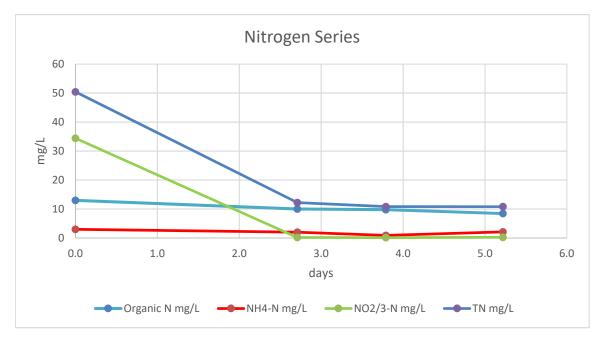
where  $\Psi$  = fraction of ammonium nitrified, assumed to be 100%

Kaiser Mead Enhanced Treatment Wetland
Pre-Design Water Quality Performance Estimates
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Prepared by Jim Bays/Jacobs Engineering Group
February 11 2020

Cell	Organic N	NH4-N	NO2/3-N	TN	TN	HRT	Cumulative HRT
	mg/L	mg/L	mg/L	mg/L	CR	d	d
Inflow	13.0	3.000	34.400	50.400	0%	0.0	0.0
Cell 1	10.0	1.988	0.193	12.216	76%	2.7	2.7
Cell 2	9.8	0.907	0.140	10.837	78%	1.1	3.8
Cell 3	8.4	2.104	0.266	10.813	79%	1.4	5.2

#### Note

100 gpm = 50 gpm inflow + 50 gpm recirc



# **Structural Calculations**

# **CALCULATIONS**

STRUCTURAL



Digitally Signed on

April 3, 2020

Liao Yang

1100 NE Circle Blvd Corvallis 5.5E+08

JOB TITLE	Kaiser	Meads	PEMB
-----------	--------	-------	------

JOB NO.	SHEET NO.	
CALCULATED BY L.Yang	DATE	12/6/19
CHECKED BY	DATE	

CS2018 Ver 2018.03.17

www.struware.com

# STRUCTURAL CALCULATIONS

FOR

**Kaiser Meads PEMB** 

1100 NE Circle Blvd Corvallis 5.48E+08

#### JOB TITLE Kaiser Meads PEMB

JOB NO.	SHEET NO.	
CALCULATED BY L.Yang	DATE	12/6/19
CHECKED BY	DATE	

www.struware.com

# **Code Search**

Code:

International Building Code 2015

Occupancy:

Occupancy Group =

U

**Utility & Miscellaneous** 

# **Risk Category & Importance Factors:**

Risk Category =

11

Wind factor = 1.00 Snow factor = 1.00 Seismic factor = 1.00

# **Type of Construction:**

Fire Rating:

Roof = 0.0 hr Floor = 0.0 hr

### **Building Geometry:**

Roof angle (θ)	3.00 / 12	14.0 deg
Building length (L)	90.0 ft	
Least width (B)	44.0 ft	
Mean Roof Ht (h)	23.0 ft	
Parapet ht above grd	0.0 ft	
Minimum parapet ht	0.0 ft	

## Live Loads:

Roof

0 to 200 sf: 20 psf

200 to 600 sf: 24 - 0.02Area, but not less than 12 psf

over 600 sf: 12 psf

#### Floor:

Typical Floor	250 psf
Partitions	15 psf
Lobbies & first floor corridors	100 psf
Corridors above first floor	80 psf
Balconies (exterior) - same as occupa	100 psf

1100 NE Circle Blvd Corvallis 547683444

#### JOB TITLE Kaiser Meads PEMB

JOB NO.	SHEET NO.	
CALCULATED BY L. Yang	DATE	12/6/19
CHECKED BY	DATE	

#### Enclosure Classification

Test for Enclosed Building:

A building that does not qualify as open or partially enclosed.

**Test for Open Building:** 

All walls are at least 80% open.

Ao ≥ 0.8Ag

Test for Partially Enclosed Building: Predominately open on one side only

	Input			Test	
Ao	500.0	sf	Ao ≥ 1.1Aoi	NO	]
Ag	600.0	sf	Ao > 4' or 0.01Ag	YES	ļ
Aoi	1000.0	sf	Aoi / Agi ≤ 0.20	YES	Building is NOT
Agi	10000.0	sf	_		Partially Enclosed

Conditions to qualify as Partially Enclosed Building. Must satisfy all of the following:

Ao ≥ 1.1Aoi

Ao > smaller of 4' or 0.01 Ag

Aoi / Agi ≤ 0.20

Where:

Ao = the total area of openings in a wall that receives positive external pressure.

Ag = the gross area of that wall in which Ao is identified.

Aoi = the sum of the areas of openings in the building envelope (walls and roof) not including Ao.

Agi = the sum of the gross surface areas of the building envelope (walls and roof) not including Ag.

## Reduction Factor for large volume partially enclosed buildings (Ri):

If the partially enclosed building contains a single room that is unpartitioned, the internal pressure coefficient may be multiplied by the reduction factor Ri.

Total area of all wall & roof openings (Aog):

0 sf

Unpartitioned internal volume (Vi):

0 cf

Ri =

1.00

### Altitude adjustment to constant 0.00256 (caution - see code) :

Grd level above sea level =

0.0 ft

Average Air Density =

0.0765 lbm/ft3

Constant =

0.00256

Adj Constant = 0.00256

1100 NE Circle Blvd Corvallis 547683444

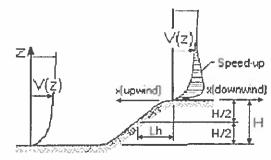
#### JOB TITLE Kaiser Meads PEMB

JOB NO.	SHEET NO.	
CALCULATED BY L. Yang	DATE	12/6/19
CHECKED BY	DATE	

# Wind Loads:

d Loads :	ASCE 7- 10	ASK	Blds do
Ultimate Wind Speed	110 mph		115
Nominal Wind Speed	85.2 mph		
Risk Category	<u></u> ●		
Exposure Category	C		
Enclosure Classif.	Enclosed Building		
Internal pressure	+/-0.18		
Directionality (Kd)	0.85		
Kh case 1	0.929		
Kh case 2	0.929		
Type of roof	Gable		

H<	15ft;exp C
	Kate 1 A



# Topographic Factor (Kzt)

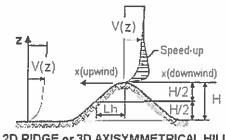
Topography	Flat
Hill Height (H)	0.0 ft
Half Hill Length (Lh)	0.0 ft
Actual H/Lh =	0.00
Use H/Lh =	0.00
Modified Lh =	0.0 ft
From top of crest: x =	200.0 ft
Bldg up/down wind?	downwind

H/Lh= 0.00	$K_1 = 0.000$
x/Lh = 0.00	$K_2 = 0.000$
z/Lh = 0.00	$K_3 = 1.000$

At Mean Roof Ht:

 $Kzt = (1+K_1K_2K_3)^2 = 1.00$ 

# **ESCARPMENT**



2D RIDGE or 3D AXISYMMETRICAL HILL

# **Gust Effect Factor**

h =	23.0 ft
B =	44.0 ft
/z (0.6h) =	15.0 ft

Flexible structure if natural frequency < 1 Hz (T > 1 second). If building h/B>4 then may be flexible and should be investigated. h/B = 0.52Rigid structure (low rise bldg)

#### G =0.85 Using rigid structure default

_	0.20	
_ t =	500 ft	
z <sub>min</sub> =	15 ft	
c =	0.20	
$g_Q, g_v =$	3.4	
$L_z =$	427.1 ft	
Q =	0.91	

Rigid Structure

$I_z =$	0.23			
G =	0.88	use	G =	= 0.85

Flexible or Dynamically Sensitive Structure					
34 1cy $(\eta_1) =$	0.0 Hz				
Damping ratio (β) = /b =	0 0.65				
/a = Vz =	0.15 92.9				
N <sub>1</sub> =	0.00				
$\kappa_n =$	0.000				
$R_h =$	28.282	η =	0.000	h =	23.0 ft
R <sub>B</sub> =	28.282	η =	0.000		
R <sub>L</sub> =	28.282	η =	0.000		

 $g_R =$ 0.000 R =0.000 Gf = 0.000

# **Jacobs Engineering** 1100 NE Circle Blvd

Corvallis 5.5E+08

#### JOB TITLE Kaiser Meads PEMB

JOB NO.		SHEET NO.	
CALCULATED BY	L.Yang	DATE	12/6/19
CHECKED BY		DATE	

## Wind Loads - h≤60' Longitudinal Direction MWFRS On Open or Partially

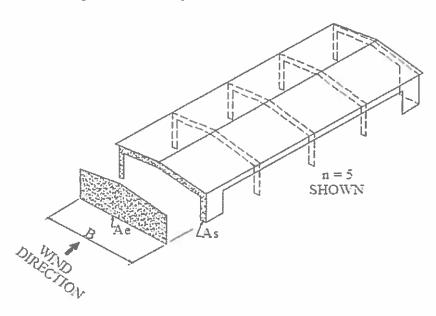
# **Enclosed Buildings with Transverse Frames and Pitched Roofs**

Base pressure (qh) = 24.5 psf GCpi =

+/-0.18 Enclosed bldg, procdure doesn't apply

Roof Angle  $(\theta)$  = 14.0 deg





B= 44.0 ft

# of frames (n) =5

Solid are of end wall including fascia (As) = 1,500.0 sf

> Roof ridge height = 25.8 ft

Roof eave height =

20.3 ft Total end wall area if soild (Ae) = 1,012.0 sf

Longidinal Directional Force (F) = pAe p= qh [(GCpf)windward -(GCpf)leeward] K<sub>B</sub> K<sub>S</sub>

Solidarity ratio  $(\Phi) =$ 1.482 5 n =

KB = 8.0

KS = 3.284

Zones 5 & 6 area = 916.9 sf

> 5E & 6E area = 95.2 sf

(GCpf) windward - (GCpf) leeward] = 0.723

46.5 psf

Total force to be resisted by MWFRS (F) =

47.0 kips applied at the centroid

of the end wall area Ae

Note: The longidudinal force acts in combination with roof loads calculated elsewhere for an open or partially enclosed building.

1100 NE Circle Blvd Corvallis 5.5E+08

#### JOB TITLE Kaiser Meads PEMB

JOB NO.	SHEET NO.
CALCULATED BY L.Yang	DATE 12/6/19
CHECKED BY	DATE

# Wind Loads - MWFRS h≤60' (Low-rise Buildings) except for open buildings

Kz = Kh (case 1) = 0.93 Base pressure (qh) = 24.5 psf +/-0.18 GCpi =

Edge Strip (a) = 4.4 ft End Zone (2a) = 8.8 ft Zone 2 length = 22.0 ft

#### Wind Pressure Coefficients

	C	ASE A			CASE B	
l f		6 = 14 deg				
Surface	GCpf	w/-GCpi	w/+GCpi	GCpf	w/-GCpi	w/+GCpi
1	0.48	0.66	0.30	-0.45	-0.27	-0.63
2	-0.69	-0.51	-0.87	-0.69	-0.51	-0.87
3	-0.44	-0.26	-0.62	-0.37	-0.19	-0.55
4	-0.37	-0.19	-0.55	-0.45	-0.27	-0.63
5				0.40	0.58	0.22
6				-0.29	-0.11	-0.47
1E	0.72	0.90	0.54	-0.48	-0.30	-0.66
2E	-1.07	-0.89	-1.25	-1.07	-0.89	-1.25
3E	-0.63	-0.45	-0.81	-0.53	-0.35	-0.71
4E	-0.56	-0.38	-0.74	-0.48	-0.30	-0.66
5E				0.61	0.79	0.43
6E				0.43	-0.25	-0.61

#### **Ultimate Wind Surface Pressures (psf)**

	10.1	7.0		
l 1	16.1	7.3	-6.6	-15.4
2	-12.5	-21.3	-12.5	-21.3
3	-6.3	-15.1	-4.6	-13.5
4	-4.8	-13.6	-6.6	-15.4
5			14.2	5.4
6			-2.7	-11.5
1E	22.1	13.3	-7.3	-16.1
2E	-21.8	-30.6	-21.8	-30.6
3E	-10.9	-19.7	-8.6	-17.4
4E	-9.2	-18.0	-7.3	-16.1
5E			19.3	10.5
6E			-6.1	-14.9

-SEE FIGURES Page 300 CF ASCE 7-10

#### **Parapet**

Windward parapet = Leeward parapet = 0.0 psf (GCpn = +1.5) 0.0 psf (GCpn = -1.0)

Windward roof overhangs =

17.1 psf (upward) add to windward roof pressure

#### Horizontal MWFRS Simple Diaphragm Pressures (psf)

#### Transverse direction (normal to L)

Interior Zone: Wall

20.9 psf

Roof

-6.2 psf \*\*

End Zone: Wall

31.3 psf

Roof

-10.8 psf \*\*

### Longitudinal direction (parallel to L)

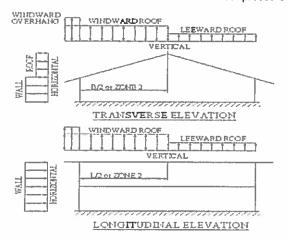
Interior Zone: Wall

End Zone: Wall

25.4 psf

\*\* NOTE: Total horiz force shall not be less than that determined by neglecting roof forces (except for MWFRS moment frames).

The code requires the MWFRS be designed for a min ultimate force of 16 psf multiplied by the wall area plus an 8 psf force applied to the vertical projection of the roof.

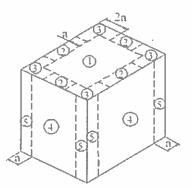


JOB NO. SHEET NO.

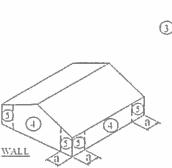
CALCULATED BY L. Yang DATE 12/6/19

CHECKED BY DATE

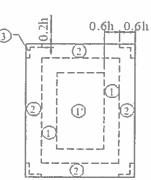
#### Location of C&C Wind Pressure Zones - ASCE 7-16



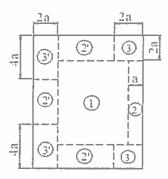
Roofs w/  $\theta \le 10^{\circ}$ and all walls h > 60°



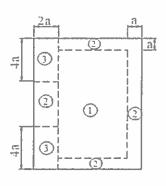
Walls h ≤ 60' & alt design h<90'



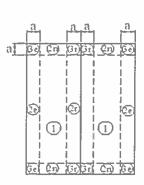
Gable, Sawtooth and Multispan Gable θ ≤ 7 degrees & Monoslope ≤ 3 degrees h ≤ 60° & alt design h<90°



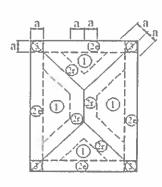
Monoslope roofs  $3^{\circ} < \theta \le 10^{\circ}$  $h \le 60^{\circ}$  & alt design h<90'



Monoslope roofs  $10^{\circ} < \theta \le 30^{\circ}$  $h \le 60^{\circ}$  & alt design h<90'

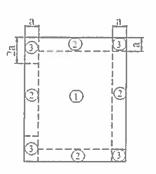


Multispan Gable & Gable 7° < 9 ≤ 45°

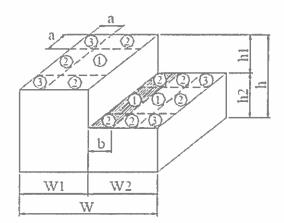


Hip 7° < 0 ≤ 27°

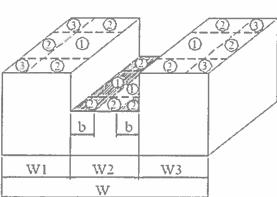




Sawtooth 10° <  $\theta \le 45$ ° h  $\le 60$ ' & alt design h<90'



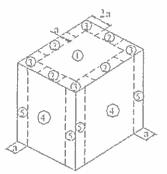
Stepped roofs  $\theta \le 3^{\circ}$ h  $\le 60^{\circ}$  & alt design h<90°



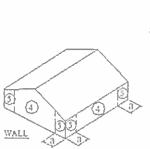
IOB	TITLE	Kaicor	Meads	DEME

JOB NO.	SHEET NO.	
CALCULATED BY L. Yang	DATE	12/6/19
CHECKED BY	DATE	

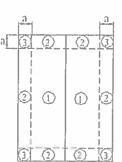
#### Location of C&C Wind Pressure Zones - ASCE 7-10 & earlier



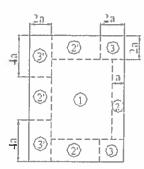
Roofs w/ θ ≤ 10° and all walls h > 60'



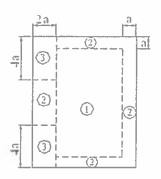
Walls h ≤ 60' & alt design h<90'



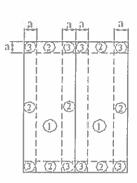
Gable, Sawtooth and Multispan Gable 0 ≤ 7 degrees & Monoslope ≤ 3 degrees h ≤ 60' & alt design h<90'



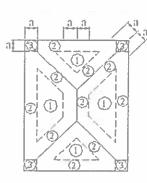
Monoslope roofs 3° < θ ≤ 10° h ≤ 60' & alt design h<90'



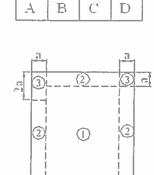
Monoslope roofs 10° < θ ≤ 30° h ≤ 60° & alt design h<90°



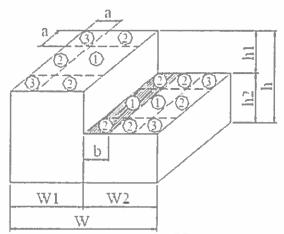
Multispan Gable & Gable 7° < 8 ≤ 45°



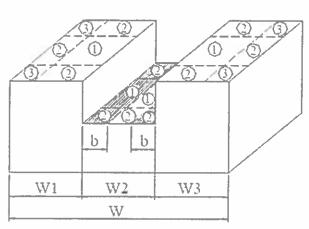
Hip 7° < θ ≤ 27°



Sawtooth  $10^{\circ} < \theta \le 45^{\circ}$ h  $\le 60^{\circ}$  & alt design h<90'



Stepped roofs 0 ≤ 3° h ≤ 60' & alt design h<90'



# **Jacobs Engineering** 1100 NE Circle Blvd

Corvallis 5.5E+08

JOB TITLE	Kaiser	Meads	PEMB

JOB NO.		SHEET NO.		
CALCULATED BY	L.Yang	DATE	12/6/19	
CHECKED BY		DATE		

**Ultimate Wind Pressures** 

Base pressure (qh) = 24.5 psf a = GCpi = Minimum parapet ht = 0.0 ft

Roof Angle (θ) = 14.0 deg Type of roof = Gable

Roof	(	3Cp +/- GC	oi		Surface Pr	essure (psf)	)	
Area	10 sf	20 sf	50 sf	100 sf	10 sf	20 sf	50 sf	100 sf
Negative Zone 1	-1.08	-1.05	-1.01	-0.98	-26.4	-25.7	-24.7	-24.0
Negative Zone 2	-1.88	-1.73	-1.53	-1.38	-46.0	-42.3	-37.4	-33.7
Negative Zone 3	-2.78	-2.6	-2.36	-2.18	-68.0	-63.6	-57.7	-53.3
Positive All Zones	0.68	0.62	0.54	0.48	16.6	16.0	16.0	16.0
Overhang Zone 2	-2.2	-2.2	-2.2	-2.2	-53.8	-53.8	-53.8	-53.8
Overhang Zone 3	-3.7	-3.34	-2.86	-2.5	-90.5	-81.7	-69.9	-61.1

23.0 ft

4.4 ft

+/-0.18

Overhang pressures in the table above assume an internal pressure coefficient (Gcpi) of 0.0 Overhang soffit pressure equals adj wall pressure (which includes internal pressure of 4.4 psf)

USei	input
75 sf	300 sf
-24.3	-24.0
-35.3	-33.7
-55.1	-53.3
16.0	16.0
I .	
-53.8	-53.8
-64.8	-61.1
1	
i	

**Parapet** 

qp = 0.0 psf

sf	Г	Surface Pressure (psf)					
Solid Parap	et Pressure	10 sf	20 sf	50 sf	100 sf	200 sf	500 sf
CASE A:	Zone 2 :	0.0	0.0	0.0	0.0	0.0	0.0
	Zone 3 :	0.0	0.0	0.0	0.0	0.0	0.0
CASE B: Edg	e zones 2 :	0.0	0.0	0.0	0.0	0.0	0.0
	er zones 3 :	0.0	0.0	0.0	0.0	0.0	0.0

E	User input
Г	40 sf
Γ	0,0
ı	0.0
ľ	
L	
Γ	0.0
ı	0.0

<u>Walls</u>	(	GCp +/- GCpi			Surface Pressure (psf)			
Area	10 sf	100 sf	200 sf	500 sf	10 sf	100 sf	200 sf	500 sf
Negative Zone 4	-1.28	-1.10	-1.05	-0.98	-31.3	-27.0	-25.7	-24.0
Negative Zone 5	-1.58	-1.23	-1.12	-0.98	-38.6	-30.0	-27.4	-24.0
Positive Zone 4 & 5	1.18	1.00	0.95	0.88	28.9	24.5	23.2	21.5

User input			
50 sf	200 sf		
-28.3	-25.7		
-32.6	-27.4		
25.8	23.2		

1100 NE Circle Blvd Corvallis 5,48E+08

JOB NO.	SHEET NO.	
CALCULATED BY L.Yang	DATE	12/6/19
CHECKED BY	DATE	

**Nominal Snow Forces** 

JOB TITLE Kaiser Meads PEMB

## Snow Loads: ASCE 7-10

Roof slope = 14.0 deg Horiz, eave to ridge dist (W) = 22.0 ft Roof length parallel to ridge (L) = 90.0 ft

Hip and gable w/ rafters Type of Roof **Ground Snow Load** Pg =39.0 psf Risk Category = Ш Importance Factor | = 1.0 Thermal Factor Ct = 1.00 Exposure Factor Ce = 1.2 Pf = 0.7\*Ce\*Ct\*I\*Pg 32.8 psf Unobstructed Slippery Surface no

Sloped-roof Factor Cs = 1.00
Balanced Snow Load = 32.8 psf

 Rain on Snow Surcharge Angle
 0.44 deg

 Code Maximum Rain Surcharge
 5.0 psf

 Rain on Snow Surcharge
 = 0.0 psf

 Ps plus rain surcharge
 = 32.8 psf

 Minimum Snow Load
 Pm
 = 20.0 psf

Uniform Roof Design Snow Load = 32.8 psf

SPOKAN CODE 36 PSF

Near ground level surface balanced snow load = 39.0 psf

NOTE: Alternate spans of continuous beams shall be loaded with half the design roof snow load so as to produce the greatest possible effect - see code for loading diagrams and exceptions for gable roofs...

#### Unbalanced Snow Loads - for Hip & Gable roofs only

Required if slope is between 7 on 12 = 30.26 deg

and 2.38 deg = 2.38 deg Unbalanced snow loads must be applied

Windward snow load = 9.8 psf = 0.3PsLeeward snow load from ridge to 9' =  $48.9 \text{ psf} = \text{hdy} / \sqrt{\text{S}} + \text{Ps}$ 

99.2 psf

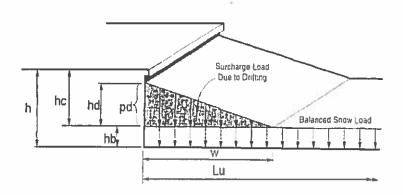
Leeward snow load from 9' to the eave = 32.8 psf = Ps

### Windward Snow Drifts 1 - Against walls, parapets, etc

lu = Upwind fetch 220.0 ft Projection height h = 5.2 ft Snow density g = 19.1 pcf hb = 1.72 ft Balanced snow height hd = 4.03 ft hc = 3.48 ft hc/hb > 0.2 = 2.0Therefore, design for drift Drift height (hc) 3.48 ft Drift width w = 18.62 ft Surcharge load: pd = y\*hd =66.4 psf Balanced Snow load: 32.8 psf

#### Windward Snow Drifts 2 - Against walls, parapets, etc.

lu = Upwind fetch 160.0 ft Projection height h = 4.0 ft g = Snow density 19.1 pcf Balanced snow height hb = 1.72 ft hd = 3.51 ft 2.28 ft hc = hc/hb > 0.2 = 1.3Therefore, design for drift Drift height (hc) 2.28 ft Drift width 18.26 ft Surcharge load:  $pd = y^*hd =$ 43.5 psf Balanced Snow load: 32.8 psf 76.3 psf



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#### JOB TITLE Kaiser Meads PEMB

JOB NO.	SHEET NO.	
CALCULATED BY L.Yang	DATE 12/6/	19
CHECKED BY	DATE	

Seismic Loads: **IBC 2015** 

Strength Level Forces

11 Risk Category: Importance Factor (I): 1.00

> Site Class: D

Ss (0.2 sec) = 33.70 %g S1 (1.0 sec) =11.60 %g

Fa = 1.530 Sms =

S<sub>DS</sub> = 0.516 0.344 Design Category = C Fv = 2.336 Sm1 =0.271  $S_{D1} =$ 0.181 Design Category = C

Seismic Design Category = C

Redundancy Coefficient p = 1.30

Number of Stories:

Structure Type: Moment-resisting frame systems of steel

Horizontal Struct Irregularities: No plan Irregularity Vertical Structural Irregularities: No vertical Irregularity

Flexible Diaphragms: No

Building System: Moment-resisting Frame Systems Seismic resisting system: Steel ordinary moment frames

System Structural Height Limit: Height not limited

Actual Structural Height (hn) = 25.8 ft

#### DESIGN COEFFICIENTS AND FACTORS

Response Modification Coefficient (R) = 3.5

Over-Strength Factor ( $\Omega$ o) =

Deflection Amplification Factor (Cd) = 3

> $S_{DS} =$ 0.344

3

S<sub>D1</sub> = 0.181

Seismic Load Effect (E) =  $Eh + -Ev = \rho Q_E + -0.2S_{DS} D$ = 1.3Qe +/- 0.069D Q<sub>E</sub> = horizontal seismic force

Special Seismic Load Effect (Em) = Emh +/- Ev =  $\Omega$ o Q<sub>E</sub> +/- 0.2S<sub>DS</sub> D = 3Qe +/- 0.069D D = dead load

#### PERMITTED ANALYTICAL PROCEDURES

**Simplified Analysis** - Use Equivalent Lateral Force Analysis

Equivalent Lateral-Force Analysis - Permitted

Building period coef.  $(C_T) =$ 0.028 Cu = 1.54 $C_T h_n^* =$ 

Approx fundamental period (Ta) = 0.377 sec Tmax = CuTa = 0.580 x = 0.80

User calculated fundamental period (T) = Use T = 0.377sec

Long Period Transition Period (TL) = ASCE7 map = 8

Seismic response coef. (Cs) = SpsI/R = 0.098 need not exceed Cs =

Sd1 I /RT = 0.137 but not less than Cs = 0.044SdsI = 0.015

USE Cs = 0.098

Design Base Shear V = 0.098W

Model & Seismic Response Analysis - Permitted (see code for procedure)

#### ALLOWABLE STORY DRIFT

Structure Type:

All other structures

Allowable story drift  $\Delta a = 0.020 hsx$ 

where hsx is the story height below level x

1100 NE Circle Blvd Corvallis 5.5E+08

#### JOB TITLE Kaiser Meads PEMB

JOB NO. SHEET NO. CALCULATED BY L.Yang 12/6/19 DATE **CHECKED BY** DATE

Seismic Loads - cont. :

Strength Level Forces

Seismic Design Category (SDC)= C

CONNECTIONS

Sds = 0.344

Force to connect smaller portions of structure to remainder of structure

 $Fp = 0.133 Sdsw_0 =$ 

0.046 Wp

or  $Fp = 0.05w_0 =$ 

0.05 Wp

 $0.05 W_{p}$ Use Fp =

w<sub>n</sub> = weight of smaller portion

Beam, girder or truss connection for resisting horizontal force parallel to member

 $F_P$  = no less than 0.05 times dead plus live load vertical reaction

Anchorage of Structural Walls to elements providing lateral support

Fp = not less than 0.2KaleWp

Flexible diaphragm span Lf =

Enter Lf to calculate Fp for flexible diaphragm

Fp =0.4SdskaleWp = 0.138 Wp, but not less than 0.2Wp (rigid diaphragm)

ka= 1 Fp = 0.200 Wp

but Fp shall not be less than 5 psf

**MEMBER DESIGN** 

Bearing Wails and Shear Walls (out of plane force)

Fp = 0.4SdsleWw = but not less than 0.138 Ww

0.10 Ww

Use Fp = 0.14 Ww

**Diaphragms** 

Fp = 0.2ISdsWp + Vpx = 0.069 Wp + Vpx

ARCHITECTURAL COMPONENTS SEISMIC COEFFICIENTS

Architectural Component: Cantilever Elements (Unbraced or Braced to Structural Frame Below Its Center of Mass):

Parapets and cantilever interior nonstructural walls

Importance Factor (Ip):

Component Amplification Factor (ap) =

2.5

h≕ 25.8 feet

Comp Response Modification Factor  $(R_n)$  =

2.5

7= 50.0 feet

z/h = 1.00

 $Fp = 0.4a_oSdsipWp(1+2z/h)/Rp =$ 

0.413 Wp

not greater than Fp = 1.6SdslpWp =

0.550 Wp

but not less than Fp = 0.3SdslpWp =

0.103 Wp

use Fp =

0.413 Wp

MECH AND ELEC COMPONENTS SEISMIC COEFFICIENTS

Mech or Electrical Component: Skirt-supported pressure vessels not within the scope of Chapter 15.

Importance Factor (Ip):

Comp Response Modification Factor  $(R_n) =$ 

Component Amplification Factor (a<sub>n</sub>) =

2.5 2.5 h= 25.8 feet

0.0 feet

z=

z/h = 0.00

 $Fp = 0.4a_oSdsipWp(1+2z/h)/Rp =$ 

0.206 Wp

not greater than Fp = 1.6SdslpWp =

0.825 Wp

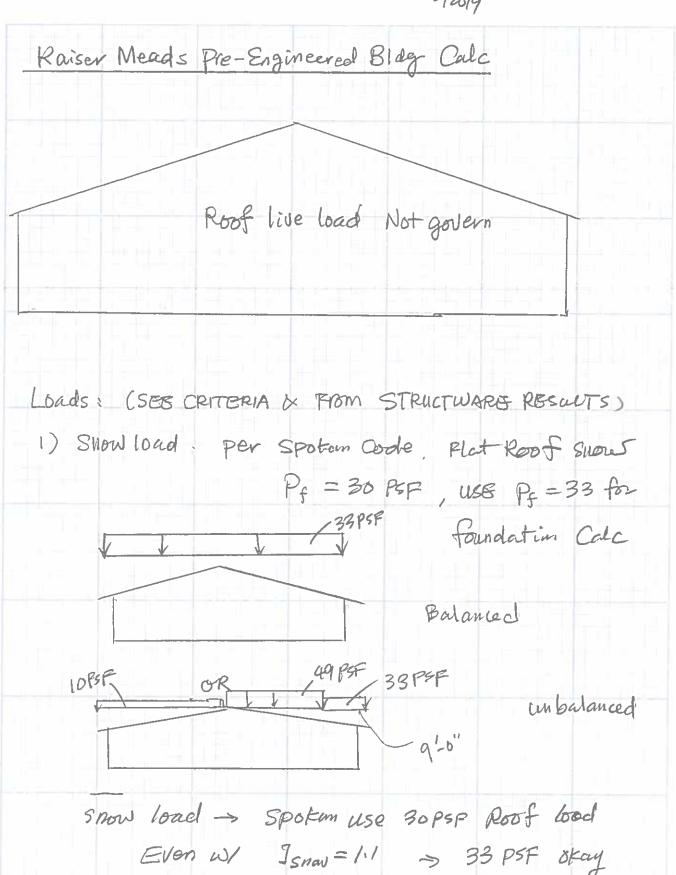
but not less than Fp = 0.3SdslpWp = 0.155 Wp use Fp =

0.206 Wp

Subject PEMB Project Kaiser Meads

POUNDATION REALT ISSUE No. 1 of

Authored by LYANGale 124, Checked by Date



Subject		Project			
		Sheet No. 2 of			
Authored by	Date	Checked by Date			

2)	Wind load (SEE CRITERIA & STRUCTWARE REGILES)
22	$ \frac{1}{2} = \frac{3E}{1} = \frac{70.9}{1} $ $ \frac{1}{1} = \frac{1}{1}$
(13.3)	Case AI ( CASE A2)
	CASE B1 & B2, SEE Table  LOADS WILL BENDART TO STAND MODEL for  Foundation Reaction Calculations
	Collateral Load - Use 10 PSF  DL Load - Use 20 PSF  0.03 KSF
LOAD	Combination - USE ASCE 7-10
	at III. 15 USED Basic Wind Pressure 29.1  W/ 120 mph $C = \frac{29.1 \text{ PSF}}{24.5 \text{ PSF}} = 1.187 \text{ N}.2 \text{ factor}$

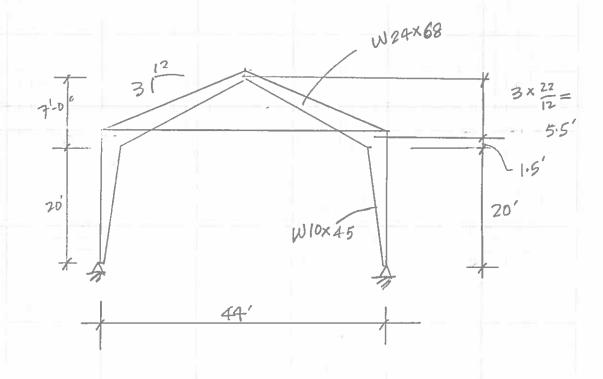
Subject			Project			
			Sheet No. 3 of			
	Authored by	Date	Checked by Date			

Inchest	Smic (C	pads dont g	overn bldg des	ign by
Design	will be	governed by	ent and BQUIP. E.	Merit AN
U:	SE Pp =	= 0.206 Wp	( conserved	5 , NO
	LE NOT	+ Harzard	apaul	Content:
		Fp = 0.206	/1.5 = 0.137 Wp	
F 1 6				
Foundate			ist Cat II	
	but 1	need desigle	if Cat III	Should
	Specia	fied !		

Subject Sheet No. Date Authored by Checked by

Reactions from PEMB Columns

Bay = 22'0" Roof. Span 44'-0"



STAAD Mode

17 19st Collateral load & 20PSF=DL use 1/2 of them W/O Beam frames weight 0.3DL + 0.6 W

 Subject
 Project

 Sheet No.
 5

 Of
 Of

 Authored by
 Date

 Date
 Date

STAAD RESULTS

Footing . Size 
$$6' \times 8' \times 1.5 \times 150^{\#/3} = 10.8^{k}$$
  
 $0.6DL = 6.48^{k}$  okay  
Try  $6' \times 6' \times 1.5 \times 0.15 \times 0.6 = 4.86^{k}$ 

+ 2.5' 86; l = 2.5 x 6x6'x 0.11/4' x0.6=5.94"

NG

L', USE 6'x 8' x 1.5' Col FTG otay

2) Thrust forces
$$T = 0.283^{\frac{1}{5}} \times 22' = 6.22^{\frac{1}{5}}$$
Assume  $f_s = 24 \text{ ks}$ :  $A_s = \frac{6.22}{24} = 0.26 \text{ in}^2$ 

Use (3) #6 okay - in Case Some Cannot

pass thru trenches...

3) Powniward Py = 1.454 x 22 = 32 k

Subject	Project			
		Sheet No.	of	
Authored by	Date	Checked by	Date	

Cs = 0.206 -> Cat III fazility

PADS Supporting EQ, DEFORM, FLOC & Sludg TANKS

Tank NAME	EQ	DEFORM	FLOC	SLUDGE	
weight	47.3K	47.3K	34 K	23.6 K	
HEIGHT	132"	132"	120"	160"	
Shear V = 0.206 W	9.7 2/0K	10 K	7 K	4,8625K	
Momont $M = V(\frac{h}{2} + 6)$	720 K-in	720 <sup>k-"</sup>	462 k-11	430 k-11	
2 = 10.7M/ P (Weight)	0.89'	0.89	0.79"	1.06'	
d=Diameter of Tank	108" A= 63.61 <sup>2</sup>	108" 63.61 A2	96" 50 ft <sup>2</sup>	90" 44 H <sup>2</sup>	
Pressuro D/O Moment = P/A	793 PSF	743 psf	680 psf	536 PSF	
$S = \frac{\pi}{32} d^3$	71.56 A3	71.56 £3	50 fe <sup>3</sup>	41.41 ft3	
07M/s=	±586	±586	±539	±605	
Man Pressure plass 8"+6" conc	+175 PSF ~/500	~1500	1394	1316	
Min Pressure	330	330	316	106	O Kony !
	1	1		Q 5	



Job Title:

Client:

Engineer:

STAAD SPACE START JOB INFORMATION ENGINEER DATE 09-Dec-19 END JOB INFORMATION INPUT WIDTH 79 UNIT FEET KIP

JOINT COORDINATES
1 0 0 0; 2 22 27 0; 3 44 20 0; 4 44 0 0; 5 0 20 0;

MEMBER INCIDENCES

1 1 5; 2 5 2; 3 2 3; 4 3 4;

DEFINE MATERIAL START

ISOTROPIC STEEL

E 4.176e+06

POISSON 0.3

**DENSITY 0.489024** 

ALPHA 6.5e-06

DAMP 0.03

TYPE STEEL

STRENGTH RY 1.5 RT 1.2

END DEFINE MATERIAL

MEMBER PROPERTY AMERICAN

2 3 TABLE ST W24X68

1 4 TABLE ST W10X45

CONSTANTS

MATERIAL STEEL ALL

**SUPPORTS** 

1 4 PINNED

DEFINE REFERENCE LOADS

LOAD R1 LOADTYPE Dead TITLE ROOF DEAD LOAD

MEMBER LOAD

2 3 UNI GY -0.03

LOAD R2 LOADTYPE Wind TITLE WIND LOAD A1

MEMBER LOAD

1 UNI GX 0.022

4 UNI GX 0.0092

2 UNI GY 0.0218

3 UNI GY 0.0197

LOAD R3 LOADTYPE Wind TITLE WIND LOAD A2

MEMBER LOAD

1 UNI GX 0.0133

4 UNI GX 0.018

2 UNI GY 0.0306

3 UNI GY 0.0109

LOAD R4 LOADTYPE Wind TITLE WIND LOAD B1

MEMBER LOAD

1 UNI GX -0.0073

4 UNI GX 0.0073

3

Job Title:

Client:

Engineer:

2 UNI GY 0.0218

3 UNI GY 0.0086

LOAD R5 LOADTYPE Wind TITLE WIND LOAD B2

MEMBER LOAD

1 UNI GX -0.0161

4 UNI GX 0.0161

2 UNI GY 0.0306

3 UNI GY 0.0174

LOAD R6 LOADTYPE Snow TITLE SNOW LOAD BALANCED

MEMBER LOAD

2 3 UNI GY -0.033

LOAD R7 LOADTYPE Snow TITLE SNOW LOAD UNBALANCED

MEMBER LOAD

3 UNI GY -0.033 9 22

2 UNI GY -0.01

3 UNI GY -0.049 0 9

END DEFINE REFERENCE LOADS

LOAD 1 LOADTYPE None TITLE DL + SBALANCED

REFERENCE LOAD

R1 1.0 R6 1.0

LOAD 2 LOADTYPE None TITLE DL + S-UNBALANCED

REFERENCE LOAD

R1 1.0 R7 1.0

LOAD 3 LOADTYPE None TITLE DL + 0.6 WA1

REFERENCE LOAD

R1 1.0 R2 0.6

LOAD 4 LOADTYPE None TITLE DL + 0.6WA2

REFERENCE LOAD

R1 1.0 R3 0.6

LOAD 5 LOADTYPE None TITLE DL + 0.6WB1

REFERENCE LOAD

R1 1.0 R4 0.6

LOAD 6 LOADTYPE None TITLE DL + 0.6WB2

REFERENCE LOAD

R1 1.0 R5 0.6

LOAD 7 LOADTYPE None TITLE DL + 0.75 (SBAL + 0.6WA1)

REFERENCE LOAD

R1 1.0 R6 0.75 R2 0.45

LOAD 8 LOADTYPE None TITLE DL + 0.75 (SBAL + 0.6WA2)

REFERENCE LOAD

R1 1.0 R6 0.75 R3 0.45

LOAD 9 LOADTYPE None TITLE DL + 0.75 (SBAL + 0.6WB1)

REFERENCE LOAD

R1 1.0 R6 0.75 R4 0.45

LOAD 10 LOADTYPE None TITLE DL + 0.75 (SBAL + 0.6WB2)

REFERENCE LOAD

R1 1.0 R6 0.75 R5 0.45



R1 0.3 R5 0.6 PERFORM ANALYSIS DEFINE ENVELOPE

**FINISH** 

END DEFINE ENVELOPE

1 TO 18 ENVELOPE 1 TYPE COLUMN

Job Title:

Client:

Engineer:

\*\*\*

LOAD 11 LOADTYPE None TITLE DL + 0.75 (SUNBAL + 0.6WA1) REFERENCE LOAD R1 1.0 R7 0.75 R2 0.45 LOAD 12 LOADTYPE None TITLE DL + 0.75 (SUNBAL + 0.6WA2) REFERENCE LOAD R1 1.0 R7 0.75 R3 0.45 LOAD 13 LOADTYPE None TITLE DL + 0.75 (SUNBAL + 0.6WB1) REFERENCE LOAD R1 1.0 R7 0.75 R4 0.45 LOAD 14 LOADTYPE None TITLE DL + 0.75 (SUNBAL + 0.6WB2) REFERENCE LOAD R1 1.0 R7 0.75 R5 0.45 LOAD 15 LOADTYPE None TITLE 0.6DL + 0.6WA1 REFERENCE LOAD R1 0.3 R2 0.6 LOAD 16 LOADTYPE None TITLE 0.6DL + 0.6WA2 REFERENCE LOAD R1 0.3 R3 0.6 LOAD 17 LOADTYPE None TITLE 0.6DL + 0.6WB1 REFERENCE LOAD R1 0.3 R4 0.6 LOAD 18 LOADTYPE None TITLE 0.6DL + 0.6WB2 REFERENCE LOAD

# **Process Mechanical Calculations**

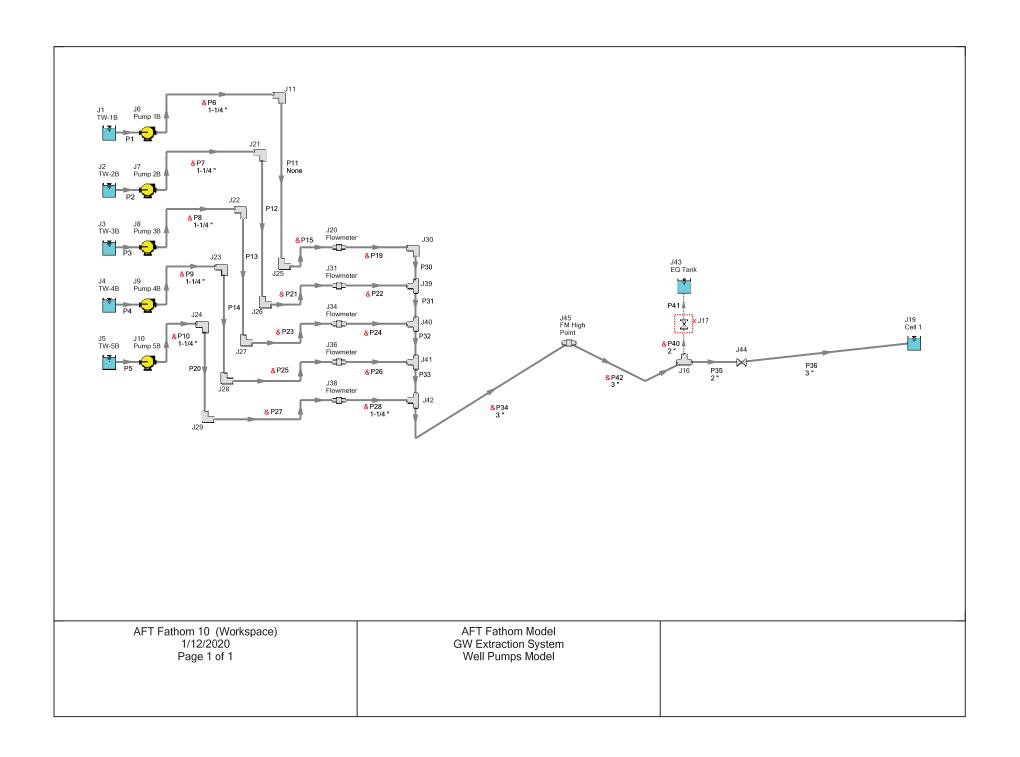
#### **CALCULATIONS**

MECHANICAL



Digitally Signed on April 3, 2020
Bill Farmer

# **Extraction Well Pumps Hydraulics** including Pipe Sizing



AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

#### Model Reference Information

#### General

Title: AFT Fathom Model

Analysis run on: 1/12/2020 8:04:12 PM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWTS\Mechanical\Fathom\GW\_to\_Cell1\_v6\_high point added.fth

Scenario: Base Scenario - HDPE Force Main/50 gpm total - 3" and 1.25"

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\GW\_to\_Cell1\_v6\_high point added\_F4.out

Execution Time= 0.17 seconds

Total Number Of Head/Pressure Iterations= 0

Total Number Of Flow Iterations= 2

Total Number Of Temperature Iterations= 0

Number Of Pipes= 35 Number Of Junctions= 36

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change Temperature Tolerance= 0.0001 relative change Flow Relaxation= (Automatic)

Flow Relaxation= (Automatic)
Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction

Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 g

Turbulent Flow Above Reynolds Number= 4000

Laminar Flow Below Reynolds Number= 2300

Total Inflow= 50.00 gal/min Total Outflow= 50.00 gal/min

Maximum Static Pressure is 115.2 psia at Pipe 8 Inlet

Minimum Static Pressure is 14.66 psia at Pipe 36 Outlet

#### **Warnings**

For an explanation of Warnings, click an item in this list and press F1 or search for 'Warnings' in the Help system.

\*\*\*CAUTION\*\*\* The performance of Pump Junction 6 (Pump 1B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

\*\*\*CAUTION\*\*\* The performance of Pump Junction 7 (Pump 2B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

#### Pump Summary

Jct	Results Diagram	Name	Vol. Flow (gal/min)	dH (feet)	Speed (Percent)	Ideal Power (hp)	Pump Efficiency (Percent)	Shaft Power (hp)	Motor Efficiency (Percent)	Motor Input Power (hp)	NPSHA (feet)
6	Show	Pump 1B	3.000	203.9	74.76	0.1545	62.05	0.2491	95.00	0.2622	41.35
7	Show	Pump 2B	4.000	204.4	75.86	0.2065	63.86	0.3234	95.00	0.3404	41.35
8	Show	Pump 3B	20.000	224.4	91.68	1.1337	65.12	1.7409	95.00	1.8325	41.35
9	Show	Pump 4B	20.000	219.4	91.05	1.1085	65.06	1.7038	95.00	1.7934	41.35
10	Show	Pump 5B	3.000	203.2	74.63	0.1540	62.06	0.2481	95.00	0.2612	41.35

Jct	NPSHR
JCI	(feet)
6	N/A
7	N/A
8	N/A
9	N/A
10	N/A

#### Valve Summary

Jct	Name	Valve Type	Vol. Flow (gal/min)	Mass Flow (Ibm/sec)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	К	Valve State
X17	Valve	REGULAR	0.00	0.000	N/A	N/A	22.66	N/A	N/A	Closed By User
44	Valve	REGULAR	50.00	6.948	6.376E-04	1.472E-03	24.74	1,980	0.02000	Open

#### Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Liquid Mass (Ibm)	Net Vol. Flow (gal/min)	Net Mass Flow (lbm/sec)
1	TW-1B	Infinite	N/A	1,773	14.70	N/A	N/A	-3.000	-0.4169
2	TW-2B	Infinite	N/A	1,773	14.70	N/A	N/A	-4.000	-0.5559
3	TW-3B	Infinite	N/A	1,773	14.70	N/A	N/A	-20.000	-2.7793
4	TW-4B	Infinite	N/A	1,773	14.70	N/A	N/A	-20.000	-2.7793
5	TW-5B	Infinite	N/A	1,773	14.70	N/A	N/A	-3.000	-0.4169
19	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	50.000	6.9483
43	EQ Tank	Infinite	N/A	1,953	14.70	N/A	N/A	0.000	0.0000

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 8 (Pump 3B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 9 (Pump 4B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 10 (Pump 5B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

#### Pipe Output Table

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)	dP Static Total (psid)
1	Pipe	(0 /	12 inch	0.008599	18.16	18.16	1,765	1,765	5.724E-09	5.724E-09
2	Pipe		12 inch	0.011465	18.16	18.16	1,765	1,765	1.330E-08	1.330E-08
3	Pipe		12 inch	0.057327	18.16	18.16	1,765	1,765	4.068E-07	4.068E-07
4	Pipe		12 inch	0.057327	18.16	18.16	1,765	1,765	4.068E-07	4.068E-07
5	Pipe		12 inch	0.007527	18.16	18.16	1,765	1,765	5.724E-09	5.724E-09
6	Pipe		1-1/4 inch	0.643506	106.48	40.07	1,765	1,918	6.641E+01	6.641E+01
7	Pipe		1-1/4 inch	0.858008	106.68	40.18	1,765	1,918	6.650E+01	6.650E+01
8	Pipe		1-1/4 inch	4.290043	115.23	44.98	1,765	1,918	7.025E+01	7.025E+01
9	Pipe		1-1/4 inch	4.290043	113.06	42.81	1,765	1,918	7.025E+01	7.025E+01
10	Pipe		1-1/4 inch	0.643506	106.17	39.76	1,765	1,918	6.641E+01	6.641E+01
11	Pipe	3.000		0.682498	40.07	39.81	1,918	1,918	2.566E-01	2.566E-01
12	Pipe	4.000		0.909997	40.18	39.82	1,918	1,918	3.567E-01	3.567E-01
13	Pipe	20.000		4.549987	44.93	40.28	1,918	1,918	4.648E+00	4.648E+00
14	Pipe	20.000		4.549987	42.76	40.30	1,918	1,918	2.461E+00	2.461E+00
15	Pipe		1-1/4 inch	0.643506	39.81	33.73	1,918	1,932	6.078E+00	6.078E+00
19	Pipe	3.000	1-1/4 inch	0.643506	33.73	33.73	1,932	1,932	4.406E-03	4.406E-03
20	Pipe	3.000		0.682498	39.76	39.71	1,918	1,918	4.934E-02	4.934E-02
21	Pipe		1-1/4 inch	0.858008	39.82	33.73	1,918	1,932	6.087E+00	6.087E+00
22	Pipe	4.000	1-1/4 inch	0.858008	33.73	33.73	1,932	1,932	7.257E-03	7.257E-03
23	Pipe	20.000	1-1/4 inch	4.290043	40.26	33.79	1,918	1,932	6.465E+00	6.465E+00
24	Pipe	20.000	1-1/4 inch	4.290043	33.79	33.67	1,932	1,932	1.237E-01	1.237E-01
25	Pipe	20.000	1-1/4 inch	4.290043	40.27	33.81	1,918	1,932	6.465E+00	6.465E+00
26	Pipe	20.000	1-1/4 inch	4.290043	33.81	33.69	1,932	1,932	1.237E-01	1.237E-01
27	Pipe	3.000	1-1/4 inch	0.643506	39.71	33.63	1,918	1,932	6.078E+00	6.078E+00
28	Pipe	3.000	1-1/4 inch	0.643506	33.63	33.63	1,932	1,932	4.408E-03	4.408E-03
30	Pipe	3.000	1-1/4 inch	0.643506	33.73	33.73	1,932	1,932	8.635E-04	8.635E-04
31	Pipe	7.000	2 inch	0.669279	33.72	33.72	1,932	1,932	5.493E-04	5.493E-04
32	Pipe	27.000	2 inch	2.581503	33.66	33.65	1,932	1,932	5.866E-03	5.866E-03
33	Pipe	47.000	2-1/2 inch	3.149527	33.60	33.59	1,932	1,932	6.716E-03	6.716E-03
34	Pipe	50.000	3 inch	2.176285	33.62	19.51	1,932	1,954	1.411E+01	1.411E+01
35	Pipe	50.000	3 inch	2.176285	24.80	24.74	1,938	1,938	5.343E-02	5.343E-02
36	Pipe	50.000	3 inch	2.176285	24.74	14.66	1,938	1,944	1.008E+01	1.008E+01
40	Pipe	0.000	3 inch	0.000000	24.83	22.66	1,938	1,943	2.166E+00	2.166E+00
41	Pipe	0.000	3 inch	0.000000	18.81	18.81	1,943	1,943	0.000E+00	0.000E+00
42	Pipe	50.000	3 inch	2.176285	24.80	19.51	1,954	1,938	-5.287E+00	-5.287E+00

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

Di	dP	dH	P Static	P Static	P Stag.	P Stag.
Pipe	Gravity (psid)	(feet)	In (psia)	Out (psia)	In (psia)	Out (psia)
1	0.000	1.321E-08	18.16	18.16	18.16	18.16
2	0.000	3.072E-08	18.16	18.16	18.16	18.16
3	0.000	9.391E-07	18.16	18.16	18.16	18.16
4	0.000	9.391E-07	18.16	18.16	18.16	18.16
5	0.000	1.321E-08	18.16	18.16	18.16	18.16
6	66.270	3.265E-01	106.48	40.07	106.48	40.07
7	66.270	5.376E-01	106.68	40.18	106.69	40.19
8	66.270	9.185E+00	115.23	44.98	115.35	45.11
9	66.270	9.185E+00	113.06	42.81	113.19	42.94
10	66.270	3.265E-01	106.17	39.76	106.18	39.76
11	0.000	5.924E-01	40.07	39.81	40.07	39.81
12	0.000	8.236E-01	40.18	39.82	40.18	39.83
13	0.000	1.073E+01	44.93	40.28	45.07	40.42
14	0.000	5.681E+00	42.76	40.30	42.90	40.44
15	6.064	3.209E-02	39.81	33.73	39.81	33.74
19	0.000	1.017E-02	33.73	33.73	33.74	33.73
20	0.000	1.139E-01	39.76	39.71	39.76	39.71
21	6.064	5.303E-02	39.82	33.73	39.83	33.74
22	0.000	1.675E-02	33.73	33.73	33.74	33.73
23	6.064	9.269E-01	40.26	33.79	40.38	33.91
24	0.000	2.857E-01	33.79	33.67	33.91	33.79
25	6.064	9.269E-01	40.27	33.81	40.40	33.93
26	0.000	2.857E-01	33.81	33.69	33.93	33.81
27	6.064	3.209E-02	39.71	33.63	39.71	33.64
28	0.000	1.018E-02	33.63	33.63	33.64	33.63
30	0.000	1.994E-03	33.73	33.73	33.73	33.73
31	0.000	1.268E-03	33.72	33.72	33.73	33.73
32	0.000	1.354E-02	33.66	33.65	33.70	33.69
33	0.000	1.551E-02	33.60	33.59	33.66	33.66
34	9.529	1.058E+01	33.62	19.51	33.65	19.54
35	0.000	1.234E-01	24.80	24.74	24.83	24.78
36	2.599	1.727E+01	24.74	14.66	24.78	14.70
40	2.166	0.000E+00	24.83	22.66	24.83	22.66
41	0.000	0.000E+00	18.81	18.81	18.81	18.81
42	-6.930	3.793E+00	19.51	24.80	19.54	24.83

All Junction Table

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Mass Flow Rate Thru Jct (lbm/sec)	Loss Factor (K)
1	TW-1B	14.70	18.16	14.70	18.16	3.000	0.4169	6.08297
2	TW-2B	14.70	18.16	14.70	18.16	4.000	0.5559	4.56223
3	TW-3B	14.70	18.16	14.70	18.16	20.000	2.7793	0.50000
4	TW-4B	14.70	18.16	14.70	18.16	20.000	2.7793	0.50000
5	TW-5B	14.70	18.16	14.70	18.16	3.000	0.4169	6.08297
6	Pump 1B	18.16	106.48	18.16	106.48	3.000	0.4169	0.00000
7	Pump 2B	18.16	106.68	18.16	106.69	4.000	0.5559	0.00000
8	Pump 3B	18.16	115.23	18.16	115.35	20.000	2.7793	0.00000
9	Pump 4B	18.16	113.06	18.16	113.19	20.000	2.7793	0.00000
10	Pump 5B	18.16	106.17	18.16	106.18	3.000	0.4169	0.00000
11	Bend	40.07	40.07	40.07	40.07	3.000	0.4169	0.30072
16	Tee or Wye	24.82	24.82	24.83	24.83	N/A	N/A	See Mult. Losses
X17	Valve	22.66	18.81	22.66	18.81	0.000	0.0000	0.00000
19	Cell 1	14.70	14.70	14.70	14.70	50.000	6.9483	0.00000
20	Flowmeter	33.73	33.73	33.74	33.74	3.000	0.4169	0.00000
21	Bend	40.18	40.18	40.19	40.18	4.000	0.5559	0.30072
22	Bend	44.98	44.93	45.11	45.07	20.000	2.7793	0.30072
23	Bend	42.81	42.76	42.94	42.90	20.000	2.7793	0.30072
24	Bend	39.76	39.76	39.76	39.76	3.000	0.4169	0.30072
25	Bend	39.81	39.81	39.81	39.81	3.000	0.4169	0.30296
26	Bend	39.82	39.82	39.83	39.83	4.000	0.5559	0.30296
27	Bend	40.28	40.26	40.42	40.38	20.000	2.7793	0.30296
28	Bend	40.30	40.27	40.44	40.40	20.000	2.7793	0.30296
29	Bend	39.71	39.71	39.71	39.71	3.000	0.4169	0.30296
30	Bend	33.73	33.73	33.73	33.73	3.000	0.4169	0.30072
31	Flowmeter	33.73	33.73	33.74	33.74	4.000	0.5559	0.00000
34	Flowmeter	33.79	33.79	33.91	33.91	20.000	2.7793	0.00000
36	Flowmeter	33.81	33.81	33.93	33.93	20.000	2.7793	0.00000
38	Flowmeter	33.63	33.63	33.64	33.64	3.000	0.4169	0.00000
39	Tee or Wye	33.72	33.72	33.73	33.73	N/A	N/A	See Mult. Losses
40	Tee or Wye	33.66	33.66	33.70	33.70	N/A	N/A	See Mult. Losses
41	Tee or Wye	33.59	33.59	33.66	33.66	N/A	N/A	See Mult. Losses
42	Tee or Wye	33.63	33.63	33.65	33.65	N/A	N/A	See Mult. Losses
43	EQ Tank	14.70	18.81	14.70	18.81	0.000	0.0000	0.00000
44	Valve	24.74	24.74	24.78	24.78	50.000	6.9483	0.02000
45	FM High Point	19.51	19.51	19.54	19.54	50.000	6.9483	0.00000

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

75 gpm through EC Bldg to Cell 1

#### Model Reference Information

#### General

Title: AFT Fathom Model

Analysis run on: 2/10/2020 8:47:38 AM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Well Pumps Model\GW to Cell1 v6 high point added.fth

Scenario: Base Scenario - HDPE Force Main/75 gpm total - thru EC Bldg with 2" pipe/75% effic pumps

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Well Pumps Model\GW to Cell1 v6 high point added F2.out

Execution Time= 0.10 seconds

Total Number Of Head/Pressure Iterations= 0

Total Number Of Flow Iterations = 2

Total Number Of Temperature Iterations= 0

Number Of Pipes= 35 Number Of Junctions= 36

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change Temperature Tolerance= 0.0001 relative change Flow Relaxation= (Automatic)

Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction

Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 g Turbulent Flow Above Reynolds Number= 4000

Laminar Flow Below Reynolds Number= 2300

Total Inflow= 75.00 gal/min Total Outflow= 75.00 gal/min

Maximum Static Pressure is 130.5 psia at Pipe 8 Inlet Minimum Static Pressure is 14.62 psia at Pipe 36 Outlet

#### **Warnings**

For an explanation of Warnings, click an item in this list and press F1 or search for 'Warnings' in the Help system.

\*\*\*CAUTION\*\*\* The performance of Pump Junction 6 (Pump 1B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

\*\*\*CAUTION\*\*\* The performance of Pump Junction 7 (Pump 2B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

#### Pump Summary

Jct	Results Diagram	Name	Vol. Flow (gal/min)	dH (feet)	Speed (Percent)	Ideal Power (hp)	Pump Efficiency (Percent)	Shaft Power (hp)	Motor Efficiency (Percent)	Motor Input Power (hp)	NPSHA (feet)
6	Show	Pump 1B	10.00	246.2	93.04	0.6220	74.76	0.8319	85.00	0.9788	41.35
7	Show	Pump 2B	15.00	253.0	97.68	0.9587	69.18	1.3859	85.00	1.6305	41.35
8	Show	Pump 3B	20.00	259.6	96.00	1.3116	75.49	1.7375	85.00	2.0441	41.35
9	Show	Pump 4B	20.00	254.5	95.39	1.2857	75.44	1.7042	85.00	2.0050	41.35
10	Show	Pump 5B	10.00	241.9	92.42	0.6110	74.70	0.8180	85.00	0.9623	41.35

Jct	NPSHR
	(feet)
6	N/A
7	N/A
8	N/A
9	N/A
10	N/A

#### Valve Summary

Jct	Name	Valve Type	Vol. Flow (gal/min)	Mass Flow (lbm/sec)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	К	Valve State
X17	Valve	REGULAR	0.00	0.00	N/A	N/A	31.25	N/A	N/A	Closed By User
44	Valve	REGULAR	75.00	10.42	6.766E-03	0.01562	32.37	911.7	0.02000	Open

#### Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Liquid Mass (lbm)	Net Vol. Flow (gal/min)	Net Mass Flow (lbm/sec)
1	TW-1B	Infinite	N/A	1,773	14.70	N/A	N/A	-10.00	-1.390
2	TW-2B	Infinite	N/A	1,773	14.70	N/A	N/A	-15.00	-2.084
3	TW-3B	Infinite	N/A	1,773	14.70	N/A	N/A	-20.00	-2.779
4	TW-4B	Infinite	N/A	1,773	14.70	N/A	N/A	-20.00	-2.779
5	TW-5B	Infinite	N/A	1,773	14.70	N/A	N/A	-10.00	-1.390
19	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	75.00	10.422
43	EQ Tank	Infinite	N/A	1,953	14.70	N/A	N/A	0.00	0.000

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 8 (Pump 3B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 9 (Pump 4B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 10 (Pump 5B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

#### Pipe Output Table

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)	dP Static Total (psid)
1	Pipe	10.00	12 inch	0.02866	18.16	18.16	1,765	1,765	6.125E-08	6.125E-08
2	Pipe	15.00	12 inch	0.04299	18.16	18.16	1,765	1,765	2.114E-07	2.114E-07
3	Pipe	20.00	12 inch	0.05733	18.16	18.16	1,765	1,765	4.068E-07	4.068E-07
4	Pipe	20.00	12 inch	0.05733	18.16	18.16	1,765	1,765	4.068E-07	4.068E-07
5	Pipe	10.00	12 inch	0.02866	18.16	18.16	1,765	1,765	6.125E-08	6.125E-08
6	Pipe	10.00	1-1/4 inch	2.14502	124.77	57.34	1,765	1,918	6.743E+01	6.743E+01
7	Pipe	15.00	1-1/4 inch	3.21753	127.68	59.02	1,765	1,918	6.865E+01	6.865E+01
8	Pipe	20.00	1-1/4 inch	4.29004	130.48	60.23	1,765	1,918	7.025E+01	7.025E+01
9	Pipe	20.00	1-1/4 inch	4.29004	128.26	58.01	1,765	1,918	7.025E+01	7.025E+01
10	Pipe	10.00	1-1/4 inch	2.14502	122.89	55.45	1,765	1,918	6.743E+01	6.743E+01
11	Pipe	10.00	None	2.27499	57.32	55.24	1,918	1,918	2.086E+00	2.086E+00
12	Pipe	15.00	None	3.41249	58.99	55.38	1,918	1,918	3.610E+00	3.610E+00
13	Pipe	20.00	None	4.54999	60.18	55.53	1,918	1,918	4.648E+00	4.648E+00
14	Pipe	20.00	None	4.54999	57.96	55.50	1,918	1,918	2.461E+00	2.461E+00
15	Pipe	10.00	1-1/4 inch	2.14502	55.23	49.05	1,918	1,932	6.180E+00	6.180E+00
19	Pipe	10.00	1-1/4 inch	2.14502	49.05	49.02	1,932	1,932	3.612E-02	3.612E-02
20	Pipe	10.00	None	2.27499	55.44	55.04	1,918	1,918	4.012E-01	4.012E-01
21	Pipe	15.00	1-1/4 inch	3.21753	55.37	49.07	1,918	1,932	6.303E+00	6.303E+00
22	Pipe	15.00	1-1/4 inch	3.21753	49.07	48.99	1,932	1,932	7.411E-02	7.411E-02
23	Pipe	20.00	1-1/4 inch	4.29004	55.50	49.04	1,918	1,932	6.465E+00	6.465E+00
24	Pipe	20.00	1-1/4 inch	4.29004	49.04	48.91	1,932	1,932	1.237E-01	1.237E-01
25	Pipe	20.00	1-1/4 inch	4.29004	55.47	49.01	1,918	1,932	6.465E+00	6.465E+00
26	Pipe	20.00	1-1/4 inch	4.29004	49.01	48.88	1,932	1,932	1.237E-01	1.237E-01
27	Pipe	10.00	1-1/4 inch	2.14502	55.03	48.85	1,918	1,932	6.180E+00	6.180E+00
28	Pipe	10.00	1-1/4 inch	2.14502	48.85	48.82	1,932	1,932	3.612E-02	3.612E-02
30	Pipe	10.00	1-1/4 inch	2.14502	49.01	49.00	1,932	1,932	6.988E-03	6.988E-03
31	Pipe	25.00	2 inch	2.39028	48.97	48.97	1,932	1,932	5.118E-03	5.118E-03
32	Pipe	45.00	2 inch	4.30250	48.82	48.80	1,932	1,932	1.456E-02	1.456E-02
33	Pipe	65.00	2-1/2 inch	4.35573	48.75	48.74	1,932	1,932	1.198E-02	1.198E-02
34	Pipe	75.00	3 inch	3.26443	48.78	29.81	1,932	1,954	1.897E+01	1.897E+01
35	Pipe	75.00	2 inch	7.08950	33.08	32.37	1,938	1,938	7.075E-01	7.075E-01
36	Pipe	75.00	3 inch	3.26443	32.63	14.62	1,938	1,944	1.801E+01	1.801E+01
40	Pipe	0.00	2 inch	0.00000	33.42	31.25	1,938	1,943	2.166E+00	2.166E+00
41	Pipe	0.00	2 inch	0.00000	19.24	18.81	1,943	1,942	-4.331E-01	-4.331E-01
42	Pipe	75.00	3 inch	3.26443	33.35	29.81	1,954	1,938	-3.538E+00	-3.538E+00

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

Pipe	dP Gravity	dH	P Static In	P Static Out	P Stag. In	P Stag. Out
1 ipe	(psid)	(feet)	(psia)	(psia)	(psia)	(psia)
1	0.0000	1.414E-07	18.16	18.16	18.16	18.16
2	0.0000	4.880E-07	18.16	18.16	18.16	18.16
3	0.0000	9.391E-07	18.16	18.16	18.16	18.16
4	0.0000	9.391E-07	18.16	18.16	18.16	18.16
5	0.0000	1.414E-07	18.16	18.16	18.16	18.16
6	66.2704	2.680E+00	124.77	57.34	124.80	57.37
7	66.2704	5.499E+00	127.68	59.02	127.75	59.09
8	66.2704	9.185E+00	130.48	60.23	130.60	60.35
9	66.2704	9.185E+00	128.26	58.01	128.39	58.14
10	66.2704	2.680E+00	122.89	55.45	122.92	55.49
11	0.0000	4.817E+00	57.32	55.24	57.36	55.27
12	0.0000	8.335E+00	58.99	55.38	59.07	55.46
13	0.0000	1.073E+01	60.18	55.53	60.32	55.67
14	0.0000	5.681E+00	57.96	55.50	58.10	55.64
15	6.0640	2.677E-01	55.23	49.05	55.26	49.08
19	0.0000	8.338E-02	49.05	49.02	49.08	49.05
20	0.0000	9.263E-01	55.44	55.04	55.48	55.07
21	6.0640	5.526E-01	55.37	49.07	55.44	49.14
22	0.0000	1.711E-01	49.07	48.99	49.14	49.06
23	6.0640	9.269E-01	55.50	49.04	55.63	49.16
24	0.0000	2.857E-01	49.04	48.91	49.16	49.04
25	6.0640	9.269E-01	55.47	49.01	55.60	49.13
26	0.0000	2.857E-01	49.01	48.88	49.13	49.01
27	6.0640	2.677E-01	55.03	48.85	55.06	48.88
28	0.0000	8.340E-02	48.85	48.82	48.88	48.85
30	0.0000	1.613E-02	49.01	49.00	49.04	49.03
31	0.0000	1.182E-02	48.97	48.97	49.01	49.00
32	0.0000	3.361E-02	48.82	48.80	48.94	48.93
33	0.0000	2.767E-02	48.75	48.74	48.88	48.87
34	9.5291	2.181E+01	48.78	29.81	48.85	29.88
35	0.0000	1.634E+00	33.08	32.37	33.42	32.71
36	2.5988	3.557E+01	32.63	14.62	32.70	14.70
40	2.1657	0.000E+00	33.42	31.25	33.42	31.25
41	-0.4331	0.000E+00	18.81	19.24	18.81	19.24
42	-6.9302	7.831E+00	29.81	33.35	29.88	33.42

All Junction Table

Name									
2         TW-2B         14.70         18.16         14.70         18.16         15.00         2.084         1.04880           3         TW-3B         14.70         18.16         14.70         18.16         20.00         2.779         0.50000           4         TW-4B         14.70         18.16         14.70         18.16         20.00         2.779         0.50000           5         TW-5B         14.70         18.16         14.70         18.16         14.70         18.16         10.00         1.390         0.50000           6         Pump 1B         18.16         124.77         18.16         124.80         10.00         1.390         0.00000           7         Pump 2B         18.16         127.68         18.16         124.80         10.00         2.084         0.00000           9         Pump 3B         18.16         122.82         10.00         1.390         0.00000           9         Pump 4B         18.16         122.89         10.00         1.390         0.00000           10         Demd         57.34         57.32         57.37         57.36         10.00         1.390         0.00000           11         Bend         <	Jct	Name	In	Out	ln	Out	Rate Thru Jct	Rate Thru Jct	Loss Factor (K)
3         TW-3B         14.70         18.16         14.70         18.16         20.00         2.779         0.50000           4         TW-4B         14.70         18.16         14.70         18.16         20.00         2.779         0.50000           5         TW-5B         14.70         18.16         14.70         18.16         10.00         1.390         1.84618           6         Pump 1B         18.16         124.78         18.16         124.80         10.00         1.390         0.00000           8         Pump 2B         18.16         127.68         18.16         127.75         15.00         2.084         0.00000           9         Pump 3B         18.16         128.26         18.16         128.39         20.00         2.779         0.00000           10         Pump 5B         18.16         128.26         18.16         128.292         10.00         1.390         0.00000           11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.0000           11         Tee or Wye         33.34         33.42         33.42         33.42         34.42         N/A         N/A         See Mult.	1	TW-1B	14.70	18.16	14.70	18.16	10.00	1.390	1.84618
4         TW-4B         14.70         18.16         14.70         18.16         20.00         2.779         0.50000           5         TW-5B         14.70         18.16         14.70         18.16         10.00         1.390         1.84618           6         Pump 1B         18.16         124.77         18.16         124.80         10.00         1.390         0.00000           7         Pump 2B         18.16         127.68         18.16         127.75         15.00         2.084         0.00000           8         Pump 3B         18.16         128.26         18.16         122.89         18.06         20.00         2.779         0.00000           10         Pump 4B         18.16         122.89         18.16         122.89         10.00         1.390         0.00000           11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.30072           16         Tee or Wye         33.34         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         0.00         0.000         0.0000           20         Eell	2	TW-2B	14.70	18.16	14.70	18.16	15.00	2.084	1.04880
5         TW-5B         14.70         18.16         14.70         18.16         10.00         1.390         1.84618           6         Pump 1B         18.16         124.77         18.16         124.80         10.00         1.390         0.00000           7         Pump 2B         18.16         127.68         18.16         127.75         15.00         2.084         0.00000           8         Pump 3B         18.16         130.48         18.16         130.60         20.00         2.779         0.00000           10         Pump 4B         18.16         122.89         18.16         122.89         18.16         122.92         10.00         1.390         0.00000           11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.30072           16         Tee or Wye         33.34         33.34         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           19         Cell 1         14.70         14.70         14.70         75.00         10.422	3	TW-3B	14.70	18.16	14.70	18.16	20.00	2.779	0.50000
6         Pump 1B         18.16         124.77         18.16         124.80         10.00         1.390         0.00000           7         Pump 2B         18.16         127.68         18.16         127.75         15.00         2.084         0.00000           8         Pump 3B         18.16         130.48         18.16         130.60         20.00         2.779         0.00000           9         Pump 4B         18.16         128.29         18.16         128.39         20.00         2.779         0.00000           10         Pump 5B         18.16         122.89         18.16         122.92         10.00         1.390         0.00000           10         Pump 5B         18.16         122.89         18.16         122.92         10.00         1.390         0.00000           10         Pump 5B         18.16         122.89         18.16         128.39         20.00         2.779         0.00000           11         Bend         57.32         57.37         57.36         10.00         1.390         0.30072           20         Ell 1         14.70         14.70         14.70         75.00         10.422         0.00000           21	4	TW-4B	14.70	18.16	14.70	18.16	20.00	2.779	0.50000
7         Pump 2B         18.16         127.68         18.16         127.75         15.00         2.084         0.00000           8         Pump 3B         18.16         130.48         18.16         130.60         20.00         2.779         0.00000           9         Pump 4B         18.16         128.26         18.16         128.39         20.00         2.779         0.00000           10         Pump 5B         18.16         122.89         18.16         122.92         10.00         1.390         0.0000           11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.30072           16         Tee or Wye         33.34         33.42         33.42         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           20         Flowmeter         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         58.99         59.09         59.07         15.00         2.084         0.30072 </td <td>5</td> <td>TW-5B</td> <td>14.70</td> <td>18.16</td> <td>14.70</td> <td>18.16</td> <td>10.00</td> <td>1.390</td> <td>1.84618</td>	5	TW-5B	14.70	18.16	14.70	18.16	10.00	1.390	1.84618
8         Pump 3B         18.16         130.48         18.16         130.60         20.00         2.779         0.00000           9         Pump 4B         18.16         128.26         18.16         128.39         20.00         2.779         0.00000           10         Pump 5B         18.16         122.89         18.16         122.92         10.00         1.390         0.0000           11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.30072           16         Tee or Wye         33.34         33.34         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           19         Cell 1         14.70         14.70         14.70         75.00         10.422         0.00000           20         Flowmeter         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         58.99         59.07         15.00         2.084         0.30072           22         Bend         55.	6	Pump 1B	18.16	124.77	18.16	124.80	10.00	1.390	0.00000
9         Pump 4B         18.16         128.26         18.16         128.39         20.00         2.779         0.00000           10         Pump 5B         18.16         122.89         18.16         122.92         10.00         1.390         0.00000           11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.30072           16         Tee or Wye         33.34         33.34         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           20         Flowmeter         49.05         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         59.99         59.09         59.07         15.00         2.084         0.30072           22         Bend         59.01         58.14         58.10         20.00         2.779         0.30072           23         Bend         55.45         55.44         55.48         10.00         1.390         0.30296           24         Bend <td>7</td> <td>Pump 2B</td> <td>18.16</td> <td>127.68</td> <td>18.16</td> <td>127.75</td> <td>15.00</td> <td>2.084</td> <td>0.00000</td>	7	Pump 2B	18.16	127.68	18.16	127.75	15.00	2.084	0.00000
10         Pump 5B         18.16         122.89         18.16         122.92         10.00         1.390         0.00000           11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.30072           16         Tee or Wye         33.34         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           19         Cell 1         14.70         14.70         14.70         75.00         10.422         0.00000           20         Flowmeter         49.05         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         58.99         59.07         15.00         2.084         0.30072           22         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30296           25         Bend         55.24	8	Pump 3B	18.16	130.48	18.16	130.60	20.00	2.779	0.00000
11         Bend         57.34         57.32         57.37         57.36         10.00         1.390         0.30072           16         Tee or Wye         33.34         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           19         Cell 1         14.70         14.70         14.70         75.00         10.422         0.00000           20         Flowmeter         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         58.99         59.09         59.07         15.00         2.084         0.30072           22         Bend         60.23         60.18         60.35         60.32         20.00         2.779         0.30072           23         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30296           27         Bend         55.53	9	Pump 4B	18.16	128.26	18.16	128.39	20.00	2.779	0.00000
Tee or Wye         33.34         33.34         33.42         33.42         N/A         N/A         See Mult. Losses           X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           19         Cell 1         14.70         14.70         14.70         75.00         10.422         0.00000           20         Flowmeter         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         58.99         59.09         59.07         15.00         2.084         0.30072           22         Bend         60.23         60.18         60.35         60.32         20.00         2.779         0.30072           23         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30296           26         Bend         55.33         55.37         55.66         55.44         15.00         2.084         0.30296           29         Bend         55.50	10	Pump 5B	18.16	122.89	18.16	122.92	10.00	1.390	0.00000
X17         Valve         31.25         18.81         31.25         18.81         0.00         0.000         0.0000           19         Cell 1         14.70         14.70         14.70         75.00         10.422         0.00000           20         Flowmeter         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         58.99         59.09         59.07         15.00         2.084         0.30072           22         Bend         60.23         60.18         60.35         60.32         20.00         2.779         0.30072           23         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30296           26         Bend         55.33         55.37         55.46         55.44         15.00         2.084         0.30296           27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           29         Bend         55.	11	Bend	57.34	57.32	57.37	57.36	10.00	1.390	0.30072
19         Cell 1         14.70         14.70         14.70         75.00         10.422         0.00000           20         Flowmeter         49.05         49.08         49.08         10.00         1.390         0.00000           21         Bend         59.02         58.99         59.09         59.07         15.00         2.084         0.30072           22         Bend         60.23         60.18         60.35         60.32         20.00         2.779         0.30072           23         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30072           25         Bend         55.24         55.23         55.27         55.26         10.00         1.390         0.30296           26         Bend         55.38         55.37         55.67         55.63         20.00         2.779         0.30296           27         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         55.	16	Tee or Wye	33.34	33.34	33.42	33.42	N/A	N/A	See Mult. Losses
Plowmeter	X17	Valve	31.25	18.81	31.25	18.81	0.00	0.000	0.00000
21         Bend         59.02         58.99         59.09         59.07         15.00         2.084         0.30072           22         Bend         60.23         60.18         60.35         60.32         20.00         2.779         0.30072           23         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30072           25         Bend         55.24         55.23         55.27         55.26         10.00         1.390         0.30296           26         Bend         55.38         55.37         55.46         55.44         15.00         2.084         0.30296           27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           30	19	Cell 1	14.70	14.70	14.70	14.70	75.00	10.422	0.00000
22         Bend         60.23         60.18         60.35         60.32         20.00         2.779         0.30072           23         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30072           25         Bend         55.24         55.23         55.27         55.26         10.00         1.390         0.30296           26         Bend         55.38         55.37         55.46         55.44         15.00         2.084         0.30296           27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowm	20	Flowmeter	49.05	49.05	49.08	49.08	10.00	1.390	0.00000
23         Bend         58.01         57.96         58.14         58.10         20.00         2.779         0.30072           24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30072           25         Bend         55.24         55.23         55.27         55.26         10.00         1.390         0.30296           26         Bend         55.38         55.37         55.46         55.44         15.00         2.084         0.30296           27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         55.04         55.03         55.07         55.06         10.00         1.390         0.30072           30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.07         49.14         49.14         15.00         2.084         0.00000           34	21	Bend	59.02	58.99	59.09	59.07	15.00	2.084	0.30072
24         Bend         55.45         55.44         55.49         55.48         10.00         1.390         0.30072           25         Bend         55.24         55.23         55.27         55.26         10.00         1.390         0.30296           26         Bend         55.38         55.37         55.46         55.44         15.00         2.084         0.30296           27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         55.04         55.03         55.07         55.06         10.00         1.390         0.30296           30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowmeter         49.01         49.16         49.16         20.00         2.779         0.00000           38         Flowmeter	22	Bend	60.23	60.18	60.35	60.32	20.00	2.779	0.30072
25         Bend         55.24         55.23         55.27         55.26         10.00         1.390         0.30296           26         Bend         55.38         55.37         55.46         55.44         15.00         2.084         0.30296           27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         55.04         55.03         55.07         55.06         10.00         1.390         0.30296           30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.0000           34         Flowmeter         49.04         49.16         49.16         20.00         2.779         0.00000           38         Flowmeter         49.01         49.13         49.13         20.00         2.779         0.00000           39         Tee or Wye         48.85	23	Bend	58.01	57.96	58.14	58.10	20.00	2.779	0.30072
26         Bend         55.38         55.37         55.46         55.44         15.00         2.084         0.30296           27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         55.04         55.03         55.07         55.06         10.00         1.390         0.30296           30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowmeter         49.04         49.16         49.16         20.00         2.779         0.00000           36         Flowmeter         49.01         49.13         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.88         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01 <td>24</td> <td>Bend</td> <td>55.45</td> <td>55.44</td> <td>55.49</td> <td>55.48</td> <td>10.00</td> <td>1.390</td> <td>0.30072</td>	24	Bend	55.45	55.44	55.49	55.48	10.00	1.390	0.30072
27         Bend         55.53         55.50         55.67         55.63         20.00         2.779         0.30296           28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         55.04         55.03         55.07         55.06         10.00         1.390         0.30296           30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowmeter         49.04         49.16         49.16         20.00         2.779         0.00000           36         Flowmeter         49.01         49.13         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.88         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.84         <	25	Bend	55.24	55.23	55.27	55.26	10.00	1.390	0.30296
28         Bend         55.50         55.47         55.64         55.60         20.00         2.779         0.30296           29         Bend         55.04         55.03         55.07         55.06         10.00         1.390         0.30296           30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowmeter         49.04         49.16         49.16         20.00         2.779         0.00000           36         Flowmeter         49.01         49.13         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.85         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.85         48.94         N/A         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75	26	Bend	55.38	55.37	55.46	55.44	15.00	2.084	0.30296
29         Bend         55.04         55.03         55.07         55.06         10.00         1.390         0.30296           30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowmeter         49.04         49.16         49.16         20.00         2.779         0.00000           36         Flowmeter         49.01         49.13         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.85         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.94         48.94         N/A         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.88         48.85         N/A         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48	27	Bend	55.53	55.50	55.67	55.63	20.00	2.779	0.30296
30         Bend         49.02         49.01         49.05         49.04         10.00         1.390         0.30072           31         Flowmeter         49.07         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowmeter         49.04         49.04         49.16         20.00         2.779         0.00000           36         Flowmeter         49.01         49.01         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.85         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.85         48.94         N/A         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.88         48.88         N/A         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.85         48.85         N/A         N/A         N/A         See Mult. Losses           43	28	Bend	55.50	55.47	55.64	55.60	20.00	2.779	0.30296
31         Flowmeter         49.07         49.14         49.14         15.00         2.084         0.00000           34         Flowmeter         49.04         49.04         49.16         20.00         2.779         0.00000           36         Flowmeter         49.01         49.13         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.85         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.85         48.94         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.88         48.88         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.85         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.00         0.0000           44         Valve         32.37         32.63         32.71         32.70	29	Bend	55.04	55.03	55.07	55.06	10.00	1.390	0.30296
34         Flowmeter         49.04         49.16         49.16         20.00         2.779         0.00000           36         Flowmeter         49.01         49.01         49.13         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.85         48.88         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.94         48.94         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.88         48.88         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.85         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.000         0.00000           44         Valve         32.37         32.63         32.71         32.70         75.00         10.422         0.020000	30	Bend	49.02	49.01	49.05	49.04	10.00	1.390	0.30072
36         Flowmeter         49.01         49.01         49.13         49.13         20.00         2.779         0.00000           38         Flowmeter         48.85         48.85         48.88         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.94         48.94         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.88         48.88         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.85         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.000         0.0000           44         Valve         32.37         32.63         32.71         32.70         75.00         10.422         0.02000	31	Flowmeter	49.07	49.07	49.14	49.14	15.00	2.084	0.00000
38         Flowmeter         48.85         48.85         48.88         48.88         10.00         1.390         0.00000           39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.85         48.94         N/A         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.88         48.88         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.85         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.000         0.0000           44         Valve         32.37         32.63         32.71         32.70         75.00         10.422         0.02000	34	Flowmeter	49.04	49.04	49.16	49.16	20.00	2.779	0.00000
39         Tee or Wye         48.96         49.01         49.01         N/A         N/A         N/A         See Mult. Losses           40         Tee or Wye         48.85         48.94         48.94         N/A         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.85         48.88         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.85         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.000         0.0000           44         Valve         32.37         32.63         32.71         32.70         75.00         10.422         0.02000	36	Flowmeter	49.01	49.01	49.13	49.13	20.00	2.779	0.00000
40         Tee or Wye         48.85         48.85         48.94         48.94         N/A         N/A         See Mult. Losses           41         Tee or Wye         48.75         48.75         48.88         48.88         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.78         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.000         0.0000           44         Valve         32.37         32.63         32.71         32.70         75.00         10.422         0.02000	38	Flowmeter	48.85	48.85	48.88	48.88	10.00	1.390	0.00000
41         Tee or Wye         48.75         48.75         48.88         48.88         N/A         N/A         See Mult. Losses           42         Tee or Wye         48.78         48.78         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.000         0.00000           44         Valve         32.37         32.63         32.71         32.70         75.00         10.422         0.020000	39	Tee or Wye	48.96	48.96	49.01	49.01	N/A	N/A	See Mult. Losses
42         Tee or Wye         48.78         48.78         48.85         48.85         N/A         N/A         See Mult. Losses           43         EQ Tank         14.70         19.24         14.70         19.24         0.00         0.000         0.0000           44         Valve         32.37         32.63         32.71         32.70         75.00         10.422         0.02000	40	Tee or Wye	48.85	48.85	48.94	48.94	N/A	N/A	See Mult. Losses
43     EQ Tank     14.70     19.24     14.70     19.24     0.00     0.000     0.0000       44     Valve     32.37     32.63     32.71     32.70     75.00     10.422     0.02000	41	Tee or Wye	48.75	48.75	48.88	48.88	N/A	N/A	See Mult. Losses
44 Valve 32.37 32.63 32.71 32.70 75.00 10.422 0.02000	42	Tee or Wye	48.78	48.78	48.85	48.85	N/A	N/A	See Mult. Losses
	43	EQ Tank	14.70	19.24	14.70	19.24	0.00	0.000	0.00000
45 FM High Point 29.81 29.88 29.88 75.00 10.422 0.00000	44	Valve	32.37	32.63	32.71	32.70	75.00	10.422	0.02000
	45	FM High Point	29.81	29.81	29.88	29.88	75.00	10.422	0.00000

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model 75 gpm to EQ Tank

#### Model Reference Information

#### General

Title: AFT Fathom Model

Analysis run on: 2/10/2020 8:42:07 AM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWT\Mechanica\Fathom\Well Pumps Mode\GW to Cell1 v6 high point added.fth

Scenario: Base Scenario - HDPE Force Main/75 gpm total - to EQ with 2" pipe

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Well Pumps Model\GW to Cell1 v6 high point added F3.out

Execution Time= 0.13 seconds

Total Number Of Head/Pressure Iterations= 0

Total Number Of Flow Iterations= 2

Total Number Of Temperature Iterations= 0

Number Of Pipes= 35

Number Of Junctions= 36

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change Temperature Tolerance= 0.0001 relative change Flow Relaxation= (Automatic)

Flow Relaxation= (Automatic)
Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction

Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 g Turbulent Flow Above Reynolds Number= 4000 Laminar Flow Below Reynolds Number= 2300

Total Inflow= 75.00 gal/min Total Outflow= 75.00 gal/min

Maximum Static Pressure is 121.8 psia at Pipe 8 Inlet Minimum Static Pressure is 16.00 psia at Pipe 36 Outlet

#### **Warnings**

For an explanation of Warnings, click an item in this list and press F1 or search for 'Warnings' in the Help system.

\*\*\*CAUTION\*\*\* The performance of Pump Junction 6 (Pump 1B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

\*\*\*CAUTION\*\*\* The performance of Pump Junction 7 (Pump 2B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

#### Pump Summary

Jct	Results Diagram	Name	Vol. Flow (gal/min)	dH (feet)	Speed (Percent)	Ideal Power (hp)	Pump Efficiency (Percent)	Shaft Power (hp)	Motor Efficiency (Percent)	Motor Input Power (hp)	NPSHA (feet)
6	Show	Pump 1B	10.00	226.2	90.14	0.5715	79.43	0.7195	85.00	0.8464	41.35
7	Show	Pump 2B	15.00	233.0	95.83	0.8830	73.57	1.2003	85.00	1.4121	41.35
8	Show	Pump 3B	20.00	239.6	93.57	1.2107	80.30	1.5077	85.00	1.7738	41.35
9	Show	Pump 4B	20.00	234.5	92.94	1.1848	80.24	1.4766	85.00	1.7371	41.35
10	Show	Pump 5B	10.00	221.9	89.50	0.5605	79.35	0.7064	85.00	0.8310	41.35

Jct	NPSHR
JCI	(feet)
6	N/A
7	N/A
8	N/A
9	N/A
10	N/A

#### Valve Summary

Jct	Name	Valve Type	Vol. Flow (gal/min)	Mass Flow (lbm/sec)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	К	Valve State
17	Valve	REGULAR	75.00	10.42	6.766E-03	0.01562	19.01	911.7	0.02000	Open
X44	Valve	REGULAR	0.00	0.00	N/A	N/A	24.77	N/A	N/A	Closed By User

#### Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Liquid Mass (lbm)	Net Vol. Flow (gal/min)	Net Mass Flow (lbm/sec)
1	TW-1B	Infinite	N/A	1,773	14.70	N/A	N/A	-10.00	-1.390
2	TW-2B	Infinite	N/A	1,773	14.70	N/A	N/A	-15.00	-2.084
3	TW-3B	Infinite	N/A	1,773	14.70	N/A	N/A	-20.00	-2.779
4	TW-4B	Infinite	N/A	1,773	14.70	N/A	N/A	-20.00	-2.779
5	TW-5B	Infinite	N/A	1,773	14.70	N/A	N/A	-10.00	-1.390
19	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	0.00	0.000
43	EQ Tank	Infinite			14.70	N/A	N/A	75.00	10.422

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 8 (Pump 3B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 9 (Pump 4B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

<sup>\*\*\*</sup>CAUTION\*\*\* The performance of Pump Junction 10 (Pump 5B) may be affected by the fluid viscosity. Apply the Viscosity Correction on the Pump Property window and rerun the model to assess the impact of the fluid viscosity.

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

#### Pipe Output Table

Pipe	Name	Vol. Flow Rate	Pipe	Velocity	P Static Max	P Static Min	Elevation Inlet	Elevation Outlet	dP Stag. Total	dP Static Total
		(gal/min)	Nominal Size	(feet/sec)	(psia)	(psia)	(feet)	(feet)	(psid)	(psid)
1	Pipe	10.00	12 inch	0.02866	18.16	18.16	1,765	1,765	6.125E-08	6.125E-08
2	Pipe	15.00	12 inch	0.04299	18.16	18.16	1,765	1,765	2.114E-07	2.114E-07
3	Pipe	20.00	12 inch	0.05733	18.16	18.16	1,765	1,765	4.068E-07	4.068E-07
4	Pipe	20.00	12 inch	0.05733	18.16	18.16	1,765	1,765	4.068E-07	4.068E-07
5	Pipe	10.00	12 inch	0.02866	18.16	18.16	1,765	1,765	6.125E-08	6.125E-08
6	Pipe	10.00	1-1/4 inch	2.14502	116.12	48.69	1,765	1,918	6.743E+01	6.743E+01
7	Pipe	15.00	1-1/4 inch	3.21753	119.02	50.37	1,765	1,918	6.865E+01	6.865E+01
8	Pipe	20.00	1-1/4 inch	4.29004	121.83	51.58	1,765	1,918	7.025E+01	7.025E+01
9	Pipe	20.00	1-1/4 inch	4.29004	119.61	49.36	1,765	1,918	7.025E+01	7.025E+01
10	Pipe	10.00	1-1/4 inch	2.14502	114.23	46.80	1,765	1,918	6.743E+01	6.743E+01
11	Pipe	10.00	None	2.27499	48.67	46.59	1,918	1,918	2.086E+00	2.086E+00
12	Pipe	15.00	None	3.41249	50.34	46.73	1,918	1,918	3.610E+00	3.610E+00
13	Pipe	20.00	None	4.54999	51.52	46.88	1,918	1,918	4.648E+00	4.648E+00
14	Pipe	20.00	None	4.54999	49.31	46.85	1,918	1,918	2.461E+00	2.461E+00
15	Pipe	10.00	1-1/4 inch	2.14502	46.58	40.40	1,918	1,932	6.180E+00	6.180E+00
19	Pipe	10.00	1-1/4 inch	2.14502	40.40	40.36	1,932	1,932	3.612E-02	3.612E-02
20	Pipe	10.00	None	2.27499	46.79	46.39	1,918	1,918	4.012E-01	4.012E-01
21	Pipe	15.00	1-1/4 inch	3.21753	46.72	40.41	1,918	1,932	6.303E+00	6.303E+00
22	Pipe	15.00	1-1/4 inch	3.21753	40.41	40.34	1,932	1,932	7.411E-02	7.411E-02
23	Pipe	20.00	1-1/4 inch	4.29004	46.85	40.38	1,918	1,932	6.465E+00	6.465E+00
24	Pipe	20.00	1-1/4 inch	4.29004	40.38	40.26	1,932	1,932	1.237E-01	1.237E-01
25	Pipe		1-1/4 inch	4.29004	46.82	40.36	1,918	1,932	6.465E+00	6.465E+00
26	Pipe	20.00	1-1/4 inch	4.29004	40.36	40.23	1,932	1,932	1.237E-01	1.237E-01
27	Pipe	10.00	1-1/4 inch	2.14502	46.38	40.20	1,918	1,932	6.180E+00	6.180E+00
28	Pipe	10.00	1-1/4 inch	2.14502	40.20	40.17	1,932	1,932	3.612E-02	3.612E-02
30	Pipe	10.00	1-1/4 inch	2.14502	40.35	40.35	1,932	1,932	6.988E-03	6.988E-03
31	Pipe	25.00	2 inch	2.39028	40.32	40.31	1,932	1,932	5.118E-03	5.118E-03
32	Pipe	45.00	2 inch	4.30250	40.17	40.15	1,932	1,932	1.456E-02	1.456E-02
33	Pipe		2-1/2 inch	4.35573	40.10	40.09	1,932	1,932	1.198E-02	1.198E-02
34	Pipe		3 inch	3.26443	40.13	21.16	1,932	1,954	1.897E+01	1.897E+01
35	Pipe		2 inch	0.00000	24.77	24.77	1,938	1,938	0.000E+00	0.000E+00
36	Pipe		3 inch	0.00000	17.29	16.00	1,938	1,941	1.299E+00	1.299E+00
40	Pipe		2 inch	7.08950	24.18	19.01	1,938	1,943	5.174E+00	5.174E+00
41	Pipe	75.00	2 inch	7.17084	19.24	18.99	1,943	1,942	-2.515E-01	-2.515E-01
42	Pipe	75.00	3 inch	3.26443	24.69	21.16	1,954	1,938	-3.538E+00	-3.538E+00

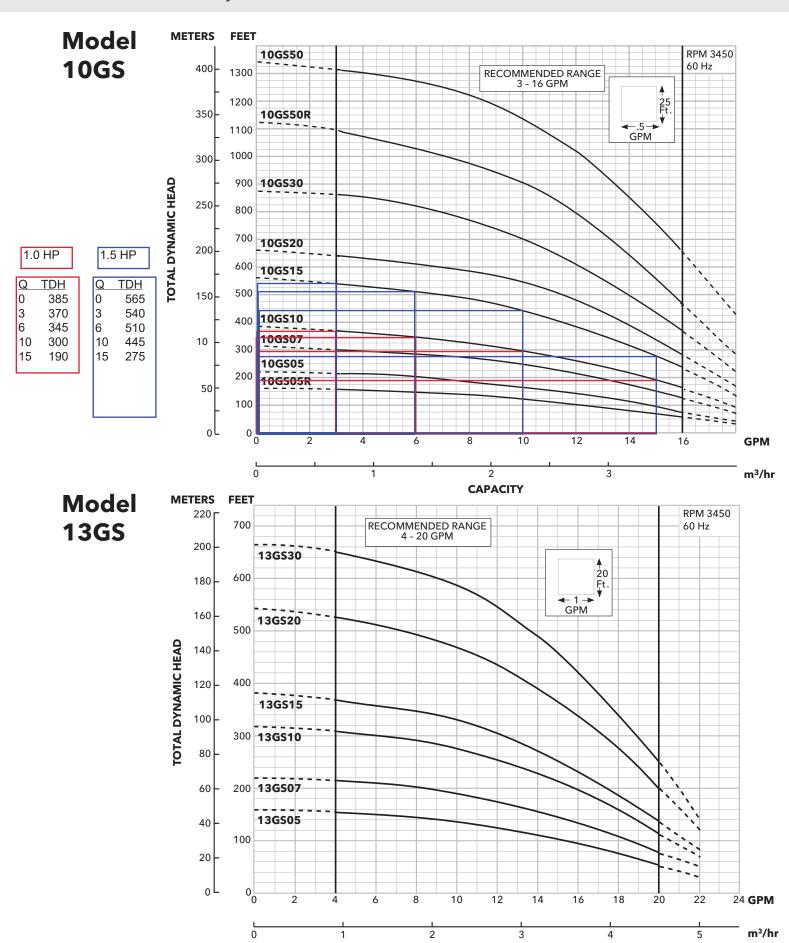
AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

	15		D 0: .:	D 0: 11	D 0:	D 0:
Pipe	dP Gravity	dH	P Static In	P Static Out	P Stag. In	P Stag. Out
1 ipe	(psid)	(feet)	(psia)	(psia)	(psia)	(psia)
1	0.0000	1.414E-07	18.16	18.16	18.16	18.16
2	0.0000	4.880E-07	18.16	18.16	18.16	18.16
3	0.0000	9.391E-07	18.16	18.16	18.16	18.16
4	0.0000	9.391E-07	18.16	18.16	18.16	18.16
5	0.0000	1.414E-07	18.16	18.16	18.16	18.16
6	66.2704	2.680E+00	116.12	48.69	116.15	48.72
7	66.2704	5.499E+00	119.02	50.37	119.09	50.44
8	66.2704	9.185E+00	121.83	51.58	121.95	51.70
9	66.2704	9.185E+00	119.61	49.36	119.73	49.49
10	66.2704	2.680E+00	114.23	46.80	114.26	46.83
11	0.0000	4.817E+00	48.67	46.59	48.71	46.62
12	0.0000	8.335E+00	50.34	46.73	50.42	46.81
13	0.0000	1.073E+01	51.52	46.88	51.66	47.02
14	0.0000	5.681E+00	49.31	46.85	49.45	46.99
15	6.0640	2.677E-01	46.58	40.40	46.61	40.43
19	0.0000	8.338E-02	40.40	40.36	40.43	40.40
20	0.0000	9.263E-01	46.79	46.39	46.82	46.42
21	6.0640	5.526E-01	46.72	40.41	46.79	40.48
22	0.0000	1.711E-01	40.41	40.34	40.48	40.41
23	6.0640	9.269E-01	46.85	40.38	46.97	40.51
24	0.0000	2.857E-01	40.38	40.26	40.51	40.39
25	6.0640	9.269E-01	46.82	40.36	46.95	40.48
26	0.0000	2.857E-01	40.36	40.23	40.48	40.36
27	6.0640	2.677E-01	46.38	40.20	46.41	40.23
28	0.0000	8.340E-02	40.20	40.17	40.23	40.20
30	0.0000	1.613E-02	40.35	40.35	40.39	40.38
31	0.0000	1.182E-02	40.32	40.31	40.36	40.35
32	0.0000	3.361E-02	40.17	40.15	40.29	40.28
33	0.0000	2.767E-02	40.10	40.09	40.23	40.22
34	9.5291	2.181E+01	40.13	21.16	40.20	21.23
35	0.0000	0.000E+00	24.77	24.77	24.77	24.77
36	1.2994	0.000E+00	17.29	16.00	17.29	16.00
40	2.1657	6.946E+00	24.18	19.01	24.52	19.35
41	-0.4331	4.194E-01	18.99	19.24	19.34	19.59
42	-6.9302	7.831E+00	21.16	24.69	21.23	24.77

All Junction Table

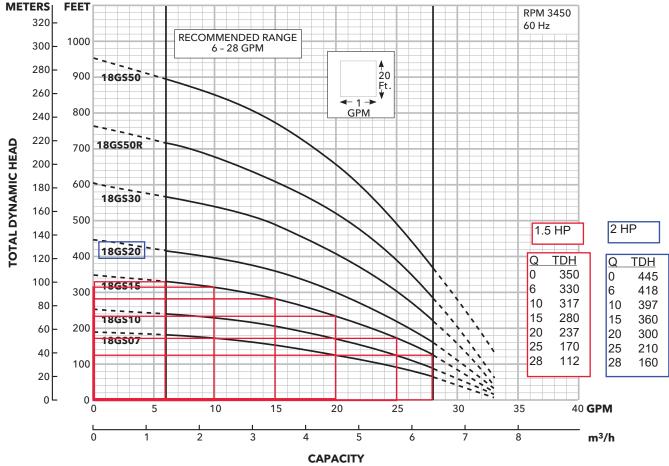
AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Mass Flow Rate Thru Jct (lbm/sec)	Loss Factor (K)
1	TW-1B	14.70	18.16	14.70	18.16	10.00	1.390	1.84618
2	TW-2B	14.70	18.16	14.70	18.16	15.00	2.084	1.04880
3	TW-3B	14.70	18.16	14.70	18.16	20.00	2.779	0.50000
4	TW-4B	14.70	18.16	14.70	18.16	20.00	2.779	0.50000
5	TW-5B	14.70	18.16	14.70	18.16	10.00	1.390	1.84618
6	Pump 1B	18.16	116.12	18.16	116.15	10.00	1.390	0.00000
7	Pump 2B	18.16	119.02	18.16	119.09	15.00	2.084	0.00000
8	Pump 3B	18.16	121.83	18.16	121.95	20.00	2.779	0.00000
9	Pump 4B	18.16	119.61	18.16	119.73	20.00	2.779	0.00000
10	Pump 5B	18.16	114.23	18.16	114.26	10.00	1.390	0.00000
11	Bend	48.69	48.67	48.72	48.71	10.00	1.390	0.30072
16	Tee or Wye	24.69	24.69	24.77	24.77	N/A	N/A	See Mult. Losses
17	Valve	19.01	18.99	19.35	19.34	75.00	10.422	0.02000
19	Cell 1	14.70	16.00	14.70	16.00	0.00	0.000	0.00000
20	Flowmeter	40.40	40.40	40.43	40.43	10.00	1.390	0.00000
21	Bend	50.37	50.34	50.44	50.42	15.00	2.084	0.30072
22	Bend	51.58	51.52	51.70	51.66	20.00	2.779	0.30072
23	Bend	49.36	49.31	49.49	49.45	20.00	2.779	0.30072
24	Bend	46.80	46.79	46.83	46.82	10.00	1.390	0.30072
25	Bend	46.59	46.58	46.62	46.61	10.00	1.390	0.30296
26	Bend	46.73	46.72	46.81	46.79	15.00	2.084	0.30296
27	Bend	46.88	46.85	47.02	46.97	20.00	2.779	0.30296
28	Bend	46.85	46.82	46.99	46.95	20.00	2.779	0.30296
29	Bend	46.39	46.38	46.42	46.41	10.00	1.390	0.30296
30	Bend	40.36	40.35	40.40	40.39	10.00	1.390	0.30072
31	Flowmeter	40.41	40.41	40.48	40.48	15.00	2.084	0.00000
34	Flowmeter	40.38	40.38	40.51	40.51	20.00	2.779	0.00000
36	Flowmeter	40.36	40.36	40.48	40.48	20.00	2.779	0.00000
38	Flowmeter	40.20	40.20	40.23	40.23	10.00	1.390	0.00000
39	Tee or Wye	40.31	40.31	40.36	40.36	N/A	N/A	See Mult. Losses
40	Tee or Wye	40.20	40.20	40.29	40.29	N/A	N/A	See Mult. Losses
41	Tee or Wye	40.10	40.10	40.23	40.23	N/A	N/A	See Mult. Losses
42	Tee or Wye	40.13	40.13	40.20	40.20	N/A	N/A	See Mult. Losses
43	EQ Tank	14.70	19.24	14.70	19.24	75.00	10.422	1.00000
X44	Valve	24.77	17.29	24.77	17.29	0.00	0.000	0.00000
45	FM High Point	21.16	21.16	21.23	21.23	75.00	10.422	0.00000

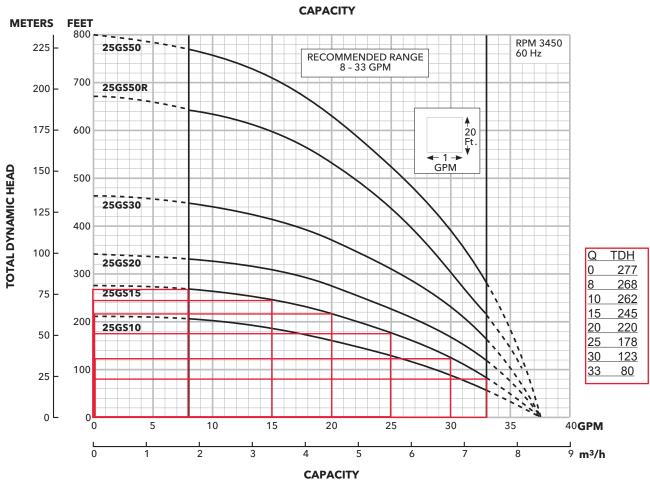


**CAPACITY** 

## Model 18GS



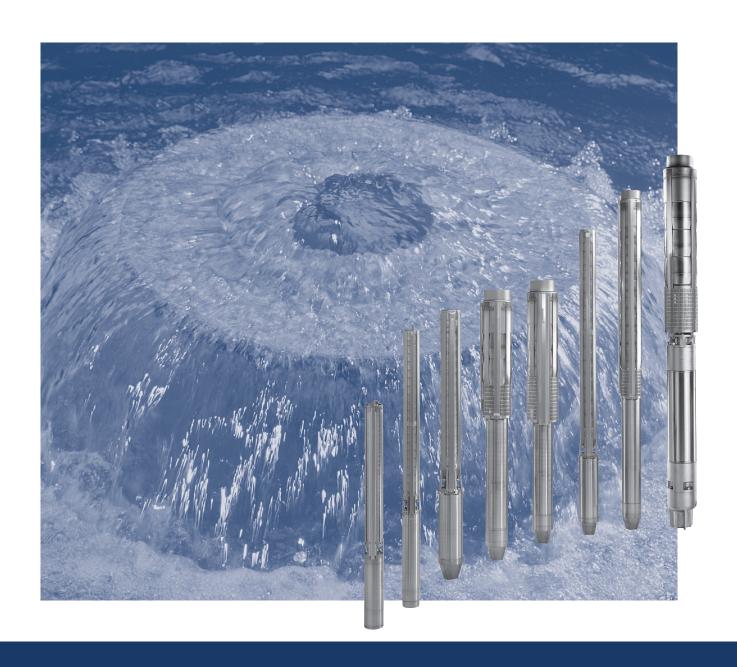
## Model 25GS



## GRUNDFOS PRODUCT GUIDE

## SP

Submersible pumps, motors, and accessories 60 Hz



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#### 1. Product introduction

#### Introduction

The Grundfos SP range of submersible pumps is renowned for high efficiency and reliability. Made entirely of corrosion resistant stainless steel, SP pumps are ideal for a wide variety of applications.

Grundfos SP pumps represent state-of-the-art hydraulic design. Built to deliver optimum efficiency during periods of high demand, SP pumps provide low long-term costs and high operating reliability regardless of the application.

The SP range offers high efficiency, high resistance to sand and other abrasives, motor burnout protection, and easy maintenance. A complete monitoring and control system is available for constant optimization of the pumping system.



Fig. 1 Grundfos SP pumps

#### **Applications**

Grundfos Large SP submersible pumps are suitable for:

- · Groundwater supply to waterworks
- Irrigation in horticulture and agriculture
- Groundwater lowering (dewatering)
- Pressure boosting
- Industrial applications
- Domestic water supply.

#### **Pumped liquids**

Grundfos SP pumps are suitable for pumping clean, thin, non-aggressive liquids without solid particles or fibers.

SP offers stainless steel construction which ensures good wear resistance and a reduced risk of corrosion where the water has minor chloride content.

Optional, upgraded stainless steel construction is available for pumping more aggressive liquids:

A complete range of zinc anodes for cathodic protection is available; see p. 97 for applications (for example, sea water applications).

For slightly polluted liquids (for example, containing oil), Grundfos offers a complete range of stainless steel SP NE pumps with all rubber parts made of FKM.

#### Features and benefits

Grundfos SP submersible pumps offer these features and benefits:

- State-of-the-art hydraulics provide high efficiency and low operating costs
- 100 % stainless steel components inside and outside for long service life
- Sand resistant
- Resistant to aggressive water
- · Dry-running protection
- Monitoring, protection and communication via protection unit MP204, and remote control, R100.

TM00 7301 1096

FM00 7302 1096

#### A wide pump range

Grundfos offers energy-efficient SP submersible pumps with a performance range of up to 1,400 gpm and 2,100 ft of head.

The pump range consists of many pump sizes, and each pump size is available with an optional number of stages to match any duty point.

#### High pump efficiency

Often pump efficiency is given less consideration than the price of a pump; however, owners who choose efficiency will find substantial savings in energy costs over time. See fig. 2 for an illustration of SP efficiencies in relation to flow.

#### Example

For example, a pump and motor with a 10 % higher efficiency than a cheaper, less efficient pump, can save its owner more than \$80,000.00 over 10 years\*.

\* If producing 880 gpm at 325 ft of head for 10 years @ 13.8 cents per kWh. U.S. kWh costs range from 6 cents to more than 20 cents, depending on region.

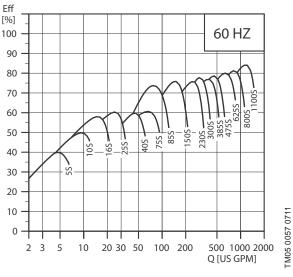


Fig. 2 SP pump/motor efficiencies in relation to flow

#### Pump design

Grundfos SP submersible pumps feature components that contribute to the superior performance and durability of the range.

#### Lower installation costs

Stainless steel means low weight for ease in the handling of pumps, resulting in lower equipment costs and reduced installation and service time.

#### Bearings with sand channels

All bearings are water-lubricated and have a squared shape enabling sand particles, if any, to leave the pump together with the pumped liquid.



Fig. 3 Bearing

Inlet strainer

The inlet strainer prevents particles over a certain size from entering the pump.



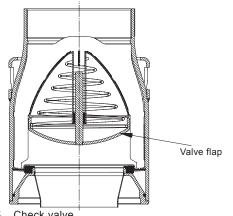
Fig. 4 Fig. Inlet straine

#### Non-return valve

All pumps are equipped with a reliable check valve in the valve casing preventing back flow in connection with pump stoppage.

Furthermore, the short closing time of the check valve means that the risk of destructive water hammer is reduced to a minimum.

The valve casing is designed for optimum hydraulic properties to minimize the pressure loss across the valve and thus to contribute to the high efficiency of the pump.



Check valve

#### **Priming screw**

All Grundfos 4" pumps are fitted with a priming screw. Consequently, dry running is prevented, because the priming screw will make sure that pump bearings are always lubricated.

Due to the semi-axial impellers of large SP pumps this priming is provided automatically.

However, it applies to all pump types that if the water table is lowered to a level below the pump inlet neither pump nor motor will be protected against dry running.



FM00 7304 1096

Fig. 6 Priming screw

#### Stop ring

The stop ring prevents damage to the pump during transport and in case of up-thrust in connection with start-up.

The stop ring, which is designed as a thrust bearing, limits axial movements of the pump shaft.

#### Example: SP 385S

The stationary part of the stop ring (A) is secured in the upper intermediate chamber.

The rotating part (B) is fitted above the split cone (C).

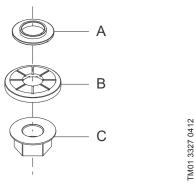


Fig. 7 Stop ring (rotating and stationary part) and the split cone

#### **Grundfos submersible motors**

#### A complete motor range

Grundfos offers a complete submersible motor range in different voltages. For an overview of motor types, sizes and voltages, see page 85.

MS 402 is designed for the domestic ground water market and covers outputs. The MS 4000 and MS6 series are designed for use in a variety of applications in water supply. When equipped with features like oversized motor, temperature measurement, cooling jacket, and SiC/SiC mechanical shaft seals, these motors are suitable for heavy-duty industrial applications such as dewatering operations.

As a standard, all external surfaces of the Grundfos MS motors in contact with water are made of AISI 304 stainless steel. For aggressive water, such as seawater or brackish water, R-versions made of AISI 904 are available.

#### Grundfos rewindable MMS motor range

Grundfos MMS motors are suitable for any submersible installation, including heavy-duty industrial applications and dewatering operations (when equipped with temperature control, oversized motor, cooling jacket, and SiC/ SiC mechanical shaft seals).

As a standard the MMS motors are supplied with black cast-iron end-bells. Optionally, the range is available in all-stainless steel AISI 316 or AISI 904 versions.

The 2-pole Grundfos MMS submersible motors are all easy to rewind. The windings of the stator are made of a special water-proof wire of pure electrolytic copper sheathed with special non-hydroscopic thermoplastic material. The fine dielectric properties of this material allow direct contact between the windings and the liquid for efficient cooling of the windings.



Fig. 8 Grundfos MS motors

FM00 7305 1096 - GrA4011 - GrA4013



Fig. 9 Grundfos MMS motors

## Industrial submersible motors and MS6 T60-versions

For heavy-duty applications Grundfos offers a complete motor range of industrial motors with up to 5 % higher efficiency than that of Grundfos' standard motors. The industrial motors are available in sizes as from 3 Hp up to 30 Hp.

The cooling of the motor is very efficient due to the large motor surface. The efficient cooling makes it possible to increase the liquid temperature to 140 °F (60 °C) at a minimum flow of 0.49 ft/s (0.15 m/s) past the motor.

The industrial motors are for customers who value low operating costs and long life higher than price.

Grundfos industrial motors are developed for difficult operating conditions. These motors will stand a higher thermal load than standard motors and thus have a longer life when subjected to high load. This applies whether the high load is caused by bad power supply, hot water, bad cooling conditions, high pump load etc. Please note that heavy duty motors are longer than motors for standard conditions.

#### Overtemperature protection

Accessories for protection against overtemperature are available for both Grundfos MS and MMS submersible motors. When the temperature becomes too high, the protection device will cut out and damage to the pump and motor be avoided.

Restart of the motor after cut-out can be achieved in two ways:

- · manual restart
- · automatic restart.

Automatic restart means that the MP 204 attempts to restart the motor after 15 minutes. If the first attempt is not successful, restarting will be reattempted at 30-minute intervals.

#### MS

TM01 7873 4799

The Grundfos MS submersible motors (with the exception of MS 402) are available with a built-in Tempcon temperature transmitter for protection against overtemperature. By means of the transmitter, it is possible to read out and/or monitor the motor temperature via an MP 204 or a PR 5714 relay.

The Grundfos MS6 submersible motors can be fitted with a Pt100. The Pt100 is fitted in the motor and connected directly to the MP 204 or monitored by the PR 5714 relay.

#### **MMS**

For the protection of the Grundfos MMS submersible motors against overtemperature Grundfos offers the Pt100 temperature sensor as an optional extra.

The Pt100 is fitted in the motor and connected directly to the MP 204 or monitored by the PR 5714 relay.

#### Protection against upthrust

In case of a very low counter pressure in connection with start-up there is a risk that the entire chamber stack may rise. This is called upthrust. Upthrust may damage both pump and motor. Both Grundfos pumps and motors are protected against upthrust as standard, preventing upthrust from occurring during the critical start-up phase. The protection consists of either a built-in stop ring or hydraulic balancing.

#### **Built-in cooling chambers**

In all Grundfos MS submersible motors, efficient cooling is ensured by cooling chambers at the top and at the bottom of the motor, and by an internal circulation of motor liquid.

See fig. 10. As long as the required flow velocity past the motor is maintained, cooling of the motor will be efficient.

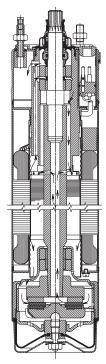


Fig. 10 MS 4000

#### Lightning protection

The smallest Grundfos submersible motors, such as the MS 402, are all insulated in order to minimize the risk of motor burnout caused by lightning strike.

TM00 5698 0996

#### Reduced risk of short-circuit

The embedded stator winding in the Grundfos MS submersible motor is hermetically enclosed in stainless steel. The result is high mechanical stability and optimum cooling. Also, this eliminates the risk of short-circuit of the windings caused by water condensation.

#### Shaft seal

#### MS 402

The shaft seal is of the lip seal type characterized by low friction against the rotor shaft.

The rubber material offers good wear resistance, good elasticity and resistance to particles, and it is approved for use in drinking water.

#### MS 4000, MS6

The material is ceramic/tungsten carbide providing optimum sealing, optimum wear resistance and long life.

The spring loaded shaft seal is designed with a large surface and a sand shield. The result is a minimum exchange of pumped and motor liquids and no penetration of particles.

Motors, version R, are supplied with a SiC/SiC shaft seal. Other combinations are available request. See fig. 11 and fig. 12 for an illustration of shaft seal components and configuration.

#### MMS rewindable motors

The standard shaft seal is a ceramic/carbon mechanical shaft seal. The shaft seal is replaceable.

The material features good wear resistance and resistance to particles.

Together with the shaft seal housing, the sand shield forms a labyrinth seal, which during normal operating conditions prevents penetration of sand particles into the shaft seal.

On request, motors can be supplied with a SiC/SiC



Fig. 11 Shaft seal, MS 4000



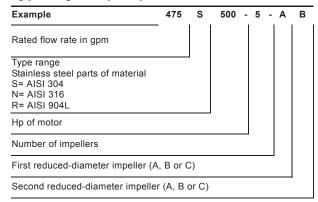
Fig. 12 Shaft seal, MS6



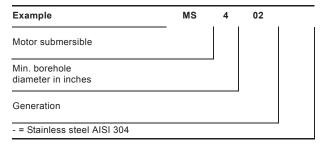
TM03 9225 3607

## Identification

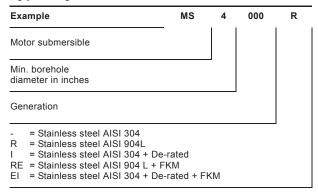
#### Type key, SP pumps



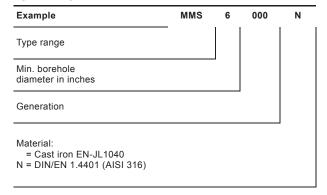
#### Type key, MS 402 motors



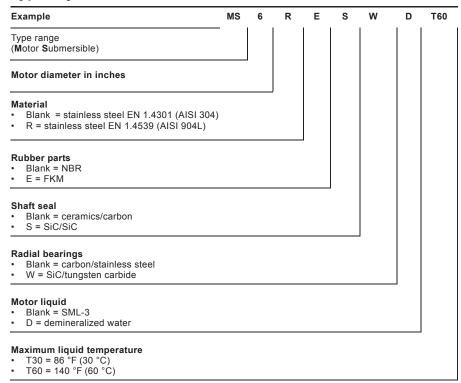
#### Type key, MS 4000 motors



#### Type key, MMS motors

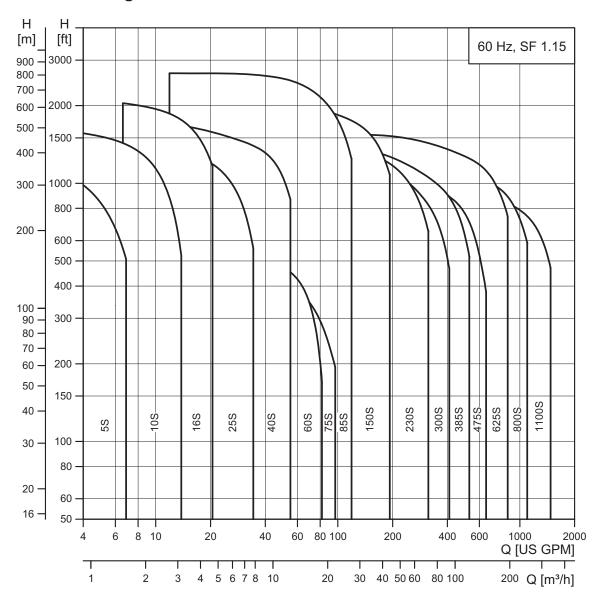


#### Type key, MS6 motors



## 2. Product overview

### Performance range 60 Hz



TM05 0056 0112

## Pump range

Туре		58	10S	16S	25S	40S	60S	75S	85S	150S	230S	300S	385S	475S	625S	800S	1100S
AISI 304 stainless	s steel	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
AISI 304 stainless steel AISI 316 stainless steel AISI 904L stainless steel				•	•	•		•	•	•	•	•	•	•	•	•	•
AISI 904L stainles	ss steel				•	•			•	•	•	•	•	•	•	•	•
Connection ★	NPT	1"	1.25"	1.25"	1.5"	2"	2"	2"	(3")	(3")	3" (4")	3" 4"	5"	5"	6"	6"	6"
Flange connectio Grundfos flange	n:												5"	5"	6"	6"	6"

 $<sup>\</sup>bigstar$  Figures in brackets ( ) indicate connection for pumps with sleeve.

### **Motor range**

Motor output [hp]	0.5	0.75	1.0	1.5	1.5	3.0	5.0	7.5	10.0	15	20	25	30	40	50	60	75	100	125	150	175	200	250
Single-phase	•	•	•	•	•	•																	
Three-phase	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Industrial motor and MS6 T60-versions						•	•	•	•	•	•	•	•										
Rewindable motor							•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Steel: AISI 304	•	•	•	•	•	•	•	•	•	•	•	•	•	•									
Steel: AISI 304 and cast iron							•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Steel: AISI 316							•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Steel: AISI 904L			•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•			
Built-in temperature transmitter in motor			•	•	•	•	•	•	•	•	•	•	•	•									

Direct-on-line starting is recommended up to 100 hp.

Soft starter or autotransformer is recommended above 100 hp.

Motors with star/delta are available from 7.5 hp.

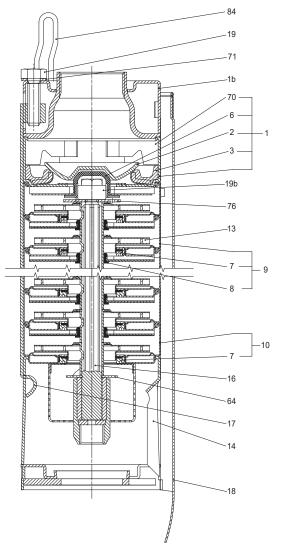
## Motor protection and controllers

Motor output [hp]	0.5	0.75	1.0	1.5	1.5	3.0	5.0	7.5	10.0	15	20	25	30	40	50	60	75	100	125	150	175	200	250
MP 204	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Pt100							•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Zinc anode				•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Vertical flow sleeve	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
Horizontal flow sleeve	•	•	•	•	•	•		•	•	•	•	•	•	•									
SA-SPM	•	•	•	•	•	•	•																
R100	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
RS-485 communication module	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•
G100	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•

Motor protection of single-phase motors, see page 85.

## 3. Construction

## Sectional drawing, SP pump, 4"



TM00 5606 1907

Fig. 13 SP pump, 4"

### Material specification, SP pump, 4"

	•		•			
Pos.	Component	Materials -	Standard			
1 03.	Component	materials	AISI			
1	Valve casing	Stainless steel	304			
1b	Discharge piece	Stainless steel	304			
2	Valve cup	Stainless steel	304			
3	Valve seat	Stainless steel/NBR	304			
6	Top bearing	NBR				
7	Neck ring	NBR/PBT				
8	Intermediate ring	NBR				
9	Intermediate chamber	Stainless steel	304			
10	Bottom intermediate chamber	Stainless steel	304			
13	Impeller	Stainless steel	304			
14	Suction interconnector	Stainless steel	304			
16	Shaft	Stainless steel	304			
17	Strap	Stainless steel	304			
18	Cable guard	Stainless steel	304			
19	Hexagon screw	Stainless steel	304			
19a	Nut	Stainless steel	316			
19b	Nut	Stainless steel	304			
20	Motor cable					
64	Priming disc	Stainless steel	304			
70	Valve guide	Stainless steel	304			
71	Washer for pos. 19	Stainless steel	316			
76	Washer	Stainless steel	304			
78	Nameplate	Stainless steel	316			
84	Hook	Stainless steel	304			
_						

## Sectional drawing, SP pump, 6"

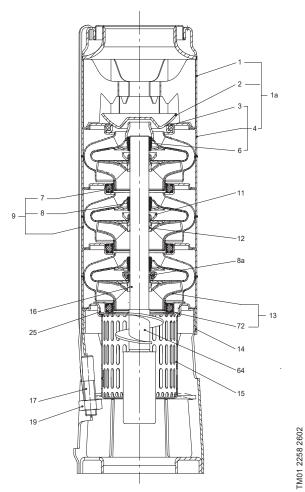
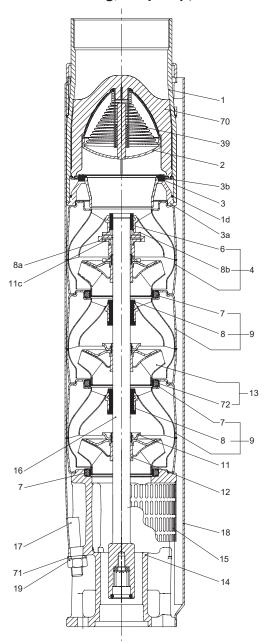


Fig. 14 SP pump, 6"

## Material specification, SP pump, 6"

_			Standard	N-version	R-version
Pos.	Component	Materials		AISI	
		Valve cas	sing		
1	Valve casing	Stainless steel	304	316	904 L
2	Valve cup	Stainless steel	304	316	904 L
3	Valve seat	Stainless steel	304	316	904 L
4	Top chamber	Stainless steel	304	316	904 L
		Chamber s	stack		
7	Neck ring	NBR/PPS			
8	Bearing	NBR			
8a	Spacing washer	Carbon/ graphite HY22 in PTFE mass			
9	Chamber	Stainless steel	304	316	904 L
11	Nut for split cone	Stainless steel	304	316	904 L
12	Split cone	Stainless steel	304	316	904 L
13	Impeller	Stainless steel	304	316	904 L
16	Shaft with coupling	Stainless steel	431	329	Si 31 803
18	Cable guard	Stainless steel	304	316	904 L
23	Rubber guard	NBR			
25	Neck ring retainer	Stainless steel	304	316	904 L
64	Priming screw	Stainless steel	304	316	904 L
72	Wear ring	Stainless steel	304	316	904 L
		Suction interc	onnector		
14	Suction interconnector	Stainless steel	304	316	904 L
	Intermediate piece for 6" motor over 40 Hp	Stainless steel	316	316	316
15	Strainer	Stainless steel	304	316	904 L
17	Strap	Stainless steel	304	316	904 L
19	Nut for strap	Stainless steel	304	316	904 L
19a	Nut	Stainless steel	316	316	316
20	Motor cable				
78	Nameplate	Stainless steel	316	316	316
		Pumps in s	leeve		
	Clamping flange (counter)	Stainless steel	304	316	904 L
	Clamping flange	Stainless steel	304	316	904 L
	Connecting piece	Stainless steel	304	316	904 L
	Sleeve	Stainless steel	304	316	904 L
	Stay bolt	Stainless steel	304	316	904 L
	Hexagon socket head screw	Stainless steel	304	316	904 L

## Sectional drawing, SP pump, 8"



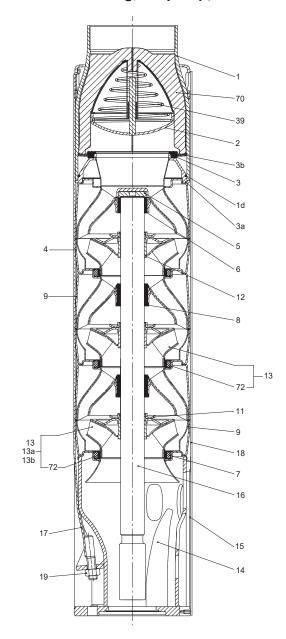
TM01 2359 2301

Fig. 15 SP pump, 8"

## Material specification, SP pump, 8"

			<u> </u>	• •	
Pos	Component	Materials	Standard	N-version	R-version
F U 3.	Component	Materials		AISI	
1	Valve casing	Stainless steel	304	316	904L
1d	O-ring	NBR			
2	Valve cup	Stainless steel	304	316	904L
3	Valve seat	Standard/ N- version: NBR R-version: FKM			
3а	Lower valve seat retainer	Stainless steel	316	316	(DIN 1.4517)
3b	Upper valve seat retainer	Stainless steel	304	316	904L
4	Top chamber	Stainless steel	304	316	904L
6	Upper bearing	Stainless steel/NBR	304	316	904L
7	Neck ring	NBR/PPS			
8	Bearing	NBR			
8a	Washer for stop ring	Carbon/ graphite HY22 in PTFE mass			
8b	Stop ring	Stainless steel	316	316	904L
9	Chamber	Stainless steel	304	316	904L
11	Split cone nut	Stainless steel	304	316	904L
11c	Nut for stop ring	Stainless steel	316	316	904L
12	Split cone	Stainless steel	304	316	904L
13	Impeller	Stainless steel	304	316	904L
14	Suction inter- connector	Stainless steel	CF8M	A744 CD4-MCu	(DIN 1.4517)
15	Strainer	Stainless steel	304	316	904L
16	Shaft complete	Stainless steel	431	329	329
17	Strap	Stainless steel	304	316	904L
18	Cable guard	Stainless steel	304	316	904L
19	Nut for strap	Stainless steel	304	316	904L
39	Spring for valve cup	Stainless steel	304	316	SAF 2205
70	Valve guide	Stainless steel	304	316	904L
71	Washer	Stainless steel	316	316	904L
72	Wear ring	Stainless steel	304	316	904L

## Sectional drawing, SP pump, 10"



TM01 2363 2701

Fig. 16 SP pump, 10"

## Material specification, SP pump, 10"

Pos.	Description	Material	Standard	N version	
Pos.	Description	wateriai	AISI		
		Valve casing			
1	Valve casing	Stainless steel	304	316	
1d	O-ring	NBR			
2	Valve cup	Stainless steel	304	316	
3	Valve seat	Stainless steel	304	316	
3a	Lower valve seat retainer	Stainless steel	304	316	
3b	Upper valve seat retainer	Stainless steel	304	316	
39	Spring for valve cup	Stainless steel	301	316	
70	Valve guide	Stainless steel	304	316	
78	Nameplate	Stainless steel	304	316	
79	Rivet	Stainless steel	304	316	
63	Connecting piece	Stainless steel	304	316	
		Chamber stack		_	
4	Top chamber	304	316		
5	Upthrust disc	Carbon/ graphite HY22 in PTFE mass			
6	Top bearing	Stainless steel/ NBR	304	316	
7	Neck ring	NBR/PPS			
8	Bearing	NBR			
9	Chamber	Stainless steel	304	316	
11	Nut for split cone	Stainless steel	304	316	
12	Split cone	Stainless steel	304	316	
13	Impeller	Stainless steel	304	316	
16	Shaft with coupling	Stainless steel	431	329	
18	Cable guard	Stainless steel	304	316	
18a, 18b	Screw for cable guard	Stainless steel	304	316	
23	Rubber guard	NBR			
72	Wear ring	Stainless steel	304	316	
	Suc	ction interconnector			
14	Suction interconnector	Stainless steel	304	316	
15	Strainer	Stainless steel	304	316	
17	Strap	Stainless steel	ss steel 304		
19	Nut for strap	Stainless steel	304	316	
19a	Nut	Stainless steel	316	316	
20	Motor cable				
22	Bolts	Stainless steel	316	316	
28, 28a	Lock for strainer	Stainless steel	329	329	

## Sectional drawing - MS motors

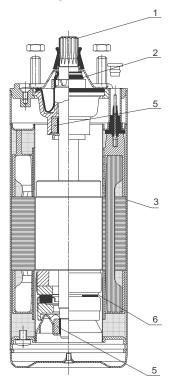


Fig. 17 MS 402 motor

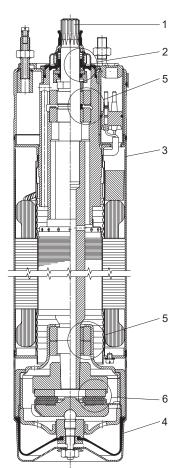


Fig. 18 MS 4000 motor

## Material specification, MS 402 and MS 4000 motors

Boo	Part	MS 402	MS 4000
F05.	rait	A	ISI
1	Shaft	431	431
2	Shaft seal	NBR	Tungsten carbide/ ceramic
3	Motor sleeve	304	304
4	Motor end shield		304
5	Radial bearing	Ceramic	Ceramic/ tungsten carbide
6	Axial bearing	Ceramic/carbon	Ceramic/carbon
	Rubber parts	NBR	NBR

## R-version motor

Pos.	Part	MS 4000			
1	Shaft 318 LN				
2	Shaft seal NBR/ceramic				
3	Motor sleeve	904L			
4	Motor end shield	904L			
5	Radial bearing	Ceramic/tungsten carbide			
6	Thrust bearing	Ceramic/carbon			
	Rubber parts	NBR			

TM00 7865 2196

## Sectional drawing - MS6 motors

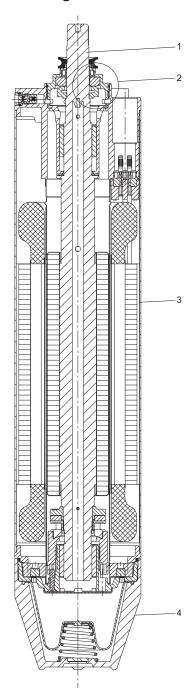


Fig. 19 MS6 motor

## Material specification - MS6 motors

Pos.	Part	MS6
202	Shaft with rotor	318LN
2	Shaft seal	Ceramic/carbon
3	Motor sleeve	304
4	Motor end cover	304
	Rubber parts	NBR/FKM

## R-version motor

Pos.	Part	MS6
1	Shaft	318LN
2	Shaft seal	SiC/SiC
3	Motor sleeve	904L
4	Motor end cover	(DIN 1.4517)
	Rubber parts	FKM

## Sectional drawing - MMS motors

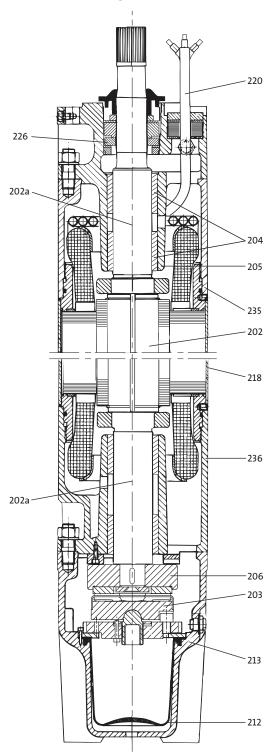


Fig. 20 MMS 10000

## **Material specification**

## MMS motors, submersible rewindable versions

_				4101	
Pos.	Component		Material	AISI	
202	Shaft		Steel	(EN 1.0533)	
202a	Shaft ends		Stainless steel	316/329	
203/	Thrust bearing	6", 0.5 - 20 Hp	Hardened steel/ EPDM		
206	Stationary/ rotating part	6", 25 - 50 Hp	Ceramic/		
	retaining part	8" - 10"	carbon		
204	Bearing bush	6" - 10"	Carbon		
205	Bearing housing,	upper	Cast iron A126 Cla		
212	Diaphragm		CR		
213	Motor end shield		Cast iron	A126 Class B	
218	Motor sleeve		Stainless steel	304	
220	Motor cable		EPDM		
226	Shaft seal		Ceramic/ carbon		
235	Intermediate hous	sing	Cast iron	A126 Class B	
236	Bearing housing,	lower	Cast iron	A126 Class B	

## MMS motors, N- and R-versions

				Version		
Pos.	Component		Material	N	R*	
				AISI		
202	Shaft		Steel	(EN 1.0533)	(EN 1.0533)	
202a	Shaft ends		Stainless steel	316/329	318LN	
203/	Thrust bearing	6", 0.5 - 20 Hp	Hardened steel/EPDM			
206	Stationary/ rotating part	6", 25 - 50 Hp	Ceramic/			
		8"-10"	carbon			
204	Bearing bush	6"-10"	Carbon			
205	Bearing housing,	upper	Stainless steel	316	904L	
212	Diaphragm		CR			
213	Motor end shield		Stainless steel	316	904L	
218	Motor sleeve		Stainless steel	316	904L	
220	Motor cable	Motor cable		EPDM		
226	Shaft seal		Ceramic/ carbon			
235	Intermediate housing		Stainless steel	316	904L	
236	Bearing housing,	lower	Stainless steel	316	904L	

<sup>\*</sup> Only MMS 6000 and MMS 8000 are available in R-versions

TM01 4985 0404

# 4. C

## 4. Operating conditions

### **Operating conditions**

Flow rate, Q: 0.44 - 1475 gpm (0.1-335 m<sup>3</sup>/h).

Head, H: Maximum 2657 ft (810 m).

#### Maximum liquid temperature

	Installation					
Motor	Flow velocity past motor	Vertical [°F (°C)]	Horizontal [°F (°C)]			
Grundfos MS 4"and MS6 T30-versions	0.49 ft/s (0.15 m/s)	86 (30)	86 (30)			
Grundfos 4" MS industry versions	0.49 ft/s (0.15 m/s)	140 (60)	140 (60)			
Grundfos MS6 T60-versions	3.28 ft/s (1.0 m/s)	140 (60)	140 (60)			
Grundfos MMS 6" to 12" rewindable with	0.49 ft/s (0.15 m/s)	77 (25)	77 (25)			
PVC in the windings	1.64 ft/s (0.50 m/s)	86 (30)	86 (30)			
Grundfos MMS 6" to 12" rewindable with PE/PA	0.49 ft/s (0.15 m/s)	104 (40)	104 (40)			
in the windings	1.64 ft/s (0.50 m/s)	113 (45)	113 (45)			

**Note:** Note: For MMS 6000, 0.5 hp; MMS 8000, 150 hp; the maximum liquid temperature is 9  $^{\circ}$ F (5  $^{\circ}$ C) lower than the values stated in the table. For MMS 10000, 250 hp, the temperature is 18  $^{\circ}$ F (10  $^{\circ}$ C) lower.

#### Operating pressure

Motor	Maximum operating pressure
Grundfos MS 4" and 6"	
Grundfos MMS 6" to 10" rewindable	870 psi (6 Mpa) (60 bar)

#### **Curve conditions**

The conditions below apply to the curves shown on pages 20 - 84:

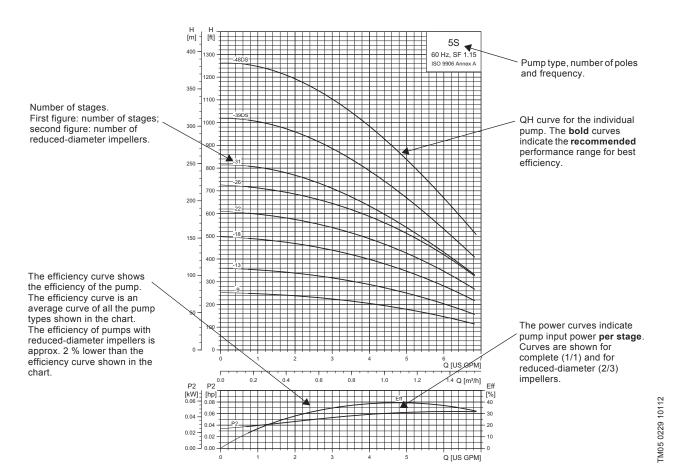
#### General

- Curve tolerances according to ISO 9906, Annex A.
- The performance curves show pump performance at actual speed, cf. standard motor range.
   The speeds of the motors are approximately these:

4" motors:  $n = 3470 \text{ min}^{-1}$ 6" motors:  $n = 3460 \text{ min}^{-1}$ 8" to 10" motors:  $n = 3525 \text{ min}^{-1}$ 

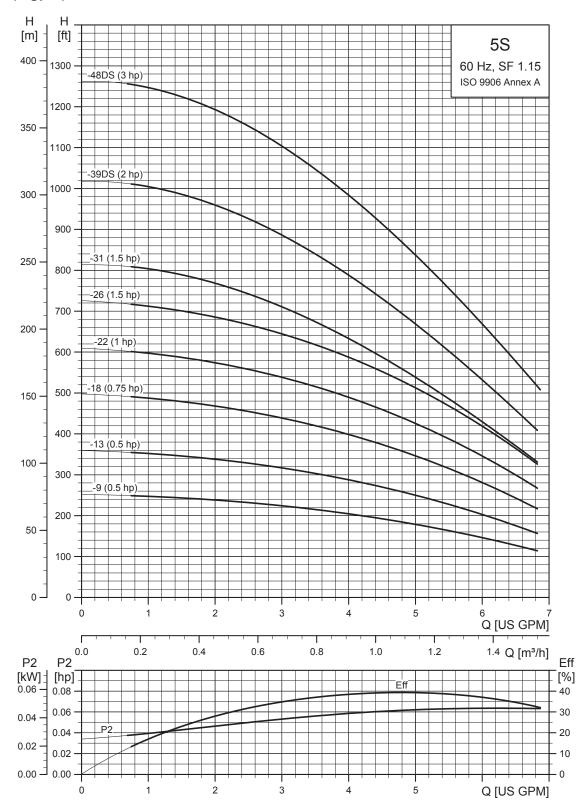
- The measurements were made with airless water at a temperature of 68 °F (20 °C). The curves apply to a kinematic viscosity of 1 mm<sup>2</sup>/s (1 cSt). When pumping liquids with a density higher than that of water, use motors with correspondingly higher outputs.
- The bold curves indicate the recommended performance range.
- The performance curves are inclusive of possible losses such as non-return valve loss.
- Q/H: The curves are inclusive of valve and inlet losses at the actual speed.
   Operation without non-return valve will increase the actual head at rated performance by 0.5 to 1.0 m.
- NPSH: The curve is inclusive of pressure loss in the suction interconnector and shows required inlet pressure.
- Power curve: P<sub>2</sub> shows pump power input at the actual speed of each individual pump size.
- Efficiency curve: Eta shows pump stage efficiency.
   If Eta for the actual pump size is needed, please consult WinCAPS or WebCAPS.

## 5. How to read the curve charts



## 6. Curve charts and technical data

## 5S (5 gpm)



6

## 5S (5 gpm)

						Dimensions				
Pump model	Nom. head [ft]	Ph	Volts [V]	Motor [Hp]	Α	В	С	D	E	_ Net weight (complete)
					[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[lb]
		5	S, mote	or dia. 4 iı	nch, 2 wire m	otor, 60 Hz	- rated flow 5	gpm (1" N	PT)	
5S05-9	171	1	230	0.5	24.57 (624)	11.03 (280)	13.55 (344)	3.74 (95)	3.97 (101)	21.6
5005.40	0.17		115	0.5	27.88 (708)	11.03 (280)	16.86 (428)	3.74 (95)	3.97 (101)	26.9
5S05-13	247	1	230	0.5	27.88 (708)	11.03 (280)	16.86 (428)	3.74 (95)	3.97 (101)	26.1
5S07-18	343	1	230	0.75	32.60 (828)	11.62 (295)	20.99 (533)	3.74 (95)	3.97 (101)	29.7
5S10-22	419	1	230	1 •	36.50 (927)	12.21 (310)	24.30 (617)	3.74 (95)	3.97 (101)	32.4
5S15-26	495	1	230	1.5	41.30 (1049)	13.71 (348)	27.60 (701)	3.74 (95)	3.97 (101)	41.4
5S15-31	527	1	230	1.5 ■	47.21 (1199)	13.71 (348)	33.51 (851)	3.74 (95)	3.97 (101)	47.7
5S05-9	171	1	230	0.5	- (- ,	11.03 (280)	13.55 (344)	3.74 (95)	3.97 (101)	22.5
		5	S, mot	or dia. 4 iı	nch, 3 wire m	otor, 60 Hz	- rated flow 5	gpm (1" N	PT)	
5S05-13	247	1	115	0.5	27.88 (708)	11.03 (280)	16.86 (428)	3.74 (95)	3.97 (101)	26.9
		-	230	0.5	27.88 (708)	11.03 (280)	16.86 (428)	3.74 (95)	3.97 (101)	25.2
5S07-18	343	1	230	0.75	32.60 (828)	11.62 (295)	20.99 (533)	3.74 (95)	3.97 (101)	28.8
5S10-22	419	1	230	1 •	36.50 (927)	12.21 (310)	24.30 (617)	3.74 (95)	3.97 (101)	32.4
		1	230	1.5	41.30 (1049)	13.71 (348)	27.60 (701)	3.74 (95)	3.97 (101)	37.8
5S15-26	495	3	230	1.5	39.81 (1011)	12.21 (310)	27.60 (701)	3.74 (95)	3.97 (101)	38.7
			460	1.5	39.81 (1011)	12.21 (310)	27.60 (701)	3.74 (95)	3.97 (101)	38.7
		1	230	1.5	47.21 (1199)	13.71 (348)	33.51 (851)	3.74 (95)	3.97 (101)	47.7
5S15-31	527	3	230	1.5	45.71 (1161)	12.21 (310)	33.51 (851)	3.74 (95)	3.97 (101)	45.0
			460	1.5	45.71 (1161)	12.21 (310)	33.51 (851)	3.74 (95)	3.97 (101)	45.0
		1	230	2 •	59.61 (1514)	19.49 (495)	40.12 (1019)	3.74 (95)	3.97 (101)	57.6
5S20-39DS	663	3	230	2 ■	53.82 (1367)	13.71 (348)	40.12 (1019)	3.74 (95)	3.97 (101)	54.0
			460	2 ■	53.82 (1367)	13.71 (348)	40.12 (1019)	3.74 (95)	3.97 (101)	54.0
		1	230	3 •	70.16 (1782)	22.60 (574)	47.56 (1208)	3.74 (95)	3.97 (101)	77.4
					05 50 (1055)	10.00 (15=:	17 50 (1065)	0.74 (05)	0.07 (40 ::	

18.00 (457) 47.56 (1208)

18.00 (457) 47.56 (1208)

3.74 (95)

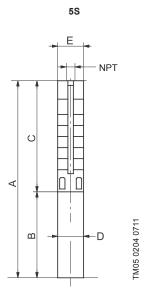
3.74 (95)

3.97 (101)

3.97 (101)

77.4

77.4



E = Maximum diameter of pump including cable guard and motor.

5S30-48DS

Control box is required for 3-wire, single-phase applications. Data does not include control box. DS designation = Built into sleeve, 1-1/4" NPT, 6" minimum well diameter. Performance conforms to ISO 9906. 1999 (E) Annex A. Minimum submergence is 2 feet.

• 65.56 (1665)

• 65.56 (1665)

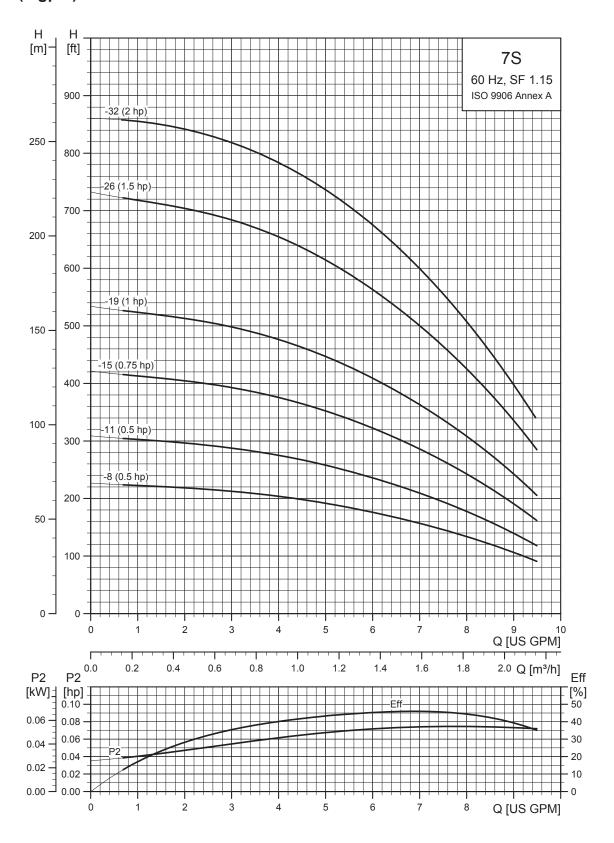
3

- MS402 motor.
- MS4000 motor.
- MS6 motor.
- Λ MMS6000 motor.
- ★ MMS8000 motor.
- Takes MS6 motor; not available as complete.
- Takes MMS6000 motor; not available as complete.

460

Takes MMS8000 motor; not available as complete. Takes MMS10000 motor; not available as complete.

## 7S (7 gpm)



6

### 7S (7 gpm)

							Dimensions			Net
Pump model	Nom. head [ft]	Ph	Volts [V]	Motor [Hp]	Α	В	С	D	E	weight (complete)
					[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[lb]
			7S, mo	tor dia. 4	inch, 2 wire	motor, 60 Hz	- rated flow 7	7 gpm (1" N	PT)	
7S05-8	151	1	230	.5 ■	23.75 (603)	11.03 (280)	12.72 (323)	3.74 (95)	3.97 (101)	21.6
7005 44	000	_	115	.5 ■	26.23 (666)	11.03 (280)	15.20 (386)	3.74 (95)	3.97 (101)	29.7
7S05-11	208	1	230	.5 ■	26.23 (666)	11.03 (280)	15.20 (386)	3.74 (95)	3.97 (101)	24.3
7S07-15	283	1	230	.75 ■	30.12 (765)	11.62 (295)	18.51 (470)	3.74 (95)	3.97 (101)	29.7
7S10-19	358	1	230	1 •	34.02 (864)	12.21 (310)	21.82 (554)	3.74 (95)	3.97 (101)	32.4
7S15-26	491	1	230	1.5	41.3 (1049)	13.71 (348)	27.60 (701)	3.74 (95)	3.97 (101)	41.4
			7S, mo	tor dia. 4	inch, 3 wire	motor, 60 Hz	- rated flow 7	7 gpm (1" N	PT)	
7S05-8	151	1	230	.5 ■	23.75 (603)	11.03 (280)	12.72 (323)	3.74 (95)	3.97 (101)	21.6
7S05-11	200	1	115	.5 ■	26.23 (666)	11.03 (280)	15.20 (386)	3.74 (95)	3.97 (101)	21.6
7505-11	208	1	230	.5 ■	26.23 (666)	11.03 (280)	15.20 (386)	3.74 (95)	3.97 (101)	30.6
7S07-15	283	1	230	.75 ■	30.12 (765)	11.62 (295)	18.51 (470)	3.74 (95)	3.97 (101)	27.9
7S10-19	358	1	230	1 •	34.02 (864)	12.21 (310)	21.82 (554)	3.74 (95)	3.97 (101)	39.6
•	•	1	230	1.5 ■	41.30 (1049)	13.71 (348)	27.60 (701)	3.74 (95)	3.97 (101)	38.7
7S15-26	491	3	230	1.5	39.81 (1011)	12.21 (310)	27.60 (701)	3.74 (95)	3.97 (101)	38.7
		3	460	1.5 ■	39.81 (1011)	12.21 (310)	27.60 (701)	3.74 (95)	3.97 (101)	38.7

19.49 (495)

13.71 (348)

13.71 (348)

32.56 (827)

32.56 (827)

32.56 (827)

3.74 (95)

3.74 (95)

3.74 (95)

3.97 (101)

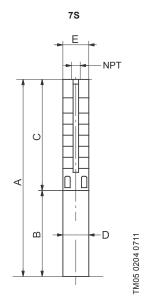
3.97 (101)

3.97 (101)

48.5

48.5

48.5



E = Maximum diameter of pump including cable guard and motor.

7S20-32

Notes:
Control box is required for 3-wire, single-phase applications. Data does not include control box.
Performance conforms to ISO 9906. 1999 (E) Annex A. Minimum submergence is 2 feet.

52.05 (1322)

46.26 (1175)

46.26 (1175)

604

- MS4000 motor.
- MS6 motor.
- Λ MMS6000 motor.
- MMS8000 motor.

230

230

3

2

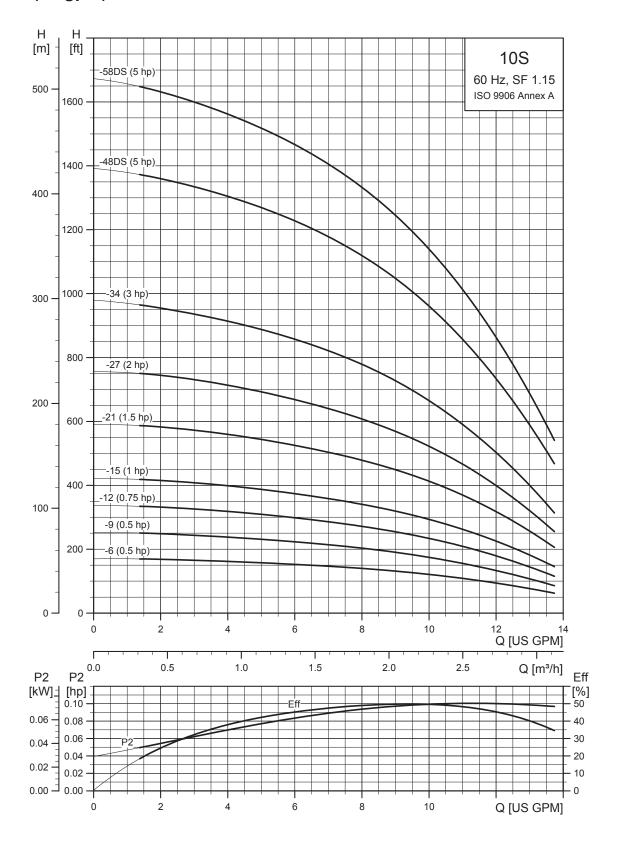
- Takes MS6 motor; not available as complete.

  Takes MMS6000 motor; not available as complete.

  Takes MMS8000 motor; not available as complete.

  Takes MMS10000 motor; not available as complete.

## 10S (10 gpm)



6

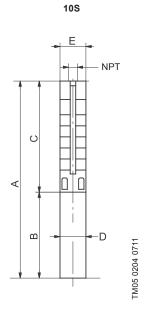
## 10S (10 gpm)

Pump model	Nom. head [ft]	Ph	Volts [V]	Moto [Hp]		Α	В	С	D	E	weight (complete)
1-1					[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[lb]	
	10	S, m	otor di	ia. 4 in	ch,	2 wire moto	or, 60 Hz - ra	ted flow 10	gpm (1.25"	NPT)	
10S05-6	116	1	230	.5	•	22.05 (560)	10.99 (279)	11.07 (281)	3.74 (95)	3.97 (101)	20.7
			115	-	_	24 52 (622)	10.00 (270)	12 FF (244)	2.74 (05)	2.07 (4.04)	24.2

Dimensions

	10S, motor dia. 4 inch, 2 wire motor, 60 Hz - rated flow 10 gpm (1.25" NPT)										
10S05-6	116	1	230	.5	•	22.05 (560)	10.99 (279)	11.07 (281)	3.74 (95)	3.97 (101)	20.7
10S05-9 174	1	115	.5	•	24.53 (623)	10.99 (279)	13.55 (344)	3.74 (95)	3.97 (101)	24.3	
	'	230	.5	•	24.53 (623)	10.99 (279)	13.55 (344)	3.74 (95)	3.97 (101)	23.4	
10S07-12	233	1	230	.75	•	27.60 (701)	11.58 (294)	16.03 (407)	3.74 (95)	3.97 (101)	24.3
10S10-15	291	1	230	1	•	30.67 (779)	12.17 (309)	18.51 (470)	3.74 (95)	3.97 (101)	29.7
10S15-21	407	1	230	1.5	•	37.17 (944)	13.71 (348)	23.47 (596)	3.74 (95)	3.97 (101)	35.1

	10	S, m	otor d	ia. 4 i	nch	, 3 wire moto	or, 60 Hz - ra	ated flow 10	gpm (1.25"	NPT)		
10S05-6	116	1	230	.5	•	24.77 (629)	13.71 (348)	11.07 (281)	3.74 (95)	3.97 (101)	21.6	
10S05-9	174	1	115	.5	-	24.53 (623)	10.99 (279)	13.55 (344)	3.74 (95)	3.97 (101)	25.4	
10202-9	174	'	230	.5	-	24.53 (623)	10.99 (279)	13.55 (344)	3.74 (95)	3.97 (101)	24.3	
10S07-12	233	1	230	.75	-	27.60 (701)	11.58 (294)	16.03 (407)	3.74 (95)	3.97 (101)	28.8	
10S10-15	291	1	230	1	-	30.67 (779)	12.17 (309)	18.51 (470)	3.74 (95)	3.97 (101)	29.7	
		1	230	1.5	-	37.17 (944)	13.71 (348)	23.47 (596)	3.74 (95)	3.97 (101)	35.1	
10S15-21	407	_	230	1.5	-	35.63 (905)	12.17 (309)	23.47 (596)	3.74 (95)	3.97 (101)	32.4	
		3	460	1.5	-	35.63 (905)	12.17 (309)	23.47 (596)	3.74 (95)	3.97 (101)	36.0	
		1	230	2	•	47.92 (1217)	19.49 (495)	28.43 (722)	3.74 (95)	3.97 (101)	45.9	
10S20-27	524	524	3	230	2	-	42.13 (1070)	13.71 (348)	28.43 (722)	3.74 (95)	3.97 (101)	44.1
		3	460	2	-	42.13 (1070)	13.71 (348)	28.43 (722)	3.74 (95)	3.97 (101)	44.1	
		1	230	3	•	58.59 (1488)	22.6 (574)	35.99 (914)	3.74 (95)	3.97 (101)	81.9	
10S30-34	659	3	230	3	•	53.98 (1371)	18.00 (457)	35.99 (914)	3.74 (95)	3.97 (101)	74.7	
		3	460	3	•	53.98 (1371)	18.00 (457)	35.99 (914)	3.74 (95)	3.97 (101)	74.7	
		1	230	5	•	74.18 (1884)	26.62 (676)	47.56 (1208)	3.74 (95)	3.97 (101)	103.5	
10S50-48DS	931	3	230	5	•	70.16 (1782)	22.60 (574)	47.56 (1208)	3.74 (95)	3.97 (101)	103.5	
		3	460	5	•	70.16 (1782)	22.60 (574)	47.56 (1208)	3.74 (95)	3.97 (101)	103.5	
		1	230	5	•	89.49 (2272)	26.62 (676)	62.88 (1597)	3.74 (95)	4.25 (108)	132.3	
10S50-58DS	1124		230	5	•	85.48 (2171)	22.60 (574)	62.88 (1597)	3.74 (95)	4.25 (108)	132.3	
		3	460	5	•	85.48 (2171)	22.60 (574)	62.88 (1597)	3.74 (95)	4.25 (108)	132.3	



Net

E = Maximum diameter of pump including cable guard and motor.

#### Notes:

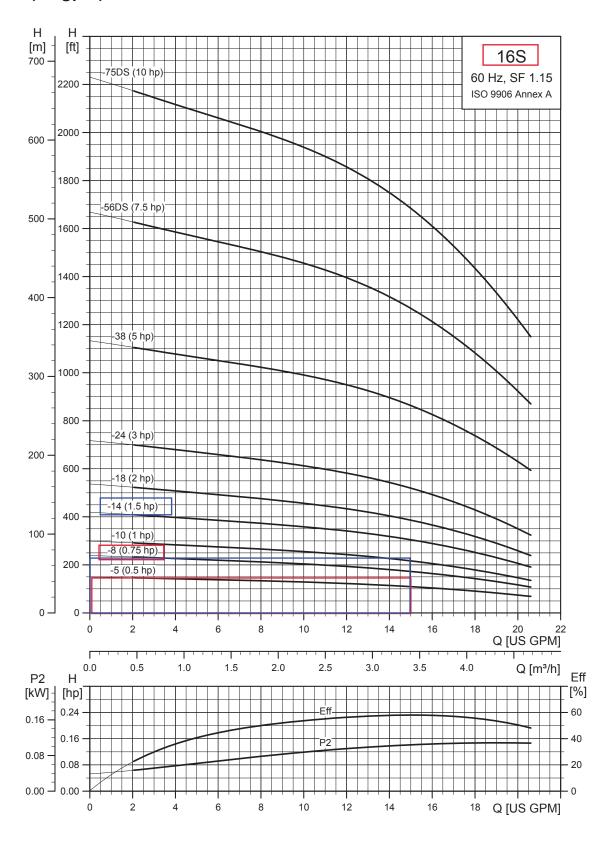
Control box is required for 3-wire, single-phase applications. Data does not include control box. DS designation = Built into sleeve, 1-1/4" NPT, 6" minimum well diameter.

Performance conforms to ISO 9906. 1999 (E) Annex A. Minimum submergence is 2 feet.

- MS402 motor.
- MS4000 motor.
- ▲ MS6 motor.
- Λ MMS6000 motor.
- ★ MMS8000 motor.
- ◆ Takes MS6 motor; not available as complete.

- Takes MMS6000 motor; not available as complete.
   Takes MMS8000 motor; not available as complete.
   Takes MMS10000 motor; not available as complete.

## 16S (16 gpm)



6

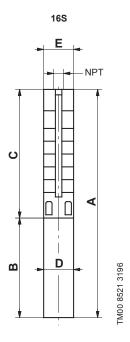
## 16S (16 gpm)

	Nom.						Dimensions			Net
Pump model	head	Ph	Volts [V]	Motor [Hp]	Α	В	С	D	E	weight (complete
	[ft]				[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[lb]
	16	SS, m	otor di	a. 4 inch	, 2 wire moto	r, 60 Hz - ra	ted flow 16 g	ıpm (1.25" l	NPT)	
		-	115	.5 ■	21.26 (540)	11.03 (280)	10.24 (260)	3.74 (95)	3.97 (101)	21.6
16S05-5	102	1	230	.5 ■	21.26 (540)	11.03 (280)	10.24 (260)	3.74 (95)	3.97 (101)	23.4
16S07-8	162	1	230	.75 ■	24.34 (618)	11.62 (295)	12.72 (323)	3.74 (95)	3.97 (101)	24.3
16S10-10	203	1	230	1 ■	26.58 (675)	12.21 (310)	14.38 (365)	3.74 (95)	3.97 (101)	27.9
16S15-14	284	1	230	1.5 ■	31.38 (797)	13.71 (348)	17.68 (449)	3.74 (95)	3.97 (101)	36.0
	16	SS, m	otor di	a. 4 inch	, 3 wire moto	r, 60 Hz - ra	ted flow 16 g	jpm (1.25" l	NPT)	
10005 5	100		115	.5 ■	21.26 (540)	11.03 (280)	10.24 (260)	3.74 (95)	3.97 (101)	21.6
16S05-5	102	1	230	.5 ■	21.26 (540)	11.03 (280)	10.24 (260)	3.74 (95)	3.97 (101)	21.6
16S07-8	162	1	230	.75 ■	24.34 (618)	11.62 (295)	12.72 (323)	3.74 (95)	3.97 (101)	27.0
16S10-10	203	1	230	1 ■	26.58 (675)	12.21 (310)	14.38 (365)	3.74 (95)	3.97 (101)	27.9
		1	230	1.5 •	31.38 (797)	13.71 (348)	17.68 (449)	3.74 (95)	3.97 (101)	32.4
16S15-14	284	_	230	1.5 ■	29.89 (759)	12.21 (310)	17.68 (449)	3.74 (95)	3.97 (101)	28.8
		3	460	1.5 ■	29.89 (759)	12.21 (310)	17.68 (449)	3.74 (95)	3.97 (101)	28.8
		1	230	2 •	40.48 (1028)	19.49 (495)	20.99 (533)	3.74 (95)	3.97 (101)	36.0
16S20-18	366	_	230	2 ■	34.69 (881)	13.71 (348)	20.99 (533)	3.74 (95)	3.97 (101)	36.0
		3	460	2 ■	34.69 (881)	13.71 (348)	20.99 (533)	3.74 (95)	3.97 (101)	36.0
		1	230	3 •	48.55 (1233)	22.60 (574)	25.95 (659)	3.74 (95)	3.97 (101)	62.1
16S30-24	487	_	230	3 •	43.94 (1116)	18.00 (457)	25.95 (659)	3.74 (95)	3.97 (101)	57.6
		3	460	3 •	43.94 (1116)	18.00 (457)	25.95 (659)	3.74 (95)	3.97 (101)	57.6
		1	230	5 •	65.91 (1674)	26.62 (676)	39.30 (998)	3.74 (95)	3.97 (101)	97.2
16S50-38	814	_	230	5 •	62.01 (1575)	22.72 (577)	39.30 (998)	3.74 (95)	3.97 (101)	90.0
		3	460	5 •	62.01 (1575)	22.72 (577)	39.30 (998)	3.74 (95)	3.97 (101)	90.0
	SP	16S,	motor	dia. 6 inc	h, 3 wire mot	tor, 60 Hz -	rated flow 16	gpm (1.25	" NPT)	
			230	7.5 ▲	95.40 (2423)	26.62 (676)	68.78 (1747)	5.63 (143)	5.51 (140)	165.1
16S75-56DS	1200	3	460	7.5 🔺	95.40 (2423)	26.62 (676)	68.78 (1747)	5.63 (143)	5.51 (140)	165.1

**1** 115.08 (2923) 30.60 (777) 84.49 (2146) 5.63 (143)

5.51 (140)

190.0



E = Maximum diameter of pump including cable guard and motor.

16S100-75DS

1607

Control box is required for 3-wire, single-phase applications. Data does not include control box. DS designation = Built into sleeve, 1-1/4" NPT, 6" minimum well diameter.

Performance conforms to ISO 9906. 1999 (E) Annex A. Minimum submergence is 2 feet.

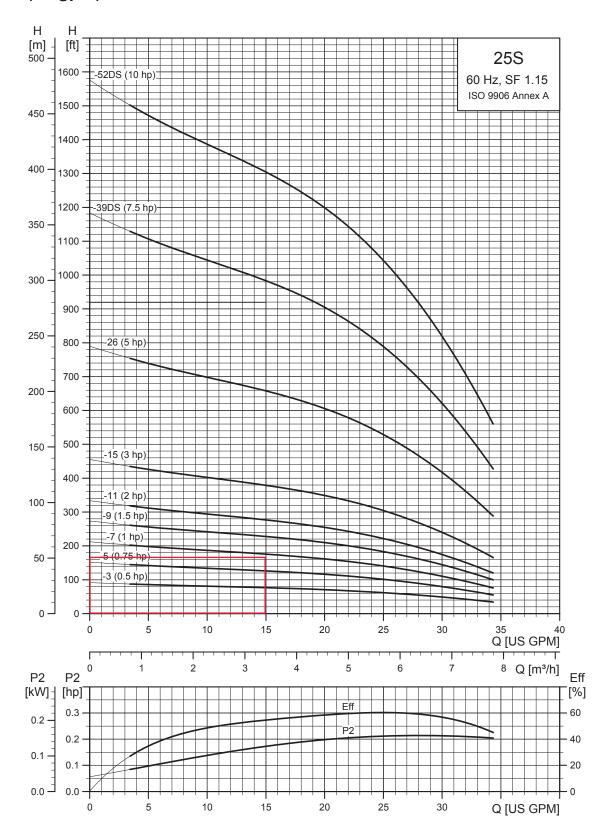
- MS402 motor.
- MS4000 motor.
- MS6 motor.
- Λ MMS6000 motor.
- ★ MMS8000 motor.
- Takes MS6 motor; not available as complete.
- Takes MMS6000 motor; not available as complete.

  Takes MMS8000 motor; not available as complete.

  Takes MMS8000 motor; not available as complete.
- Takes MMS10000 motor; not available as complete.

460

## 25S (25 gpm)



6

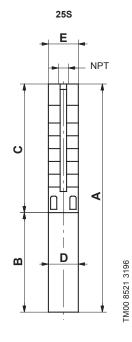
## 25S (25 gpm)

	Nom.						Dimensions			Net
Pump model	head	Ph	Volts [V]	Motor [Hp]	Α	В	С	D	E	weight (complete
	[ft]				[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[in (mm)]	[lb]
	25	S, mo	otor dia	. 4 inch, 2	wire motor,	60 Hz - rat	ed flow 25 g <sub>l</sub>	om (1.5" NP	T)	
			115	.5	19.61 (498)	11.03 (280)	8.59 (218)	3.74 (95)	3.97 (101)	21.6
25S05-3	60	1	230	.5 ■	19.61 (498)	11.03 (280)	8.59 (218)	3.74 (95)	3.97 (101)	21.6
25S07-5	99	1	230	.75	21.86 (555)	11.62 (295)	10.24 (260)	3.74 (95)	3.97 (101)	23.4
25S10-7	139	1	230	1 •	24.10 (612)	12.21 (310)	11.89 (302)	3.74 (95)	3.97 (101)	25.2
25S15-9	179	1	230	1.5 ■	27.25 (692)	13.71 (348)	13.55 (344)	3.74 (95)	3.97 (101)	28.8
	25	S, mo	otor dia	. 4 inch, 3	wire motor,	60 Hz - rat	ed flow 25 g <sub>l</sub>	om (1.5" NP	T)	
			115	.5	19.61 (498)	11.03 (280)	8.59 (218)	3.74 (95)	3.97 (101)	21.6
25S05-3	60	1	230	.5	19.61 (498)	11.03 (280)	8.59 (218)	3.74 (95)	3.97 (101)	21.6
25S07-5	99	1	230	.75 ■	21.86 (555)	11.62 (295)	10.24 (260)	3.74 (95)	3.97 (101)	23.4
25S10-7	139	1	230	1 •	24.10 (612)	12.21 (310)	11.89 (302)	3.74 (95)	3.97 (101)	25.2
		1	230	1.5 ■	27.25 (692)	13.71 (348)	13.55 (344)	3.74 (95)	3.97 (101)	29.7
25S15-9	179	_	230	1.5 ■	25.75 (654)	12.21 (310)	13.55 (344)	3.74 (95)	3.97 (101)	27.0
		3	460	1.5	25.75 (654)	12.21 (310)	13.55 (344)	3.74 (95)	3.97 (101)	28.8
		1	230	2 •	34.69 (881)	19.49 (495)	15.20 (386)	3.74 (95)	3.97 (101)	33.1
25S20-11	219		230	2 ■	28.90 (734)	13.71 (348)	15.20 (386)	3.74 (95)	3.97 (101)	37.0
		3	460	2 ■	28.90 (734)	13.71 (348)	15.20 (386)	3.74 (95)	3.97 (101)	33.3
		1	230	3 •	41.11 (1044)	22.60 (574)	18.51 (470)	3.74 (95)	3.97 (101)	61.2
25S30-15	298	_	230	3 •	36.50 (927)	18.00 (457)	18.51 (470)	3.74 (95)	3.97 (101)	53.1
		3	460	3 •	36.50 (927)	18.00 (457)	18.51 (470)	3.74 (95)	3.97 (101)	53.1
		1	230	5 •	54.22 (1377)	26.62 (676)	27.60 (701)	3.74 (95)	3.97 (101)	72.9
25S50-26	517	_	230	5 •	50.32 (1278)	22.72 (577)	27.60 (701)	3.74 (95)	3.97 (101)	72.9
		3	460	5 •	50.32 (1278)	22.72 (577)	27.60 (701)	3.74 (95)	3.97 (101)	72.9
	SP 2	.5S, r	notor d	ia. 6 inch	, 3 wire moto	or, 60 Hz - ra	ated flow 25	gpm (1.5" N	IPT)	
			230	7.5 ▲	64.81 (1646)	22.25 (565)	42.56 (1081)	5.63 (143)	5.43 (138)	122.1
25S75-39DS	775	3	460	7.5	64.81 (1646)	22 25 (565)	42.56 (1081)	5.63 (143)	5.43 (138)	122.1

**88.71 (2253)** 23.23 (590) 65.48 (1663) 5.63 (143)

5.51 (140)

163.1



E = Maximum diameter of pump including cable guard and motor.

25S100-52DS

Control box is required for 3-wire, single-phase applications. Data does not include control box. DS designation = Built into sleeve, 1-1/2" NPT, 6" minimum well diameter.

Performance conforms to ISO 9906. 1999 (E) Annex A. Minimum submergence is 2 feet.

- MS402 motor.
- MS4000 motor.
- ▲ MS6 motor.
- Λ MMS6000 motor.
- MMS8000 motor.
- Takes MS6 motor; not available as complete.
- Takes MMS6000 motor; not available as complete.
- Takes MMS8000 motor; not available as complete.
- † Takes MMS10000 motor; not available as complete.

## **Electrical data**

#### Grundfos submersible pump motors - 60 Hz

					Gr	undfos subme	ersible pump	motors - 60	Hz			
Нр	Ph	Volt	S.F	Circuit	breaker	Ampe	erage	Full	load	Max. thrust	Nameplate	Product
		[V]		Std.	Delay	Start [A]	Max. [A]	Eff. [%]	PF [%]	[lbs]	number	number
	ingle-ph	ase, 2-wire n	•									
.5	1	115	1.60	35	15	55.0	12.0	62	76	900	79922102	96465574
.5	_	_	1.60	15	7	34.5	6.0	62	76	900	79952102	96465616
.75	- 1	230 -	1.50	20	9	40.5	8.4	62	75	900	79952103	96465618
1	-	-	1.40	25	12	48.4	9.8	63	82	900	79952104	96465620
1.5			1.30	35	15	62.0	13.1	64	85	900	79952105	96465622
	• .	ase, 3-wire n										
.5	1	115	1.60	35	15	42.5	12.0	61	76	900	79423102	96023039
.5	_	_	1.60	15	7	21.5	6.0	62	76	900	79453102	96465606
.75	_	_	1.50	20	9	31.4	8.4	62	75	900	79453103	96465608
1	- ,	-	1.40	25	12	37.0	9.8	63	82	900	79453104	96465610
1.5	- 1	230	1.30	35	15	45.9	11.6	69	89	900	79453105	96465612
3	_	-	1.25	35 45	20 30	57.0 77.0	13.2 17.0	72 74	86 93	1500 1500	79454506 79454507	96449947 96449948
5	-	-	1.15	70	45	110.0	27.5	77	93	1500	79454507	96449949
				70	40	110.0	21.5	11	92	1300	79434309	90449949
incn, th	ıree-pna	se, 3-wire m										
4.5	_	230	1.30	15	8	40.3	7.3	75	72	900	79302005	96465629
1.5	3	460	1.30	10	4	20.1	3.7	75	72	900	79362005	96465651
		575	1.30	10	4	16.1	2.9	75	72	900	79392005	96785912
2	3	230	1.25	20 10	10 5	48 24	8.7	76 76	75 75	900	79302006	96465630
2	3	460	1.25				4.4			900	79362006	96465652
		575 230	1.25	10 30	4	19.2 56	3.5 12.2	76 77	75 75	900	79392006	96785917 96405801
3	3	460	1.15	15	15 7	28	6.1	77	75	1500	79304507 79354507	96405810
3	3	575	1.15	15	6	22	4.8	77	75	1500	79394507	96405815
		230	1.15	40	25	108	19.8	80	82	1500	79304509	96405802
5	3	460	1.15	20	12	54	9.9	80	82	1500	79354509	96405811
Ü	Ü	575	1.15	15	9	54	7.9	80	82	1500	79394509	96405816
		230	1.15	60	30	130	25.0	81	82	1500	79305511	96405805
7.5	3	460	1.15	35	15	67	13.2	81	82	1500	79355511	96405814
		575	1.15	30	15	67	10.6	81	82	1500	79395511	96405819
10	3	460	1.15	50	30	90	18	81	80	1500	79355512	96440318
inch th	ree-nha	se, 3-wire m	otors									
	nee pna			0.5	40	100 110	07.00.0	00.00	0.5	1000	70005544	00400040
7.5	3	208-230	1.15	65	40	102-116	27-23.6	82-23	85	1686	78285541	96168843
		460 208-230	1.15	30 90	17 50	54 142-162	11.8 35.5-32	83 82-84	85 86-84	1686 1686	78355541 78285542	96168823 96168844
10	3	460	1.15	40	25	75	16.0	84	85	1686	78355542	96168824
		208-230	1.15	130	75	390-500	52-47	83-84	86-84	6182	78285544	96168846
15	3	460	1.15	60	35	112	23.6	85	84	6182	78355544	96168826
		208-230	1.15	175	100	265-305	70-63.5	83-85	86-84	6182	78285546	96168848
20	3	460	1.15	80	45	154	32.0	85	84	6182	78355546	96168828
		208-230	1.15	200	125	410-520	86-78	84-85	87-84	6182	78285547	96168849
25	3	460	1.15	100	60	196	39	85	84	6182	78355547	96168829
		208-230	1.15	250	150	405-475	102-92.5	84-85	87-85	6182	78285548	96168850
	_	200 200										
30	3	460	1.15	125	70	238	46.0	85	85	6182	78355548	96168830
30 40	3			125 170	70 90	238 330	46.0 63.5	85 86	85 84	6182 6182	78355548 78355550	96168830 96168832
		460	1.15									
40 50	3	460 460	1.15 1.15 1.15	170	90	330	63.5	86	84	6182	78355550	96168832
40 50	3	460 460 460	1.15 1.15 1.15 otors	170	90	330	63.5 68.7	86	84	6182	78355550 96476890	96168832 96023200
40 50 inch, th	3 3 nree-pha	460 460 460 se, 3-wire m	1.15 1.15 1.15 otors 1.15	170 225	90 125	330 470	63.5	86 84	84 83	6182 6182	78355550 96476890 96530180	96168832
40 50 inch, th	3 3 nree-pha	460 460 460 se, 3-wire m	1.15 1.15 1.15 otors	170 225 175	90 125 100	330 470 380	63.5 68.7 55.7	86 84 83	84 83 85	6182 6182 13000	78355550 96476890	96168832 96023200 96023204
40 50 inch, th 40 50	3 3 nree-pha 3 3	460 460 460 se, 3-wire m 460 460	1.15 1.15 1.15 0tors 1.15	170 225 175 225	90 125 100 125	330 470 380 550	63.5 68.7 55.7 67.8	86 84 83 84	84 83 85 85	6182 6182 13000 13000	78355550 96476890 96530180 96530182	96168832 96023200 96023204 96023205
40 50 inch, th 40 50 60	3 3 nree-pha 3 3	460 460 460 se, 3-wire m 460 460	1.15 1.15 1.15 otors 1.15 1.15	170 225 175 225 250	90 125 100 125 150	330 470 380 550 640	63.5 68.7 55.7 67.8 80.4	86 84 83 84 86	84 83 85 85 85	6182 6182 13000 13000 13000	78355550 96476890 96530180 96530182 96476891	96168832 96023200 96023204 96023205 96023206
40 50 inch, th 40 50 60 75	3 3 nree-pha 3 3 3	460 460 460 se, 3-wire m 460 460 460	1.15 1.15 1.15 otors 1.15 1.15 1.15	170 225 175 225 250 300	90 125 100 125 150 175	330 470 380 550 640 580	63.5 68.7 55.7 67.8 80.4 97.4	86 84 83 84 86 86	84 83 85 85 85 86	6182 6182 13000 13000 13000 13000	78355550 96476890 96530180 96530182 96476891 96476892	96168832 96023200 96023204 96023205 96023206 96023207
40 50 inch, th 40 50 60 75 100	3 3 nree-pha 3 3 3 3 3	460 460 460 <b>se, 3-wire m</b> 460 460 460 460	1.15 1.15 0tors 1.15 1.15 1.15 1.15 1.15	170 225 175 225 250 300 400	90 125 100 125 150 175 225	330 470 380 550 640 580 570	63.5 68.7 55.7 67.8 80.4 97.4 130.4	86 84 83 84 86 86 87	84 83 85 85 85 86 86	6182 6182 13000 13000 13000 13000 13000	78355550 96476890 96530180 96530182 96476891 96476892 96476893	96168832 96023200 96023204 96023205 96023206 96023207 96023208
40 50 <b>Einch, th</b> 40 50 60 75 100 125	3 3 nree-pha 3 3 3 3 3 3 3	460 460 460 se, 3-wire m 460 460 460 460 460 460	1.15 1.15 1.15 otors 1.15 1.15 1.15 1.15 1.15 1.15 1.15	170 225 175 225 250 300 400 500	90 125 100 125 150 175 225 300	330 470 380 550 640 580 570 600	63.5 68.7 55.7 67.8 80.4 97.4 130.4 160.0	86 84 83 84 86 86 87 87	84 83 85 85 85 86 86 86	6182 6182 13000 13000 13000 13000 13000 13000	78355550 96476890 96530180 96530182 96476891 96476892 96476893 96476894	96168832 96023200 96023204 96023205 96023206 96023207 96023208 96023209
40 50 -inch, th 40 50 60 75 100 125 150	3 3 3 3 3 3 3 3 3 3 3 3 4 three-pha	460 460 460 se, 3-wire m 460 460 460 460 460 460 460 460	1.15 1.15 1.15 0tors 1.15 1.15 1.15 1.15 1.15 1.15 1.15 1.1	170 225 175 225 250 300 400 500 600	90 125 100 125 150 175 225 300 350	330 470 380 550 640 580 570 600 580	63.5 68.7 55.7 67.8 80.4 97.4 130.4 160.0 191.3	86 84 83 84 86 86 87 87 87	84 83 85 85 85 86 86 87 87	6182 6182 13000 13000 13000 13000 13000 13000 13000	78355550 96476890 96530180 96530182 96476891 96476892 96476893 96476894 96511375	96168832 96023204 96023205 96023205 96023206 96023207 96023208 96023209 96023210
40 50 -inch, th 40 50 60 75 100 125	3 3 nree-pha 3 3 3 3 3 3 3	460 460 460 se, 3-wire m 460 460 460 460 460 460	1.15 1.15 1.15 otors 1.15 1.15 1.15 1.15 1.15 1.15 1.15	170 225 175 225 250 300 400 500	90 125 100 125 150 175 225 300	330 470 380 550 640 580 570 600	63.5 68.7 55.7 67.8 80.4 97.4 130.4 160.0	86 84 83 84 86 86 87 87	84 83 85 85 85 86 86 86	6182 6182 13000 13000 13000 13000 13000 13000	78355550 96476890 96530180 96530182 96476891 96476892 96476893 96476894	96168832 96023200 96023204 96023205 96023206 96023207 96023208 96023209

#### .Other motor manufacturers

- Hitachi motors: Refer to the Hitachi submersible motors application maintenance manual.
- Franklin motors: Refer to the Franklin submersible motors application maintenance manual.

# COPSS

## 7. Accessories

#### **MP 204**

The MP 204 is an electronic motor protector, designed for the protection of an asynchronous motor or a pump.

The motor protector consists of:

- · a cabinet incorporating transformers and electronics
- a control panel with operating buttons and display for reading of data.

The MP 204 operates with two sets of limits:

- · a set of warning limits and
- · a set of trip limits.

If one or more of the warning limits are exceeded, the motor continues to run, but the warnings will appear in the MP 204 display.

Some values only have a warning limit.

The warning can also be read out by means of the Grundfos R100 remote control.

If one of the trip limits is exceeded, the trip relay will stop the motor. At the same time, the signal relay is operating to indicate that the limit has been exceeded.

#### **Applications**

The MP 204 can be used as a stand-alone motor protector.

The MP 204 can be monitored via a Grundfos GENIbus.

The power supply to the MP 204 is in parallel with the supply to the motor. Motor currents up to 120 A are passed directly through the MP 204. The MP 204 protects the motor primarily by measuring the motor current by means of a true RMS measurement. The MP 204 disconnects the contactor if, for example, the current exceeds the preset value.

Secondarily, the motor is protected via temperature measuring by a Tempcon sensor, a Pt100/Pt1000 sensor and a PTC sensor/thermal switch.

The MP 204 is designed for single- and three-phase motors. In single-phase motors, the starting and run capacitors are also measured. Cos  $\boldsymbol{\phi}$  is measured in both single- and three-phase systems.

#### **Benefits**

The MP 204 offers these benefits:

- · Suitable for both single- and three-phase motors
- · Dry-running protection
- · Overload protection
- · Very high accuracy
- · Made for submersible pumps.

#### Many monitoring options

The MP 204 monitors the following parameters:

- · Insulation resistance before start-up
- Temperature (Tempcon, Pt sensor and PTC/thermal switch)
- Overload/underload
- Overvoltage/undervoltage
- Phase sequence
- · Phase failure
- · Power factor
- · Power consumption
- · Harmonic distortion
- · Operating hours and number of starts.



TM03 1471 2205

Fig. 21 MP 204

Five sizes of single-turn transformers, 120-999 A. **Note:** Monitoring of motor temperature is not possible when single-turn transformers are used.



FM03 2033 3505

Fig. 22 Single-turn transformers

#### **Product numbers**

Product	Product number
MP 204	96079927
R100	625333

#### **Functions**

- · Phase-sequence monitoring
- Indication of current or temperature (user selection)
- Indication of temperature in °F or °C (user selection)
- · 4-digit, 7-segment display
- Setting and status reading with the R100
- · Setting and status reading via the GENIbus.

#### **Tripping conditions**

- Overload
- Underload (dry running)
- Temperature (Tempcon sensor, PTC/thermal switch and Pt sensor)
- · Phase failure
- Phase sequence
- Overvoltage
- Undervoltage
- Power factor (cos φ)
- · Current unbalance.

#### Warnings

- Overload
- Underload
- · Temperature (Tempcon and Pt sensor)
- · Overvoltage
- Undervoltage
- Power factor (cos φ)

**Note:** In connection with single- and three-phase connection.

- Run capacitor (single-phase operation)
- Starting capacitor (single-phase operation)
- · Loss of communication in network
- · Harmonic distortion.

#### Learning function

- Phase sequence (three-phase operation)
- Run capacitor (single-phase operation)
- Starting capacitor (single-phase operation)
- Identification and measurement of Pt100/Pt1000 sensor circuit.

#### **External current transformers**

When fitted with external current transformers, the MP 204 unit can handle currents from 120 to 999 A. Grundfos can supply approved current transformers from stock (200/5A, 300/5A, 500/5A, 750/5A, 1000/5A).

#### Remote control R100

The R100 remote control from Grundfos allows for wireless infrared remote control of your MP 204 unit.

With the R100, you get access to a full range of options such as factory setting adjustment, service and fault finding.

#### Ready for bus communication

The MP 204 allows for monitoring and communication via GENIbus — a Grundfos-designed bus for exchange of pump data, alarms, status information, and setpoints. This enables users to connect the MP 204 to, for instance, SCADA systems.

96651601

#### Technical data - MP 204

Enclosure class IP 20

Ambient temperature -4 °F to +140 °F (-20 °C to +60 °C)

Relative air humidity 99%

Voltage range 100-480 VAC Current range 3-999 A Frequency 50 to 60 Hz IEC trip class 1-45 Special Grundfos trip class 0.1 to 30 s

Voltage variation -25 %/+15 % of nominal voltage EN 60947, EN 60335, UL/CSA 508 Approvals

CE, cUL, C-tick Marking Consumption Max. 5 W Plastic type Black PC / ABS

	Measuring range	Accuracy	Resolution
Current without external current transformers	3-120 A	±1 %	0.1 A
Current with external current transformers	120-999 A	±1 %	1 A
Phase-to-phase voltage	80-610 VAC	±1 %	1 V
Frequency	47-63 Hz	±1 %	0.5 Hz
Power	0-1 MW	±2 %	1 W
Power factor	0-0.99	±2 %	0.01
Energy consumption	0-4x10 <sup>9</sup> kWh	±5 %	1 kWh

IO 112 Description Product number



The IO 112 is a measuring module and a 1-channel protection unit for use in connection with the MP 204 motor protection unit. The module can be used for protection of pump against other factors than the electrical conditions, for instance dry-running. It can also be used as a stand-alone protection module.

The IO 112 interface has three inputs for measured values one potentiometer for setting of limits indicator lights indicating the

- · measured value of the input
- value of the limit set
- · alarm source
- pump status.

#### Electrical data:

- Supply voltage: 24 VAC ±10% 50/60 Hz or 24 VDC ±10%
   Supply current: Min. 2.4 A; max. 8 A
   Power consumption:Max. 5 W

Ambient temperature: =13 °F to+149 °F (=25 °C to +65 °C) • Enclosure class: IP 20

## **Control functions**

This table describes the protection provided by MP 204.

Control parameters	Function	Problem	Advantages
	The motor temperature is measured by means of the built-in Tempcon temperature transmitter and a signal is sent to MP 204 via the phase leads. In MP 204 the measured temperature is compared with the factory-set value (167 °F (75 °C)).	Overload, frequent starts/stops, operation against blocked discharge pipe, insufficient flow velocity past the motor.	Longer motor life, safe operating conditions, service indication.
Temperature	MMS The motor temperature is measured by means of the Pt100. The signal is sent to the MP 204 where the measured temperature is compared with the factory-set value. Temperature protection requires a submersible motor with a Pt100.		
	The motor temperature must be monitored during frequency converter operation.		
Overvoltage/ undervoltage	If the set trip value is exceeded, the motor will stop.	The installation is close to a transformer. The mains do not absorb load variations.	Important installation parameter, possibility of improving operating conditions.
Overload	The motor power input is measured on each of the three phases. The registered power input is an average of these three values. If the factory-set value is exceeded, the motor will stop.	Incorrect sizing of pump/motor, voltage supply failure, defective cable, blocking, wear or corrosion.	Longer pump life, safe operating conditions, service indication.
Underload (dry running)	The motor power input is measured on each of the three phases. The registered power input is an average of these three values. If the average value is lower than the factory-set value, the motor will stop.	Pump exposed to dry running or underload, for example caused by wear.	Traditional dry-running protection is no longer necessary, no extra cables.
Current unbalance	The power input of the motor is measured on each of the three phases.	Mains load is uneven, incipient motor defect, phase voltages diverging.	Motor protection against overload, service indication.
Phase sequence	MP 204 and motor are installed so that the phase sequence corresponds to correct direction of rotation. MP 204 monitors changes in the phase sequence.	Two phases are wrongly connected.	Ensures correct pump performance.
Phase failure	MP 204 checks the phases connected, phase failure will cause an alarm.	Phase failure	Indication of phase failure, and alarm.

#### R100 menus

#### 0. GENERAL

See the operating instructions for the R100.

#### 1. OPERATION

- · Operating mode
- · Actual trip
- · Actual warning 1
- · Actual warning 2
- Alarm log 1
- · Alarm log 2
- Alarm log 3
- · Alarm log 4
- · Alarm log 5.

#### 2. STATUS

Display of

- · Supply overview
- · Average current
- · Average voltage
- · Tempcon sensor
- Pt100/Pt1000 sensor
- Power input and energy consumption (described in the following)
- · Energy trip counter
- · Phase sequence
- · Current unbalance
- · Operating hours and number of starts
- · Trip counter of hours and starts
- · Starting capacitor
- · Run capacitor
- · Insulation resistance
- Cos φ
- · Harmonic distortion.

#### 3. LIMITS

Display and setting of warning and trip limits.

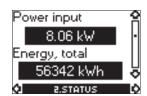
- · Tempcon sensor
- · Pt sensor
- · Tripping current
- · Current warning
- · Nominal voltage
- · Voltage limits
- · Current unbalance
- · Starting capacitor
- · Run capacitor
- · Insulation resistance
- Cos φ trip
- Cos φ warning.

#### 4. INSTALLATION

Setting and display of

- · Supply mains
- · Trip class (described in the following)
- Trip delay
- External current transformers
- · Power-on delay
- · Restarting (described in the following)
- Automatic restarting (described in the following)
- Tempcon sensor
- · Pt sensor
- Insulation resistance measurement
- PTC/thermal switch
- · Resetting of trip counters
- · Service interval
- · Number of automatic restarts
- · Units/display
- · MP 204 display
- · GENIbus ID number
- · Learning function.

#### Power input and energy consumption



Actual input power and motor energy consumption.

The energy consumption is an accumulated value which cannot be reset.

The power is calculated like this:

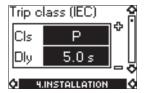
$$U_{average} = \frac{U_{L1-L2} + U_{L2-L3} + U_{L3-L1}}{3}[V]$$

$$I_{average} = \frac{I_{L1} + I_{L2} + I_{L3}}{3} [A]$$

$$cos\phi_{average} = \frac{cos\phi_{L1} + cos\phi_{L2} + cos\phi_{L3}}{3}[\text{-}]$$

$$P = (U_{average} \times I_{average} \times \sqrt{3} \times \cos \varphi_{average})[W]$$

#### Trip class



Line 1: Select IEC trip class (1 to 45).

If manual indication of trip delay in the case of overload is required, select trip class "P".

#### **Factory setting:**

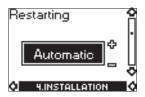
· Cls (trip class): P.

Line 2: Select trip delay.

#### **Factory setting:**

• Dly (trip delay): 10 s.

#### Restarting



Set whether restarting after tripping is to be

- Automatic (factory setting)
- Manual.

Setting of time, see section "Automatic restarting".

#### **Automatic restarting**



Set the time after which the MP 204 is to attempt automatic restarting of motor after cut-out.

The time runs from the moment when the value which triggered the fault has returned to normal.

### Factory setting:

• 300 s.

# G100 gateway for communication with Grundfos products

The G100 offers a wide selection of options for integration of Grundfos products provided with GENIbus interface into main control and monitoring systems.

The G100 enables a pump installation to meet future demands for optimum pump operation in terms of reliability, operating costs, centralization and automation.



Fig. 23 G100

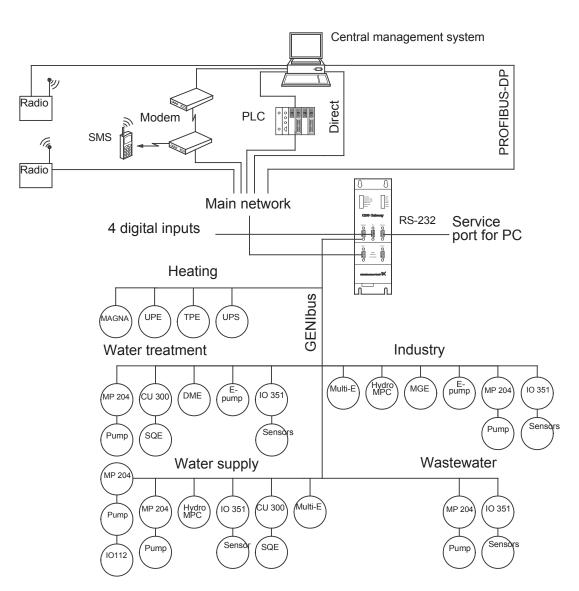


Fig. 24 Examples of G100 applications

MAN 0224 360'

#### **Product description**

The G100 Gateway enables communication of operating data, such as measured values and setpoints, between Grundfos products with GENIbus interface and a main network for control and monitoring.

As indicated in the illustration on page 92, the G100 is suitable for use in applications such as water supply, water treatment, wastewater, building automation and industry.

Common to above applications is that downtime is usually costly, and extra investments are therefore often made to achieve maximum reliability by monitoring selected operating variables.

The day-to-day operation, such as starting and stopping of pumps and changing of setpoints, can also be effected from the main system by communication with the G100. In addition, the G100 can be set up to send event-controlled status indications such as alarms via the SMS to mobile phones, and to make automatic alarm call-backs to a central management system.

#### **Data logging**

Besides the possibility of data communication, the G100 offers logging of up to 350,000 time-stamped data. The logged data can be transmitted to the main system or a PC for further analysis in a spreadsheet or similar program.

For the data logging, the "PC Tool G100 Data Log" software tool is used. The tool is part of the PC Tool G100 package, which is supplied with the G100.

#### Other features

- · Four digital inputs.
- Stop of all pumps in case of failing communication with the management system (optional).
- · Access code for modem communication (optional).
- · Alarm log.

#### Installation

Installation of the G100 is effected by the system integrator. The G100 is connected to the GENIbus as well as to the main network. All units on the GENIbus can thus be controlled from a central management system on the main network.

The "G100 Support Files" CD-ROM supplied with the G100 contains examples of programs to be used when the G100 is connected to the various main network systems. Included is also a description of the data points available in Grundfos products with GENIbus interface.

The "PC Tool G100" software tool included can be used for the installation and use of G100.

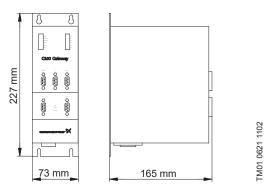


Fig. 25 Dimensional sketch

#### Technical data

#### Overview of protocols

Main system	Software protocol
PROFIBUS-DP	DP
Radio	Satt Control COMLI/Modbus
Modem	Satt Control COMLI/Modbus
PLC	Satt Control COMLI/Modbus
GSM mobile phone	SMS, UCP

#### Other possible connections

GENIbus RS-485: Connection of up to 32 units. Service port RS-232: For direct connection to a PC

or via radio modem.

Digital inputs: 4.

Voltage supply: 1 x 110-240 V, 50/60 Hz.

Ambient temperature: In operation:

-4 °F to +140 °F (-20 °C to +60 °C).

Enclosure class: IP 20. Weight: 1.8 kg.

#### Accessories

- PC Tool G100 package (supplied with the product)
- G100 Support Files CD-ROM (supplied with product)

#### **Product numbers**

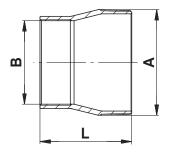
Product	Product number
G100 with Profibus-DP expansion board*	96411135
G100 with Radio/Modem/PLC expansion board*	96411136
G100 Basic Version*	96411137
PC Tool G100 package	96415783

<sup>\*</sup> CD-ROM with G100 Support Files included.

## **Connecting pieces**

The tables below show the range of connecting pieces for connection of thread-to-flange and thread-to-thread.

### Thread-to-thread





M01 2397 1698 - GrA2555

Fig. 26 Dimensional sketch and photo of connecting piece thread-to-thread

			Dimension	Product number			
Туре	Connecting piece	Thread-	to-thread	ı	— Floudt number		
		A	В	[in (mm)]	304 stainless steel	316 stainless steel	
385S	NPT 5→ NPT 4	NPT 5	NPT 4	4.76 (121)	190064	190586	
475S	NPT 5→ NPT 6	NPT 5	NPT 6	5.91 (150)	190070	190592	
625S 800S 1100S	NPT 6→ NPT 5	NPT 6	NPT 5	5.91 (150)	200135	200645	

#### Zinc anodes

#### **Application**

Cathodic protection by means of zinc can be used for corrosion protection of SP pumps in chloride-containing liquids such as brackish water and seawater.

Sacrificial anodes are placed on the outside of the pump and motor as protection against corrosion.

The number of anodes required depends on the pump and motor in question.

Please contact Grundfos for further details.

#### Liquid temperatures

- Seawater: Up to 95 °F (35 °C).
- Brackish water (min. 1500 ppm (g/m³) chloride): Up to 95 °F (35 °C).

#### Anode life

The zinc anodes have a life of one to four years, depending on operating conditions (temperature, flow and chloride content).

#### **SA-SPM 5 control boxes**

#### **Application**

SA-SPM 5 control boxes are used as starting units for single-phase, 3-wire motors, types MS 402B with power input lower than or equal to 1.5 hp (1.1 kW).

SA-SPM 5 is available in two versions, standard and DeLuxe. The standard version incorporates a motor -protective circuit breaker and thus protects the motor against overload. The DeLuxe version is identical to the standard version with the following addition a motor contactor is included for connection and disconnection of the power supply.

#### **Technical data**

Enclosure class: IP 42.

Ambient temperature: -4 °F to +140 °F

 $(-20 \, ^{\circ}\text{C to } +60 \, ^{\circ}\text{C}).$ 

Relative humidity: Maximum 95 %, normal

non-aggressive atmosphere.

#### **Product numbers**

#### Product numbers of zinc anodes

		Z	inc a	nodes	for p	umps	;				
		Used for pump type									
Product number	SP 5S to 75S	858	150S	2308	3008	385S	475S	625S	8008	1100S	
96421444	•	-	-	-	-	-	-	-	-	-	
96421445	-	•	•	•	•	-	-	-	-	-	
96421447	-	-	-	-	-	•	•	-	-	-	
96421448	-	-	-	-	-	-	•	-	-	-	
96421449	-	-	-	-	-	-	-	•	-	-	
96421450	-	-	-	-	-	-	-	•	•	•	

	Zinc anode	s for motors	
4" motors	6" motors	8" motors	10" motors
96421444	96421446	96421450	96564808



Fig. 27 SA-SPM 5 control box

2 0450 0507

		Des	crip	tion		
Product	1 x 220-230 V	1.5 hp	2.0 hp	3.0 hp	5.0 hp	Product number
SA-SPM 5 (Standard version)	•	•	-	-	-	91126212
SA-SPM 5 (DeLuxe version)	•	•	-	-	-	91126213
SA-SPM 5 (Standard version)	•	-	•	-	-	91126214
SA-SPM 5 (DeLuxe version)	•	-	•	-	-	91126215
SA-SPM 5 (Standard version)	•	-	-	•	-	91126216
SA-SPM 5 (DeLuxe version)	•	-	-	•	-	91126217
SA-SPM 5 (Standard version)	•	-	-	-	•	91126218
SA-SPM 5 (DeLuxe version)	•	-	-	-	•	91126219

#### Pt100

The Pt100 sensor offers these features:

- · Continuous monitoring of the motor temperature
- Protection against too high motor temperature.

Protecting the motor against too high motor temperature is the simplest and cheapest way of avoiding that motor lifetime is reduced. Pt100 ensures that operating conditions are not exceeded and indicates when it is time for service of the motor.

Monitoring and protection by means of Pt100 require the following parts:

- · Pt100 sensor
- · Relay, type PR 5714
- · Cable.

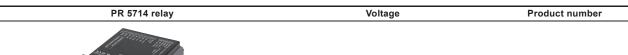
The PR 5714 relay is fitted with a Pt100 module. For both relays the following temperature limits are preset on delivery:

- +60 °C (+140 °F) warning limit
- +75 °C (+167 °F) stop limit.

#### **Technical data**

	Relay type
	PR 5714
Enclosure class	IP 65 (mounted in a control panel)
Ambient temperature	-4 °F to +140 °F (-20 °C to +60 °C)
Relative humidity	95 % (condensating)
Voltage variation	• 1 x 24-230 VAC ±10 %, 50 - 60 Hz. • 24-250 VDC ±20 %.
Approvals	UL, DNV
Mark	CE

	Cable length			Product num	ber
Pt100 sensor with/without PR 5714 relay and cable	[ft (m)]	PR 5714	MS6	MMS 6000, MMS 8000	MMS 10000, MMS 12000
	65.6 (20)	Yes	96408953	96494596	96437287
	131.2 (40)	Yes	96408681	96494597	96437288
	196.9 (60)	Yes	96408954	96494598	96437289
	262.5 (80)	Yes	96408955	96494599	96437290
	328.1 (100)	Yes	96408956	96494610	96437291
	65.6 (20)	No	96658626	96658629	96658633
	131.2 (40)	No	96658627	96658630	96658634
	196.9 (60)	No	96658628	96658631	96658635
	262.5 (80)	No	96658637	96658632	96658636
	328.1 (100)	No	96658638	96658639	96658640





24-230 VAC, 50/60 Hz / 24-250 VDC

96621274

	Cable length	Product	number
Pt100 sensor including cable	[ft (m)]	MS6, MMS 6000, MMS 8000	MMS 10000 MMS 12000
	65.6 (20)	96408957	96437784
	131.2 (40)	96408684	96437785
	196.9 (60)	96408958	96437786
	262.5 (80)	96408959	96437787
	328.1 (100)	96408960	96437788

Staybolts for Pt100	Description	Product number
	Bolt KIT for Pt100 (for MS6)	96611899

## 8. Energy consumption

# Energy consumption of submersible pumps

The percentage distribution of service life costs of a submersible pump for water supply is:

5 % initial costs (pump)

85 % operating costs / energy consumption

10 % maintenance costs.

It is obvious that the highest savings can be achieved within energy consumption!

The annual energy consumption, E, of a submersible pump can be calculated as follows:

 $E = c x h x P_1 (USD)$ 

c = specific energy price (USD/kWh)

h = operating hours/year (hours)

 $P_1$  = power input of the submersible pump (hp).

**Example:** Calculation of the annual energy consumption of the submersible pump, type 625S-3.

625S-3 with MS 8000, 60 hp, 3 x 460 V, 60 Hz.

**Duty point:** 

Flow rate: Q = 528 GPM

Total head: H = 335 ft

Specific energy price: c = USD 0.15/kWh

(consisting of day and night rate)

Operating hours/year: h = 3200.

$$P_1 = \frac{Q \times H \times \rho}{367 \times \eta_{pump} \times \eta_{motor}} \text{in kW}$$

Q = GPM

H = ft

Density  $\rho = \text{lb/ft}^3$  (assumed 1)

367 = conversion factor

 $\eta_{motor}$  = (example 84.5 %, in equation 0.845)

 $\eta_{pump}$  = (not to be confused with the stage

efficiency curve).

By showing the  $P_2/Q$  curve we make it easier for you to calculate the energy consumption.

$$P_1 = \frac{P_2}{\eta \text{ motor}}$$

 $P_2$  = 35 hp (power requirement of 625S-3 pump at 88 GPM, from curve  $P_2$  / Q.

#### Calculation of motor efficiency at duty point

As standard the SP 625S-3 is equipped with a 60 hp (45 kW for P1) MS6 motor.

At duty point (Q = 528 GPM) the pump requires 59 hp (44 kW for P1), thus:

a motor load of 87 % (44 kw / 45 kw) and a power reserve of 2 %.

From the table on page 72 the motor efficiency can be read as:

84.6 % at a load of 75 %. ( $\eta_{75\%}$ )

85.6 % at a load of 100 %.  $(\eta_{100\%})$ 

The interpolated value in this example is

 $\eta_{motor} = 85.1 \%$ ,  $\eta_{motor} = 0.851$ .

$$P_1 = \frac{44}{0.851} = 51.7 \text{ kW}$$

E = 0.15 USD/kWh x 3200 h x 51.7 kW.

The annual energy costs amount to USD 24816.

The pay-off time, A, (months) is calculated as follows:

$$A = \frac{Purchase price of energy-efficiency pump}{Energy savings/year} \times 12$$

#### Cable sizing

In order to obtain an economical duty of the pump the voltage drop should be low.

Today large water works already size cables for a maximum voltage drop of 1 %).

The hydraulic resistance in the discharge pipe should be as low as possible.

### 9. Cables

Grundfos offers submersible drop cables for all applications: 3-core cable, 4-core cable, single leads.

Cables for Grundfos 4" submersible motors are available with or without plugs. The submersible drop cable is chosen according to application and type of installation.

Standard version: Max. liquid temperature

+140 °F +60 °C).

Hot water version: Max. liquid temperature

+158 °F (+70 °C), for short periods

up to 194 °F (+90 °C)

(for MS only).

#### Tables indicating cable dimension in borehole

The tables indicate the maximum length of drop cables in meters from motor starter to pump at direct-on-line starting at different cable dimensions.

If star/delta starting is used the current will be reduced by  $\sqrt{3}$  (I x 0.58), meaning that the cable length may be  $\sqrt{3}$  longer (L x 1.73) than indicated in the tables.

If for example the operating current is 10 % lower than the full-load current, the cable may be 10 % longer than indicated in the tables.

The calculation of the cable length is based on a maximum voltage drop of 1 % to 3 % of the rated voltage and a water temperature of maximum +86  $^{\circ}$ F (30  $^{\circ}$ C).

In order to minimize operating losses the cable cross section may be increased compared to what is indicated in the tables. This is economical only if the borehole provides the necessary space, and if the operational time of the pump is long, especially if the operating voltage is below the rated voltage.

The table values are calculated on the basis of the formula:

Max. cable length of a single-phase submersible pump:

$$L = \frac{U \times \Delta U}{I \times 2 \times 100 \times \left(\cos \phi \times \frac{\rho}{q} + \sin \phi \times X_L\right)} [ft]$$

Max. cable length of a three-phase submersible pump:

$$L = \frac{U \times \Delta U}{I \times 1.73 \times 100 \times \left(\cos\phi \times \frac{\rho}{q} + \sin\phi \times X_L\right)} [ft]$$

where

U = Rated voltage [V]

 $\Delta U = Voltage drop [\%]$ 

I = Rated current of the motor [A]

q = Cross-section of submersible drop cable [in<sup>2</sup>]

 $X_L$  = Inductive resistance: 0.024 x 10<sup>-3</sup> [ $\Omega$ /ft]

cos<sub>Φ</sub>= Power factor

$$\sin \varphi = \sqrt{1 - \cos^2 \varphi}$$

ρ = Specific resistance: 9.5 X 10<sup>-6</sup> [Ω in<sup>2</sup>/ft]

Example

Motor size: 40 hp, MMS 8000

Rated current: 64.0 A

Rated voltage: 3 x 460 V, 60 Hz

Starting method: Direct-on-line

Power factor:  $\cos \varphi = 0.85$ 

Voltage drop: 3 %

Cross-section: 0.025 in<sup>2</sup>

 $\sin \varphi$ : 0.53

$$=\frac{460\times3}{64.0\times1.73\times100\times\left(0.85\times\frac{0.0000095}{0.025}+0.53\times0.024\times10^{-3}\right)}$$

L = 370 ft

#### Cable dimensions at 1 x 220 V, 60 Hz

Motor	hp	I <sub>n</sub> [A]	0.002 in <sup>2</sup>	0.004 in <sup>2</sup>	0.006 in <sup>2</sup>	0.009 in <sup>2</sup>	0.016 in <sup>2</sup>
	0.33	3.3	315	522	833	1243	2047
	0.50	4.4	239	397	630	938	1548
4"	0.75	6.6	157	262	417	620	1020
	1.00	7.7	121	203	321	482	797
	1.50	9.0	98	164	259	387	643

Maximum cable length in feet from motor starter to pump.

## Cable sizing chart

							1 phase, 6	0 Hz						
Motor	rating						С	opper wire siz	ze					
		14	12	10	8	6	4	2	0	00	000	0000	250	300
Volts	Нр					Maximum	motor cable le	ngth (motor s	ervice to entr	ance) [ft/m]				
	0.33	130 (40)	210 (64)	340 (104)	540 (165)	840 (256)	1300 (396)	1960 (597)	2910 (887)					
	0.5	100 (30)	160 (49)	250 (76)	390 (119)	620 (189)	960 (293)	1460 (445)	2160 (658)					
	0.33	550 (168)	880 (268)	1390 (424)	2190 (668)	3400 (1036)	5250 (1600)	7960 (2426)						
· •	0.5	400 (122)	650 (198)	1020 (311)	1610 (491)	2510 (765)	3880 (1183)	5880 (1792)						
· •	0.75	300 (91)	480 (146)	760 (232)	1200 (366)	1870 (570)	2890 (881)	4370 (1332)	6470 (1972)					
115	1	250 (76)	400 (122)	630 (192)	990 (302)	1540 (469)	2380 (725)	3610 (1100)	5360 (1634)	6520 (1987)				
115	1.5	190 (58)	310 (94)	480 (146)	770 (235)	1200 (366)	1870 (570)	2850 (869)	4280 (1305)	5240 (1597)				
	2	150 (46)	250 (76)	390 (119)	620 (189)	970 (296)	1530 (466)	2360 (719)	3620 (1103)	4480 (1366)				
•	3	120 (37)	190 (58)	300 (91)	470 (143)	750 (229)	1190 (363)	1850 (564)	2890 (881)	3610 (1100)				
	5		•	180 (55)	280 (85)	450 (137)	710 (216)	1110 (338)	1740 (530)	2170 (661)			•	
	7.5		•		200 (61)	310 (94)	490 (149)	750 (229)	1140 (347)	1410 (430)			•	
•	10					250 (76)	390 (119)	600 (183)	930 (283)	1160 (354)				

							3 phase, 6	0 Hz	·			·		
Motor	rating						C	opper wire size	ze					
		14	12	10	8	6	4	2	0	00	000	0000	250	300
Volts	Нр					Maximum	motor cable le	ength (motor s	ervice to entr	ance) [ft/m]				
	1.5	310 (94)	500 (152)	790 (241)	1260 (384)									
•	2	240 (73)	390 (119)	610 (186)	970 (296)	1520 (463)								
•	3	180 (55)	290 (88)	470 (143)	740 (226)	1160 (354)	1810 (552)							
•	5		170 (52)	280 (85)	440 (134)	690 (210)	1080 (329)	1660 (506)						
	7.5			200 (61)	310 (94)	490 (149)	770 (235)	1180 (360)	1770 (539)					
208	10				230 (70)	370 (113)	570 (174)	880 (268)	1330 (405)	1640 (500)				
	15					250 (76)	390 (119)	600 (183)	910 (277)	1110 (338)	1340 (408)			
•	20						300 (91)	460 (140)	700 (213)	860 (262)	1050 (320)	1270 (387)		
•	25							370 (113)	570 (174)	700 (213)	840 (256)	1030 (314)	1170 (357)	
•	30							310 (94)	470 (143)	580 (177)	700 (213)	850 (259)	970 (296)	1110 (338
	1.5	360 (110)	580 (177)	920 (280)	1450 (442)									
•	2	280 (85)	450 (137)	700 (213)	1110 (338)	1740 (530)								
	3	210 (64)	340 (104)	540 (165)	860 (262)	1340 (408)	2080 (634)							
•	5		200 (61)	320 (98)	510 (155)	800 (244)	1240 (378)	1900 (579)						
	7.5			230 (70)	360 (110)	570 (174)	890 (271)	1350 (411)	2030 (619)					
230	10				270 (82)	420 (128)	660 (201)	1010 (308)	1520 (463)	1870 (570)				
	15					290 (88)	450 (137)	690 (210)	1040 (317)	1280 (390)	1540 (469)			
	20						350 (107)	530 (162)	810 (247)	990 (302)	1200 (366)	1450 (442)		
	25						280 (85)	430 (131)	650 (198)	800 (244)	970 (296)	1170 (357)	1340 (408)	
•	30							350 (107)	540 (165)	660 (201)	800 (244)	970 (296)	1110 (338)	1270 (387
	1.5	1700 (518)												
•	2	1300 (396)	2070 (631)											
•	3	1000 (305)	1600 (488)	2520 (768)										
	5	590 (180)	950 (290)	1500 (457)	2360 (719)									
•	7.5	420 (128)	680 (207)	1070 (326)	1690 (515)	2640 (805)								
•	10	310 (94)	500 (152)	790 (241)	1250 (381)	1960 (597)	3050 (930)							
	15			540 (165)	850 (259)	1340 (408)	2090 (637)	3200 (975)						
•	20			410 (125)	650 (198)	1030 (314)	1610 (491)	2470 (753)	3730 (1137)					
	25				530 (162)	830 (253)	1300 (396)	1990 (607)	3010 (917)	3700 (1128)				
460	30				430 (131)	680 (207)	1070 (326)	1640 (500)	2490 (759)	3060 (933)	3700 (1128)			
	40						790 (241)	1210 (369)	1830 (558)	2250 (686)	2710 (826)	3290 (1003)		
•	50						640 (195)	980 (299)	1480 (451)	1810 (552)	2190 (668)	2650 (808)	3010 (917)	
•	60							830 (253)	1250 (381)	1540 (469)	1850 (564)	2240 (683)	2540 (774)	2890 (881
•	75								1030 (314)	1260 (384)	1520 (463)	1850 (564)	2100 (640)	2400 (732
•	100									940 (287)	1130 (344)	1380 (421)	1560 (475)	1790 (546
•	125											1080 (329)	1220 (372)	1390 (424
•	150												1050 (320)	1190 (363
•	200												1080 (329)	1300 (396)
	250													1080 (329)

Cables

							3 phase, 6	) Hz						
Motor	rating						С	opper wire siz	ze					
V. II.		14	12	10	8	6	4	2	0	00	000	0000	250	300
Volts	Нр					Maximum	motor cable le	ngth (motor s	ervice to entr	ance) [ft/m]				
	1.5	2620 (799)												
	2	2030 (619)												
	3	1580 (482)	2530 (771)											
	5	920 (280)	1480 (451)	2330 (710)										
	7.5	660 (201)	1060 (323)	1680 (512)	2650 (808)									
	10	490 (149)	780 (238)	1240 (378)	1950 (594)									
575	15		530 (162)	850 (259)	1340 (408)	2090 (637)								
373	20			650 (198)	1030 (314)	1610 (491)	2520 (768)							
	25			520 (158)	830 (253)	1300 (396)	2030 (619)	3110 (948)						
	30				680 (207)	1070 (326)	1670 (509)	2560 (780)	3880 (1183)					
	40					790 (241)	1240 (378)	1900 (579)	2860 (872)	3510 (1070)	•	•		
	50						1000 (305)	1540 (469)	2310 (704)	2840 (866)	3420 (1042)	•		
	60						850 (259)	1300 (396)	1960 (597)	2400 (732)	2890 (881)	3500 (1067)		
	75							1060 (323)	1600 (488)	1970 (600)	2380 (725)	2890 (881)	3290 (1003)	

- CAUTION: Use of wire size smaller than listed will void warranty.

  Notes:

  1. If aluminum conductor is used, multiply lengths by 0.5 Maximum allowable length of aluminum is considerably shorter than copper wire of same size.

  2. The portion of the total cable which is between the service entrance and a 3ø motor starter should not exceed 25% of the total maximum length to assure reliable starter operation. Single-phase control boxes may be connected at any point of the total cable length.

  3. Cables #14 to #0000 are AWG sizes, and 250 to 300 are MCM sizes.

## 10. Friction loss tables

		.5"	.75"	1"	1.25"	1.5"	2"	2.5"	3"	4"
U.S. gpm	U.S. gph	ID 0.622"	ID 0.824"	ID 1.049"	ID 1.380"	ID 1.610"	ID 2.067"	ID 2.469"	ID 3.068"	ID 4.026"
					Friction loss in	feet of head per	100 feet of pipe			
2	120	4.8								
3	180	10.0	2.5							
4	240	17.1	4.2							
5	300	25.8	6.3	1.9						
6	360	36.5	8.9	2.7						
7	420	48.7	11.8	3.6						
8	480	62.7	15.0	4.5						
9	540	78.3	18.8	5.7						
10	600	95.9	23.0	6.9						
12	720		32.6	9.6	2.5	1.2				
14	840		43.5	12.8	3.3	1.5				
16	960		56.3	16.5	4.2	2.0				
20	1,200		86.1	25.1	6.3	2.9				
25	1,500			38.7	9.6	4.5	1.3			
30	1,800			54.6	13.6	6.3	1.8			
35	2,100			73.3	18.2	8.4	2.4			
40	2,400			95.0	23.5	10.8	3.1	1.3		
45	2,700				29.4	13.5	3.9	1.6		
50	3,000				36.0	16.4	4.7	1.9		
60	3,600				51.0	23.2	6.6	2.7		
70	4,200				68.8	31.3	8.9	3.6	1.2	
80	4,800				89.2	40.5	11.4	4.6	1.6	
90	5,400					51.0	14.2	5.8	2.0	
100	6,000					62.2	17.4	7.1	2.4	
120	7,200						24.7	10.1	3.4	
140	8,400						33.2	13.5	4.5	1.2
160	9,600						43.0	17.5	5.8	1.5
200	12,000						66.3	27.0	8.9	2.3
260	15,600							45.0	14.8	3.7
300	18,000							59.6	19.5	4.9

Friction loss table - SCH 40 PVC pipe												
		.5"	.75"	1"	1.25"	1.5"	2"	2.5"	3"	4"		
J.S. gpm	U.S. gph	ID 0.622"	ID 0.824"	ID 1.049"	ID 1.380"	ID 1.610"	ID 2.067"	ID 2.469"	ID 3.068"	ID 4.026		
		Friction loss in feet of head per 100 feet of pipe										
2	120	4.1										
3	180	8.7	2.2									
4	240	14.8	3.7									
5	300	22.2	5.7	1.8								
6	360	31.2	8.0	2.5								
7	420	41.5	10.6	3.3								
8	480	53.0	13.5	4.2								
9	540	66.0	16.8	5.2								
10	600	80.5	20.4	6.3	1.7							
12	720		28.6	8.9	2.3	1.1						
14	840		38.0	11.8	3.1	1.4						
16	960		48.6	15.1	4.0	1.9						
20	1,200		60.5	22.8	6.0	2.8						
25	1,500			38.7	9.1	4.3	1.3					
30	1,800				12.7	6.0	1.8					
35	2,100				16.9	8.0	2.4					
40	2,400				21.6	10.2	3.0	1.1				
45	2,700				28.0	12.5	3.8	1.4				
50	3,000					15.4	4.6	1.7				
60	3,600					21.6	6.4	2.3				
70	4,200					28.7	8.5	3.0	1.2			
80	4,800					36.8	10.9	3.8	1.4			
90	5,400					45.7	13.6	4.8	1.8			
100	6,000					56.6	16.5	5.7	2.2			
120	7,200						23.1	8.0	3.0			
140	8,400						30.6	10.5	4.0	1.1		
160	9,600						39.3	13.4	5.0	1.4		
200	12,000						66.3	20.1	7.6	2.1		
260	15,600							32.4	12.2	3.4		
300	18,000							42.1	15.8	4.4		

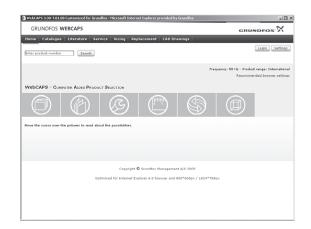
	Pipe and fitting	Nominal size of fitting and pipe							
Type of fitting and application		1/2"	3/4"	1"	1.25"	1.5"	2"	2.5"	
		Friction loss in equivalent length of straight pipe in feet							
Insert coupling	Plastic	3	3	3	3	3	3	3	
Threaded adapter (plastic to thread)	Plastic	3	3	3	3	3	3	3	
90° standard elbow	Steel	2	2	3	4	4	5	6	
90 Standard elbow -	Plastic	2	2	3	4	4	5	6	
Standard tee	Steel	1	2	2	3	3	4	4	
(flow through run)	Plastic	1	2	2	3	3	4	4	
Standard tee	Steel	4	5	6	7	8	11	13	
(flow through side)	Plastic	4	5	6	7	8	11	13	
Gate valve <sup>1</sup>	Steel	1	1	1	1	2	2	2	
Swing check valve <sup>1</sup>	Steel	5	7	9	12	13	17	21	

Notes: Based on Schedule 40 steel and plastic fittings

<sup>&</sup>lt;sup>1</sup>Friction loss figures are for screwed valves and are based on equivalent lengths of steel pipe.

# 11. Further product documentation

# **WebCAPS**

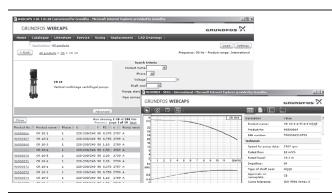


WebCAPS is a **Web**-based **C**omputer **A**ided **P**roduct **S**election program available on www.grundfos.com.

WebCAPS contains detailed information on more than 185,000 Grundfos products in more than 20 languages.

In WebCAPS, all information is divided into 6 sections:

- Catalog
- Literature
- Service
- Sizing
- Replacement
- CAD drawings.



# Catalog (

This section is based on fields of application and pump types, and contains

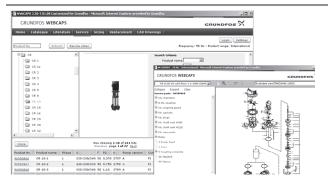
- · technical data
- curves (QH, Eta, P1, P2, etc) which can be adapted to the density and viscosity of the pumped liquid and show the number of pumps in operation
- · product photos
- dimensional drawings
- wiring diagrams
- · quotation texts, etc.



# Literature

In this section you can access all the latest documents of a given pump, such as  $\,$ 

- product guides
- installation and operating instructions
- service documentation, such as Service kit catalog and Service kit instructions
- quick guides
- · product brochures, etc.



### Service (3)

This section contains an easy-to-use interactive service catalog. Here you can find and identify service parts of both existing and discontinued Grundfos pumps.

Furthermore, this section contains service videos showing you how to replace service parts.

# Sizing (

This section is based on different fields of application and installation examples, and gives easy step-by-step instructions in how to

- · select the most suitable and efficient pump for your installation
- carry out advanced calculations based on energy consumption, payback periods, load profiles, life cycle costs, etc.
- analyse your selected pump via the built-in life cycle cost tool
- determine the flow velocity in wastewater applications, etc.

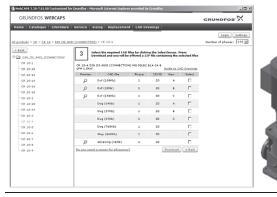


# Replacement (

In this section you find a guide to selecting and comparing replacement data of an installed pump in order to replace the pump with a more efficient Grundfos pump.

The section contains replacement data of a wide range of pumps produced by other manufacturers than Grundfos.

Based on an easy step-by-step guide, you can compare Grundfos pumps with the one you have installed on your site. When you have specified the installed pump, the guide will suggest a number of Grundfos pumps which can improve both comfort and efficiency.



# CAD drawings

In this section it is possible to download 2-dimensional (2D) and 3-dimensional (3D) CAD drawings of most Grundfos pumps.

These formats are available in WebCAPS:

### 2-dimensional drawings:

- · .dxf, wireframe drawings
- .dwg, wireframe drawings.

### 3-dimensional drawings:

- .dwg, wireframe drawings (without surfaces)
- · .stp, solid drawings (with surfaces)
- .eprt, E-drawings.

# **WinCAPS**



Fig. 28 WinCAPS CD-ROM

WinCAPS is a **Win**dows-based **C**omputer **A**ided **P**roduct **S**election program containing detailed information on more than 185,000 Grundfos products in more than 20 languages.

The program contains the same features and functions as WebCAPS, but is an ideal solution if no Internet connection is available.

WinCAPS is available on CD-ROM and updated once a year.



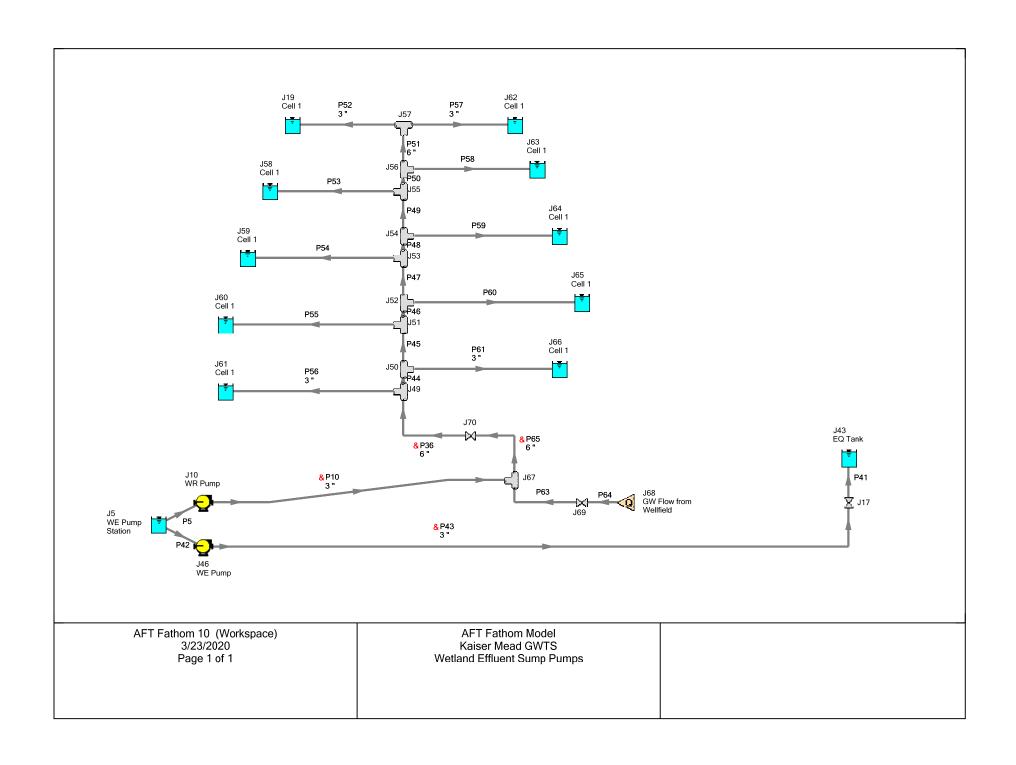
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- US



Wetlands Effluent Pump Station including Pipe Sizing



### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

### Model Reference Information

### General

Title: AFT Fathom Model

Analysis run on: 3/23/2020 3:03:33 PM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWT\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps v6.fth

Scenario: Base Scenario - HDPE Piping/Two Pumps - 50 gpm

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps\_v6\_F2.out

Execution Time= 0.13 seconds

Total Number Of Head/Pressure Iterations= 67

Total Number Of Flow Iterations= 11
Total Number Of Temperature Iterations= 0

Number Of Pipes= 27 Number Of Junctions= 28

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change Temperature Tolerance= 0.0001 relative change

Flow Relaxation= (Automatic)
Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 g

Turbulent Flow Above Reynolds Number= 4000 Laminar Flow Below Reynolds Number= 2300

Total Inflow= 150.0 gal/min Total Outflow= 150.0 gal/min

Maximum Static Pressure is 23.30 psia at Pipe 43 Inlet Minimum Static Pressure is 14.80 psia at Pipe 57 Outlet

**Warnings** 

No Warnings

**Pump Summary** 

### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

Jct	Results Diagram	Name	Vol. Flow (gal/min)	dH (feet)	Speed (Percent)	Ideal Power (hp)	Pump Efficiency (Percent)	Shaft Power (hp)	Motor Efficiency (Percent)	Motor Input Power (hp)	NPSHA (feet)
10	Show	WR Pump	50.00	10.62	65.25	0.1341	52.15	0.2572	80.00	0.3215	38.35
46	Show	WE Pump	50.00	14.95	74.49	0.1888	50.58	0.3733	80.00	0.4667	38.35

Jct	NPSHR
UCI	(feet)
10	N/A
46	N/A

# Valve Summary

Jct	Name	Valve Type	Vol. Flow (gal/min)	Mass Flow (lbm/sec)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	K	Valve State
17	Valve	REGULAR	50.00	6.948	0.0102928	0.023763	18.84	492.8	0.3229	Open
69	Valve	REGULAR	50.00	6.948	0.0102304	0.023619	16.75	494.3	0.3228	Open
70	Valve	REGULAR	100.00	13.897	0.0009805	0.002264	14.83	3,193.5	0.1197	Open

# Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Liquid Mass (Ibm)	Net Vol. Flow (gal/min)	Net Mass Flow (lbm/sec)
5	WE Pump Station	Infinite	N/A	1,936	14.70	N/A	N/A	-100.000	-13.8966
19	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	13.190	1.8329
43	EQ Tank	Infinite	N/A	1,950	14.70	N/A	N/A	50.000	6.9483
58	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	8.831	1.2272
59	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	7.294	1.0137
60	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	6.804	0.9455
61	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	7.611	1.0577
62	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	15.929	2.2136
63	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	11.296	1.5697
64	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	9.881	1.3731
65	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	8.862	1.2315
66	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	10.301	1.4315

# Pipe Output Table

Pi	ре	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)	dP Static Total (psid)
5	5	Pipe	50.000	12 inch	0.1433	16.86	16.86	1,931	1,931	0.000002168	0.000002168
1	0	Pipe	50.000	3 inch	2.1763	21.43	14.85	1,931	1,944	6.575308889	6.575308889

Pipe	dP Gravity (psid)	dH (feet)	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)
5	0.000	0.000005006	16.86	16.86	16.86	16.86
10	5.523	2.430565406	21.43	14.85	21.46	14.89

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)	dP Static Total (psid)
36	Pipe	100.000	6 inch	1.1033	14.83	14.82	1,944	1,944	0.015501299	0.015501299
41	Pipe	50.000	3 inch	2.1699	18.83	18.81	1,940	1,940	0.015918499	0.015918499
42	Pipe	50.000	12 inch	0.1433	16.86	16.86	1,931	1,931	0.000002168	0.000002168
43	Pipe	50.000	3 inch	2.1763	23.30	18.84	1,931	1,940	4.467759967	4.467759967
44	Pipe	92.391	6 inch	1.0194	14.82	14.82	1,944	1,944	0.000149734	0.000149734
45	Pipe	82.087	6 inch	0.9057	14.82	14.81	1,944	1,944	0.004856489	0.004856489
46	Pipe	75.284	6 inch	0.8306	14.82	14.82	1,944	1,944	0.000104170	0.000104170
47	Pipe	66.421	6 inch	0.7328	14.82	14.81	1,944	1,944	0.003339110	0.003339110
48	Pipe	59.127	6 inch	0.6524	14.81	14.81	1,944	1,944	0.000067984	0.000067984
49	Pipe	49.246	6 inch	0.5433	14.81	14.81	1,944	1,944	0.001970631	0.001970631
50	Pipe	40.414	6 inch	0.4459	14.81	14.81	1,944	1,944	0.000034819	0.000034819
51	Pipe	29.119	6 inch	0.3213	14.81	14.81	1,944	1,944	0.000785073	0.000785073
52	Pipe	13.190	3 inch	0.5741	14.81	14.80	1,944	1,944	0.008958963	0.008958963
53	Pipe	8.831	3 inch	0.3844	14.81	14.80	1,944	1,944	0.007655961	0.007655961
54	Pipe	7.294	3 inch	0.3175	14.81	14.80	1,944	1,944	0.008256774	0.008256774
55	Pipe	6.804	3 inch	0.2961	14.81	14.80	1,944	1,944	0.009765550	0.009765550
56	Pipe	7.611	3 inch	0.3313	14.82	14.80	1,944	1,944	0.011843837	0.011843837
57	Pipe	15.929	3 inch	0.6933	14.81	14.80	1,944	1,944	0.008893607	0.008893607
58	Pipe	11.296	3 inch	0.4917	14.81	14.80	1,944	1,944	0.007819287	0.007819287
59	Pipe	9.881	3 inch	0.4301	14.81	14.80	1,944	1,944	0.008524268	0.008524268
60	Pipe	8.862	3 inch	0.3857	14.81	14.80	1,944	1,944	0.010269552	0.010269552
61	Pipe	10.301	3 inch	0.4484	14.82	14.80	1,944	1,944	0.012494212	0.012494212
63	Pipe	50.000	3 inch	2.1699	16.74	14.85	1,940	1,944	1.889579415	1.889579415
64	Pipe	50.000	3 inch	2.1699	17.02	16.75	1,940	1,940	0.265304714	0.265304714
65	Pipe	100.000	6 inch	1.1033	14.85	14.83	1,944	1,944	0.018947665	0.018947665

# AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

Pipe	dP Gravity	dH (feet)	P Static In	P Static Out	P Stag.	P Stag.
36	(psid)	,	(psia)	(psia) 14.82	(psia) 14.84	(psia)
	0.000	0.035788202	14.83			14.83
41	0.000	0.036751401	18.83	18.81	18.86	18.84
42	0.000	0.000005006	16.86	16.86	16.86	16.86
43	3.898	1.314819203	23.30	18.84	23.34	18.87
44	0.000	0.000345694	14.82	14.82	14.83	14.83
45	0.000	0.011212286	14.82	14.81	14.83	14.82
46	0.000	0.000240499	14.82	14.82	14.82	14.82
47	0.000	0.007709079	14.82	14.81	14.82	14.82
48	0.000	0.000156957	14.81	14.81	14.82	14.82
49	0.000	0.004549640	14.81	14.81	14.82	14.81
50	0.000	0.000080388	14.81	14.81	14.81	14.81
51	0.000	0.001812516	14.81	14.81	14.81	14.81
52	0.000	0.020683761	14.81	14.80	14.81	14.80
53	0.000	0.017675493	14.81	14.80	14.81	14.80
54	0.000	0.019062603	14.81	14.80	14.81	14.80
55	0.000	0.022545949	14.81	14.80	14.81	14.80
56	0.000	0.027344136	14.82	14.80	14.82	14.80
57	0.000	0.020532873	14.81	14.80	14.81	14.80
58	0.000	0.018052565	14.81	14.80	14.81	14.80
59	0.000	0.019680172	14.81	14.80	14.81	14.80
60	0.000	0.023709550	14.81	14.80	14.81	14.80
61	0.000	0.028845672	14.82	14.80	14.82	14.80
63	1.624	0.612515037	16.74	14.85	16.78	14.89
64	0.000	0.612515037	17.02	16.75	17.05	16.79
65	0.000	0.043744905	14.85	14.83	14.86	14.84

# All Junction Table

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Mass Flow Rate Thru Jct (lbm/sec)	Loss Factor (K)
5	WE Pump Station	14.70	, ,	14.70	16.86	N/A	N/A	See Mult. Losses
10	WR Pump	16.86	21.43	16.86	21.46	50.000	6.9483	0.0000
17	Valve	18.84	18.83	18.87	18.86	50.000	6.9483	0.3229
19	Cell 1	14.70	14.80	14.70	14.80	13.190	1.8329	0.0000
43	EQ Tank	14.70	18.81	14.70	18.81	50.000	6.9483	1.0000
46	WE Pump	16.86	23.30	16.86	23.34	50.000	6.9483	0.0000
49	Tee or Wye	14.82	14.82	14.83	14.83	N/A	N/A	See Mult. Losses
50	Tee or Wye	14.82	14.82	14.83	14.83	N/A	N/A	See Mult. Losses
51	Tee or Wye	14.82	14.82	14.82	14.82	N/A	N/A	See Mult. Losses
52	Tee or Wye	14.82	14.82	14.82	14.82	N/A	N/A	See Mult. Losses

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Mass Flow Rate Thru Jct (lbm/sec)	Loss Factor (K)
53	Tee or Wye	14.81	14.81	14.82	14.82	N/A	N/A	See Mult. Losses
54	Tee or Wye	14.81	14.81	14.82	14.82	N/A	N/A	See Mult. Losses
55	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A	See Mult. Losses
56	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A	See Mult. Losses
57	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A	See Mult. Losses
58	Cell 1	14.70	14.80	14.70	14.80	8.831	1.2272	0.0000
59	Cell 1	14.70	14.80	14.70	14.80	7.294	1.0137	0.0000
60	Cell 1	14.70	14.80	14.70	14.80	6.804	0.9455	0.0000
61	Cell 1	14.70	14.80	14.70	14.80	7.611	1.0577	0.0000
62	Cell 1	14.70	14.80	14.70	14.80	15.929	2.2136	0.0000
63	Cell 1	14.70	14.80	14.70	14.80	11.296	1.5697	0.0000
64	Cell 1	14.70	14.80	14.70	14.80	9.881	1.3731	0.0000
65	Cell 1	14.70	14.80	14.70	14.80	8.862	1.2315	0.0000
66	Cell 1	14.70	14.80	14.70	14.80	10.301	1.4315	0.0000
67	Tee or Wye	14.84	14.84	14.86	14.86	N/A	N/A	See Mult. Losses
68	GW Flow from Wellfield	17.02	17.02	17.05	17.05	50.000	6.9483	0.0000
69	Valve	16.75	16.74	16.79	16.78	50.000	6.9483	0.3228
70	Valve	14.83	14.83	14.84	14.84	100.000	13.8966	0.1197

### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

### Model Reference Information

### General

Title: AFT Fathom Model

Analysis run on: 3/23/2020 2:59:32 PM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWT\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps v6.fth

Scenario: Base Scenario - HDPE Piping/Two Pumps - 50 gpm

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps\_v6\_F2.out

Execution Time= 0.59 seconds

Total Number Of Head/Pressure Iterations= 163

Total Number Of Flow Iterations= 35
Total Number Of Temperature Iterations= 0

Number Of Pipes= 27 Number Of Junctions= 28

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change Temperature Tolerance= 0.0001 relative change Flow Relaxation= (Automatic)

Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction

Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 g Turbulent Flow Above Reynolds Number= 4000

Laminar Flow Below Reynolds Number= 4000 Laminar Flow Below Reynolds Number= 2300

Total Inflow= 100.0 gal/min Total Outflow= 100.0 gal/min

Maximum Static Pressure is 23.30 psia at Pipe 43 Inlet Minimum Static Pressure is 14.80 psia at Pipe 57 Outlet

**Warnings** 

No Warnings

**Pump Summary** 

### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

Jct	Results Diagram	Name	Vol. Flow (gal/min)	dH (feet)	Speed (Percent)	Ideal Power (hp)	Pump Efficiency (Percent)	Shaft Power (hp)	Motor Efficiency (Percent)	Motor Input Power (hp)	NPSHA (feet)
10	Show	WR Pump	50.00	10.55	65.10	0.1333	52.17	0.2555	80.00	0.3193	38.35
46	Show	WE Pump	50.00	14.95	74.49	0.1888	50.58	0.3733	80.00	0.4667	38.35

Jct	NPSHR
UCI	(feet)
10	N/A
46	N/A

# Valve Summary

Jct	Name	Valve Type	Vol. Flow (gal/min)	Mass Flow (lbm/sec)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	К	Valve State
17	Valve	REGULAR	50.00	6.948	0.0102928	0.0237632	18.84	492.8	0.3229	Open
X69	Valve	REGULAR	0.00	0.000	N/A	N/A	N/A	N/A	N/A	Closed By User
70	Valve	REGULAR	50.00	6.948	0.0002451	0.0005659	14.81	3,193.5	0.1197	Open

# Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Liquid Mass (Ibm)	Net Vol. Flow (gal/min)	Net Mass Flow (lbm/sec)
5	WE Pump Station	Infinite	N/A	1,936	14.70	N/A	N/A	-100.0000010	-13.8965778
19	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	7.8196244	1.0866601
43	EQ Tank	Infinite	N/A	1,950	14.70	N/A	N/A	50.0000005	6.9482889
58	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	5.3080660	0.7376395
59	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	2.8974053	0.4026402
60	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	0.0009158	0.0001273
61	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	0.0011539	0.0001603
62	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	9.4649772	1.3153079
63	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	6.7910798	0.9437277
64	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	5.9779765	0.8307341
65	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	5.4021968	0.7507204
66	Cell 1	Infinite	N/A	1,944	14.70	N/A	N/A	6.3365328	0.8805612

# Pipe Output Table

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)
5	Pipe	50.0000018	12 inch	0.14331666	16.86	16.86	1,931	1,931	2.168E-06
10	Pipe	50.0000018	3 inch	2.17628548	21.40	14.82	1,931	1,944	6.575E+00

Pipe	dP Static Total (psid)	dP Gravity (psid)	dH (feet)	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)
5	2.168E-06	0.000	0.0000050062	16.86	16.86	16.86	16.86
10	6.575E+00	5.523	2.4305654062	21.40	14.82	21.43	14.86

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)
36	Pipe	50.0000018	6 inch	0.55165316	14.81	14.81	1,944	1,944	4.477E-03
41	Pipe	50.0000018	3 inch	2.16994703	18.83	18.81	1,940	1,940	1.592E-02
42	Pipe	50.0000018	12 inch	0.14331666	16.86	16.86	1,931	1,931	2.168E-06
43	Pipe	50.0000018	3 inch	2.17628548	23.30	18.84	1,931	1,940	4.468E+00
44	Pipe	49.9988488	6 inch	0.55164044	14.81	14.81	1,944	1,944	5.060E-05
45	Pipe	43.6623182	6 inch	0.48172910	14.81	14.81	1,944	1,944	1.595E-03
46	Pipe	43.6614021	6 inch	0.48171899	14.81	14.81	1,944	1,944	3.988E-05
47	Pipe	38.2592084	6 inch	0.42211625	14.81	14.81	1,944	1,944	1.265E-03
48	Pipe	35.3618430	6 inch	0.39014944	14.81	14.81	1,944	1,944	2.756E-05
49	Pipe	29.3837489	6 inch	0.32419275	14.81	14.81	1,944	1,944	7.976E-04
50	Pipe	24.0756800	6 inch	0.26562849	14.81	14.81	1,944	1,944	1.409E-05
51	Pipe	17.2846014	6 inch	0.19070209	14.81	14.81	1,944	1,944	3.174E-04
52	Pipe	7.8196244	3 inch	0.34035469	14.81	14.80	1,944	1,944	3.620E-03
53	Pipe	5.3080659	3 inch	0.23103733	14.81	14.80	1,944	1,944	3.189E-03
54	Pipe	2.8974053	3 inch	0.12611162	14.81	14.80	1,944	1,944	1.144E-03
55	Pipe	0.0009158	3 inch	0.00003986	14.80	14.80	1,944	1,944	3.452E-07
56	Pipe	0.0011539	3 inch	0.00005022	14.80	14.80	1,944	1,944	8.208E-08
57	Pipe	9.4649770	3 inch	0.41196983	14.81	14.80	1,944	1,944	3.596E-03
58	Pipe	6.7910799	3 inch	0.29558656	14.81	14.80	1,944	1,944	3.245E-03
59	Pipe	5.9779765	3 inch	0.26019566	14.81	14.80	1,944	1,944	3.584E-03
60	Pipe	5.4021967	3 inch	0.23513444	14.81	14.80	1,944	1,944	4.382E-03
61	Pipe	6.3365327	3 inch	0.27580207	14.81	14.80	1,944	1,944	5.401E-03
63	Pipe	0.0000000	3 inch	0.00000000	16.45	14.82	1,940	1,944	1.624E+00
64	Pipe	0.0000000	3 inch	0.00000000	No Solution	No Solution	1,940	1,940	0.000E+00
65	Pipe	50.0000018	6 inch	0.55165316	14.82	14.81	1,944	1,944	5.489E-03

# AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

D'	dP Static	dP.	dH	P Static In	P Static	P Stag. In	P Stag. Out
Pipe	Total (psid)	Gravity (psid)	(feet)	(psia)	Out (psia)	(psia)	(psia)
36	4.477E-03	0.000	0.0103362881	14.81	14.81	14.82	14.81
41	1.592E-02	0.000	0.0367514009	18.83	18.81	18.86	18.84
42	2.168E-06	0.000	0.0000050062	16.86	16.86	16.86	16.86
43	4.468E+00	3.898	1.3148192031	23.30	18.84	23.34	18.87
44	5.060E-05	0.000	0.0001168188	14.81	14.81	14.81	14.81
45	1.595E-03	0.000	0.0036825613	14.81	14.81	14.81	14.81
46	3.988E-05	0.000	0.0000920606	14.81	14.81	14.81	14.81
47	1.265E-03	0.000	0.0029210473	14.81	14.81	14.81	14.81
48	2.756E-05	0.000	0.0000636212	14.81	14.81	14.81	14.81
49	7.976E-04	0.000	0.0018413838	14.81	14.81	14.81	14.81
50	1.409E-05	0.000	0.0000325381	14.81	14.81	14.81	14.81
51	3.174E-04	0.000	0.0007327803	14.81	14.81	14.81	14.81
52	3.620E-03	0.000	0.0083571079	14.81	14.80	14.81	14.80
53	3.189E-03	0.000	0.0073622822	14.81	14.80	14.81	14.80
54	1.144E-03	0.000	0.0026413374	14.81	14.80	14.81	14.80
55	3.452E-07	0.000	0.0000007970	14.80	14.80	14.80	14.80
56	8.208E-08	0.000	0.0000001895	14.80	14.80	14.80	14.80
57	3.596E-03	0.000	0.0083033092	14.81	14.80	14.81	14.80
58	3.245E-03	0.000	0.0074909847	14.81	14.80	14.81	14.80
59	3.584E-03	0.000	0.0082734305	14.81	14.80	14.81	14.80
60	4.382E-03	0.000	0.0101162907	14.81	14.80	14.81	14.80
61	5.401E-03	0.000	0.0124685988	14.81	14.80	14.81	14.80
63	1.624E+00	1.624	0.0000000000	16.45	14.82	16.45	14.82
64	0.000E+00	0.000	0.0000000000	No Solution	No Solution	No Solution	No Solution
65	5.489E-03	0.000	0.0126726979	14.82	14.81	14.82	14.82

# All Junction Table

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Mass Flow Rate Thru Jct (lbm/sec)
5	WE Pump Station	14.70	16.86	14.70	16.86	N/A	N/A
10	WR Pump	16.86	21.40	16.86	21.43	50.0000018	6.9482889
17	Valve	18.84	18.83	18.87	18.86	50.0000018	6.9482889
19	Cell 1	14.70	14.80	14.70	14.80	7.8196244	1.0866601
43	EQ Tank	14.70	18.81	14.70	18.81	50.0000018	6.9482889
46	WE Pump	16.86	23.30	16.86	23.34	50.0000018	6.9482889
49	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
50	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
51	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
52	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A

Jct	Loss Factor (K)
5	See Mult. Losses
10	0.0000
17	0.3229
19	0.0000
43	1.0000
46	0.0000
49	See Mult. Losses
50	See Mult. Losses
51	See Mult. Losses
52	See Mult. Losses

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Mass Flow Rate Thru Jct (lbm/sec)
53	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
54	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
55	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
56	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
57	Tee or Wye	14.81	14.81	14.81	14.81	N/A	N/A
58	Cell 1	14.70	14.80	14.70	14.80	5.3080659	0.7376395
59	Cell 1	14.70	14.80	14.70	14.80	2.8974053	0.4026402
60	Cell 1	14.70	14.80	14.70	14.80	0.0009158	0.0001273
61	Cell 1	14.70	14.80	14.70	14.80	0.0011539	0.0001603
62	Cell 1	14.70	14.80	14.70	14.80	9.4649770	1.3153079
63	Cell 1	14.70	14.80	14.70	14.80	6.7910799	0.9437277
64	Cell 1	14.70	14.80	14.70	14.80	5.9779765	0.8307341
65	Cell 1	14.70	14.80	14.70	14.80	5.4021967	0.7507204
66	Cell 1	14.70	14.80	14.70	14.80	6.3365327	0.8805612
67	Tee or Wye	14.82	14.82	14.82	14.82	N/A	N/A
68	GW Flow from Wellfield	No Solution	No Solution	No Solution	No Solution	0.0000000	0.0000000
X69	Valve	No Solution	16.45	No Solution	16.45	0.0000000	0.0000000
70	Valve	14.81	14.81	14.82	14.82	50.0000018	6.9482889

Jct	Loss Factor (K)
53	See Mult. Losses
54	See Mult. Losses
55	See Mult. Losses
56	See Mult. Losses
57	See Mult. Losses
58	0.0000
59	0.0000
60	0.0000
61	0.0000
62	0.0000
63	0.0000
64	0.0000
65	0.0000
66	0.0000
67	See Mult. Losses
68	0.0000
X69	0.0000
70	0.1197

### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

### Model Reference Information

### General

Title: AFT Fathom Model

Analysis run on: 3/23/2020 2:54:35 PM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWT\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps v6.fth

Scenario: Base Scenario - HDPE Piping/Two Pumps - 75 gpm

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps\_v6\_F1.out

Execution Time= 0.18 seconds

Total Number Of Head/Pressure Iterations= 78

Total Number Of Flow Iterations= 12 Total Number Of Temperature Iterations= 0

Number Of Pipes= 27 Number Of Junctions= 28

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change Temperature Tolerance= 0.0001 relative change Flow Relaxation= (Automatic)

Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 g

Turbulent Flow Above Reynolds Number= 4000

Laminar Flow Below Reynolds Number= 2300

Total Inflow= 225.0 gal/min Total Outflow= 225.0 gal/min

Maximum Static Pressure is 23.94 psia at Pipe 43 Inlet Minimum Static Pressure is 14.80 psia at Pipe 57 Outlet

**Warnings** 

No Warnings

**Pump Summary** 

### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

Jct	Results Diagram	Name	Vol. Flow (gal/min)	dH (feet)	Speed (Percent)	Ideal Power (hp)	Pump Efficiency (Percent)	Shaft Power (hp)	Motor Efficiency (Percent)	Motor Input Power (hp)	NPSHA (feet)
10	Show	WR Pump	75.00	13.47	79.92	0.2553	51.55	0.4953	80.00	0.6191	38.35
46	Show	WE Pump	75.00	16.50	85.60	0.3126	52.28	0.5979	80.00	0.7473	38.35

Jct	NPSHR (feet)
10	N/A
46	N/A

# Valve Summary

Jct	Name	Valve Type	Vol. Flow (gal/min)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	К	Valve State
17	Valve	REGULAR	75.00	0.003860	0.008911	18.85	1,207.2	0.05381	Open
69	Valve	REGULAR	75.00	0.023018	0.053143	17.10	494.3	0.32278	Open
70	Valve	REGULAR	150.00	0.002206	0.005093	14.86	3,193.5	0.11966	Open

# Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Net Vol. Flow (gal/min)
5	WE Pump Station	Infinite	N/A	1,936	14.70	N/A	-150.00
19	Cell 1	Infinite	N/A	1,944	14.70	N/A	20.07
43	EQ Tank	Infinite	N/A	1,950	14.70	N/A	75.00
58	Cell 1	Infinite	N/A	1,944	14.70	N/A	13.28
59	Cell 1	Infinite	N/A	1,944	14.70	N/A	10.90
60	Cell 1	Infinite	N/A	1,944	14.70	N/A	10.11
61	Cell 1	Infinite	N/A	1,944	14.70	N/A	11.23
62	Cell 1	Infinite	N/A	1,944	14.70	N/A	24.20
63	Cell 1	Infinite	N/A	1,944	14.70	N/A	16.99
64	Cell 1	Infinite	N/A	1,944	14.70	N/A	14.78
65	Cell 1	Infinite	N/A	1,944	14.70	N/A	13.20
66	Cell 1	Infinite	N/A	1,944	14.70	N/A	15.24

# Pipe Output Table

Pip	ре	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)	dP Static Total (psid)
5	5	Pipe	75.00	12 inch	0.2150	16.86	16.86	1,931	1,931	0.000004289	0.000004289
10	0	Pipe	75.00	3 inch	3.2644	22.63	14.91	1,931	1,944	7.718771547	7.718771547

Pipe	dP Gravity (psid)	dH (feet)	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)
5	0.000	0.000009903	16.86	16.86	16.86	16.86
10	5.523	5.070503691	22.63	14.91	22.70	14.98

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)	dP Static Total (psid)
36	Pipe	150.00	6 inch	1.6550	14.86	14.83	1,944	1,944	0.032241736	0.032241736
41	Pipe	75.00	3 inch	3.2549	18.84	18.81	1,940	1,940	0.032788716	0.032788716
42	Pipe	75.00	12 inch	0.2150	16.86	16.86	1,931	1,931	0.000004289	0.000004289
43	Pipe	75.00	3 inch	3.2644	23.94	18.85	1,931	1,940	5.088187099	5.088187099
44	Pipe	138.77	6 inch	1.5311	14.83	14.83	1,944	1,944	0.000308779	0.000308779
45	Pipe	123.53	6 inch	1.3630	14.84	14.83	1,944	1,944	0.010038104	0.010038104
46	Pipe	113.42	6 inch	1.2514	14.83	14.83	1,944	1,944	0.000215569	0.000215569
47	Pipe	100.22	6 inch	1.1058	14.83	14.82	1,944	1,944	0.006920303	0.006920303
48	Pipe	89.32	6 inch	0.9855	14.82	14.82	1,944	1,944	0.000141024	0.000141024
49	Pipe	74.54	6 inch	0.8224	14.83	14.82	1,944	1,944	0.004094475	0.004094475
50	Pipe	61.26	6 inch	0.6759	14.82	14.82	1,944	1,944	0.000072375	0.000072375
51	Pipe	44.27	6 inch	0.4885	14.82	14.82	1,944	1,944	0.001634465	0.001634465
52	Pipe	20.07	3 inch	0.8737	14.82	14.80	1,944	1,944	0.018662866	0.018662866
53	Pipe	13.28	3 inch	0.5780	14.82	14.80	1,944	1,944	0.015542499	0.015542499
54	Pipe	10.90	3 inch	0.4745	14.82	14.80	1,944	1,944	0.016543591	0.016543591
55	Pipe	10.11	3 inch	0.4401	14.82	14.80	1,944	1,944	0.019351661	0.019351661
56	Pipe	11.23	3 inch	0.4887	14.83	14.80	1,944	1,944	0.023215324	0.023215324
57	Pipe	24.20	3 inch	1.0533	14.82	14.80	1,944	1,944	0.018513128	0.018513128
58	Pipe	16.99	3 inch	0.7395	14.82	14.80	1,944	1,944	0.015926303	0.015926303
59	Pipe	14.78	3 inch	0.6433	14.82	14.80	1,944	1,944	0.017167186	0.017167186
60	Pipe	13.20	3 inch	0.5745	14.82	14.80	1,944	1,944	0.020500557	0.020500557
61	Pipe	15.24	3 inch	0.6632	14.83	14.80	1,944	1,944	0.024689401	0.024689401
63	Pipe	75.00	3 inch	3.2549	17.08	14.91	1,940	1,944	2.170749694	2.170749694
64	Pipe	75.00	3 inch	3.2549	17.65	17.10	1,940	1,940	0.546474993	0.546474993
65	Pipe	150.00	6 inch	1.6550	14.90	14.86	1,944	1,944	0.039337013	0.039337013

# AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

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Pipe	dP Gravity	dH	P Static In	P Static Out	P Stag. In	P Stag. Out
i ipe	(psid)	(feet)	(psia)	(psia)	(psia)	(psia)
36	0.000	0.074437229	14.86	14.83	14.88	14.85
41	0.000	0.075700056	18.84	18.81	18.91	18.88
42	0.000	0.000009903	16.86	16.86	16.86	16.86
43	3.898	2.747213454	23.94	18.85	24.01	18.92
44	0.000	0.000712885	14.83	14.83	14.85	14.85
45	0.000	0.023175199	14.84	14.83	14.85	14.84
46	0.000	0.000497689	14.83	14.83	14.84	14.84
47	0.000	0.015977061	14.83	14.82	14.84	14.83
48	0.000	0.000325585	14.82	14.82	14.83	14.83
49	0.000	0.009453009	14.83	14.82	14.83	14.83
50	0.000	0.000167093	14.82	14.82	14.83	14.83
51	0.000	0.003773526	14.82	14.82	14.83	14.82
52	0.000	0.043087384	14.82	14.80	14.82	14.80
53	0.000	0.035883321	14.82	14.80	14.82	14.80
54	0.000	0.038194566	14.82	14.80	14.82	14.80
55	0.000	0.044677621	14.82	14.80	14.82	14.80
56	0.000	0.053597747	14.83	14.80	14.83	14.80
57	0.000	0.042741681	14.82	14.80	14.82	14.80
58	0.000	0.036769419	14.82	14.80	14.82	14.80
59	0.000	0.039634274	14.82	14.80	14.82	14.80
60	0.000	0.047330104	14.82	14.80	14.82	14.80
61	0.000	0.057000981	14.83	14.80	14.83	14.80
63	1.624	1.261659265	17.08	14.91	17.15	14.98
64	0.000	1.261659265	17.65	17.10	17.72	17.17
65	0.000	0.090818258	14.90	14.86	14.92	14.88

# All Junction Table

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Loss Factor (K)
5	WE Pump Station	14.70	16.86	14.70	16.86	N/A	See Mult. Losses
10	WR Pump	16.86	22.63	16.86	22.70	75.00	0.00000
17	Valve	18.85	18.84	18.92	18.91	75.00	0.05381
19	Cell 1	14.70	14.80	14.70	14.80	20.07	0.00000
43	EQ Tank	14.70	18.81	14.70	18.81	75.00	1.00000
46	WE Pump	16.86	23.94	16.86	24.01	75.00	0.00000
49	Tee or Wye	14.84	14.84	14.85	14.85	N/A	See Mult. Losses
50	Tee or Wye	14.84	14.84	14.85	14.85	N/A	See Mult. Losses
51	Tee or Wye	14.83	14.83	14.84	14.84	N/A	See Mult. Losses
52	Tee or Wye	14.83	14.83	14.84	14.84	N/A	See Mult. Losses

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Loss Factor (K)
53	Tee or Wye	14.83	14.83	14.83	14.83	N/A	See Mult. Losses
54	Tee or Wye	14.83	14.83	14.83	14.83	N/A	See Mult. Losses
55	Tee or Wye	14.82	14.82	14.83	14.83	N/A	See Mult. Losses
56	Tee or Wye	14.82	14.82	14.83	14.83	N/A	See Mult. Losses
57	Tee or Wye	14.82	14.82	14.82	14.82	N/A	See Mult. Losses
58	Cell 1	14.70	14.80	14.70	14.80	13.28	0.00000
59	Cell 1	14.70	14.80	14.70	14.80	10.90	0.00000
60	Cell 1	14.70	14.80	14.70	14.80	10.11	0.00000
61	Cell 1	14.70	14.80	14.70	14.80	11.23	0.00000
62	Cell 1	14.70	14.80	14.70	14.80	24.20	0.00000
63	Cell 1	14.70	14.80	14.70	14.80	16.99	0.00000
64	Cell 1	14.70	14.80	14.70	14.80	14.78	0.00000
65	Cell 1	14.70	14.80	14.70	14.80	13.20	0.00000
66	Cell 1	14.70	14.80	14.70	14.80	15.24	0.00000
67	Tee or Wye	14.87	14.87	14.92	14.92	N/A	See Mult. Losses
68	GW Flow from Wellfield	17.65	17.65	17.72	17.72	75.00	0.00000
69	Valve	17.10	17.08	17.17	17.15	75.00	0.32278
70	Valve	14.86	14.86	14.88	14.88	150.00	0.11966

### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

### Model Reference Information

### General

Title: AFT Fathom Model

Analysis run on: 3/23/2020 2:49:45 PM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWT\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps v6.fth

Scenario: Base Scenario - HDPE Piping/Two Pumps - 75 gpm

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Wetland Sump Pumps Model\Wetland Sump Pumps\_v6\_F1.out

Execution Time= 0.18 seconds

Total Number Of Head/Pressure Iterations= 61

Total Number Of Flow Iterations= 11
Total Number Of Temperature Iterations= 0

Number Of Pipes= 27 Number Of Junctions= 28

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change

Temperature Tolerance= 0.0001 relative change

Flow Relaxation= (Automatic)
Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction

Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 g

Turbulent Flow Above Reynolds Number= 4000

Laminar Flow Below Reynolds Number= 2300

Total Inflow= 150.0 gal/min Total Outflow= 150.0 gal/min

Maximum Static Pressure is 23.94 psia at Pipe 43 Inlet

Minimum Static Pressure is 14.80 psia at Pipe 57 Outlet

**Warnings** 

No Warnings

**Pump Summary** 

### AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

Jct	Results Diagram	Name	Vol. Flow (gal/min)	dH (feet)	Speed (Percent)	Ideal Power (hp)	Pump Efficiency (Percent)	Shaft Power (hp)	Motor Efficiency (Percent)	Motor Input Power (hp)	NPSHA (feet)
10	Show	WR Pump	75.00	13.33	79.63	0.2525	51.49	0.4904	80.00	0.6130	38.35
46	Show	WE Pump	75.00	16.50	85.60	0.3126	52.28	0.5979	80.00	0.7473	38.35

Jct	NPSHR
001	(feet)
10	N/A
46	N/A

# Valve Summary

Jct	Name	Valve Type	Vol. Flow (gal/min)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	К	Valve State
17	Valve	REGULAR	75.00	3.860E-03	8.911E-03	18.85	1,207	0.05381	Open
X69	Valve	REGULAR	0.00	N/A	N/A	N/A	N/A	N/A	Closed By User
70	Valve	REGULAR	75.00	5.515E-04	1.273E-03	14.82	3,194	0.11966	Open

# Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Net Vol. Flow (gal/min)
5	WE Pump Station	Infinite	N/A	1,936	14.70	N/A	-150.000
19	Cell 1	Infinite	N/A	1,944	14.70	N/A	9.796
43	EQ Tank	Infinite	N/A	1,950	14.70	N/A	75.000
58	Cell 1	Infinite	N/A	1,944	14.70	N/A	6.611
59	Cell 1	Infinite	N/A	1,944	14.70	N/A	5.483
60	Cell 1	Infinite	N/A	1,944	14.70	N/A	5.134
61	Cell 1	Infinite	N/A	1,944	14.70	N/A	5.770
62	Cell 1	Infinite	N/A	1,944	14.70	N/A	11.846
63	Cell 1	Infinite	N/A	1,944	14.70	N/A	8.457
64	Cell 1	Infinite	N/A	1,944	14.70	N/A	7.425
65	Cell 1	Infinite	N/A	1,944	14.70	N/A	6.678
66	Cell 1	Infinite	N/A	1,944	14.70	N/A	7.798

# Pipe Output Table

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Elevation Inlet Outlet (feet) (feet)		dP Stag. Total (psid)
5	Pipe	75.000	12 inch	0.2150	16.86	16.86	1,931	1,931	0.000004289
10	Pipe	75.000	3 inch	3.2644	22.56	14.84	1,931	1,944	7.718771547

Pipe	dP Static Total (psid)	dP Gravity (psid)	dH (feet)	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)
5	0.000004289	0.000	0.000009903	16.86	16.86	16.86	16.86
10	7.718771547	5.523	5.070503691	22.56	14.84	22.63	14.91

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)
36	Pipe	75.000	6 inch	0.8275	14.82	14.81	1,944	1,944	0.009243161
41	Pipe	75.000	3 inch	3.2549	18.84	18.81	1,940	1,940	0.032788716
42	Pipe	75.000	12 inch	0.2150	16.86	16.86	1,931	1,931	0.000004289
43	Pipe	75.000	3 inch	3.2644	23.94	18.85	1,931	1,940	5.088187099
44	Pipe	69.232	6 inch	0.7638	14.81	14.81	1,944	1,944	0.000089820
45	Pipe	61.431	6 inch	0.6778	14.81	14.81	1,944	1,944	0.002909022
46	Pipe	56.298	6 inch	0.6211	14.81	14.81	1,944	1,944	0.000062354
47	Pipe	49.619	6 inch	0.5474	14.81	14.81	1,944	1,944	0.001996994
48	Pipe	44.136	6 inch	0.4870	14.81	14.81	1,944	1,944	0.000040640
49	Pipe	36.711	6 inch	0.4050	14.81	14.81	1,944	1,944	0.001176912
50	Pipe	30.099	6 inch	0.3321	14.81	14.81	1,944	1,944	0.000020794
51	Pipe	21.642	6 inch	0.2388	14.81	14.81	1,944	1,944	0.000468478
52	Pipe	9.796	3 inch	0.4264	14.81	14.80	1,944	1,944	0.005344160
53	Pipe	6.611	3 inch	0.2878	14.81	14.80	1,944	1,944	0.004647734
54	Pipe	5.483	3 inch	0.2387	14.81	14.80	1,944	1,944	0.005056470
55	Pipe	5.134	3 inch	0.2235	14.81	14.80	1,944	1,944	0.006023690
56	Pipe	5.770	3 inch	0.2512	14.81	14.80	1,944	1,944	0.007357982
57	Pipe	11.846	3 inch	0.5156	14.81	14.80	1,944	1,944	0.005307817
58	Pipe	8.457	3 inch	0.3681	14.81	14.80	1,944	1,944	0.004736490
59	Pipe	7.425	3 inch	0.3232	14.81	14.80	1,944	1,944	0.005202680
60	Pipe	6.678	3 inch	0.2906	14.81	14.80	1,944	1,944	0.006303891
61	Pipe	7.798	3 inch	0.3394	14.81	14.80	1,944	1,944	0.007720843
63	Pipe	0.000	3 inch	0.0000	16.46	14.84	1,940	1,944	1.624274701
64	Pipe	0.000	3 inch	0.0000	No Solution	No Solution	1,940	1,940	0.000000000
65	Pipe	75.000	6 inch	0.8275	14.83	14.82	1,944	1,944	0.011312632

# AFT Fathom Model Kaiser Mead GWTS Wetland Sump Pumps Model

Dim -	dP Static	dP	dH	P Static In	P Static	P Stag. In	P Stag. Out
Pipe	Total (psid)	Gravity (psid)	(feet)	(psia)	Out (psia)	(psia)	(psia)
36	0.009243161	0.000	0.021339897	14.82	14.81	14.83	14.82
41	0.032788716	0.000	0.075700056	18.84	18.81	18.91	18.88
42	0.000004289	0.000	0.000009903	16.86	16.86	16.86	16.86
43	5.088187099	3.898	2.747213454	23.94	18.85	24.01	18.92
44	0.000089820	0.000	0.000207369	14.81	14.81	14.82	14.82
45	0.002909022	0.000	0.006716126	14.81	14.81	14.82	14.81
46	0.000062354	0.000	0.000143959	14.81	14.81	14.81	14.81
47	0.001996994	0.000	0.004610506	14.81	14.81	14.81	14.81
48	0.000040640	0.000	0.000093826	14.81	14.81	14.81	14.81
49	0.001176912	0.000	0.002717163	14.81	14.81	14.81	14.81
50	0.000020794	0.000	0.000048008	14.81	14.81	14.81	14.81
51	0.000468478	0.000	0.001081586	14.81	14.81	14.81	14.81
52	0.005344160	0.000	0.012338184	14.81	14.80	14.81	14.80
53	0.004647734	0.000	0.010730329	14.81	14.80	14.81	14.80
54	0.005056470	0.000	0.011673987	14.81	14.80	14.81	14.80
55	0.006023690	0.000	0.013907031	14.81	14.80	14.81	14.80
56	0.007357982	0.000	0.016987542	14.81	14.80	14.81	14.80
57	0.005307817	0.000	0.012254278	14.81	14.80	14.81	14.80
58	0.004736490	0.000	0.010935243	14.81	14.80	14.81	14.80
59	0.005202680	0.000	0.012011547	14.81	14.80	14.81	14.80
60	0.006303891	0.000	0.014553937	14.81	14.80	14.81	14.80
61	0.007720843	0.000	0.017825287	14.81	14.80	14.81	14.80
63	1.624274701	1.624	0.000000000	16.46	14.84	16.46	14.84
64	0.000000000	0.000	0.000000000	No Solution	No Solution	No Solution	No Solution
65	0.011312632	0.000	0.026117731	14.83	14.82	14.84	14.83

# All Junction Table

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Loss Factor (K)
5	WE Pump Station	14.70	16.86	14.70	16.86	N/A	See Mult. Losses
10	WR Pump	16.86	22.56	16.86	22.63	75.000	0.00000
17	Valve	18.85	18.84	18.92	18.91	75.000	0.05381
19	Cell 1	14.70	14.80	14.70	14.80	9.796	0.00000
43	EQ Tank	14.70	18.81	14.70	18.81	75.000	1.00000
46	WE Pump	16.86	23.94	16.86	24.01	75.000	0.00000
49	Tee or Wye	14.81	14.81	14.82	14.82	N/A	See Mult. Losses
50	Tee or Wye	14.81	14.81	14.82	14.82	N/A	See Mult. Losses
51	Tee or Wye	14.81	14.81	14.81	14.81	N/A	See Mult. Losses
52	Tee or Wye	14.81	14.81	14.81	14.81	N/A	See Mult. Losses

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Loss Factor (K)
53	Tee or Wye	14.81	14.81	14.81	14.81	N/A	See Mult. Losses
54	Tee or Wye	14.81	14.81	14.81	14.81	N/A	See Mult. Losses
55	Tee or Wye	14.81	14.81	14.81	14.81	N/A	See Mult. Losses
56	Tee or Wye	14.81	14.81	14.81	14.81	N/A	See Mult. Losses
57	Tee or Wye	14.81	14.81	14.81	14.81	N/A	See Mult. Losses
58	Cell 1	14.70	14.80	14.70	14.80	6.611	0.00000
59	Cell 1	14.70	14.80	14.70	14.80	5.483	0.00000
60	Cell 1	14.70	14.80	14.70	14.80	5.134	0.00000
61	Cell 1	14.70	14.80	14.70	14.80	5.770	0.00000
62	Cell 1	14.70	14.80	14.70	14.80	11.846	0.00000
63	Cell 1	14.70	14.80	14.70	14.80	8.457	0.00000
64	Cell 1	14.70	14.80	14.70	14.80	7.425	0.00000
65	Cell 1	14.70	14.80	14.70	14.80	6.678	0.00000
66	Cell 1	14.70	14.80	14.70	14.80	7.798	0.00000
67	Tee or Wye	14.83	14.83	14.84	14.84	N/A	See Mult. Losses
68	GW Flow from Wellfield	No Solution	No Solution	No Solution	No Solution	0.000	0.00000
X69	Valve	No Solution	16.46	No Solution	16.46	0.000	0.00000
70	Valve	14.82	14.82	14.83	14.83	75.000	0.11966



# Customer Date 02.01.2020 Contact Project Phone number Project no. Email Project no.



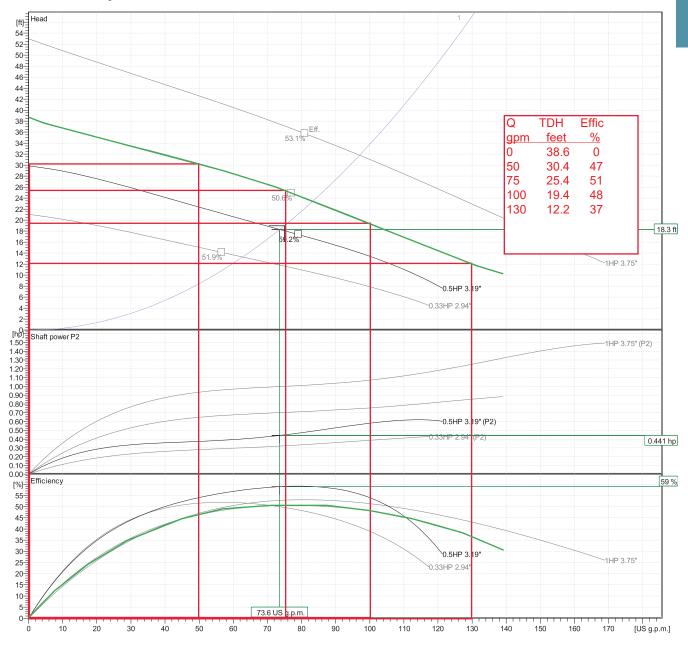
# 3WD51C0JA

### Hydraulic Data

Operating Data Sp	pecification	Hydraulic da	ata (duty point)	Impeller design		
Flow	75 US g.p.m.			Impeller R	33/16"	
Head	19 ft	Flow	73.6 US g.p.m.	Frequency	60 Hz	
Static head	0 ft	Head	18.3 ft	Speed	3500 rpm	

Power datas referced to:

Water [100%]; 39.2°F; 62.4lb/ft³; 1.69E-5ft²/s Performance according to ISO 9906 - Annex A





Wastewater

# Goulds Pumps 2WD/3WD Submersible 2" Non-Clog Sewage Pump

Dual Seal with Seal Sensor Probe





Goulds Pumps is a brand of ITT Corporation.

www.goulds.com

# Engineered for life

### **FEATURES**

- Impeller: Cast iron, semi-open or enclosed, non-clog, dynamically balanced with pump out vanes for mechanical seal protection.

  Optional silicon bronze impeller available.
- Casing: Cast iron flanged volute type for maximum efficiency. Designed for easy installation on A10-20 guide rail.
- Dual Mechanical Seals:
  - Lower Seal: SILICON CARBIDE VS. SILICON CARBIDE sealing faces for superior abrasive resistance, stainless steel metal parts, BUNA-N elastomers.
  - Upper Seal: CARBON VS. CERAMIC sealing faces, stainless steel metal parts, BUNA-N elastomers.
- Seal Sensor Probe: Located in oil-filled chamber. If pumpage should begin to leak past lower seal it indicates to pump control panel a fault has occurred. Requires optional Seal Fail Circuit in the control panel.
- Shaft: Corrosion resistant, 400 series stainless steel. Threaded design. Locknut on all models to guard against component damage on accidental reverse rotation.
- Fasteners: 300 series stainless steel.
- Capable of running dry without damage to components.
- Designed for continuous operation, when fully submerged.

### **APPLICATIONS**

Specifically designed for the following uses:

- Sewage systems
- Dewatering/Effluent
- · Water transfer
- Light industrial
- Commercial applications

Anywhere waste or drainage must be disposed of quickly, quietly and efficiently.

### **SPECIFICATIONS**

### **Pump**

- Solids handling capabilities: 2" maximum.
- Capacities: up to 183 GPM.
- Total heads: up to 52' TDH.
- Discharge size: 2" NPT threaded companion flange on 2WD.
   3" NPT threaded companion flange on 3WD.
- Temperature: 104° F (40° C) continuous, 140° F (60° C) intermittent.

### **MOTORS**

- Fully submerged in high grade turbine oil for lubrication and efficient heat transfer. All ratings are within the working limits of the motor.
- Class F insulation.

### Single phase (60 Hz):

- All single phase models feature capacitor start motors for maximum starting torque.
- Built-in overload with automatic reset.
- ½ and ½ HP 16/3 SJTOW with 115 V or 230 V three prong plug.
- $\frac{3}{4}$  and 1 HP 14/3 STOW with bare leads.

### Three phase (60 Hz):

- Overload protection must be provided in starter unit.
- $\frac{1}{2}$ -1 HP 14/4 STOW with bare leads.
- Designed for Continuous Operation: Pump ratings are within the motor manufacturer's recommended working limits, can be operated continuously without damage when fully submerged.
- Bearings: Upper and lower heavy duty ball bearing construction.
- Power and Control Cable: Severe duty rated, oil and water resistant. Epoxy seal on motor end provides secondary moisture barrier in case of outer jacket damage and to prevent oil wicking. 20 foot standard with optional lengths available.

### **AGENCY LISTINGS**



Tested to UL 778 and CSA 22.2 108 Standards

By Canadian Standards Association
File #LR38549

US Goulds Pumps is ISO 9001 Registered.

### NOMENCLATURE DESCRIPTION

### 1st Character – Discharge Size

2 = 2" discharge 3 = 3" discharge

### 2nd and 3rd Characters – Series/Solids Size

WD = wastewater, 2" solids handling, dual seal with seal fail probe in pump.

### 4th Character – Mechanical Seals

- 5 = silicon carbide/silicon carbide/BUNA lower seal and carbon/ceramic/BUNA upper seal (standard)
- 3 = silicon carbide/tungsten carbide/BUNA lower seal and carbon/ceramic/BUNA upper seal (optional)

### 5th Character - Cycle/RPM

1 = 60 Hz/3500 RPM 5 = 50 Hz/2900 RPM 2 = 60 Hz/1750 RPM 6 = 50 Hz/1450 RPM

### 6th Character - Horsepower

 $B = \frac{1}{3} HP$   $C = \frac{1}{2} HP$   $D = \frac{3}{4} HP$  E = 1 HP

### 7th Character - Phase/Voltage/Enclosure

0 = single phase, 115 V 4 = three phase, 460 V 1 = single phase, 230 V 5 = three phase, 575 V 2 = three phase, 200 V 8 = single phase, 208 V 3 = three phase, 230 V 9 = single phase, 220 V, 50 Hz

### 8th Character – Impeller Diameter

### 9th Character – Cord Length (Power and Sensor)

A = 20' (standard) F = 50'D = 30' J = 100'

### 10th Character - Options

B = Bronze impeller E = Epoxy paint F = Both epoxy paint and bronze impeller

### Last Character - Option

H = Pilot duty thermal sensors

# **Goulds Pumps**

# **MODEL AND MOTOR INFORMATION**

Order No.	НР	Phase	Volts	RPM	Impel	ler	Maximum	L.R.	KVA	F.L. Motor	Resi	stance	Wt.
Order No.	IIIF	riiase	VOILS	IVLIAI	Dia. (in.)	Code	Amps	Amps	Code	Efficiency %	Start	Line-Line	(lbs.)
2WD52B0EA			115	]			10.7	30.0	М	54	11.9	1.7	
2WD52B8EA	0.33	1	208	1750	4.69	E	6.8	19.5	K	51	9.1	4.2	90
2WD52B1EA			230				4.9	14.1	L	53	14.5	8.0	
2WD52C0DA			115				14.5	31.1	J	55	9.3	1.4	
2WD52C8DA		1	208	]			8.0	19.5	K	51	9.1	4.2	
2WD52C1DA			230	]			7.3	16.5	J	54	11.7	5.6	
2WD52C2DA	0.5		200	1750	5.00	D	3.8	12.3	K	75	NA	6.7	94
2WD52C3DA		3	230	]			3.3	9.7	K	75	NA	9.9	
2WD52C4DA		٥	460				1.7	4.9	K	75	NA	39.4	
2WD52C5DA			575				1.4	4.3	K	68	NA	47.8	
2WD52D8CA		1	208				11.0	39.0	K	65	2.6	1.4	
2WD52D1CA	]	'	230	]			9.4	24.8	J	57	4.8	2.3	
2WD52D2CA	7.75		200	1750	F 20		4.1	21.2	Н	74	NA	4.3	]
2WD52D3CA	0.75		230	1750	5.38	С	3.6	17.3	J	76	NA	5.6	- 98
2WD52D4CA	1	3	460	1			1.8	8.9	J	76	NA	22.4	
2WD52D5CA	1	575	1			1.5	7.3	J	71	NA	29.2	1	
2WD52E8BA		4	208				14.0	39.0	K	65	2.6	1.4	
2WD52E1BA	1	1	230	1			12.3	30.5	Н	60	4.3	1.8	1
2WD52E2BA			200	1750	5.75	В	6.0	21.2	Н	74	NA	4.3	104
2WD52E3BA		_	230	1750			5.8	17.3	J	76	NA	5.6	
2WD52E4BA		3	460	1			2.9	8.9	J	76	NA	22.4	
2WD52E5BA			575	1			2.4	7.3	J	71	NA	29.2	1
2WD51B0KA			115			2.94 K	12.4	46.0	М	54	7.5	1.0	
2WD51B8KA	0.33	1 208		3500 2.94	2.94		6.8	31.0	K	68	9.7	2.4	90
2WD51B1KA	1		230				6.2	34.5	М	53	9.6	4.0	
2WD51C0JA			115				14.5	46.0	М	54	7.5	1.0	
2WD51C8JA	1	1	208	1			8.4	31.0	K	68	9.7	2.4	94
2WD51C1JA	1		230	1			7.6	34.5	М	53	9.6	4.0	
2WD51C2JA	0.5		200	3500	3.19	را	4.9	22.6	R	68	NA	3.8	
2WD51C3JA	1		230				3.6	18.8	R	70	NA	5.8	'
2WD51C4JA	1	3	460	1			1.8	9.4	R	70	NA	23.2	•
2WD51C5JA	1		575	1			1.5	7.5	R	62	NA	35.3	1
2WD51D8HA			208				11.0	31.0	K	68	9.7	2.4	
2WD51D1HA	1	1	230	1			10.0	27.5	J	65	12.2	2.7	1
2WD51D2HA	1		200	1			6.2	20.6	L	64	NA	5.7	
2WD51D3HA	0.75		230	3500	3.44	Н	5.4	15.7	K	68	NA NA	8.6	- 98
2WD51D4HA	1	3	460	1			2.7	7.9	K	68	NA NA	34.2	1
2WD51D5HA	1		575	1			2.7	9.9	L	78	NA NA	26.5	
2WD51E8AA			208				14.5	59.0	K	68	9.3	1.1	
2WD51E1AA	1	1	230	1			13.0	36.2	J	69	10.3	2.1	1
2WD51E2AA	1		200	1			8.6	37.6	M	77	NA	2.7	104
2WD51E3AA	1		230	3500	3.75	Α	7.5	24.1	L	79	NA NA	4.1	
2WD51E4AA	1	3	460		"	3.8	12.1	L	79	NA NA	16.2	-	
2WD51E4AA 2WD51E5AA	1	э 	575				3.0	9.9	L	79	NA NA	26.5	-
ZWDDTEDAA			2/3				3.1	9.9	L	/ 0	IVA	20.5	

To order a pump with a 3" NPT discharge, change the 1st character to a 3, ex. 3WD51E5AA

### **APPLICATION DATA**

Maximum Solid Size	2"
Minimum Casing Thickness	5/16"
Casing Corrosion Allowance	1/8"
Maximum Working Pressure	22 PSI
Maximum Submergence	50 feet
Minimum Submergence	Fully submerged for continuous operation
Willimidili Submergence	6" below top of motor for intermittent operation
Maximum Environmental	40°C (104°F) continuous operation
Temperature	60°C (140°F) intermittent operation

### **CONSTRUCTION DETAILS**

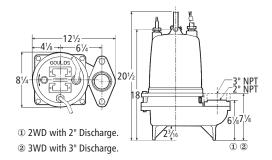
	16/3, type SJTOW: single phase, ½ HP				
Power Cable – Type	14/3, type STOW: single phase, 3/4 & 1 HP				
	14/4, type STOW: all three phase				
Sensor Cable – Type	16/2, type SJTOW: seal sensor only				
Selisor Cable – Type	18/4, type SJTOW: optional seal/heat sensor				
Motor Cover	Gray Cast Iron – ASTM A48 Class 30				
Bearing Housing	Gray Cast Iron – ASTM A48 Class 30				
Seal Housing	Gray Cast Iron – ASTM A48 Class 30				
Casing	Gray Cast Iron – ASTM A48 Class 30				
Impeller	Gray Cast Iron — ASTM A48 or Cast Bronze — ASTM B584 C87600				
Motor Shaft	AISI 300 Series Stainless Steel				
Motor Design	NEMA 48 Frame, oil filled with Class F Insulation				
	Single Phase: on winding thermal overload protection				
Motor Overload Protection	Three Phase: require ambient compensated Class 10, quick trip overloads in the control panel.				
Motor Seal Fail (Moisture) Detection	Seal fail sensor in an oil-filled seal chamber. Connect to an optional relay in control panel.				
Optional Motor Thermal Protection	Normally closed on-winding thermostats open at 275° F (135 °C) and close at 112° F (78° C). Require terminal connection in the control panel.				
External Hardware	300 Series Stainless Steel				
Impeller Type	Semi-opened with pump out vanes on back shroud - 1750 RPM				
Illipeller Type	Enclosed with pump out vanes on back shroud - 3500 RPM				
Oil Capacity – Seal Chamber	10 ounces				
Oil Capacity – Motor Chamber	4.0 quarts				
·					

### **STANDARD PARTS**

Ball Bearing	Upper	Single row ball — SKF™ 6203-2Z
Dail Dealing	Lower	Single row ball — SKF™ 6203-2Z
Mechanical Seals – Standard	Upper	Carbon/Ceramic; John Crane Type 6
Mechanical Scals Standard	Lower	Silicon Carbon/Silicon Carbon; Type 16
Mechanical Seals – Optional Lo	ower	Silicon Carbide/Tungsten Carbide: Type 16
O-Ring – Stuffing Box		BUNA-N, AS 568A-163
O-Ring — Motor Cover		BUNA-N, AS 568A-166

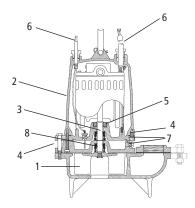
### **DIMENSIONS**

(All dimensions are in inches. Do not use for construction purposes.)



### **MATERIALS OF CONSTRUCTION**

Item	Part N	2mo			ı	Mate	rial		
No.	Part IV	anie			Standard		Optional		
1	Impelle	er		1003			1179		
2	Motor	cover		1003					
3	Shaft				300 Series S				
4	Fasten	ers		300 Series SS					
5	Ball bearings				Steel				
	Power	cable			CTOW 20 f-		A	dditional	
6	Seal se	nsor cable		STOW, 20 fe		er		engths	
7	0-ring			BUNA-N					
	Outer Mech. Seal	Service	Rotary		Stationary	Elasto- mers		Metal Parts	
8	OPT	Heavy duty	Silicon Carbide	- 1	Tungsten Carbide	BUN	IA-N	300 Series SS	
	STD	Mild abrasives	Silic	on	on Carbide BUN		BUNA-N 30 Serie		
	Mater	ial Code			Engineering	y Star	ndard		
	1	Cast iron — ASTM A48 Class 30							
	1	179	Silicon bronze — ASTM C87600						





ITT

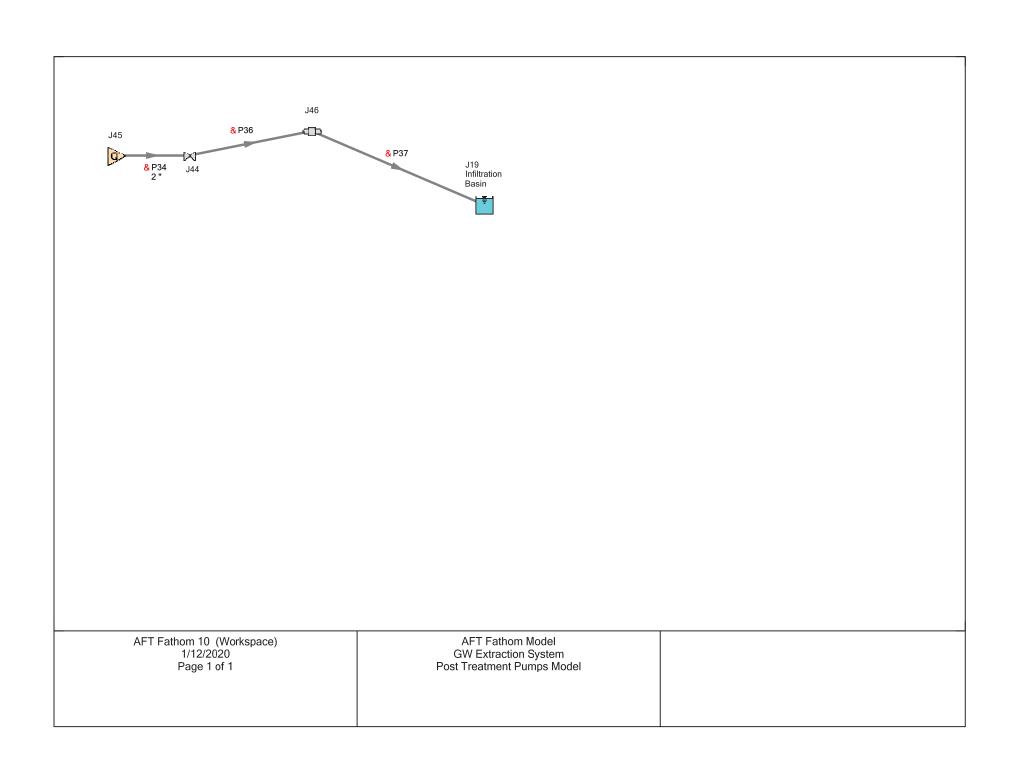
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# Post-Treatment Pumping and Piping Sizing Hydraulic Check



AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

### Model Reference Information

### General

Title: AFT Fathom Model

Analysis run on: 1/12/2020 8:25:08 PM

Application version: AFT Fathom Version 10 (2019.03.28)

Input File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Post Treatment Pumps v1 added high point.fth

Scenario: Base Scenario/Assigned Flow 75 gpm

Output File: C:\Kaiser Mead GWTS\Mechanical\Fathom\Post Treatment Pumps\_v1\_added high point\_F1.out

Execution Time= 0.09 seconds

Total Number Of Head/Pressure Iterations= 0

Total Number Of Flow Iterations= 2

Total Number Of Temperature Iterations= 0

Number Of Pipes= 3 Number Of Junctions= 4

Matrix Method= Gaussian Elimination

Pressure/Head Tolerance= 0.0001 relative change Flow Rate Tolerance= 0.0001 relative change Temperature Tolerance= 0.0001 relative change

Flow Relaxation= (Automatic)
Pressure Relaxation= (Automatic)

Constant Fluid Property Model Fluid Database: AFT Standard

Fluid: Water at 1 atm

Max Fluid Temperature Data= 212 deg. F Min Fluid Temperature Data= 32 deg. F

Temperature= 60 deg. F Density= 62.37215 lbm/ft3 Viscosity= 2.72848 lbm/hr-ft Vapor Pressure= 0.25024 psia Viscosity Model= Newtonian

Apply laminar and non-Newtonian correction to: Pipe Fittings & Losses, Junction K factors, Junction Special Losses, Junction

Polynomials

Corrections applied to the following junctions: Branch, Reservoir, Assigned Flow, Assigned Pressure, Area Change, Bend, Tee or Wye, Spray Discharge, Relief Valve

Ambient Pressure (constant)= 1 atm Gravitational Acceleration= 1 a

Turbulent Flow Above Reynolds Number= 4000

Laminar Flow Below Reynolds Number= 2300

Total Inflow= 75.00 gal/min Total Outflow= 75.00 gal/min

Maximum Static Pressure is 30.12 psia at Pipe 34 Inlet Minimum Static Pressure is 11.44 psia at Pipe 36 Outlet

### **Warnings**

No Warnings

Valve Summary

AFT Fathom Model Kaiser Mead GWTS Well Pumps Model

Jct	Name	Valve Type	Vol. Flow (gal/min)	Mass Flow (Ibm/sec)	dP Stag. (psid)	dH (feet)	P Static In (psia)	Cv	К	Valve State
44	Valve	REGULAR	75.00	10.42	8.940E-03	0.02064	29.28	793.2	0.02000	Open

# Reservoir Summary

Jct	Name	Туре	Liq. Height (feet)	Liq. Elevation (feet)	Surface Pressure (psia)	Liquid Volume (feet3)	Liquid Mass (lbm)	Net Vol. Flow (gal/min)	Net Mass Flow (lbm/sec)
19	Infiltration Basin	Infinite	N/A	1,921	14.70	N/A	N/A	75.00	10.42

# Pipe Output Table

Pipe	Name	Vol. Flow Rate (gal/min)	Pipe Nominal Size	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	Elevation Inlet (feet)	Elevation Outlet (feet)	dP Stag. Total (psid)	dP Static Total (psid)	dP Gravity (psid)
34	Pipe	75.00	2 inch	8.149	30.12	29.28	1,944	1,944	0.8493	0.8493	0.000
36	Pipe	75.00	3 inch	3.264	29.64	11.44	1,944	1,954	18.1972	18.1972	4.331
37	Pipe	75.00	3 inch	3.264	14.62	11.44	1,954	1,921	-3.1797	-3.1797	-14.294

	dH	P Static	P Static	P Stag.	P Stag.	
Pipe		In	Out	In	Out	
	(feet)	(psia)	(psia)	(psia)	(psia)	
34	1.961	30.12	29.28	30.57	29.72	
36	32.012	29.64	11.44	29.71	11.52	
37	25.659	11.44	14.62	11.52	14.70	

# All Junction Table

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Thru Jct (gal/min)	Mass Flow Rate Thru Jct (lbm/sec)	Loss Factor (K)
19	Infiltration Basin	14.70	14.70	14.70	14.70	75.00	10.42	0.00000
44	Valve	29.28	29.64	29.72	29.71	75.00	10.42	0.02000
45	Assigned Flow	30.12	30.12	30.57	30.57	75.00	10.42	0.00000
46	General Component	11.44	11.44	11.52	11.52	75.00	10.42	0.00000

# Heating, Ventilation and Air Conditioning Calculations

Equipment	Sizing

### CALCULATIONS

HVAC



Digitally Signed on April 3, 2020

Carl Shank



#### **Calculations Cover Sheet**

Client	Kaiser Mea	ead Custodial Trust			Project No.		KMCT2019	
Project:	Kaiser Mea	ad Groundwater Rer	nediation Interim Action	on				
Calculation Title: Equipment Sizing - EC Build				ding and Pump C	ontrol House	9		
Calculation	Identifier:							
Rev.	No.		ginator ture/Date	-	hecker ature/Date			
; ; ;	0 James Cutz 1-Nov-2019 1 James Cutz 2-Jan-2020 2 James Cutz January 7, 2020 Carl Shank January 20, 2020 3 4 5 6							
Comment	s:					Seal and S	Signature (if Req'd)	
2 Jan 202	0: Added Pu	mp Control House S	equipment in the EC I Sizing, updated HAP fo Carl Shank (increased	or 90% phase	CFM to accomdate re	otary screw co	mpressor).	
Informatio	on Requiring (	Confirmation:						

### Find

Determine ventilation only cooling rate for the EC Building based on Carrier HAP output.

### Solution

Space Load	<b>77,356</b> BTU/hr	НАР
Summer Design Temperature Space Design Temperature	92.6 degF 104 degF	ASHRAE United Rentals
Air Coefficient	1.08	Standard Conditions
Cooling Airflow Rate Say	6282.976 CFM 6,300 CFM	

#### Find

Winter Heating Load for the purpose of sizing unit heaters

#### Solution

Unit heaters will provide heating for the envelope load and make-up air volume

Envelope Load (HAP)	20616 BTU/hr	НАР
Ventilation Load Extraction Airflow Rate Outdoor Design Temperature Space Design Temperature	200 CFM 2.5 degF 40 degF	Design Extraction Rate ASHRAE United Rentals
Air Coefficient	1.08	Standard Conditions
Ventilation Load	8100 BTU/hr	
Total Heating Load Equivalent kW Say	28716 BTU/hr 8.416178 kW 10 kw	

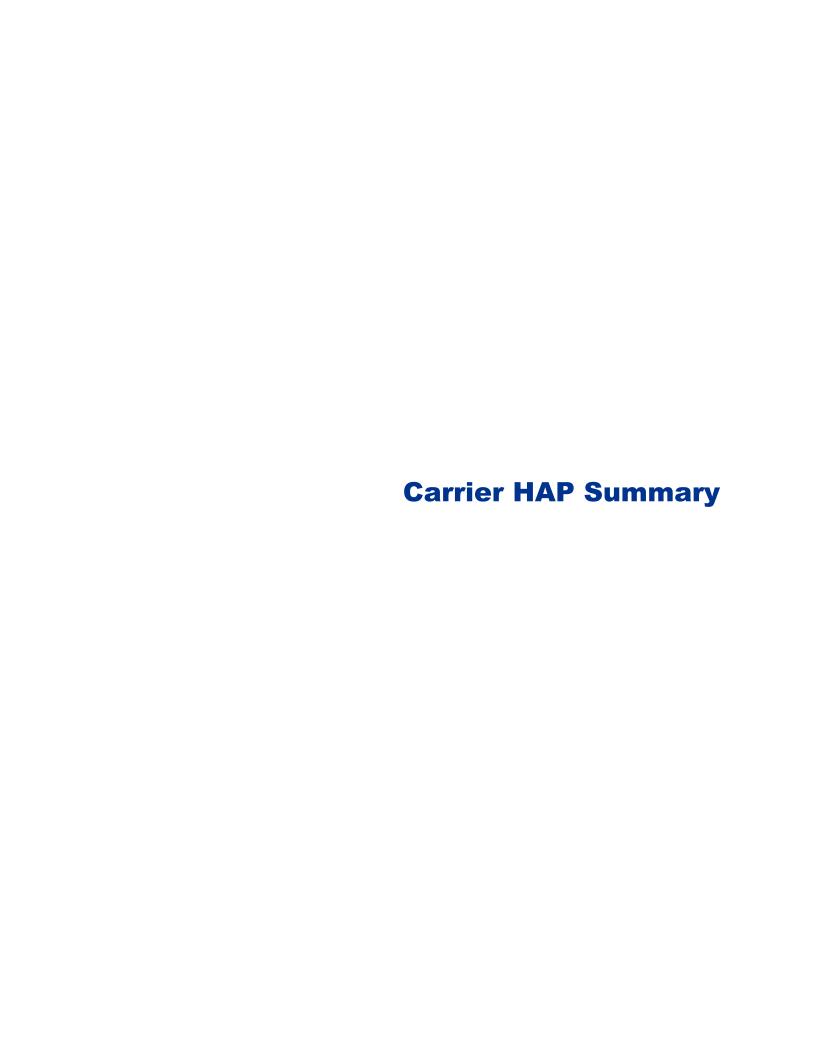
#### Find:

Determine the ventilation-only cooling rate required for maintaining space temperatures below 104 degF for the pump control house in peak cooling season.

#### Solution

Space Load	6,042 BTU/hr	НАР
Summer Design Temperature Space Design Temperature	92.6 degF 104 degF	ASHRAE
Air Coefficient	1.08	Standard Conditions
Cooling Airflow Rate Say	490.7 CFM 500 CFM	

NOTE: Equipment in the pump control house is protected by either it's own control panel w/heat device or freeze protection not required. No additional heat provided.



### **Calculations Cover Sheet**

Client	Kaiser Mea	ad Custodial Trust				Project No.		KMCT2019
Project:	Kaiser Mead	d Groundwater Remediation Interim Action			ion			
Calculation	ı Title:	Carrier HAP	Summa	ıry - EC	Building & Pu	ımphouse She	ed	
Calculation	ı Identifier:							
Rev	. No.		nator ıre/Date		_	ecker ure/Date		
0 1 2 3 4		James Cutz James Cutz		v-2019 n-2020	Carl Shank	20-Jan-2020	Seal and	l Signature (if Reg'd)
Comments:  1-Nov-2019: Original calculation based on 30% design.  7-Jan-2020: Updated calculation based on 90% design. Refined building construction details and added small factor of safety.								
Information Requiring Confirmation:								

#### **EC Building**

#### 1. General Details:

Floor Area	ft <sup>2</sup>
Avg. Ceiling Height	ft
Building Weight70.0	lb/ft²

#### 1.1. OA Ventilation Requirements:

Space Usage	User-Defined	
OA Requirement 1	0.0	CFM/person
OA Requirement 2	0.00	CFM/ft <sup>2</sup>
Space Usage Defaults	ASHRAE Std 62.1-2013	

#### 2. Internals:

#### 2.1. Overhead Lighting:

Fixture Type	Recessed (Unvented)	
Wattage	1.00	W/ft <sup>2</sup>
Ballast Multiplier	1.00	
Schedule	Lighting Schedule	

#### 2.2. Task Lighting:

Wattage	0 W/ft <sup>2</sup>
Schedule Non	е

#### 2.3. Electrical Equipment:

Wattage	16940.0	Watts
Schedule	Lighting Schedule	

#### 3. Walls, Windows, Doors:

2.4.	Peo	ple:

Occupancy	0.0	Person
Activity Level	Office Work	
Sensible	245.0	BTU/hr/person
Latent	205.0	BTU/hr/person
Schedule	None	•

#### 2.5. Miscellaneous Loads:

Sensible	0	BTU/hr
Schedule	None	
Latent		BTU/hr
Schedule	None	

Ехр.	Wall Gross Area (ft²)	Window 1 Qty.	Window 2 Qty.	Door 1 Qty.
N	1970.0	0	0	2
S	1970.0	0	0	0
W	990.0	0	0	1
Е	990.0	0	0	1

#### 3.1. Construction Types for Exposure N

Wall Type	EC - Insulated Metal Wall 1
Door Type	FC - Single Door Hollow Metal

#### 3.2. Construction Types for Exposure S

Wall Type \_\_\_\_\_ EC - Insulated Metal Wall 1

#### 3.3. Construction Types for Exposure W

Wall Type	E	С	- Insulated Metal Wall 1
Door Type			EC - Overhead

#### 3.4. Construction Types for Exposure E

Wall Type	EC - Insulated Metal Wall 1
Door Type	EC - Overhead

#### 4. Roofs, Skylights:

Exp.	Roof Gross Area (ft²)	Roof Slope (deg.)	Skylight Qty.
I	3894.0	0	0

#### 4.1. Construction Types for Exposure H

Roof Type ..... EC - Insulated Roof 1

#### 5. Infiltration:

Design Cooling	0.00	CFM
Design Heating	0.00	CFM
Energy Analysis	0.00	CFM
and the second s		

Infiltration occurs only when the fan is off.

#### 6. Floors:

Kaiser Mead CH2M

Type	Slab Floor On Grade	
Floor Area	3894.0	ft²
Total Floor U-Value	0.100	BTU/(hr·ft²·°F)
Exposed Perimeter	268.0	ft
Edge Insulation R-Value	0.00	$(hr \cdot ft^2 \cdot {}^{\circ}F)/BTU$

7. Partitions: (No partition data).

## Air System Sizing Summary for EC HVAC System

 Project Name: Kaiser Mead
 01/10/2020

 Prepared by: CH2M
 09:14AM

Air System Information Air System Name EC HVA	AC Systom		Number of zenes	1	
Equipment Class	UNDEF			3894.0	ft²
Air System Type	SZCAV			Spokane, Washington	
Sizing Calculation Information					
Calculation Months				Sum of space airflow rates	
Sizing Data	Calculated		Space CFM Sizing	Individual peak space loads	
Supply Fan Sizing Data					
Actual max CFM	7123	CFM	Fan motor BHP	3.90	BHP
Standard CFM	6511	CFM	Fan motor kW	3.09	kW
Actual max CFM/ft²	1.83	CFM/ft²	Fan static	2.00	in wg
Outdoor Ventilation Air Data					
Design airflow CFM	0	CFM	CFM/person	0.00	CFM/person
CFM/ft²	0.00	CFM/ft <sup>2</sup>			

### **Zone Sizing Summary for EC HVAC System**

09:14AM

Project Name: Kaiser Mead Prepared by: CH2M 01/10/2020

**Air System Information** 

Air System Name	EC HVAC System	Number of zones	1	
Equipment Class	UNDEF	Floor Area	3894.0	ft²
Air System Type	SZCAV	Location	Spokane, Washington	

**Sizing Calculation Information** 

Calculation Months	Jan to Dec	Zone CFM Sizing	Sum of space airflow rates
Sizing Data	Calculated	Space CFM Sizing	Individual peak space loads

#### **Zone Terminal Sizing Data**

Zone Name	Design Supply Airflow (CFM)	Minimum Supply Airflow (CFM)	Zone CFM/ft²	Reheat Coil Load (MBH)	Reheat Coil Water gpm @ 20.0 °F	Zone Htg Unit Coil Load (MBH)	Zone Htg Unit Water gpm @ 20.0 °F	Mixing Box Fan Airflow (CFM)
Zone Name	(CEIVI)	(CFIVI)	CFIVI/IL	(INIDIT)	@ 20.0	(INDI)	@ 20.0 F	(CEIVI)
Zone 1	7123	7123	1.83	0.0	0.00	0.0	0.00	0

#### **Zone Peak Sensible Loads**

	Zone Cooling	Time of	Zone Heating	Zone Floor
	Sensible	Peak Sensible	Load	Area
Zone Name	(MBH)	Cooling Load	(MBH)	(ft²)
Zone 1	77.4	Jul 1400	20.6	3894.0

#### **Space Loads and Airflows**

Zone Name / Space Name	Mult.	Cooling Sensible (MBH)	Time of Peak Sensible Load	Air Flow (CFM)	Heating Load (MBH)	Floor Area (ft²)	Space CFM/ft²
Zone 1							
EC Building	1	77.4	Jul 1400	7123	20.6	3894.0	1.83

Hourly Analysis Program 5.11 Page 2 of 4

## Air System Design Load Summary for EC HVAC System

Project Name: Kaiser Mead Prepared by: CH2M 01/10/2020 09:14AM

	DES	IGN COOLING		DES	SIGN HEATING			
	NO COOLING DATA			<b>HEATING DATA A</b>	HEATING DATA AT DES HTG HEATING OA DB / WB 2.5 °F / -0.7 °F			
	NO COOLING OA	NO COOLING OA DB / WB						
		Sensible	Latent		Sensible	Latent		
ZONE LOADS	Details	(BTU/hr)	(BTU/hr)	Details	(BTU/hr)	(BTU/hr)		
Window & Skylight Solar Loads	0 ft²	-	-	0 ft²	-	-		
Wall Transmission	5469 ft²	-	-	5469 ft <sup>2</sup>	8198	-		
Roof Transmission	3894 ft²	-	-	3894 ft²	3841	-		
Window Transmission	0 ft²	-	-	0 ft²	0	-		
Skylight Transmission	0 ft²	-	-	0 ft²	0	-		
Door Loads	451 ft²	-	-	451 ft²	2190	-		
Floor Transmission	3894 ft²	-	-	3894 ft²	4513	-		
Partitions	0 ft²	-	-	0 ft²	0	-		
Ceiling	0 ft²	-	-	0 ft²	0	-		
Overhead Lighting	-	-	-	0	0	-		
Task Lighting	-	-	-	0	0	-		
Electric Equipment	-	-	-	0	0	-		
People	-	-	-	0	0	0		
Infiltration	-	-	-	-	0	0		
Miscellaneous	-	-	-	-	0	0		
Safety Factor	10% / 10%	-	-	10%	1874	0		
>> Total Zone Loads	-	-	-	-	20616	0		
Zone Conditioning	-	-	-	-	10560	0		
Plenum Wall Load	0%	-	-	0	0	-		
Plenum Roof Load	0%	-	-	0	0	-		
Plenum Lighting Load	0%	-	-	0	0	-		
Return Fan Load	-	-	-	7123 CFM	0	-		
Ventilation Load	-	-	-	0 CFM	0	0		
Supply Fan Load	-	-	-	7123 CFM	-10560	-		
Space Fan Coil Fans	-	-	-	-	0	-		
Duct Heat Gain / Loss	0%	-	-	0%	0			
>> Total System Loads	-	-	-	-	0	0		
>> Total Conditioning	-	-	-	-	0	0		
Key:	Positive v	alues are clg lo	ads	Positive	values are htg lo	ads		
	Negative v	values are htg lo	ads	Negative values are clg loads				

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## Zone Design Load Summary for EC HVAC System

Project Name: Kaiser Mead Prepared by: CH2M 01/10/2020 09:14AM

Zone 1	DE	DESIGN COOLING			DESIGN HEATING			
	COOLING DATA	AT Jul 1400		HEATING DATA AT DES HTG				
	COOLING OA DI	B / WB 91.8 °F	/ 61.7 °F	HEATING OA DB / WB 2.5 °F / -0.7 °F				
	OCCUPIED T-ST	AT 104.0 °F		OCCUPIED T-S	TAT 40.0 °F			
		Sensible	Latent		Sensible	Latent		
ZONE LOADS	Details	(BTU/hr)	(BTU/hr)	Details	(BTU/hr)	(BTU/hr)		
Window & Skylight Solar Loads	0 ft²	0	-	0 ft²	-	-		
Wall Transmission	5469 ft <sup>2</sup>	-821	-	5469 ft <sup>2</sup>	8198	-		
Roof Transmission	3894 ft²	1048	-	3894 ft²	3841	-		
Window Transmission	0 ft²	0	-	0 ft²	0	-		
Skylight Transmission	0 ft²	0	-	0 ft²	0	-		
Door Loads	451 ft²	-988	-	451 ft²	2190	-		
Floor Transmission	3894 ft²	0	-	3894 ft²	4513	-		
Partitions	0 ft²	0	-	0 ft²	0	-		
Ceiling	0 ft²	0	-	0 ft²	0	-		
Overhead Lighting	3894 W	13286	-	0	0	-		
Task Lighting	0 W	0	-	0	0	-		
Electric Equipment	16940 W	57799	-	0	0	-		
People	0	0	0	0	0	0		
Infiltration	-	0	0	-	0	0		
Miscellaneous	-	0	0	-	0	0		
Safety Factor	10% / 10%	7032	0	10%	1874	0		
>> Total Zone Loads	-	77356	0	-	20616	0		

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#### **Pump Shed**

	_			_			
	Ge	no	ral	ח	<b>^</b>	ail	

Floor Area ..... \_\_\_\_\_200.0 ft<sup>2</sup> Building Weight \_\_\_\_\_\_\_30.0 lb/ft²

1.1. OA Ventilation Requirements:

Space Usage \_\_\_\_\_\_ User-Defined OA Requirement 1 \_\_\_\_\_\_ 0.0 CFM/person OA Requirement 2 \_\_\_\_\_\_\_ 0.00 CFM/ft² Space Usage Defaults \_\_\_\_\_ ASHRAE Std 62.1-2013

2. Internals:

2.1. Overhead Lighting:
Fixture Type ...... Recessed (Unvented) Ballast Multiplier \_\_\_\_\_\_1.00 Schedule Lighting Schedule

2.2. Task Lighting:

Wattage \_\_\_\_\_\_ 0.00 W/ft² 

2.3. Electrical Equipment:

Wattage ..... .....1050.0 Watts Schedule Lighting Schedule

2.4. People:

Occupancy	0.0	Person
Activity Level	Office Work	
Sensible	245.0	BTU/hr/person
Latent	205.0	BTU/hr/person
Schedule	None	•

#### 2.5. Miscellaneous Loads:

Sensible	<b>0</b> BTU/hr	r
Schedule	None	
Latent	<b>0</b> BTU/hr	r
Schedule	None	

#### 3. Walls, Windows, Doors:

Ехр.	Wall Gross Area (ft²)	Window 1 Qty.	Window 2 Qty.	Door 1 Qty.
N	180.0	0	0	0
S	180.0	0	0	0
Е	90.0	0	0	1
W	90.0	0	0	0

#### 3.1. Construction Types for Exposure N

Wall Type ......Pump Shed Wall

3.2. Construction Types for Exposure S

Wall Type ..... **Pump Shed Wall** 

3.3. Construction Types for Exposure E

Wall Type Pump Shed Wall
Door Type Pump Shed Door (metal)

3.4. Construction Types for Exposure W

Wall Type .... **Pump Shed Wall** 

#### 4. Roofs, Skylights:

Е	хр.	Roof Gross Area (ft²)	Roof Slope (deg.)	Skylight Qty.
	Η	200.0	0	0

#### 4.1. Construction Types for Exposure H

Roof Type .. **Pump Shed Roof** 

5. Infiltration:

Design Cooling	0.00	CFM
Design Heating	0.00	CFM
Energy Analysis	0.00	CFM

Infiltration occurs only when the fan is off.

#### 6. Floors:

Type	Slab Floor On Grade	
Floor Area	200.0	ft²
Total Floor U-Value	0.100	BTU/(hr·ft <sup>2</sup> ·°F)
Exposed Perimeter	60.0	ft
Edge Insulation R-Value	0.00	(hr·ft²·°F)/BTU

7. Partitions: (No partition data).

## **Air System Sizing Summary for Pump House Fan**

 Project Name: Kaiser Mead
 01/10/2020

 Prepared by: CH2M
 09:17AM

Air System Information Air System Name	Dump House Fon		Number of Zenes	1	
Fauinment Class	UNDEF			200.0	ft²
Equipment Class Air System Type	SZCAV			Spokane, Washington	
Sizing Calculation Information					
Calculation Months				Sum of space airflow rates	
Sizing Data	Calculated		Space CFM Sizing	Individual peak space loads	
Supply Fan Sizing Data					
Actual max CFM			Fan motor BHP	0.18	BHP
Standard CFM	491	CFM	Fan motor kW	0.15	kW
Actual max CFM/ft²			Fan static	1.25	in wg
Outdoor Ventilation Air Data					
Design airflow CFM	0	CFM	CFM/person	0.00	CFM/person
CFM/ft²	0.00	CFM/ft <sup>2</sup>			

## **Zone Sizing Summary for Pump House Fan**

Project Name: Kaiser Mead Prepared by: CH2M

01/10/2020 09:17AM

**Air System Information** 

Air System Name	Pump House Fan	Number of zones	1	
Equipment Class	UNDEF	Floor Area	200.0	ft²
Air System Type	SZCAV	Location	Spokane, Washington	

**Sizing Calculation Information** 

Calculation Months	Jan to Dec	Zone CFM SizingSum of space airflow rates
Sizing Data	Calculated	Space CFM SizingIndividual peak space loads

#### **Zone Terminal Sizing Data**

Zone Name	Design Supply Airflow (CFM)	Minimum Supply Airflow (CFM)	Zone CFM/ft²	Reheat Coil Load (MBH)	Reheat Coil Water gpm @ 20.0 °F	Zone Htg Unit Coil Load (MBH)	Zone Htg Unit Water gpm @ 20.0 °F	Mixing Box Fan Airflow (CFM)
Zone Name	(CLIVI)	(CFIVI)	CFIVI/IL	(IVIDIT)	@ 20.0 F	(IVIDIT)	@ 20.0 F	(CFIVI)
Zone 1	537	537	2.68	0.0	0.00	0.0	0.00	0

#### **Zone Peak Sensible Loads**

	Zone Cooling	Time of	Zone Heating	Zone Floor
Zone Name	Sensible (MBH)	Peak Sensible Cooling Load	Load (MBH)	Area (ft²)
Zone 1	6.0	Jul 1400	3.7	200.0

#### **Space Loads and Airflows**

Zone Name / Space Name	Mult.	Cooling Sensible (MBH)	Time of Peak Sensible Load	Air Flow (CFM)	Heating Load (MBH)	Floor Area (ft²)	Space CFM/ft²
Zone 1							
Pump Shed	1	6.0	Jul 1400	537	3.7	200.0	2.68

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## **Air System Design Load Summary for Pump House Fan**

Project Name: Kaiser Mead Prepared by: CH2M 01/10/2020 09:17AM

	DES	IGN COOLING		DES	IGN HEATING							
	NO COOLING DAT	Ά		HEATING DATA A	HEATING DATA AT DES HTG							
	NO COOLING OA	DB / WB		HEATING OA DB / WB 2.5 °F / -0.7 °F								
		Sensible	Latent		Sensible	Latent						
ZONE LOADS	Details	(BTU/hr)	(BTU/hr)	Details	(BTU/hr)	(BTU/hr)						
Window & Skylight Solar Loads	0 ft²	-	-	0 ft²	-	-						
Wall Transmission	520 ft²	-	-	520 ft <sup>2</sup>	1870	-						
Roof Transmission	200 ft <sup>2</sup>	-	-	200 ft <sup>2</sup>	795	-						
Window Transmission	0 ft²	-	-	0 ft²	0	-						
Skylight Transmission	0 ft²	-	-	0 ft²	0	-						
Door Loads	20 ft²	-	-	20 ft <sup>2</sup>	148	-						
Floor Transmission	200 ft <sup>2</sup>	-	-	200 ft <sup>2</sup>	541	-						
Partitions	0 ft²	-	-	0 ft²	0	-						
Ceiling	0 ft²	-	-	0 ft²	0	-						
Overhead Lighting	-	-	-	0	0	-						
Task Lighting	-	-	-	0	0	-						
Electric Equipment	-	-	-	0	0	-						
People	-	-	-	0	0	0						
Infiltration	-	-	-	-	0	0						
Miscellaneous	-	-	-	-	0	0						
Safety Factor	10% / 10%	-	-	10%	335	0						
>> Total Zone Loads	-	-	-	-	3690	0						
Zone Conditioning	-	-	-	-	497	0						
Plenum Wall Load	0%	-	-	0	0	-						
Plenum Roof Load	0%	-	-	0	0	-						
Plenum Lighting Load	0%	-	-	0	0	-						
Return Fan Load	-	-	-	537 CFM	0	-						
Ventilation Load	-	-	-	0 CFM	0	0						
Supply Fan Load	-	-	-	537 CFM	-497	-						
Space Fan Coil Fans	-	-	-	-	0	-						
Duct Heat Gain / Loss	0%	-	-	0%	0	-						
>> Total System Loads	-	-	-	_	0	0						
>> Total Conditioning	-	-	-	_	0	0						
Key:	Positive v	alues are clg lo	ads	Positive v	alues are htg lo	ads						
	Negative v	values are htg lo	ads	Negative values are clg loads								

Hourly Analysis Program 5.11 Page 3 of 4

## **Zone Design Load Summary for Pump House Fan**

Project Name: Kaiser Mead Prepared by: CH2M 01/10/2020 09:17AM

Zone 1	DE	SIGN COOLIN	G	D	ESIGN HEATING	3					
	COOLING DATA	AT Jul 1400		HEATING DATA AT DES HTG							
	COOLING OA DE	3 / WB 91.8 °F	/ 61.7 °F	HEATING OA D	B / WB 2.5 °F /	-0.7 °F					
	OCCUPIED T-ST	AT 104.0 °F		OCCUPIED T-S	TAT 50.0 °F						
		Sensible	Latent		Sensible	Latent					
ZONE LOADS	Details	(BTU/hr)	(BTU/hr)	Details	(BTU/hr)	(BTU/hr)					
Window & Skylight Solar Loads	0 ft <sup>2</sup>	0	-	0 ft²	-	-					
Wall Transmission	520 ft <sup>2</sup>	460	-	520 ft <sup>2</sup>	1870	-					
Roof Transmission	200 ft <sup>2</sup>	819	-	200 ft <sup>2</sup>	795	-					
Window Transmission	0 ft <sup>2</sup>	0	-	0 ft²	0	-					
Skylight Transmission	0 ft²	0	-	0 ft²	0	-					
Door Loads	20 ft <sup>2</sup>	-51	-	20 ft²	148	-					
Floor Transmission	200 ft <sup>2</sup>	0	-	200 ft <sup>2</sup>	541	-					
Partitions	0 ft²	0	-	0 ft²	0	-					
Ceiling	0 ft²	0	-	0 ft²	0	-					
Overhead Lighting	200 W	682	-	0	0	-					
Task Lighting	0 W	0	-	0	0	-					
Electric Equipment	1050 W	3583	-	0	0	-					
People	0	0	0	0	0	0					
Infiltration	-	0	0	-	0	0					
Miscellaneous	-	0	0	-	0	0					
Safety Factor	10% / 10%	549	0	10%	335	0					
>> Total Zone Loads	-	6042	0	-	3690	0					

Hourly Analysis Program 5.11 Page 4 of 4

**Louver Sizing** 

### **Calculations Cover Sheet**

Client	Kaiser Mea	ad Custodial Trust				Project I	No.	KMCT2019
Project:	Kaiser Mead	Groundwater Remo	ediation Inte	erim Acti	on			
Calculation	Title:	Louver Sizin	g - EC Bu	ıilding a	& Pump Cont	rol House		
Calculation	Identifier:							
		Origi				cker		
	No.	Signatu				re/Date		
(	)	James Cutz	1-Nov-2	2019	C. Shank	20-Jan-2020		
]	l <u>2</u>							
	<u>2</u> 3							
2								
							Seal and	Signature (if Req'd)
Commen	ts:							
lf	D i-i	O fi +i						
informati	on Requiring	Confirmation:						

 PROJECT NUMBER:
 KMCT2019
 CALCULATED BY:
 James Cutz

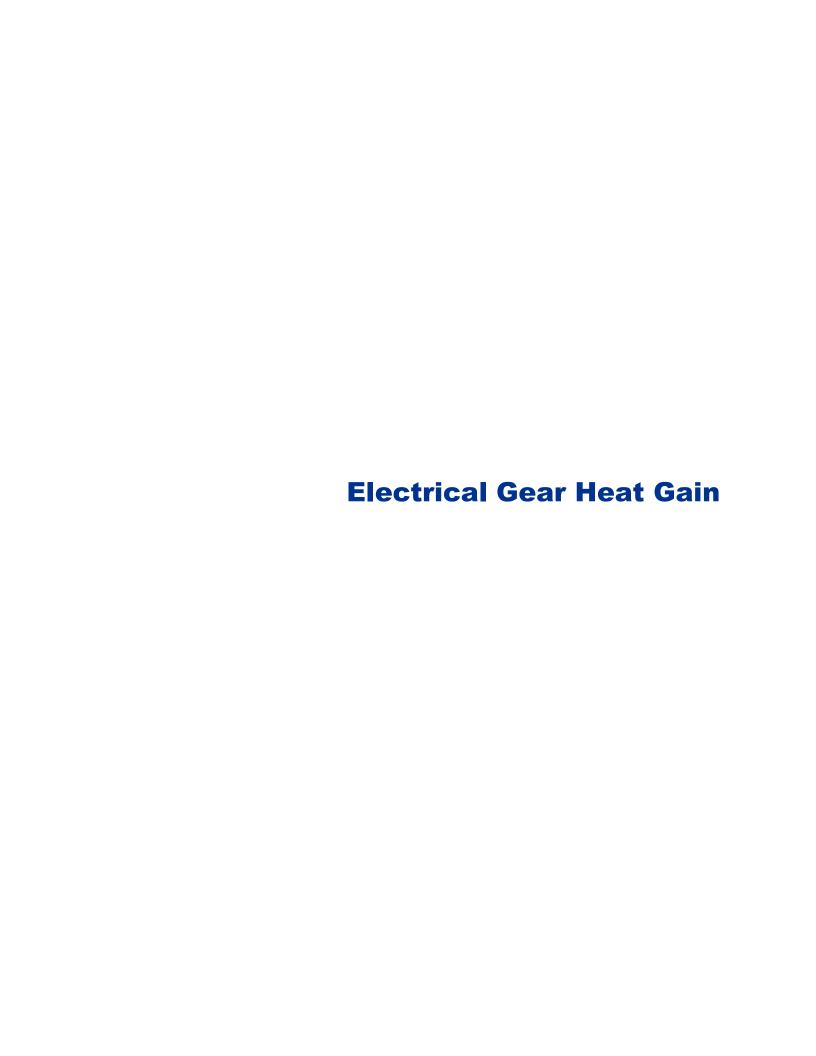
 PROJECT NAME:
 Kaiser Mead Groundwater Remediation Interim Action
 DATE:
 1-Nov-2019

 CALCULATION TITLE:
 Louver Sizing - EC Building & Pump Control House
 1-Nov-2019

														Square	Louver	Round	Louver	Rectangu	ılar Louver										
Building	Room Served	Primary Airflow, ACFM	Louver No.	Associated Fan	Motorized Damper Tag Number		Calculated Unit Airflow, ACFM	Total Air Flow, ACFM	Louver Model	Free Area Velocity, fpm		Required,	Guess Louver Face Area Required, sq. ft.	Dimension	Square Dimension	Round	Round Diameter		Louver Size ( Width, ft	Initial Guess Louver Free Area, %	Selected Louver Siz Height X Width, in.		Louver ee Face Area,	Free Area Check - Selected Free Area greater than Required?	Difference,		Difference	Selected	Combined Design Free Area Check (Selected > Guess)?
Single s	systems																												
Intake Louver	EC Building	6,300	1	Supply	03-MD-02 & 03-MD-03	Intake	6,300	6,300	RUSKIN ELF375DX	600	0.05	10.50	21.00	4.58	55.0	5.01	60.1	4 ft, 0 in	5 ft, 4 in	50%	48 64	51%	21.33	Size OK	(-0.333)	579	21	7	OK Free Area
Exhaust Louver	EC Building	6,300	2	Exhaust	03-MD-01	Ducted Exhaust	6,300	6,300	RUSKIN ELF375DX	1,000	0.10	6.30	12.60	3.55	42.6	3.88	46.6	3 ft, 6 in	4 ft, 6 in	50%	42 54	50%	15.75	Size OK	(-3.150)	800	200	9	OK Free Area
Intake Louver	Pump Control House	500	3	Supply	NA	Intake	400	400	RUSKIN ELF375DX	600	0.05	0.67	2.38	1.54	18.5	1.69	20.2	1 ft, 0 in	2 ft, 6 in	28%	12 30	28%	2.50	Size OK	(-0.119)	571	29	6	OK Free Area
Exhaust Louver	Pump Control House	500	4	Exhaust	NA	Open Exhaust	500	500	RUSKIN ELF375DX	600	0.05	0.83	2.78	1.67	20.0	1.82	21.9	1 ft, 6 in	2 ft, 0 in	30%	18 24	34%	3.00	Size OK	(-0.222)	490	110	6	OK Free Area

0.05 0.05 0.10

Input Data Cells  Max. Intake Velocity, fpm  Max. Open Exhaust Velocity, fpm  Max. Ducted Exhaust Velocity, fpm		600 600 1,000	Louver Pressure Drop Intake louver max. pressure drop, in. w.c. Open Exhaust louver max. pressure drop, in. v Ducted Exhaust louver max. pressure drop, in	
	Free Ar	ea Percentage Startir	a Point	0
Free Area, Extra Small Louvers	x < 18"	25%	3	0%
Free Area, Small Louvers	18" <= x < 24"	30%		0%
Free Area, Medium Louvers	24" <= x < 30"	40%		0%
Free Area, Large Louvers	30" <= x < 36"	42%		0%
Free Area, Extra Large Louvers	36" <= x < 48"	47%		0%
Free Area, Extra, Extra Large Louvers	x >= 48"	50%		0%
Free Area, Acoustical Louvers		30%		0%





#### **Calculation Cover Sheet**

Project:	Kaiser Mead Groundwater Remediation Interim Action		
Client:	Kaiser Mead Custodial Trust	Project No.	KMCT2019

Calculation Title:	Elect	rical Gear Heat Ge	eneration								
alculation Identifier	:										
	Or	iginator	Ch	necker							
Rev. No.	Signature	Date	Signature	Date	e						
0	James Cutz	October 2, 2019									
1	James Cutz	January 2, 2020									
2	James Cutz	January 7, 2020	C. Shank	January 20, 2020							
					Seal and Signature (if Req'd)						
Commonto:				<u> </u>	ocar and orginatare (in recq a)						
Comments:	Landa Barri										
all and Out of the all and											
		4. J. E.O. D. (1.15)	of the controller control at a second con-								
uary 2: Added Pur	np Control House, upda	ted EC Building per Unite	d Rental's updated sco	ope.							
uary 2: Added Pur			d Rental's updated sco	ope.							
uary 2: Added Pur	np Control House, upda		d Rental's updated sco	ope.							
uary 2: Added Pur	np Control House, upda		d Rental's updated sco	ope.							
	np Control House, upda		d Rental's updated sco	ope.							
uary 2: Added Pur uary 7: Refined fol	np Control House, upda lowing brief QC review.		d Rental's updated sα	ope.							
uary 2: Added Pur uary 7: Refined fol	np Control House, upda lowing brief QC review.		d Rental's updated sα	ope.							
uary 2: Added Pur uary 7: Refined fol	np Control House, upda lowing brief QC review.		d Rental's updated sα	ope.							
uary 2: Added Pur	np Control House, upda lowing brief QC review.		d Rental's updated sα	ope.							

James Cutz 2-Jan-2020 PROJECT NUMBER: CALCULATED BY: PROJECT NAME: Kaiser Mead Custodial Trust ORIGINAL DATE:

DESCRIPTION: **Electrical Gear Heat Generation** Data Provided By: Mariah Alexander/CVO United Rentals Revision 1 Provided By: REVISED 1 DATE: 0-Jan-1900

Revision 2 Provided By: REVISED 2 DATE: 0-Jan-1900 Revision 3 Provided By: **REVISED 3 DATE:** 0-Jan-1900 Revision 4 Provided By: REVISED 4 DATE: 0-Jan-1900 SPACE:

BUILDING: EC Building

BUILDING:	EC Building	SPACE					
Equipment	Description	Installed Quantity	Peak Operating Quantity	Heat Loss per Unit (Watts)	Total Watts	Total (BTU/hr)	Comments
Electrical Equipment List							
AFDs - See Data Table Tab							HP
	Duplex EC Feed Pumps VFDs	2	1	110	110	376	3
	Post EC Pump VFDs	2	1	110	110	376	3
	Post Treatment Pump VFDs	2	1	225	225	768	5
	Water Reuse Pump VFDs	2	1	110	110	376	2
Assume 95% Efficiency	Rectifiers 48VDC/2000AMP; Input: 460V/3ph/145 amp	2	1	4,400	4,400	15,026	150
				-	-	-	
				-	-	-	
				-	-	-	
					-	-	
Power Panel				<u> </u>			
Panel Board	225 Amp, 42 Circuit	1	1	300	300	1,025	Main Electrical Panel; 30 amp
ighting Panel	225 Amp, 42 Circuit	1	'	300	-	1,025	wan Electrical Faller, 30 dill
HVAC Panel	225 Amp, 42 Circuit			300	-	-	
Process Panel	225 Amp, 42 Circuit			300		-	
480V Panel	225 Amp, 42 Circuit			300			
TOV I UIICI	24V, Battery Charging			300	-	-	
	Medium Voltage 4000 Amp		-	2,400	_	_	
ighting (If no HAP calculation)	1 W/SF		-	-	_	_	Using HAP for Lighting
Miscellaneous Equipment	1 11/5		-	<del> </del>			Comg Tit a Tor Eignang
Battery Inverter				500	-	_	
Emergency Panel Transfer Switch				200	-	_	
<u> </u>							
				i .		•	•
I&C Equipment List							
Centrifuge Panels	Per cabinet (no UPS)			400	_	-	
LCP Panel	Per cabinet (no UPS)			200	_	-	
Network Panel	Per cabinet (no UPS)			200	-	-	
FACP Panel	Per cabinet (no UPS)			200	-	-	
JPS Panel	Per cabinet (no UPS)			200	-	-	
JPS Bypass Panel	Per cabinet (no UPS)			200	-	-	
ighting Panel	Per cabinet (no UPS)			200	-	-	
HCP Cabinet	Per cabinet (no UPS)			200	-	-	
DDC Cabinet - Process	Per cabinet (no UPS)	1	1	200	200	683	Control Cabinet - 60 amps
JPS (For I&C Equipment)	1.5 KVA			117	-	-	
	5 KVA			305	-	1	
	10 KVA			649	÷ .	-	
	15 KVA			840	-	-	
	20 KVA			886	-	-	
	30 KVA			1,602	-	-	
Computer	Average Value			55	-	-	
<u> </u>	Conservative			65	-	-	
	Highly Conservative			75	-	-	
Printer	Laser			100	-	-	
Monitor	Small (13-15 in.)			55	-	-	
	Medium (16-18 in.)			70	-	-	
	Large (19-20 in.)			80	-	-	
· · · · · · · · · · · · · · · · · · ·	"Count"	12	7		Watts	BTU/hr	Tons

**Grand Total:** 

CALCULATED BY:

1/10/2020 9:35 AM

James Cutz 2-Jan-2020 Kaiser Mead Custodial Trust ORIGINAL DATE: **Electrical Gear Heat Generation** Data Provided By:

Revision 1 Provided By: REVISED 1 DATE: 0-Jan-1900 Revision 2 Provided By: REVISED 2 DATE: 0-Jan-1900 Revision 3 Provided By: REVISED 3 DATE: 0-Jan-1900 Revision 4 Provided By:

BUILDING: EC Building **REVISED 4 DATE:** 0-Jan-1900

PROJECT NUMBER:

PROJECT NAME:

DESCRIPTION:

SPACE:

Equipment	Description	Installed Quantity	Operating Quantity	per Unit (Watts)	Total Watts	Total (BTU/hr)	Comments
Electrical Equipment List							
AFDs - See Data Table Tab							HP
	Pump House Pump VFDs	5	5	90	450	1,537	1
					-		
					-		
					-		
					-		
					-		
					-		
Panel Board	225 Amp, 42 Circuit	1	1	300	300	1,025	VFD Control Panel
Lighting Panel	225 Amp, 42 Circuit	1	1	300	300	1,025	Lighting Sub Panel
HVAC Panel	225 Amp, 42 Circuit			300	-	-	
Process Panel	225 Amp, 42 Circuit			300	-	-	
480V Panel	225 Amp, 42 Circuit			300	-	-	
	24V, Battery Charging			300	-	-	
Lighting (If no HAP calculation)	1 W/SF			-	-	-	Using HAP for Lighting
Miscellaneous Equipment							
Battery Inverter				500	-	-	
Emergency Panel Transfer Switch				200	-	-	
	"Count"	7	7		Watts	BTU/hr	Tons
			Grand Tot	al:	1,050	3,586	0.3





#### **Calculations Cover Sheet**

Project: Kaiser Mead Groundwater Remediation Interim Action  Calculation Title: Equipment Heat Loads - EC Building and Pump House  Calculation Identifier:  Originator Signature/Date Signature/Date  O James Cutz 1-Nov-2019 1 James Cutz 2-Jan-2020 2 James Cutz January 7, 2020 C. Shank January 20, 2020  3 4 5 6  Comments:  1 Nov 2019: Initial calculation with preliminary UR information. 2 Jan 2020: Updating heat load values and equipment counts per UR's revised scope from 12-24-2019. 7 Jan 2020: Updated per QC Review with Carl Shank to include heat gain associated with Rotary Screw Compressor.	lient Kaiser I	Mead Custodial Trust			Project No. KMCT2019					
Calculation Identifier:    Coriginator   Checker   Signature/Date	oject: Kaiser I	Mead Groundwater Rem	ediation Interim Action	n		-				
Rev. No.  Signature/Date  O James Cutz James Cutz 2-Jan-2020 2 James Cutz James Cutz January 7, 2020 C. Shank  Seal and Signature (if F  Comments:  1 Nov 2019: Initial calculation with preliminary UR information. 2 Jan 2020: Updating heat load values and equipment counts per UR's revised scope from 12-24-2019.	ulation Title:		Equipment He	eat Loads - I	EC Building and P	ump House				
Rev. No. Signature/Date Signature/Date  0 James Cutz 1-Nov-2019 1 James Cutz 2-Jan-2020 2 James Cutz January 7, 2020 C. Shank January 20, 2020 3 4 5 6  Comments: 1 Nov 2019: Initial calculation with preliminary UR information. 2 Jan 2020: Updating heat load values and equipment counts per UR's revised scope from 12-24-2019.	ulation Identifier:									
1 James Cutz 2-Jan-2020 2 James Cutz January 7, 2020 C. Shank January 20, 2020 3 4 5 6 Seal and Signature (if Figure 1)   Comments: 1 Nov 2019: Initial calculation with preliminary UR information. 2 Jan 2020: Updating heat load values and equipment counts per UR's revised scope from 12-24-2019.	Rev. No.			-						
Comments:  1 Nov 2019: Initial calculation with preliminary UR information.  2 Jan 2020: Updating heat load values and equipment counts per UR's revised scope from 12-24-2019.	1 2 3 4 5	James Cutz	2-Jan-2020	C. Shank	January 20, 2020					
Comments:  1 Nov 2019: Initial calculation with preliminary UR information.  2 Jan 2020: Updating heat load values and equipment counts per UR's revised scope from 12-24-2019.						Seal and S	Signature (if Reg'd)			
	Nov 2019: Initial Jan 2020: Updat	ing heat load values and	l equipment counts p				SOT.			

	T			
JACO	DRS			
Equipment Heat	Loods FC Building	and Dump House		
Equipment neat	Loads - EC Building	and Pump House		
Calculation Title:	Equipment Heat Loads - EC	Building and Pump House		
Client:	Kaiser Mead Custodial Trust			
Project Name:	Kaiser Mead Groundwater Ro	emediation Interim Action		
Project Number:				
Date:				
Engineer:	James Cutz			
Count	Facility	Room	Watts	Btu/hr
	EC Building	EC Building	11,485	39,199
	EO Building	EO Building	11,400	00,100
	EC Building	EC Building - Carryover from Electrical Heat Gain Calc	5,455	18,629
			5,100	10,020
		Total HAP Input	16,940	57,828
	Pump House	Pump House (No mechanical equipment)	0	0
	Domes Have	Down Have Commence from Florida - Have Coin Colo	4.050	0.504
	Pump House	Pump House - Carryover from Electrical Heat Gain Calc	1,050	3,581
		Total HAP Input	1.050	3,581
	+		-,	-,

#### **HVAC COOLING LOADS FROM MECHANICAL EQUIPMENT EC** Building

PROJECT NUMBER: **CALCULATED BY:** James Cutz PROJECT NAME: Kaiser Mead DATE: October 9, 2019

Provided by United Rentals via Jim Stefanoff/SPK FACILITY: **EC** Building ORIGINAL DATA BY:

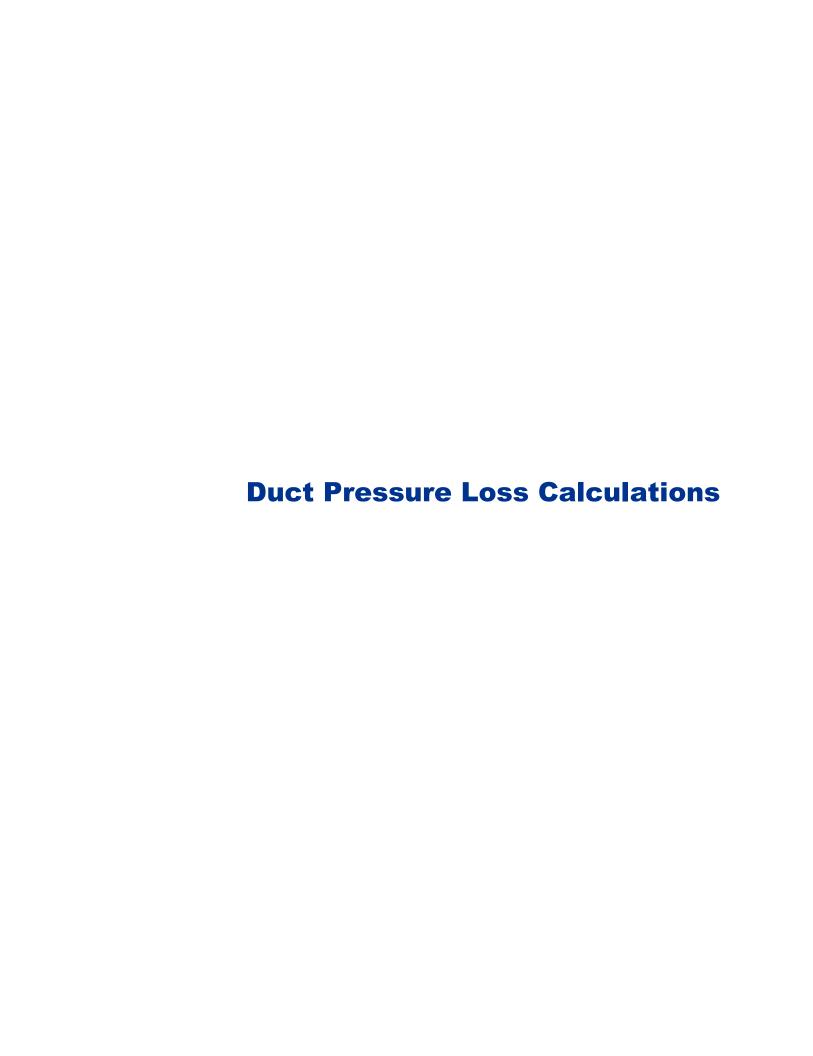
Revision 1 Provided By: James Cutz Revision 1 Date: 2-Jan-2020 Revision 2 Provided By: Revision 2 Date: Revision 3 Provided By: **Revision 3 Date:** 

Revision 4 Provided By: **Revision 4 Date:** Revision 5 Provided By: Revision 5 Date: Revision 6 Provided By: Revision 6 Date:

Facility and Equipment Name	Installed Quantity	Motor HP	Peak Quantity Operating	Duty Cycle	Efficiency	Heat to Space (Watts)	Heat to Space (BTU/hr)	Comments
EC Building								
Rotary Screw Air Compressor - Kaeser SK-20	1	20	1	0.40	60,000	7,032	24,000	Anticipated use at 40% per United Rentals. Heat rejection is 60,000 BTU/hr per Kaeser Compressor (phone call to district office). Used efficiency column to document the heat rejection for this line item only. Model is 20 HP w/aftercoole and internal fan.
Hoist Trolley (3 ton/7.5 HP)	1	7 1/2	1	0.15	87.5%	120	409	Anticipated use is 2 times/week.
Auger Motor/Bulk Handling System	1	2	1	1.00	84.0%	284	970	
Shaker Motor/Bulk Handling System	1	1	1	1.00	80.0%	186	636	
Winch Motor (Belt Filter Press)	1	3	1	1.00	85.5%	379	1,295	
Water Reuse Pumps (2HP max)	1	2	1	1.00	84.0%	284	970	
Sump Pump - 1 HP Zoeller	1	1	1	1.00	80.0%	186	636	
EQ Tank Mixer	1	1 1/2	1	1.00	82.5%	237	810	
Defoam Tank Agitator	1	1 1/2	1	1.00	82.5%	237	810	
Flocc Tank Agitator	1	1	1	1.00	80.0%	186	636	
CaCl Tank Agitator	1	1/2	1	1.00	68.0%	175	599	
Polymer Tank Agitator	1	1/2	1	1.00	68.0%	175	599	
EC Feed Pumps	2	3	1	1.00	85.5%	379	1,295	
Polymer Tank Pumps	2	1/4	1	1.00	55.0%	153	521	
Post-EC Pumps	2	3	1	1.00	85.5%	379	1,295	
Post-Treatment Pumps	2	5	1	1.00	85.5%	632	2,158	
CaCl Pumps (Chemical Metering)	2	1/4	1	1.00	55.0%	153	521	
Acid Pumps (Chemical Metering)	4	1/4	2	1.00	55.0%	305	1,041	
AODD Pumps - Air Operated	3	0	3	1.00	#N/A	#N/A	#N/A	Air operated pump
ROOM TOTAL						11,485	39,199	
	_					Watts	BTU/hr	
					TOTA:	4.4.40-	00 100	<b>1</b>

input cell

TOTAL 11,485 39,199



# <u>Calculations Cover Sheet \*</u> \*Light yellow cells are to be edited by the user.

Client	Kaiser N	Mead Custo	odial Trus	st		Project No. KMCT2019						
Calculat	tion Title:		Duct F	Pressure Loss Calc	ulations - EC Bui	lding and Pump	Control Hou	se				
Calculat	tion Identifie	r:										
				nator		cker						
Rev.	No.		Signatu	ire/Date	Signatu	ıre/Date						
C	)	James	Cutz	2-Jan-20								
1	1	James	Cutz	7-Jan-20	C. Shank	20-Jan-20						
2												
3	3											
4	1											
							Seal and	d Signature (if Req'd)				
Comme												
				equipment selection								
7-Jan-20	020: Revise	d calculation	on to refle	ect increased airflow	vs in EC Building	for accomadation	on of compre	ssor heat load.				
	. 5	2 5										
Informat	tion Requiri	ng Confirma	ation:									

PROJECT NAME:	Kaiser Mead Custodial Trust	TEMPERATURE:	70	DEGREES F	G - GALVANIZED (SPIRAL SEAM) DUCT ABSOLUTE ROUGHNESS FACTOR		
PROJECT NUMBER	KMCT2019	ELEVATION:	1900	FT.	A - ALUMINUM, CARBON STEEL, PVC DUCT ABSOLUTE ROUGHNESS FACTOR:		
TAG NUMBER:	03-SF-01	DUCT PRESSURE DROP CRITERIA:	0.10	IN. W.C. PER 100 FT.	C - CONCRETE OR FLEXIBLE DUCT ABSOLUTE ROUGHNESS FACTOR:		
CALCULATED BY:	James Cutz	DUCT VELOCITY CRITERIA:	2,000	FPM	F - FRP DUCT OR DUCT LINER ABSOLUTE ROUGHNESS FACTOR:		
DATE:	3-Jan-20	FLEX PRESSURE DROP CRITERIA:	0.10	IN. W.C. PER 100 FT.	S - STAINLESS STEEL DUCT ABSOLUTE ROUGHNESS FACTOR:		
QC REVIEW BY:		FLEX VELOCITY CRITERIA:	600	FPM	X - FLEXIBLE DUCT ABSOLUTE ROUGHNESS FACTOR:		
DATE:		SAFETY FACTOR:	10	PERCENT	FLEXIBLE DUCT PERCENT COMPRESSION:	20.0000	% (Taken From ASHRAE 2013 Fundamentals: Chap. 21, Figure 8)
COMMENTS:		ABSOLUTE AIR PRESSURE:	27.923	13.71465	O1 - OTHER DUCT ABSOLUTE ROUGHNESS FACTOR:		
		CORRECTED AIR DENSITY:	0.0697	0.069666	O2 - OTHER DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0300	ft (Manual Input Value)

Duct	Fitting	Duct	Duct	Duct	Airflow	Rectang	ular Duct	Flat 0	Oval Duct	Round	Equivelant	Hydraulic	Actual Duct	Velocity	Calculated	Friction	Duct	Fitting Loss	Other	<b>Duct Pressure</b>	<b>Duct Pressure</b>	Section	Pressure	
Section	Number	Material	Roughness	Element		Width	Height	Major	Minor	Diameter	Diameter	Diameter	Velocity	Pressure	Reynold's	Factor - f	Length	Coefficient	Losses	Drop	Drop	Press. Drop	Loss	Velocity
			E, ft		(CFM)	(in)	(in)	(in)	(in)	(in)	(in)	(in)	(FPM)		Number		(ft)		(In W.C.)	(In W.C./ft)	(In W.C./100 ft)	(In W.C.)	Test	Test
1		G	0.0003	Intake Louver + Screen	6,300	64	48				60	55	295	0.005	128,258	0.017			0.12	0.0000	0.002	0.120		
2	SR4-2	G	0.0003	Transition	6,300	64	48				60	55	295	0.005	128,258	0.017		16.31		0.0000	0.002	0.082		
3		G	0.0003	Backdraft Damper	6,300	26	26				28	26	1,342	0.104	276,249	0.016			0.05	0.0008	0.077	0.050		
4		G	0.0003	Flex Connection	6,300	26	26				28	26	1,342	0.104	276,249	0.016			0.05	0.0008	0.077	0.050		
5		G	0.0003	Filter Housing + Filter Allowance	6,300	26	26				28	26	1,342	0.104	276,249	0.016			0.90	0.0008	0.077	0.900		
6		G	0.0003	Fan	6,300						0	0	0	0.000	0	0.000			0.00	0.0000	0.000	0.000		
7		G	0.0003	Flex Connection	6,300	26	26				28	26	1,342	0.104	276,249	0.016			0.05	0.0008	0.077	0.050		
8	SR5-15	G		Bullhead Tee	3,150	26	26				28	26	671	0.026	138,124	0.018		3.33		0.0002	0.021	0.087		
9	SR4-2	G		Transition	3,150	22	22				24	22	937	0.051	163,238	0.017		0.08		0.0005	0.048	0.004		
10		G	0.0003		3,150	22	22				24	22	937	0.051	163,238	0.017	8			0.0005	0.048	0.004		
11	SR5-13	G		Tee - Supply Grille - Cross Grilles	3,150	22	22				24	22	937	0.051	163,238	0.017		0.99		0.0005	0.048	0.050		
12		G	0.0003		1,050	14	14				15	14	771	0.034	85,506	0.020	8			0.0006	0.058	0.005		
13		G		Volume Damper	1,050	14	14				15	14	771	0.034	85,506	0.020			0.10	0.0006	0.058	0.100		
14		G		Supply Grille	1,050	14	14				15	14	771	0.034	85,506	0.020			0.10	0.0006	0.058	0.100		
15		G		Space Pressurization	1,050						0	0	0	0.000	0	0.000			0.02	0.0000	0.000	0.020		
16	CR6-1	G		Exaust Screen	6,300					28	28	28	1,473	0.126	326,607	0.016		0.44		0.0008	0.083	0.055		
17		G	0.0003		6,300					28	28	28	1,473	0.126	326,607	0.016	22			0.0008	0.083	0.018		
18		G		Motorized Damper	6,300					28	28	28	1,473	0.126	326,607	0.016			0.10	0.0008	0.083	0.100		
19	ER2-4	G	0.0003	Plenum Entrance	6,300	64	42				56	51	338	0.007	135,518	0.017		0.25		0.0000	0.003	0.002		
20		G	0.0003	Exhaust Louver + Screen	6,300	64	42				56	51	338	0.007	135,518	0.017			0.12	0.0000	0.003	0.120		

Note: This table created for the use of calculating static pressure loss in air systems. The worksheet

will calculate the columns that are grayed out and protected: Equivalent Round Duct Size, Duct Velocity,
Velocity Pressure, Reynolds Number, Duct Friction, Duct Section Pressure Drop, and Total System Pressure drop.
Simply add the duct absolute roughness factor from ASHRAE and add any additional losses.

Total
Press. Drop
(In W.C.)
1.92
Safety Factor
Total S.P.: 2.11

PROJECT NAME:	Kaiser Mead Custodial Trust	TEMPERATURE:	70	DEGREES F	G - GALVANIZED (SPIRAL SEAM) DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0003	ft (Taken From ASHRAE 2009 Fundamentals: Chap. 21, Table 1)
PROJECT NUMBER	KMCT2019	ELEVATION:	1900	FT.	A - ALUMINUM, CARBON STEEL, PVC DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0001	ft (Taken From ASHRAE 2009 Fundamentals: Chap. 21, Table 1)
TAG NUMBER:	03-EF-01	DUCT PRESSURE DROP CRITERIA:	0.10	IN. W.C. PER 100 FT.	C - CONCRETE OR FLEXIBLE DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0100	ft (Taken From ASHRAE 2009 Fundamentals: Chap. 21, Table 1)
CALCULATED BY:	James Cutz	DUCT VELOCITY CRITERIA:	2,000	FPM	F - FRP DUCT OR DUCT LINER ABSOLUTE ROUGHNESS FACTOR:		
DATE:	3-Jan-20	FLEX PRESSURE DROP CRITERIA:	0.10	IN. W.C. PER 100 FT.	S - STAINLESS STEEL DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0002	ft (Extrapolated from ASHRAE 2009 Fundamentals: Chap 21, Table 1)
QC REVIEW BY:		FLEX VELOCITY CRITERIA:	600	FPM	X - FLEXIBLE DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0030	ft (Taken From ASHRAE 2013 Fundamentals: Chap. 21, Page 21.6)
DATE:		SAFETY FACTOR:	10	PERCENT	FLEXIBLE DUCT PERCENT COMPRESSION:	20.0000	% (Taken From ASHRAE 2013 Fundamentals: Chap. 21, Figure 8)
COMMENTS:		ABSOLUTE AIR PRESSURE:	27.923	13.71465	O1 - OTHER DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0200	ft (Manual Input Value)
		CORRECTED AIR DENSITY:	0.0697	0.069666	O2 - OTHER DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0300	ft (Manual Input Value)

Duct	Fitting	Duct	Duct	Duct	Airflow	Rectang	ular Duct	Flat C	Val Duct	Round	Equivelant	Hydraulic	Actual Duct	Velocity	Calculated	Friction	Duct	Fitting Loss	Other	<b>Duct Pressure</b>	<b>Duct Pressure</b>	Section	Pressure	
Section	Number	Material	Roughness	Element		Width	Height	Major	Minor	Diameter	Diameter	Diameter	Velocity	Pressure	Reynold's	Factor - f	Length	Coefficient	Losses	Drop	Drop	Press. Drop	Loss	Velocity
			E, ft		(CFM)	(in)	(in)	(in)	(in)	(in)	(in)	(in)	(FPM)		Number		(ft)		(In W.C.)	(In W.C./ft)	(In W.C./100 ft)	(In W.C.)	Test	Test
1	CR6-1	G	0.0003	Exhaust Screen	200					10	10	10	367	0.008	29,032	0.025		0.44		0.0002	0.023	0.003		
2		G	0.0003	Duct	200					10	10	10	367	0.008	29,032	0.025	11			0.0002	0.023	0.003		
3	CR3-14	G	0.0003	Elbow-90 deg	200					10	10	10	367	0.008	29,032	0.025		0.38		0.0002	0.023	0.003		
4		G	0.0003	Vertical Duct	200					10	10	10	367	0.008	29,032	0.025	5			0.0002	0.023	0.001		
5	CR3-14	G	0.0003	Elbow-90 deg	200					10	10	10	367	0.008	29,032	0.025		0.38		0.0002	0.023	0.003		
6		G	0.0003	Duct	200					10	10	10	367	0.008	29,032	0.025	33			0.0002	0.023	0.008		
7	CR3-14	G	0.0003	Elbow-90 deg	200					10	10	10	367	0.008	29,032	0.025		0.38		0.0002	0.023	0.003		
8		G	0.0003	Vertical Duct	200					10	10	10	367	0.008	29,032	0.025	4			0.0002	0.023	0.001		
9	CR3-14	G	0.0003	Elbow-90 deg	200					10	10	10	367	0.008	29,032	0.025		0.38		0.0002	0.023	0.003		
10		G		Duct	200					10	10	10	367	0.008	29,032	0.025	2			0.0002	0.023	0.000		
11	ER4-2	G	0.0003	Transition	200	10	10				11	10	288	0.005	22,801	0.026		0.15		0.0001	0.015	0.001		
12		G	0.0003	Flex Connection	200		10				11	10	288	0.005	22,801	0.026			0.05	0.0001	0.015	0.050		
13		G		Fan	200						0	0	0	0.000	0	0.000			0.00	0.0000	0.000	0.000		
14		G		Flex Connection	200		10				11	10	288	0.005	22,801	0.026			0.05	0.0001	0.015	0.050		
15	ER4-2	G		Transition	200		,	,		10	10	10	367	0.008	29,032	0.025		0.15		0.0002	0.023	0.001		
16		G	0.0003	Motorized Damper	200		,	,		10	10	10	367	0.008	29,032	0.025			0.10	0.0002	0.023	0.100		
17		G		Duct	200					10	10	10	367	0.008	29,032	0.025	2			0.0002	0.023	0.000		
18	ER2-4	G	0.0003	Plenum Entrance	200		,	,		10	10	10	367	0.008	29,032	0.025		0.48		0.0002	0.023	0.004		
19		G	0.0003	Exhaust Louver + Screen	200	48	36				45	41	17	0.000	5,429	0.037			0.12	0.0000	0.000	0.120		

Note: This table created for the use of calculating static pressure loss in air systems. The worksheet

will calculate the columns that are grayed out and protected: Equivalent Round Duct Size, Duct Velocity,
Velocity Pressure, Reynolds Number, Duct Friction, Duct Section Pressure Drop, and Total System Pressure drop.
Simply add the duct absolute roughness factor from ASHRAE and add any additional losses.

	Total
	Press. Dro
	(In W.C.)
	0.35
fety Factor	0.04
Total S.P.:	0.39

PROJECT NAME:	Kaiser Mead Custodial Trust	TEMPERATURE:	70	DEGREES F	G - GALVANIZED (SPIRAL SEAM) DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0003	ft (Taken From ASHRAE 2009 Fundamentals: Chap. 21, Table 1)
PROJECT NUMBER	KMCT2019	ELEVATION:	1900	FT.	A - ALUMINUM, CARBON STEEL, PVC DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0001	ft (Taken From ASHRAE 2009 Fundamentals: Chap. 21, Table 1)
TAG NUMBER:	XX-EF-01	DUCT PRESSURE DROP CRITERIA:	0.10	IN. W.C. PER 100 FT.	C - CONCRETE OR FLEXIBLE DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0100	ft (Taken From ASHRAE 2009 Fundamentals: Chap. 21, Table 1)
CALCULATED BY:	James Cutz	DUCT VELOCITY CRITERIA:	2,000	FPM	F - FRP DUCT OR DUCT LINER ABSOLUTE ROUGHNESS FACTOR:	0.0030	ft (Taken From ASHRAE 2009 Fundamentals: Chap. 21, Table 1)
DATE:	3-Jan-20	FLEX PRESSURE DROP CRITERIA:	0.10	IN. W.C. PER 100 FT.	S - STAINLESS STEEL DUCT ABSOLUTE ROUGHNESS FACTOR:		
QC REVIEW BY:		FLEX VELOCITY CRITERIA:	600	FPM	X - FLEXIBLE DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0030	ft (Taken From ASHRAE 2013 Fundamentals: Chap. 21, Page 21.6)
DATE:		SAFETY FACTOR:	10	PERCENT	FLEXIBLE DUCT PERCENT COMPRESSION:	20.0000	% (Taken From ASHRAE 2013 Fundamentals: Chap. 21, Figure 8)
COMMENTS:		ABSOLUTE AIR PRESSURE:	27.923	13.71465	O1 - OTHER DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0200	ft (Manual Input Value)
		CORRECTED AIR DENSITY:	0.0697	0.069666	O2 - OTHER DUCT ABSOLUTE ROUGHNESS FACTOR:	0.0300	ft (Manual Input Value)

Duct	Fitting	Duct	Duct	Duct	Airflow	Rectang	Jular Duct	Flat (	Oval Duct	Round	Equivelant	Hydraulic	Actual Duct	Velocity	Calculated	Friction	Duct	Fitting Loss	Other	<b>Duct Pressure</b>	<b>Duct Pressure</b>	Section	Pressure	
Section	Number	Material	Roughness	Element		Width	Height	Major	Minor	Diameter	Diameter	Diameter	Velocity	Pressure	Reynold's	Factor - f	Length	Coefficient	Losses	Drop	Drop	Press. Drop	Loss	Velocity
			E, ft		(CFM)	(in)	(in)	(in)	(in)	(in)	(in)	(in)	(FPM)		Number		(ft)		(In W.C.)	(In W.C./ft)	(In W.C./100 ft)	(In W.C.)	Test	Test
1		G	0.0003	Intake Louver + Screen	400	18	18				20	18	178	0.002	25,335	0.025			0.12	0.0000	0.003	0.120		
2	SR4-2	G	0.0003	Transition	400	12	12				13	12	400	0.009	38,002	0.023		2.03		0.0002	0.021	0.019		
3		G	0.0003	Flex Connection	400	12	12				13	12	400	0.009	38,002	0.023			0.05	0.0002	0.021	0.050		
4		G	0.0003	Filter Housing + Loaded Filter Allowance	400	12	12				13	12	400	0.009	38,002	0.023			0.90	0.0002	0.021	0.900		
5		G	0.0003	Fan	400						0	0	0	0.000	0	0.000			0.00	0.0000	0.000	0.000		
6		G	0.0003	Supply Grille	400	12	12				13	12	400	0.009	38,002	0.023			0.10	0.0002	0.021	0.100		
7		G	0.0003	Space Pressurization	400						0	0	0	0.000	0	0.000			0.02	0.0000	0.000	0.020		
8		G	0.0003	Exhaust Louver + Screen	400	18	18				20	18	178	0.002	25,335	0.025			0.12	0.0000	0.003	0.120		

Note: This table created for the use of calculating static pressure loss in air systems. The worksheet

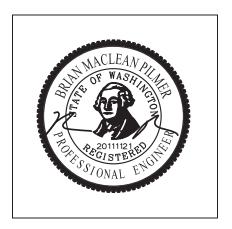
will calculate the columns that are grayed out and protected: Equivalent Round Duct Size, Duct Velocity,
Velocity Pressure, Reynolds Number, Duct Friction, Duct Section Pressure Drop, and Total System Pressure drop.
Simply add the duct absolute roughness factor from ASHRAE and add any additional losses.

Total
Press. Drop
(In W.C.)
1.33
Safety Factor
Total S.P.: 1.46

# **Electrical Calculations**

# **CALCULATIONS**

ELECTRICAL



Digitally Signed

on April 3, 2020

Brian Pilmer

Load Flow

Project: Kaiser\_Power\_Draw

**Base Project** 

# **Load Flow Summary Report**

# **Load Flow Study Settings**

Include Source Impedance	Yes	Bus Voltage Drop %	5.00
Solution Method	Exact (Iterative)	Branch Voltage Drop %	3.00
Load Specification	Demand Load		
•			

## **Swing Generators**

Source	In/Out Service	Vpu	Angle	kW	kvar	VD%	Utility Impedance
AVISTA-UTILITY-240V_P	1 In	1.00	0.00	8.9	4.9	0.00	0.00 + <i>j</i> 0.00
AVISTA-UTILITY-480V_	3 In	1.00	0.00	402.8	299.5	0.00	0.00 +j 0.00

#### Buses

Bus Name	In/Out Service	Design Volts	LF Volts	Angle Degree	PU Volts	%VD
02-PC-01	In	240	115	-1.25	0.48	52.11
03-LCP-01	In	240	200	-1.05	0.83	16.75
03-PB-01	In	480	470	-0.88	0.98	2.06

Bus Name	In/Out Service	Design Volts	LF Volts	Angle Degree	PU Volts	%VD	
03-PB-01-CKT-13 MPC	,15- In	480	468	-0.70	0.97	2.58	
SUB_PANEL	In	240	239	-0.07	1.00	0.23	

## Cables

From Bus To Bus	Component Name	In/Out Service	%VD	kW Loss	kvar Loss	kVA Loss	LF Amps Rating %	PF
02-PC-01	PMP-201-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0087				0.0	0.0	0.0	0.0	
02-PC-01	PMP-202-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0088				0.0	0.0	0.0	0.0	
03-LCP-01	003-EH-01-CBL	In	0.17	3.3	2.5	4.1	5.1	0.80
BUS-0060				0.0	0.0	0.0	25.4	
03-LCP-01	003-EH-02-CBL	In	0.17	3.3	2.5	4.1	5.1	0.80
BUS-0061				0.0	0.0	0.0	25.4	
03-LCP-01	003-EH-04-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0063				0.0	0.0	0.0	0.0	

From Bus To Bus	Component Name	In/Out Service	%VD	kW Loss	kvar Loss	kVA Loss	LF Amps Rating %	PF
03-LCP-01	003-EH-03-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0064				0.0	0.0	0.0	0.0	
03-LCP-01	003-EH-05-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0065				0.0	0.0	0.0	0.0	
03-LCP-01	003-EH-06-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0066				0.0	0.0	0.0	0.0	
03-LCP-01	03-EP-01-CBL	In	0.74	10.8	8.0	13.4	38.8	0.80
BUS-0072				0.1	0.0	0.1	193.9	
03-PB-01	02-PC-01-XFMR-C BL-PRI	. In	0.52	8.5	6.4	10.6	13.1	0.80
03-PB-01-CKT-13, 15-MPC				0.1	0.0	0.1	17.4	
03-PB-01	03-EF-01-CBL	In	0.03	0.6	0.5	0.8	0.9	0.80
BUS-0059				0.0	0.0	0.0	4.6	
03-PB-01	03-SF-01-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0067				0.0	0.0	0.0	0.0	

From Bus To Bus	Component Name	In/Out Service	%VD	kW Loss	kvar Loss	kVA Loss	LF Amps Rating %	PF
03-PB-01	EC_CONTROLS_C BL	C In	0.34	53.5	40.0	66.7	82.0	0.80
BUS-0069				0.2	0.1	0.3	63.0	
03-PB-01	WATER_HTR-CBI	L In	10.66	84.9	54.6	101.0	124.0	0.84
BUS-0079				12.9	0.6	13.0	55.1	
03-PB-01	01XFMR0002-CBL PRI	- In	0.37	21.1	15.8	26.4	32.4	0.80
EC-PRI-BUS				0.1	0.0	0.1	19.1	
03-PB-01	EC-RECTIFIER-1_ CBL	In	0.86	97.5	72.8	121.6	149.4	0.80
EC-RECTIFIER-1- DSW				1.0	0.4	1.1	76.6	
03-PB-01	EC-RECTIFIER-2_ CBL	In	1.03	97.7	72.8	121.8	149.6	0.80
EC-RECTIFIER-1- DSW0				1.3	0.4	1.4	88.0	
03-PB-01	EC-AIR_COMPRES_CBL	S In	1.51	18.4	13.5	22.8	28.0	0.81
EC-RECTIFIER-1- DSW1				0.4	0.0	0.4	93.3	
03-PB-01	EC-HOIST_CBL	In	0.43	3.3	2.5	4.2	5.1	0.80
EC-RECTIFIER-1- DSW2				0.0	0.0	0.0	25.6	

From Bus To Bus	Component Name	In/Out Service	%VD	kW Loss	kvar Loss	kVA Loss	LF Amps Rating %	PF
03-PB-01	EC-CACL2_CBL	In	0.47	3.7	2.7	4.6	5.6	0.80
EC-RECTIFIER-1- DSW3				0.0	0.0	0.0	28.2	
03-PB-01	EC_WINCH_CBL	In	0.41	3.2	2.4	4.0	4.9	0.80
EC-RECTIFIER-1- DSW4				0.0	0.0	0.0	24.6	
BUS-0015	01XFMR0002-CBL SEC	In	0.81	20.9	15.6	26.1	74.8	0.80
03-LCP-01				0.2	0.2	0.3	28.8	
BUS-0017	02-PC-01-XFMR-C BL-SEC	. In	0.12	8.3	6.2	10.4	52.2	0.80
02-PC-01				0.0	0.0	0.0	36.0	
BUS-0037	WF-CBL-01	In	0.01	0.4	0.3	0.5	1.2	0.80
BUS-0021				0.0	0.0	0.0	6.0	
BUS-0038	WF-CBL-02	In	0.01	0.4	0.3	0.5	1.2	0.80
BUS-0022				0.0	0.0	0.0	6.0	
BUS-0039	WF-CBL-03	In	0.01	0.4	0.3	0.5	1.2	0.80
BUS-0023				0.0	0.0	0.0	6.0	

From Bus To Bus	Component Name	In/Out Service	%VD	kW Loss	kvar Loss	kVA Loss	LF Amps Rating %	PF
BUS-0040	WF-CBL-04	In	0.01	0.4	0.3	0.5	1.2	0.80
BUS-0024				0.0	0.0	0.0	6.0	
BUS-0041	WF-CBL-05	In	0.01	0.4	0.3	0.5	1.2	0.80
BUS-0025				0.0	0.0	0.0	6.0	
BUS-0043	02XFMR0001-CBL SEC	In	0.03	8.9	6.7	11.1	26.8	0.80
SUB_PANEL				0.0	0.0	0.0	2.1	
BUS-0076	01XFMR0001-CBL SEC	- In	0.04	399.1	289.1	492.8	605.0	0.81
03-PB-01				0.1	0.2	0.2	36.0	
BUS-0077	02XFMR0001-CBL PRI	In	0.00	8.9	4.9	10.2	0.8	0.88
BUS-0062				0.0	-1.8	1.8	0.1	
BUS-0078	01XFMR0001-CBL PRI	In	0.00	402.8	299.5	501.9	23.2	0.80
BUS-0075				0.0	-1.8	1.8	5.9	
SUB_PANEL	WF-HEATER-CBL	In	0.00	0.0	0.0	0.0	0.0	0.00
BUS-0081				0.0	0.0	0.0	0.0	

# 2-Winding Transformers

From Bus To Bus	Component Name	In/Out Service	%VD	kW Loss	kvar Loss	kVA Loss	LF Amps Rating %	PF
03-PB-01-CKT-1 3,15-MPC	02-PC-01-XFMR	In	1.52	8.4	6.4	10.6	13.0	0.79
BUS-0017				0.1	0.2	0.2	20.9	
BUS-0062	02XFMR0001	In	0.21	8.9	6.7	11.1	1.0	0.80
BUS-0043				0.0	0.0	0.0	2.1	
BUS-0075	01XFMR0001	In	2.01	402.7	301.2	502.9	23.0	0.80
BUS-0076				3.6	12.1	12.6	50.3	
EC-PRI-BUS	01XFMR0002	In	13.51	21.0	15.8	26.3	32.0	0.80
BUS-0015				0.1	0.2	0.2	20.7	



AMSTA-UIILITY-480V\_3P Rated Voltage 12470 V 03PB0l SystemNominalValtage 4800\* DemmdLoad 43335 kW LF\*W5# 184 % IniSymPAWS 3P 286020A ubSC\_AsymLL A:232722A B:232722A C:00A | GBPBG CXT25.27.29 | Municitaret CITLE BHAM | FarneWhold LD | Sensor File | The Auto-| Farne F OSPBOLCKT2.4.6
Munificaner CUTLIRHAM
Funr/Model Di
Sensor Tip 900.A
Pag 900.A
Setings
Fred

WATER HTRCH.
Systersbrittanholage 4800 V
Size 2MV G
Gondoxter Dace 3 UCG
Length 1000 G
Ampachy 1500.A 03PB01 CKEV 39.41
Manufacture CUIERHAM
FranceModel FD
SensorTip 150A
Plug 150A
Settings
Freed

EC.WNCH, OB.
System Normal Vitage 4800 V
Size 12AWG
ConductarDase 3-1/CGG
Length 1500
Ampacity 200A OSPBOLCKT323436
Manufatuer/CITLIRHAM
FrameModel IPD
Sensorfitp 150A
Plug 150A
Setings
Fixed
Fixed
Fixed
SystemNonimalVatge 4800 V
See 12AWG
Conductor Day 5 J.C.G.G.
Length 1500 f
Ampaciny 200A OGPBOLCKES 333.8

Munificum CUTLERHAMP
Finnr/Model DD
Sensor/Tip 150A
Plug 150A
Setings
Fired

ECHEST\_CH
System/svinal/tokage-4800 V
Size 12AWG
Graduster Date 34CG
Length 1500
Ampacity 200A GPB01CKT262830
Mininfuture(UTLIB-HAM
Imm/Model) D Sensor flip 300A
Plug 300A
Settings
Fred
FLAIR, (UMPRISS, CH.
System-Nariaulfolage-48010 Sets 104 NG
Conductor Dace 34CG
Lengh 1800 E OSPBOLCKEJ 2224
Munfatuer CUTLENHAM
FlarmAded JD
Sensor Fip 175.0A
Bug 175.0A
Setings
Thermat Curve Fixed
NST G 10x Tip 15 SETA
LITERATURE JD
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See 12AWG
Conductor Dec 34G+G
Longh 6108
Aupacity 200A (6-PB01 CKF-9.11

Menufacturer CUTLERHAMM
Planne/Model DBB
Plang ISOA
Settings
Fixed

GBEF01 CHE.
System/Nominal/Mage 4800 V
Size 12AWG
Conductor Desc 34/CrG
Conductor Desc 34/CrG
Langle 6008
Auspaciny 200A 03FB01 CKF-19-21.23
Manufacture CITIERHAM
Frame Model H9
Sensor Tip 800 A
Senings
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SystemNorinalVolage 4400 V
Ser 4AWG
Graductor/Desc 31/CsG
Length 600 A
Ampacity 950A DePRICACELLS
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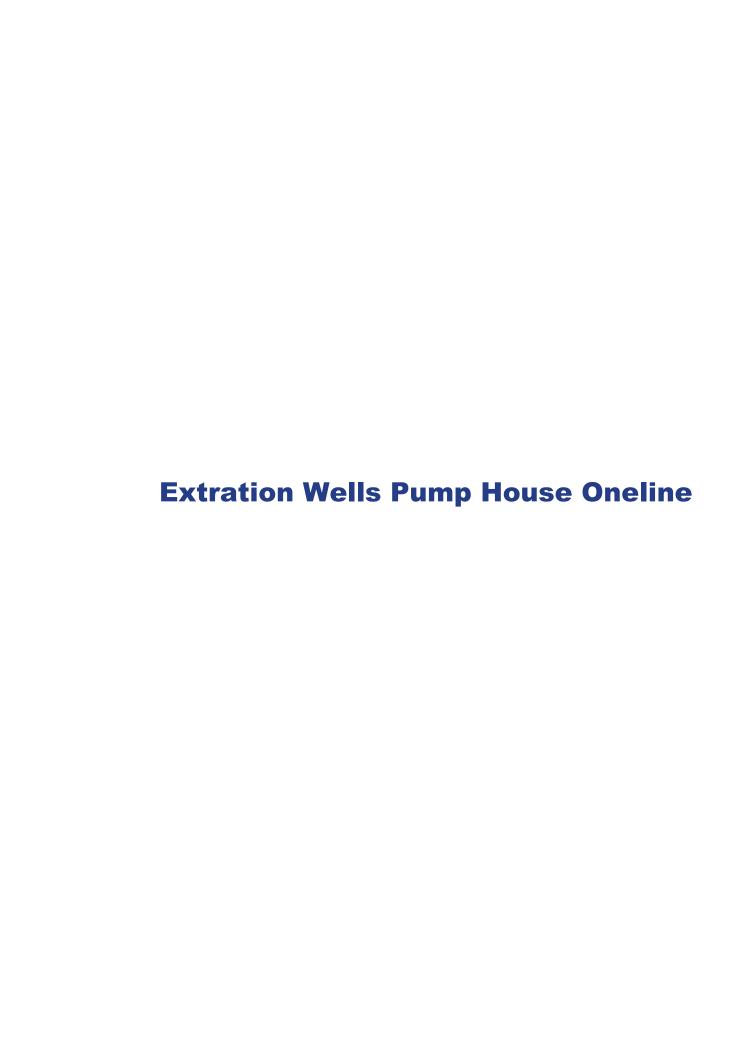
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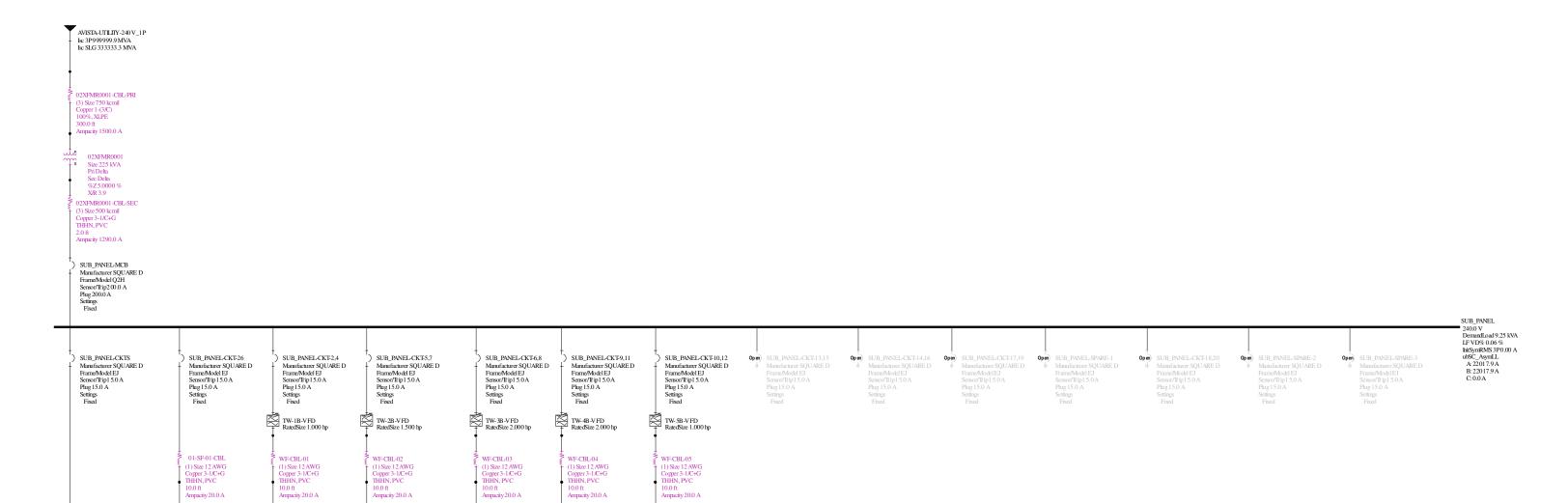
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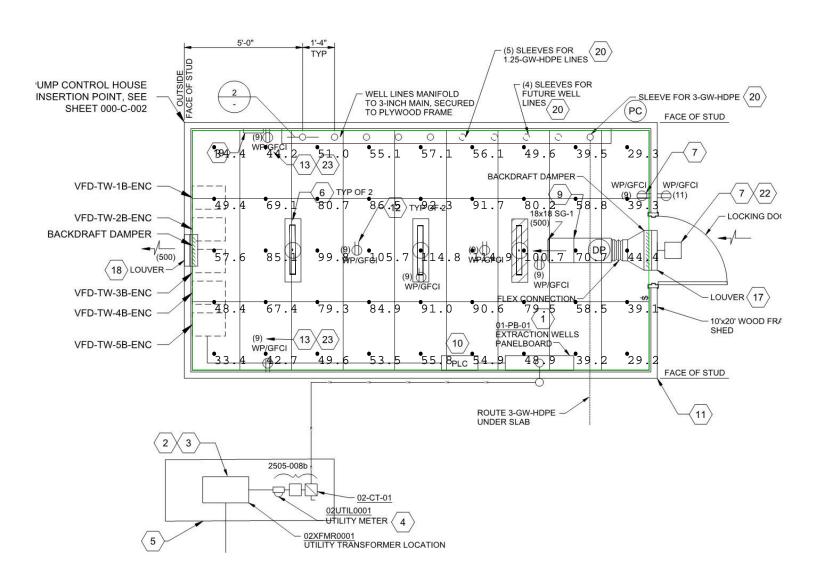
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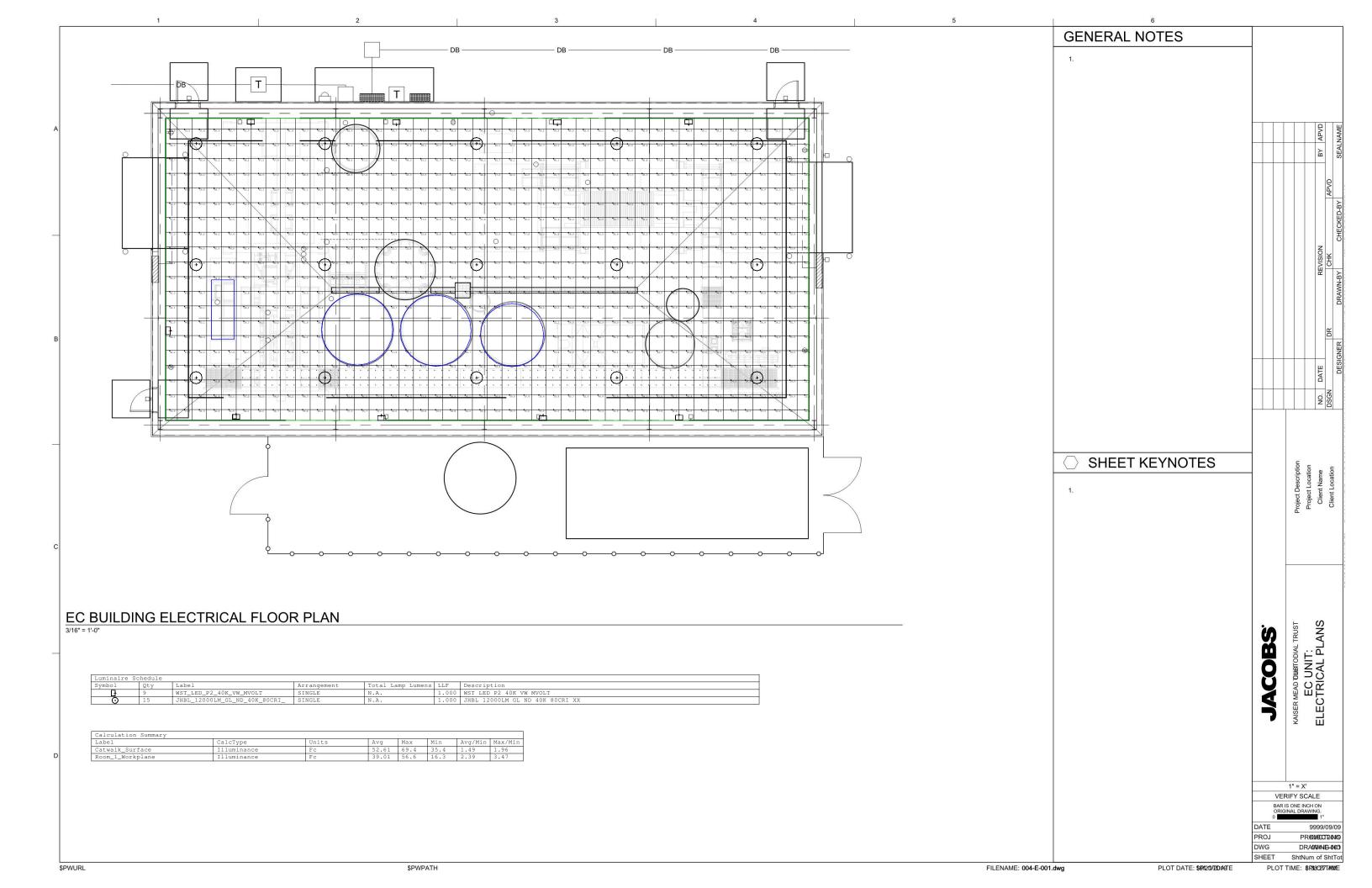




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# Appendix E SEPA Environmental Checklist

# SEPA ENVIRONMENTAL CHECKLIST

#### Purpose of checklist:

Governmental agencies use this checklist to help determine whether the environmental impacts of your proposal are significant. This information is also helpful to determine if available avoidance, minimization or compensatory mitigation measures will address the probable significant impacts or if an environmental impact statement will be prepared to further analyze the proposal.

This Checklist was prepared by the Mead Custodial Trust (MCT) at the request of Washington Department of Ecology (Ecology) Industrial Section. This Checklist follows the SEPA Environmental Checklist template obtained from the Ecology website (<a href="https://ecology.wa.gov/Regulations-Permits/SEPA/Environmental-review/SEPA-document-templates">https://ecology.wa.gov/Regulations-Permits/SEPA/Environmental-review/SEPA-document-templates</a>) on November 15, 2018. The Checklist is identical to the template with the following exceptions:

- All text added to the template by MCT is shown in italicized fonts.
- The original template contains hotlinks that link to instruction on how to complete the template.
   These hotlinks have been removed for clarity.

# A. Background

- 1. Name of proposed project, if applicable: Kaiser Mead NPL Site Groundwater Interim Action
- 2. Name of applicant: Mead Custodial Trust
- 3. Address and phone number of applicant and contact person:

Dan Silver Mead Custodial Trust 606 Columbia St. NW, Ste. 212 Olympia, WA 98501 (360) 754-9343

- 4. Date checklist prepared: January 30, 2019
- 5. Agency requesting checklist: Washington Department of Ecology, Industrial Section
- 6. Proposed timing or schedule (including phasing, if applicable):

Engineering design is anticipated to begin in 2019. Construction would begin after Ecology approvals, expected to occur in 2019.

7. Do you have any plans for future additions, expansion, or further activity related to or connected with this proposal? If yes, explain.

No changes are anticipated.

8. List any environmental information you know about that has been prepared, or will be prepared, directly related to this proposal.

The project is described in the February 2019 "Kaiser Mead Interim Action Workplan" prepared by Hydrometrics for the Mead Custodial Trust. Additional information is available in the October 2018 "Supplemental Feasibility Study for Kaiser Mead NPL Site" prepared by Hydrometrics for the Mead Custodial Trust.

9. Do you know whether applications are pending for governmental approvals of other proposals directly affecting the property covered by your proposal? If yes, explain.

There are no pending applications.

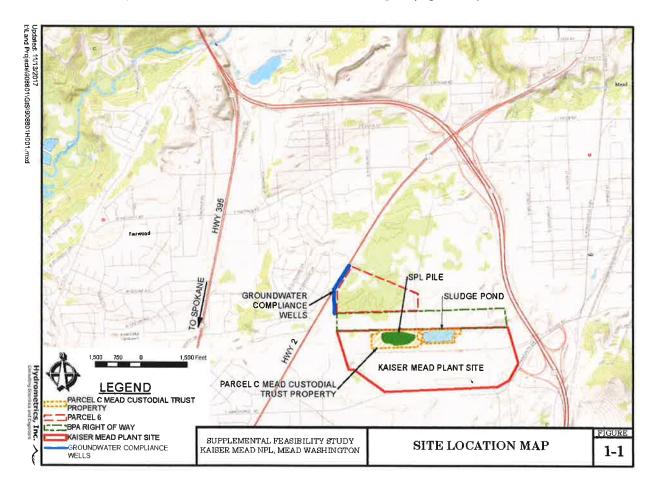
- 10. List any government approvals or permits that will be needed for your proposal, if known.
  - Notice of Intent for construction of dewatering/resource protection wells.
  - Compliance with substantive requirements of State Waste Discharge Permit for discharge treated water to groundwater as described in Appendix A of the Interim Action Workplan.
  - Electric permit from WA Labor and Industries
  - Local (Spokane County) permits or approvals are anticipated and may include:
    - o Building Permit
    - o Erosion and Control Plan approval
    - Critical and Hazardous Materials List/Hazardous Material Management Plan approval
    - Septic system permit.
- 11. Give brief, complete description of your proposal, including the proposed uses and the size of the project and site. There are several questions later in this checklist that ask you to describe certain aspects of your proposal. You do not need to repeat those answers on this page. (Lead agencies may modify this form to include additional specific information on project description.)

The proposal is to construct a "pump and treat" system for remediation of groundwater at the Kaiser Mead NPL Site. This will include the following elements:

- Installation and operation of approximately 4 to 8 groundwater extraction wells to extract approximately 50 gpm of contaminated groundwater.
- Construction of pipelines to convey the pumped groundwater to a water treatment system.
- Construction and operation of an approximately 3 acre constructed wetland water treatment system.
- Construction and operation of an electrocoagulation water treatment system housed in an approximately 10,000 ft<sup>2</sup> building.
- Construction and operation of an approximately 0.25 acre infiltration pond and associated piping for discharge of treated groundwater to the underlying groundwater system.

12. Location of the proposal. Give sufficient information for a person to understand the precise location of your proposed project, including a street address, if any, and section, township, and range, if known. If a proposal would occur over a range of area, provide the range or boundaries of the site(s). Provide a legal description, site plan, vicinity map, and topographic map, if reasonably available. While you should submit any plans required by the agency, you are not required to duplicate maps or detailed plans submitted with any permit applications related to this checklist.

The project location is the Kaiser Mead NPL Site located at 2111 E Hawthorne Rd, Mead, WA 99021 within Section 16, Township 26 North, Range 43 East, approximately 7 miles north of Spokane, Washington and 1 mile southwest of Mead, Washington (Figure 1-1).



#### **B.** Environmental Elements

#### 1. Earth

a. General description of the site:

(circle one): Flat, rolling, hilly, steep slopes, mountainous, other

The site is flat.

b. What is the steepest slope on the site (approximate percent slope)?

Approximately 2 to 4 percent

c. What general types of soils are found on the site (for example, clay, sand, gravel, peat, muck)? If you know the classification of agricultural soils, specify them and note any agricultural land of long-term commercial significance and whether the proposal results in removing any of these soils.

Natural soils are fine to medium sand.

 d. Are there surface indications or history of unstable soils in the immediate vicinity? If so, describe.

No unstable soils are present.

e. Describe the purpose, type, total area, and approximate quantities and total affected area of any filling, excavation, and grading proposed. Indicate source of fill.

Approximately 3 acres will be graded to construct the wetland treatment system and approximately 0.25 acres for the infiltration pond. The conceptual design is to balance cut and fill to achieve a neutral material balance so that no import or export of fill is required.

f. Could erosion occur as a result of clearing, construction, or use? If so, generally describe.

Erosion is unlikely and best management practices (BMPs) will be implemented consistent with the State Department of Ecology Stormwater Management Manual for Eastern Washington (Ecology, 2004).

g. About what percent of the site will be covered with impervious surfaces after project construction (for example, asphalt or buildings)?

The area where the constructed wetland and electrocoagulation water treatment systems will be built are currently covered with impervious surfaces (asphalt). Thus, no increase in impervious surfaces is expected.

h. Proposed measures to reduce or control erosion, or other impacts to the earth, if any:

As part of engineering design for the project, a SWPP will be developed and BMPs will be implemented consistent with the State Department of Ecology Stormwater Management Manual for Eastern Washington (Ecology, 2004).

#### 2. Air

a. What types of emissions to the air would result from the proposal during construction, operation, and maintenance when the project is completed? If any, generally describe and give approximate quantities if known.

Insignificant amounts of fugitive dust may be generated during excavation and construction. No air emissions would occur during operation and maintenance.

b. Are there any off-site sources of emissions or odor that may affect your proposal? If so, generally describe.

No off-site emissions or odors are expected.

c. Proposed measures to reduce or control emissions or other impacts to air, if any:

Not applicable.

#### 3. Water

- a. Surface Water:
  - 1) Is there any surface water body on or in the immediate vicinity of the site (including year-round and seasonal streams, saltwater, lakes, ponds, wetlands)? If yes, describe type and provide names. If appropriate, state what stream or river it flows into.

The closest surface water to the Project is the Little Spokane River, located approximately two miles northwest of the Site.

2) Will the project require any work over, in, or adjacent to (within 200 feet) the described waters? If yes, please describe and attach available plans.

No.

3) Estimate the amount of fill and dredge material that would be placed in or removed from surface water or wetlands and indicate the area of the site that would be affected. Indicate the source of fill material.

Not applicable.

4) Will the proposal require surface water withdrawals or diversions? Give general description, purpose, and approximate quantities if known.

No.

5) Does the proposal lie within a 100-year floodplain? If so, note location on the site plan.

No.

6) Does the proposal involve any discharges of waste materials to surface waters? If so, describe the type of waste and anticipated volume of discharge.

No.

b. Ground Water:

1) Will groundwater be withdrawn from a well for drinking water or other purposes? If so, give a general description of the well, proposed uses and approximate quantities withdrawn from the well. Will water be discharged to groundwater? Give general description, purpose, and approximate quantities if known.

Groundwater withdrawn will be treated but will not be used for drinking water or any other beneficial purposes.

Treated groundwater that meets discharge requirements described in Appendix A of the Interim Action Plan will be discharged to groundwater at the approximate rate of 50 gallons per minute. Expected quality of treated water is further described in Table 6-1 of the Interim Action Workplan.

2) Describe waste material that will be discharged into the ground from septic tanks or other sources, if any (for example: Domestic sewage; industrial, containing the following chemicals. . . ; agricultural; etc.). Describe the general size of the system, the number of such systems, the number of houses to be served (if applicable), or the number of animals or humans the system(s) are expected to serve.

The project will require very limited staffing (1 or less full time employees) for operation of the treatment plant and thus domestic sewage generation will be limited. Handling of domestic sewage will be determined during engineering design and may include a small on-site septic system or the use of temporary holding facilities (e.g., Porta potties).

Treated groundwater that meets discharge requirements described in Appendix A of the Interim Action Plan will be discharged to groundwater at the approximate rate of 50 gallons per minute. Expected quality of treated water is further described in Table 6-1 of the Interim Action Workplan.

- c. Water runoff (including stormwater):
  - Describe the source of runoff (including storm water) and method of collection and disposal, if any (include quantities, if known). Where will this water flow?
     Will this water flow into other waters? If so, describe.

Rain falling on the wetland treatment cell will be captured and will not runoff. Pipeline disturbances will be reclaimed with soil and revegetated after construction and will not generate runoff. Roof runoff from the electrocoagulation building will disperse and flow to surrounding areas.

2) Could waste materials enter ground or surface waters? If so, generally describe.

No. Waste materials (sludge) from the water treatment system will be contained, temporarily stored in a roofed and secure area, and shipped off-site to a landfill for disposal.

Does the proposal alter or otherwise affect drainage patterns in the vicinity of the site? If so, describe.No.

d. Proposed measures to reduce or control surface, ground, and runoff water, and drainage pattern impacts, if any:

As part of engineering design for the project, a SWPP will be developed and BMPs will be implemented consistent with the State Department of Ecology Stormwater Management Manual for Eastern Washington (Ecology, 2004).

#### 4. Plants

a. Check the types of vegetation found on the site:

c	leciduous tree: alder, maple, aspen, other
_Xe	evergreen tree: fir, cedar, pine, other
_X_	shrubs
X	_grass
p	pasture
c	rop or grain
	Orchards, vineyards or other permanent crops.
	wet soil plants: cattail, buttercup, bullrush, skunk cabbage, other
v	vater plants: water lily, eelgrass, milfoil, other
c	other types of vegetation

b. What kind and amount of vegetation will be removed or altered?

Vegetation (primarily grass and possibly trees) may be temporarily removed during well installation, pipeline construction and infiltration pond construction.

c. List threatened and endangered species known to be on or near the site.

The site where the water treatment system will be constructed is a former industrial facility covered with asphalt and no significant vegetation is present. The area where the pipelines and wells will be constructed is a grassy sparse evergreen forest. WA Natural Heritage Program responded to an information request on December 4, 2018 and indicated the following:

"We've searched the Natural Heritage Information System for information on significant natural features in your project area. Currently, we have no records for rare plants or rare/high quality ecological communities in the vicinity of your project.

The information provided by the Washington Natural Heritage Program is based solely on existing information in the database. In the absence of field inventories, we cannot state whether or not a given site contains high quality ecosystems or rare plant species; there may be significant natural features in your study area of which we are not aware." (email from Jasa Holt, WA NHP to Scott Mason, Hydrometrics)

d. Proposed landscaping, use of native plants, or other measures to preserve or enhance vegetation on the site, if any:

Not applicable. Primary area of disturbance is currently asphalt within an industrial setting.

e. List all noxious weeds and invasive species known to be on or near the site.

Not applicable. Primary area of disturbance is currently asphalt within an industrial setting.

#### 5. Animals

a. <u>List</u> any birds and <u>other</u> animals which have been observed on or near the site or are known to be on or near the site.

#### Examples include:

birds: hawk, heron, eagle, songbirds, other: mammals: deer, bear, elk, beaver, other: fish: bass, salmon, trout, herring, shellfish, other

The site where the water treatment system will be constructed is a former industrial facility covered with asphalt and no significant wildlife is present or to be expected. The area where the pipelines and wells will be constructed is a grassy sparse evergreen forest where deer and other upland mamals may be present. A search of the US Fish and Wildlife Service "Information for Planning and Consultation" search engine on November 28, 2018 identified the following migratory species that may be present on or near the site: Bald eagle, Cassin's finch, Golden eagle, Lesser yellowlegs, Olive-sided flycatcher, Rufous hummingbird.

b. List any threatened and endangered species known to be on or near the site.

The site where the water treatment system will be constructed is a former industrial facility covered with asphalt and no significant wildlife is present or to be expected. The area where the pipelines and wells will be constructed is a grassy sparse evergreen forest. A search of the US Fish and Wildlife Service "Information for Planning and Consultation" search engine on November 28, 2018 identified the following species that may be present on or near the site:

Endangered Species: None.

- Threatened species: Yellow-billed Cuckoo (Coccyzus americanus). The project site is outside the critical habitat for this species.
- c. Is the site part of a migration route? If so, explain.

Unknown, but not believed to be.

d. Proposed measures to preserve or enhance wildlife, if any:

None proposed. The site where the water treatment system will be constructed is a former industrial facility covered with asphalt and no significant wildlife is present or to be expected.

e. List any invasive animal species known to be on or near the site.

None known.

#### 6. Energy and Natural Resources

a. What kinds of energy (electric, natural gas, oil, wood stove, solar) will be used to meet the completed project's energy needs? Describe whether it will be used for heating, manufacturing, etc.

Energy will be used in the water treatment system, in heating/cooling the water treatment building, and pumping groundwater. Electricity will be used for pumping and treating water. Gas or electric will be used for heating and cooling the building.

b. Would your project affect the potential use of solar energy by adjacent properties? If so, generally describe.

No.

c. What kinds of energy conservation features are included in the plans of this proposal? List other proposed measures to reduce or control energy impacts, if any:

None are proposed at this time but will be evaluated during engineering design as an important cost factor.

#### 7. Environmental Health

- a. Are there any environmental health hazards, including exposure to toxic chemicals, risk of fire and explosion, spill, or hazardous waste, that could occur as a result of this proposal? If so, describe.
  - 1) Describe any known or possible contamination at the site from present or past uses.

The Site is a state and federal superfund site undergoing cleanup under WA Model Toxics Control Act. Contamination includes cyanide and fluoride contamination of soil and groundwater associated with the former aluminum plant that occupied the site previously.

 Describe existing hazardous chemicals/conditions that might affect project development and design. This includes underground hazardous liquid and gas transmission pipelines located within the project area and in the vicinity.

The Site is a state and federal superfund site undergoing cleanup under WA Model Toxics Control Act. Contamination includes cyanide and fluoride contamination of soil and groundwater associated with the former aluminum plant that occupied the site previously. Waste contained in the existing engineered on-site containment facility known as the Spent Potliner Pile contains material that may be listed or characterized as dangerous or hazardous waste.

 Describe any toxic or hazardous chemicals that might be stored, used, or produced during the project's development or construction, or at any time during the operating life of the project.

Certain reagents (e.g., sodium hydroxide, calcium chloride, sulfuric acid, anionic or cationic polymers) that might be employed during water treatment may be harmful if mishandled or spilled. Proper engineering controls, PPE and standard operating procedures will be developed for storage, handling and use of potentially harmful chemicals. No existing hazardous chemicals or conditions are known.

The water treatment process will generate approximately 1,000 tons/year of sludge that will contain fluoride and cyanide. The sludge is not expected to have hazardous characteristics but is a listed hazardous waste (K088) as it is derived from spent polliner with is a listed hazardous material.

4) Describe special emergency services that might be required.

None known.

5) Proposed measures to reduce or control environmental health hazards, if any:

The contractor that is hired by MCT will be responsible for preparing a Project and Work Sitespecific Health and Safety Plan (HASP) for the interim action. The Contractor will submit the plan to Ecology a minimum of two weeks prior to commencing excavation work at the Site.

#### b. Noise

1) What types of noise exist in the area which may affect your project (for example: traffic, equipment, operation, other)?

None.

2) What types and levels of noise would be created by or associated with the project on a short-term or a long-term basis (for example: traffic, construction, operation, other)? Indicate what hours noise would come from the site.

Construction noise will be generated by a variety of construction equipment such as truck engines, generators and other small engines, and earthmoving equipment. Construction noise will be limited to daytime hours and is not expected to create adverse impacts.

3) Proposed measures to reduce or control noise impacts, if any:

Construction activities will be carried out in a manner consistent with Spokane County municipal code and State environmental noise standards.

#### 8. Land and Shoreline Use

a. What is the current use of the site and adjacent properties? Will the proposal affect current land uses on nearby or adjacent properties? If so, describe.

The Kaiser Mead NPL Site is located on the former Kaiser Aluminum Chemical Corporation smelter complex. The facility was a prebake aluminum smelter that was constructed by the US government during WWII in 1942. The smelter complex covers approximately 240 acres and the area immediately adjacent to the smelter is zoned for heavy industrial use. The nearest residential properties are located approximately 1,500 feet to the northwest of the smelter.

b. Has the project site been used as working farmlands or working forest lands? If so, describe. How much agricultural or forest land of long-term commercial significance will be converted to other uses as a result of the proposal, if any? If resource lands have not been designated, how many acres in farmland or forest land tax status will be converted to nonfarm or nonforest use?

Not applicable.

1) Will the proposal affect or be affected by surrounding working farm or forest land normal business operations, such as oversize equipment access, the application of pesticides, tilling, and harvesting? If so, how:

No.

c. Describe any structures on the site.

Current structures on the site consists of a capped waste pile, fencing, and a metal-sided building with a footprint of approximately 20' by 40'.

d. Will any structures be demolished? If so, what?

No.

e. What is the current zoning classification of the site?

HI, heavy industrial under the Spokane County Zoning Code.

- f. What is the current comprehensive plan designation of the site?
- HI, heavy industrial under the Spokane County Zoning Code.
- g. If applicable, what is the current shoreline master program designation of the site?

Not applicable.

h. Has any part of the site been classified as a critical area by the city or county? If so, specify.

No.

- i. Approximately how many people would reside or work in the completed project?
- It is anticipated that 1 to 2 people (0.5 to 1 full time equivalent) will work at the water treatment plant.
- j. Approximately how many people would the completed project displace?

None.

k. Proposed measures to avoid or reduce displacement impacts, if any:

None.

L. Proposed measures to ensure the proposal is compatible with existing and projected land uses and plans, if any:

None.

m. Proposed measures to reduce or control impacts to agricultural and forest lands of long-term commercial significance, if any:

None.

#### 9. Housing

 a. Approximately how many units would be provided, if any? Indicate whether high, middle, or low-income housing.

None.

b. Approximately how many units, if any, would be eliminated? Indicate whether high, middle, or low-income housing.

None.

c. Proposed measures to reduce or control housing impacts, if any:

None.

#### 10. Aesthetics

a. What is the tallest height of any proposed structure(s), not including antennas; what is the principal exterior building material(s) proposed?

To be determined during engineering design, preliminary estimate of water treatment building is less than 30 feet; exterior to be determined, possibly metal siding.

b. What views in the immediate vicinity would be altered or obstructed?

None.

b. Proposed measures to reduce or control aesthetic impacts, if any:

None.

#### 11. Light and Glare

a. What type of light or glare will the proposal produce? What time of day would it mainly occur?

Minimal, lighting will only be required for security.

b. Could light or glare from the finished project be a safety hazard or interfere with views?

Not believed to be likely.

c. What existing off-site sources of light or glare may affect your proposal?

None known.

d. Proposed measures to reduce or control light and glare impacts, if any:

None.

#### 12. Recreation

a. What designated and informal recreational opportunities are in the immediate vicinity?

None. Site is heavy industrial.

b. Would the proposed project displace any existing recreational uses? If so, describe.

No.

c. Proposed measures to reduce or control impacts on recreation, including recreation

None.

#### 13. Historic and cultural preservation

- a. Are there any buildings, structures, or sites, located on or near the site that are over 45 years old listed in or eligible for listing in national, state, or local preservation registers? If so, specifically describe.
- A search of the Spokane City/County Historic Preservation Office online records (<a href="http://properties.historicspokane.org">http://properties.historicspokane.org</a>) on December 7, 2018 revealed no identified historic properties associated with the Site. The smelter complex itself is over 45 years old. The sole structure on the Trust portion of the complex is an approximately 50' by 120' storage shed of unknown age.
- b. Are there any landmarks, features, or other evidence of Indian or historic use or occupation? This may include human burials or old cemeteries. Are there any material evidence, artifacts, or areas of cultural importance on or near the site? Please list any professional studies conducted at the site to identify such resources.

None known.

c. Describe the methods used to assess the potential impacts to cultural and historic resources on or near the project site. Examples include consultation with tribes and the department of archeology and historic preservation, archaeological surveys, historic maps, GIS data, etc.

No formal assessment performed. The project site is the Kaiser Mead NPL Site located on the former Kaiser Aluminum Chemical Corporation smelter complex. The area is primarily asphalt covered. The Spokane Tribe will be consulted prior to construction to determine the likelihood of potential cultural resources in the project area. An "Inadvertent Discovery Plan" will be prepared for the project that will describe the appropriate measures that will be taken during construction to ensure cultural resources are identified and protected and that appropriate notifications are made.

d. Proposed measures to avoid, minimize, or compensate for loss, changes to, and disturbance to resources. Please include plans for the above and any permits that may be required.

None.

#### 14. Transportation

a. Identify public streets and highways serving the site or affected geographic area and describe proposed access to the existing street system. Show on site plans, if any.

See Figure 1-1 above. The Site is bounded by Hawthorne Drive to the South and Highway 2 to the north. Access to the site is from Hawthrone Drive through the Kaiser Mead Plant Site, owned by Spokane Recycling Company.

b. Is the site or affected geographic area currently served by public transit? If so, generally describe. If not, what is the approximate distance to the nearest transit stop?

Yes, nearest Spokane Transit Authority bus stop is approximately 0.5 miles west of site at corner of Hawthorne Road and Nevada Street.

c. How many additional parking spaces would the completed project or non-project proposal have? How many would the project or proposal eliminate?

None.

d. Will the proposal require any new or improvements to existing roads, streets, pedestrian, bicycle or state transportation facilities, not including driveways? If so, generally describe (indicate whether public or private).

No.

e. Will the project or proposal use (or occur in the immediate vicinity of) water, rail, or air transportation? If so, generally describe.

No.

- f. How many vehicular trips per day would be generated by the completed project or proposal? If known, indicate when peak volumes would occur and what percentage of the volume would be trucks (such as commercial and nonpassenger vehicles). What data or transportation models were used to make these estimates?
- To be determined during final engineering design. Based on professional judgement, approximately 2 to 4 trips per day are estimated for water treatment plant staff plus additional occasional trips (1 to 2 times/week) for supplies and deliveries.
- g. Will the proposal interfere with, affect or be affected by the movement of agricultural and forest products on roads or streets in the area? If so, generally describe.

No.

h. Proposed measures to reduce or control transportation impacts, if any:

None.

#### 15. Public Services